

### ● Efficiency of T/F :-

$$\text{Efficiency } \eta = \frac{P_{out}}{P_{in}} = \frac{P_{out}}{P_{out} + \text{losses}} = \frac{P_{out}}{P_{out} + P_{cu} + P_c}$$

$B_{max}$  remains practically constant from no load to full load condition.

Full load condition is the condition when the coils are carrying the rated current.

- ⊛ Core loss  $P_c$  is practically constant/fixed.
- ⊛ Depending on the loading condition the copper loss  $P_{cu}$  will vary.

$$P_{cu} = |\bar{I}_2'|^2 (R_{eq}) \quad \text{at any current } \bar{I}_2'$$

During SC test the wattmeter reads cu loss at full load current =  $(P_{cu})_{fl}$

During OC test the wattmeter reads core loss at rated voltage and it will be constant/fixed

Now if the T/F is loaded in such that it carries  $k$  times of the rated current then

$$k = \frac{\text{Actual current}}{\text{Full load current}}$$

$$\text{Cu loss will be} = k^2 (P_{cu})_{fl}$$

$k$  is known as the degree of loading on the T/F where

$$0 \leq k \leq 1$$

Therefore at  $k$  degree of loading

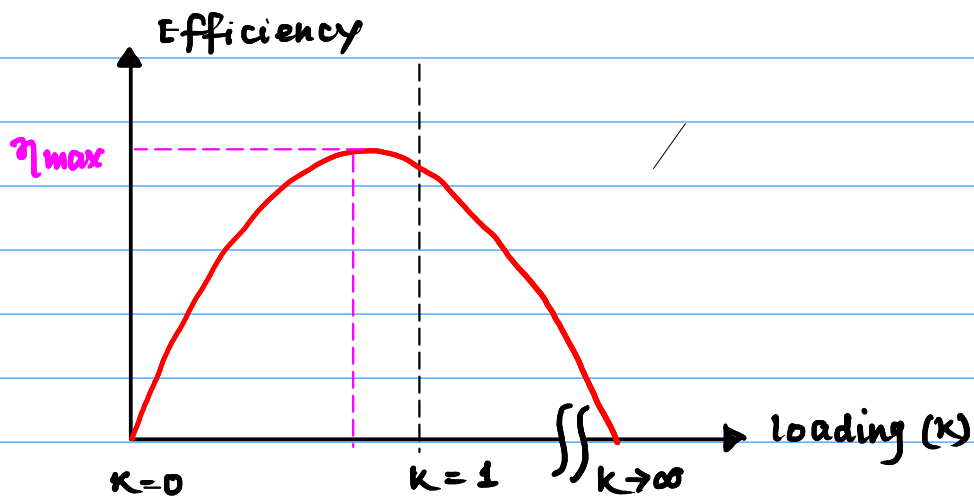
$$\eta_k = \frac{(P_{out})_k}{(P_{out})_k + P_c + (P_{cu})_k}$$

$\cos \theta = \text{power factor of the load}$

$$= \frac{k S \cos \theta}{k S \cos \theta + P_c + k^2 (P_{cu})_{fl}}$$

When  $k=0$  then  $\eta_k=0$

When  $k \rightarrow \infty$  (Theoretically)  $\eta_k \rightarrow 0$



We will keep power factor of the load  $\cos \theta$  constant, we will vary the degree of loading  $k$

$$\eta_k = \frac{kS \cos \theta}{kS \cos \theta + P_c + k^2(P_{cu})_{fl}}$$

$$= \frac{S \cos \theta}{S \cos \theta + \frac{P_c}{k} + k(P_{cu})_{fl}}$$

$$\frac{d\eta_k}{dk} = 0$$

Now  $\eta_k$  will be max. when the denominator is minimum

$$\frac{d}{dk} \left[ S \cos \theta + \frac{P_c}{k} + k(P_{cu})_{fl} \right]_{k=k_m} = 0$$

$$\Rightarrow -\frac{P_c}{k_m} + (P_{cu})_{fl} = 0 \quad \Rightarrow k_m^2 (P_{cu})_{fl} = P_c$$

