



**Carnegie Mellon University**

# **Hydrogen Purification and Storage in Electrolysers**

*Mathematical Modelling in Chemical Engineering*

Carnegie Mellon University – April 2025

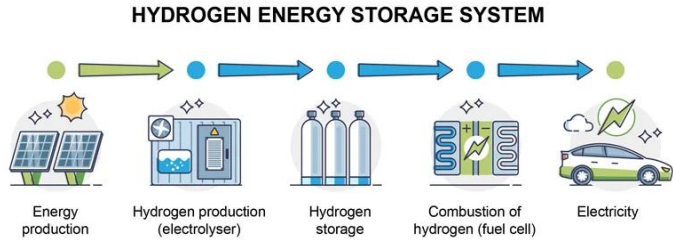
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# Motivation & Context



- Hydrogen is a key player in clean energy transitions.
- PEM (Proton Exchange Membrane) electrolyzers are efficient systems for green hydrogen production.
- However, hydrogen must be purified and safely stored to be usable.
- Understanding the **diffusion behaviour through membranes** enables improved design and operation of these systems.
- Modelling these systems mathematically helps predict and optimise performance before experimental deployment.

# Project Objective

- Develop a simulation model for hydrogen diffusion and purification through a PEM membrane.
- Study the effects of:
  - Feed pressure and temperature
  - Membrane thickness
  - Porosity ( $\epsilon$ ) and Tortuosity ( $\tau$ )
- Compare steady-state and transient diffusion behaviors.
- Optimize the membrane configuration to maximize hydrogen flux.

# System Setup

- **Material:** Nafion-based PEM membrane
- **Geometry:**
  - Membrane thickness: 20–300  $\mu\text{m}$
  - Length: 0.75–50  $\mu\text{m}$
- **Operating Conditions:**
  - Temperature: 350–500 K
  - Feed Pressure: 100–400 kPa
  - Permeate Pressure: 100 kPa
- **Transport Properties:**
  - Diffusivity (D):  $1 \cdot 10^{-5}$  to  $5 \cdot 10^{-10} \text{ m}^2/\text{s}$
  - Porosity ( $\epsilon$ ) and Tortuosity ( $\tau$ ) affect effective permeability

# Steady-State Diffusion – Governing Equation & Setup

## Steady-State Hydrogen Diffusion through PEM

- Governing Equation:  $\frac{d^2C}{dx^2} = 0$  Derived from Fick's Second Law under steady-state ( $\frac{\partial C}{\partial t} = 0$ )
- Fick's First Law of Diffusion (for flux computation):  $J = -D \frac{dC}{dx}$
- Boundary Conditions:  $C(0) = C_{\text{feed}} = \sqrt{p_{\text{feed}}}$        $C(L) = C_{\text{permeate}} = \sqrt{p_{\text{perm}}}$
- Numerical Solution Approach
  - Domain length L split into Nx points.
  - Central difference applied to second derivative:  $\frac{C_{i+1} - 2C_i + C_{i-1}}{\Delta x^2} = 0$
- Matrix Formulation:  $AC=b$  where A Tridiagonal matrix from discretization and b is RHS with boundary conditions.

**scipy.linalg.solve:** Direct solution of linear system

**scipy.optimize.root / fsolve:** Nonlinear root finders used to solve the same system as residual function

# Hydrogen Flux vs. Membrane Thickness vs. Diffusion Coefficient

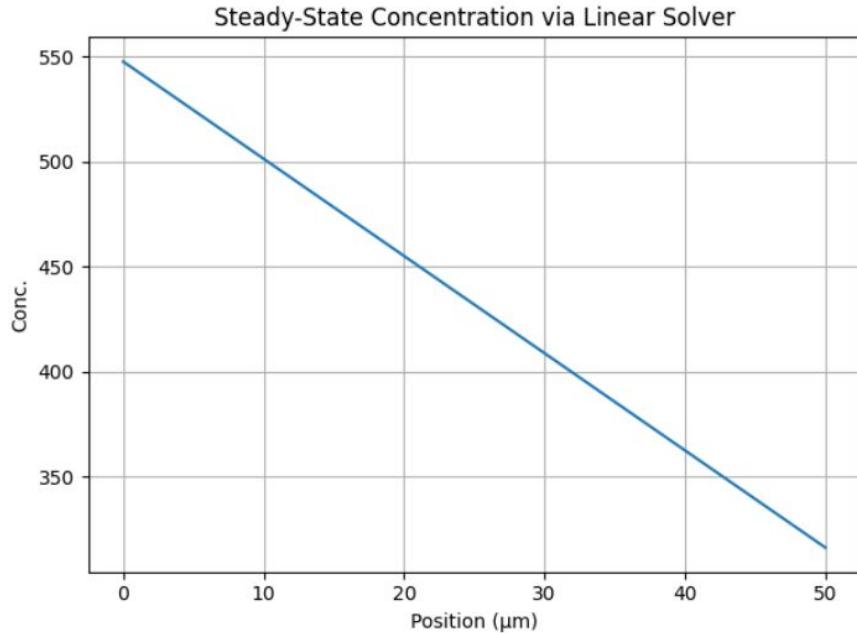
## Effect of Membrane Thickness on Hydrogen Flux

