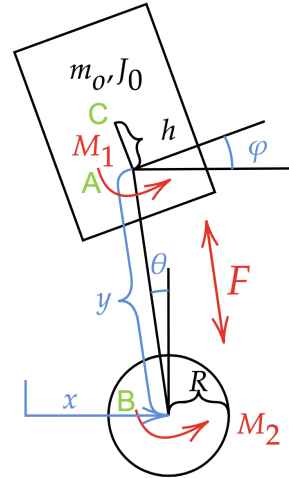


State Estimation and Control of a Bipedal Robot

Derivation of **Kinetic Equations** Based on **Lagrange equation**

$$\begin{aligned}\frac{(m_0 + m_1 + m_2 + \frac{J_2}{R^2})}{m_0} \ddot{x} - y_0 \ddot{\theta} - h \ddot{\varphi} &= -\frac{M_2}{m_0 R} \\ \ddot{y} &= \frac{F}{m_0} - g \\ -y_0 \ddot{x} + (\frac{J_1}{m_0} + y_0^2) \ddot{\theta} + h y_0 \ddot{\varphi} &= \frac{M_1 - M_2}{m_0} + g y_0 \theta \\ -h \ddot{x} + h y_0 \ddot{\theta} + (\frac{J_0}{m_0} + h^2) \ddot{\varphi} &= -\frac{M_1}{m_0} + g h \varphi\end{aligned}$$



Optimal Control Algorithm

We designed control algorithms
based on **LQR**
(implemented on the real-world robot)
and **MPC**
(tested in simulation)

Slip Detection and State Estimation

Based on **physical first principle** that the contact points are relatively stationary for pure rolling, we assume that the contact points of the two wheels and the ground are moving relative to each other when slipping

$$\begin{aligned}\vec{v}_{WL} &= \vec{v}_0 + \vec{\omega} \times \left(-\frac{1}{2} \vec{W} + \vec{l}_L + R \hat{t} \right) + \vec{v}_L + \vec{\omega}_L \times R \hat{t} \\ \vec{v}_{WR} &= \vec{v}_0 + \vec{\omega} \times \left(\frac{1}{2} \vec{W} + \vec{l}_R + R \hat{t} \right) + \vec{v}_R + \vec{\omega}_R \times R \hat{t} \\ \Rightarrow \vec{v}_{WR} - \vec{v}_{WL} &= \vec{\omega} \times \left(\vec{W} + \vec{l}_R - \vec{l}_L \right) + \vec{v}_R - \vec{v}_L + (\vec{\omega}_R - \vec{\omega}_L) \times R \hat{t} \\ |\vec{v}_{WR} - \vec{v}_{WL}| > v_{\text{threshold}} &\text{ implies the wheel is slipping}\end{aligned}$$

$$\begin{aligned}s' &= As + Bu + g \\ P' &= APA^\top + Q \\ s &= s' + P'H^\top (HP'H^\top + R)^{-1} (z - Hs') \\ P &= (I - KH)P'\end{aligned}$$

When slipping, we switch the **Kalman filter**'s observation noise covariance matrix