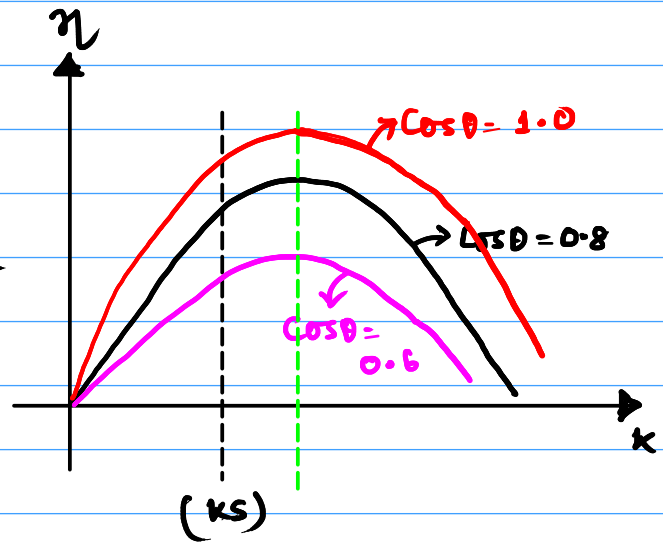
$$\Rightarrow k_m = \sqrt{\frac{P_c}{(P_{cu})_{fl}}}$$

$\eta_k$  will be max, when variable loss is equal to the fixed loss.

$S = \text{Rated kVA of T/F}$

$$(\eta_k)_{\max} = \frac{k_m S \cos \theta}{k_m S \cos \theta + 2P_c}$$

we will keep  $k$  fixed  
 i.e.  $(kS)$  also will be fixed  
 Now we want to see the  
 effect of variation of  
 power factor.



$$\eta = \frac{kS \cos \theta}{kS \cos \theta + k^2 (P_{cu})_{fl} + P_c}$$

You can find out  $\frac{d\eta}{d\theta} = 0$

$\eta$  is maximum when  $\cos \theta = 1$

① Example:-

T/F rating  $\Rightarrow$  10 kVA, 2500/250 V (50 Hz)

OC Test :- 250 V, 0.8 A, 50 W

SC Test :- 60 V, 4 A, 80 W

Q. calculate efficiency at 25% of full load @ 0.8 pf

Q. Load kVA at which max efficiency occurs.

Soln

$$(P_{cu})_{fl} = 80 \text{ kW}$$

$$(P_c) = 50 \text{ W}$$

$$K = 0.25$$

$$\eta_{0.25} = \frac{K S \cos \theta}{K S \cos \theta + P_c + K^2 (P_{cu})_{fl}} \times 100$$

$$= \frac{0.25 \times 10 \times 10^3 \times 0.8}{0.25 \times 10 \times 10^3 \times 0.8 + 50 + (0.25)^2 \times 80} \times 100$$

$$= ?$$

$$K_m = \sqrt{\frac{P_c}{(P_{cu})_{fl}}} = \sqrt{\frac{50}{80}} = ?$$

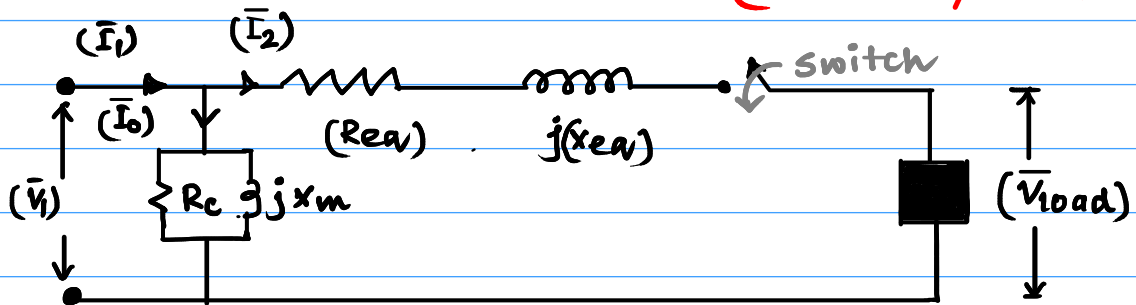
$$I_{HV} = K_m (I_{fl}) = K_m (I_{fl})_{HV} =$$

