

T/F is a static Device

Flect
$$\frac{V_1}{I/p}$$
 $\frac{V_2}{O/p}$ Elect $\frac{V_1}{I/p}$ $\frac{V_2}{I/p}$ $\frac{V_2}{I/p}$ $\frac{V_3}{I/p}$ $\frac{V_4}{I/p}$ $\frac{$

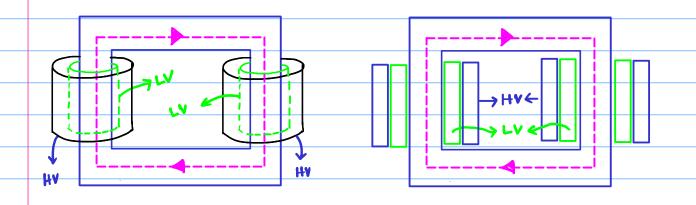
The main components of T/F are >

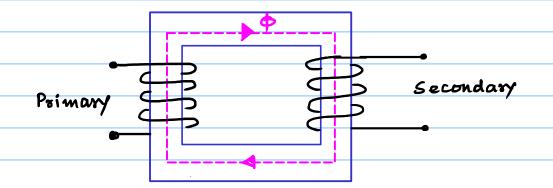
- 1. Magnetic Core
- 2. Primary and secondary windings
- 3. Tank, oil, cooling arrangement

Maquetic Core:

Base on magnetic core T/F can be of core type and Shell type.

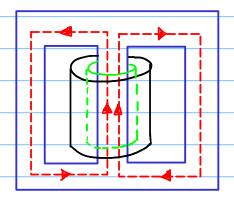
Ore Type T/F:-

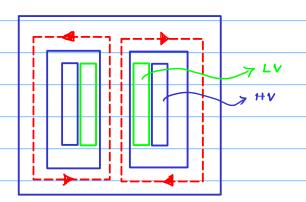


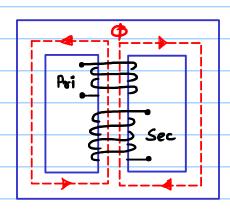


- 1. One iron path.
- 2. This is not used for small transformer as the shape makes installation difficulties.

D Shell type T/F:0-



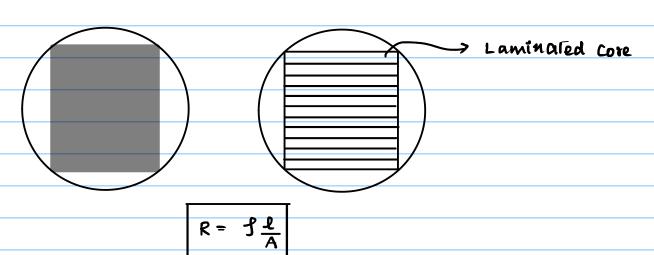




- i) two iron paltis
- ii) primary and secondary windings are wound on the central Limb one above another.

□ Core :-

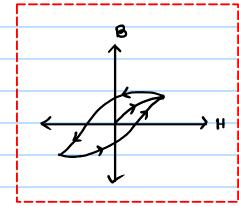
- i) Magnetic core is laminated iron core
- ii) Thin silicon steel cut into particular sizes and stacked together to form the core.
- iii) Reduce the eddy current loss.
- iv) Laminated sheets are insulated by thick layer of vernish
- v) Thickness is 0.4 mm or less.



(Ferromagnetic Materials)

Special Si-Steel (Si Content 4-5%)
is used as lamination.

Hysteresis loss depends on the area of the B-H curve



Special si-steel has less area and high saturation flux density.

9+ also has high resistivity that reduces eddy current loss.

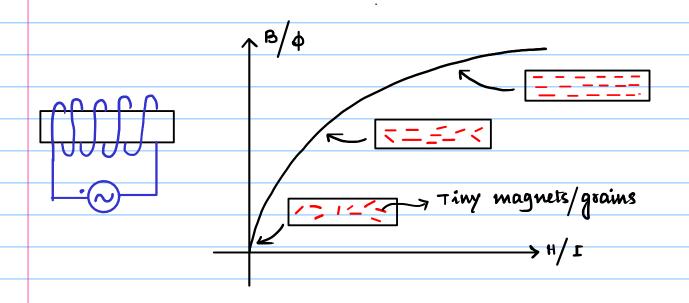
$$P_{H} = Bm f K_{H}$$

$$P_{E} = Bm f^{2} K_{E}$$

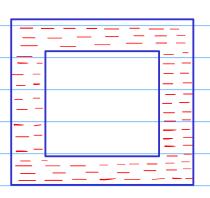
be used for higher freq.

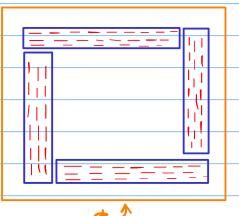
Pi = Iron loss = PH+PE

In recent days cold-rolled-grain-oriented (CR40) Si-Steel is used for the construction of core.



- i) By cold-rolling of the laminated sheets, the grains are made to orient to some extent in the dir? of rolling.
- ii) Thus required magnetizing current will be small.
- manner that the orientation of grains is parallel to the fur bath.

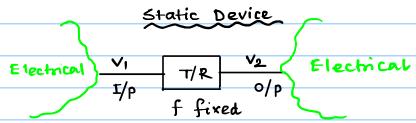




Grain Oriented Steel

Flux path

TRANSFORMER BASICS %-



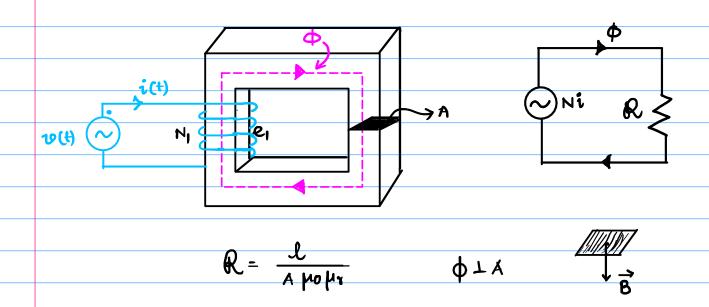
∈fficiency is high (96-98%)

 $V_1 > V_2 \Rightarrow \text{Step down T/F}$ $V_1 < V_2 \Rightarrow \text{Step up T/F}$

$$e = - \frac{N d\phi}{dt} = - \frac{N d\phi}{dt}$$
(Static Device)

$$e = -\frac{d\lambda}{dt} = -\frac{N}{dt} = -\frac{NA}{dt} =$$

$$\lambda = \text{flux linkage} = N\phi$$



We Know
$$\phi = \overrightarrow{B} \cdot \overrightarrow{A} = BACOSWt = \phi_m COSWt$$

$$e_1 = -N_1 \frac{d\phi}{dt} = N_1 \omega \phi m S \dot{m} (\omega t) = (e_1)_m Cos(\omega t - \pi/2)$$

$$E_1 = (e_1)_{8MS} = \frac{N_1 W \phi M}{\sqrt{2}} = \sqrt{2} \pi f N_1 \phi M$$

$$\Phi_{M} = \frac{E_{1}}{\sqrt{2} \pi f N_{1}} = \frac{V_{1}}{\sqrt{2} \pi f N_{1}}$$

- 1 Important Observations:-
- i) om only depends on M, f for a particular coil.
- from core to core. That is for any core is V, f and N are fixed then pmax also will be fixed.