$$\text{Load kVA} = I_{HV} V_{HV} = ?$$

## ⊙ Voltage regulation:-

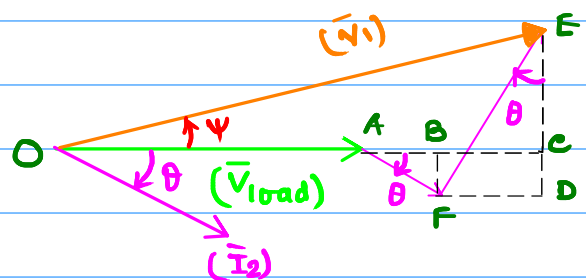
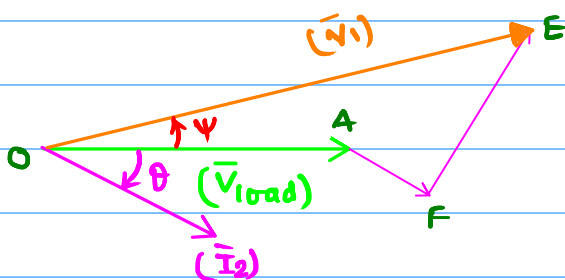
Voltage Regulation is a measure of how the terminal load voltage varies from no load to full load condition.

(say 230V/115V, 1 kVA)



As a consumer our requirement is to maintain 115V at load terminal at any loading

$$\% \text{ Reg} = \frac{|(\bar{V}_{\text{load}})^{\text{NL}}| - |(\bar{V}_{\text{load}})^{\text{FL}}|}{|(\bar{V}_{\text{load}})^{\text{FL}}|} \times 100$$



$$|(\bar{V}_{\text{load}})^{\text{NL}}| = OE \approx OC \quad \text{as } \psi \text{ is very small as the}$$

resistance and leakage reactance of a T/F is low.

$$|(\bar{V}_{load})^{FL}| = OA$$

$$\text{Therefore } \% \text{ Reg} = \frac{OC - OA}{OA} \times 100$$

$$OC = OA + AB + BC$$

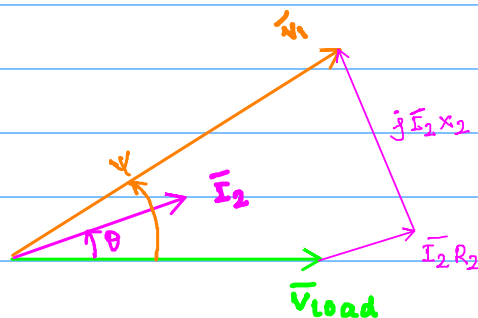
$$= OA + AB + FD$$

$$= OA + I_2 (R_{eq}) \cos \theta + I_2 (X_{eq}) \sin \theta$$

$$OC - OA = I_2 (R_{eq}) \cos \theta + I_2 (X_{eq}) \sin \theta$$

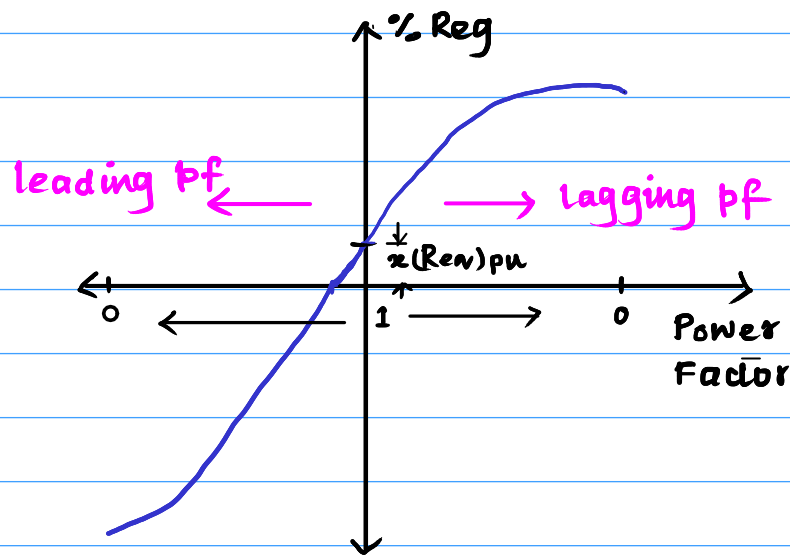
$$\% \text{ Voltage Regulation} = \frac{(I_2) [(R_{eq}) \cos \theta + (X_{eq}) \sin \theta]}{(V_{load})^{FL}} \times 100$$

[Approximate]



$$\% \text{ voltage Regulation} = \frac{I_2 [R_{eq} \cos \theta - X_{eq} \sin \theta]}{(V_{load})^{FL}}$$

[Approximate]



### Maximum Voltage Regulation

$$VR = \frac{I_2 (R_{ew} \cos \theta + x_{ew} \sin \theta)}{(V_{load} FL)}$$

$$\frac{d(VR)}{d\theta} = \frac{I_2 (-R_{ew} \sin \theta + x_{ew} \cos \theta)}{(V_{load} FL)}$$

$$\frac{d(VR)}{d\theta} = 0 \quad \Rightarrow \quad -R_{ew} \sin \theta + x_{ew} \cos \theta = 0$$

$$\Rightarrow \quad \tan \theta = \frac{x_{ew}}{R_{ew}}$$

$$\cos \theta = \frac{R_{ew}}{\sqrt{(R_{ew})^2 + (x_{ew})^2}}$$



### ① Zero voltage Regulation:-

Zero voltage Regulation is possible only for leading load.

For leading load the voltage Regulation is

$$VR = \frac{I_2 [R_{eq} \cos \theta - X_{eq} \sin \theta]}{(V_{load}^{FL})}$$

$$VR = 0 \Rightarrow R_{eq} \cos \theta = X_{eq} \sin \theta$$

$$\Rightarrow \boxed{\tan \theta = \frac{R_{eq}}{X_{eq}}}$$

$$\boxed{\cos \theta = \frac{X_{eq}}{\sqrt{(R_{eq})^2 + (X_{eq})^2}}}$$

⊙ Example :-

T/F rating  $\Rightarrow$  10 kVA, 2500/250 V (50 Hz)

OC Test :- 250 V, 0.8 A, 50 W

SC Test :- 60 V, 4 A, 80 W

- & calculate approximate voltage regulation under rated load for 0.8 pf (lag & lead).
- & calculate the power factor at zero voltage regulation

Sol<sup>n</sup>  $Z_{eq} = \frac{V_{sc}}{I_{sc}} = \frac{60}{4} = 15 \Omega$

$$R_{eq} = \frac{P_{sc}}{(I_{sc})^2} = \frac{80}{16} = 5 \Omega \quad X_{eq} = \sqrt{(15)^2 - (5)^2} = 14.1421 \Omega$$

$$\text{Approx. VR(\%)} = \frac{I (R_{eq} \cos \theta \pm X_{eq} \sin \theta)}{(V_{load})}$$

$$\text{for (lag pf)} = \frac{4 \times (5 \times 0.8 + 14.1421 \times 0.6)}{2500} = ?$$

$$\text{for (lead pf)} = \frac{4 \times (5 \times 0.8 - 14.1421 \times 0.6)}{2500} = ?$$

Zero regulation is possible for leading pf

$$\tan \theta = \frac{R_{eq}}{X_{eq}} = ? \quad \cos \theta = ? \quad (\text{lead})$$