- Equation Used:  $J = \frac{P}{L} (\sqrt{p_{\text{feed}}} - \sqrt{p_{\text{perm}}})$  where  $P = P_0 \exp(-\frac{E_a}{RT})$  Temperature-dependent permeability, L: Membrane thickness.
- As membrane thickness increases, flux decreases sharply.
- Thinner membranes enhance transport, but trade-offs exist (mechanical strength, durability).

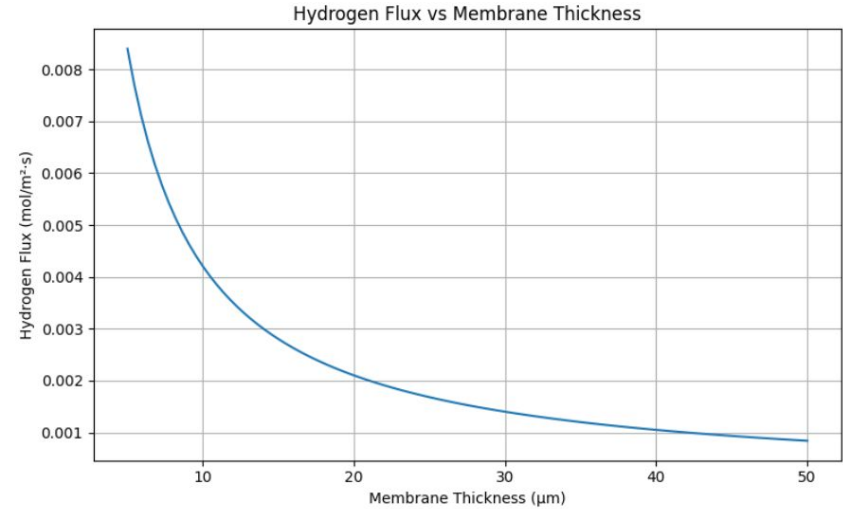
## Effect of Diffusion Coefficient on Flux

- Equation Used:  $J = \frac{D(C_1 - C_2)}{L}$
- Simulation Parameters:
  - L=125μm fixed
  - D=1×10<sup>-10</sup> to 5×10<sup>-10</sup> m<sup>2</sup>/s,
  - Boundary concentrations: C<sub>1</sub> = 1.0, C<sub>2</sub> = 0.0

# Steady state: Concentration and flux

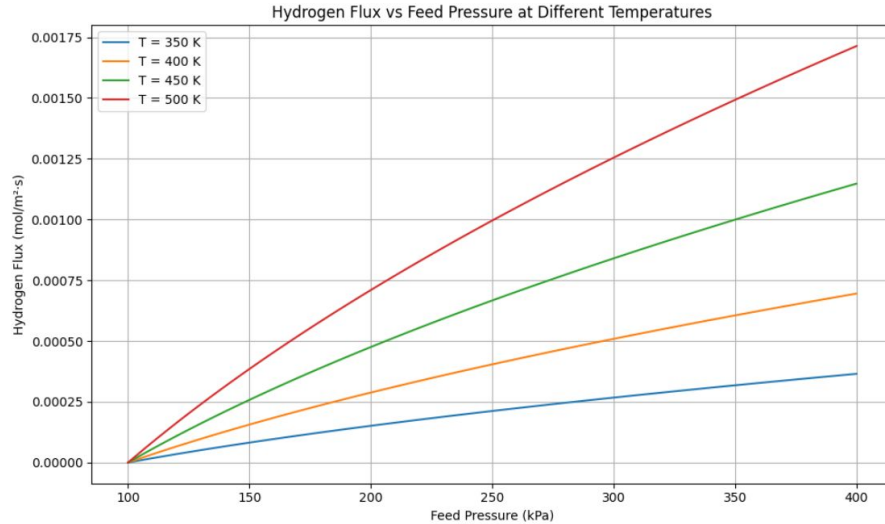


Steady state concentration solved by `scipy.linalg`. The Fick's law gives linear value for conc. vs position

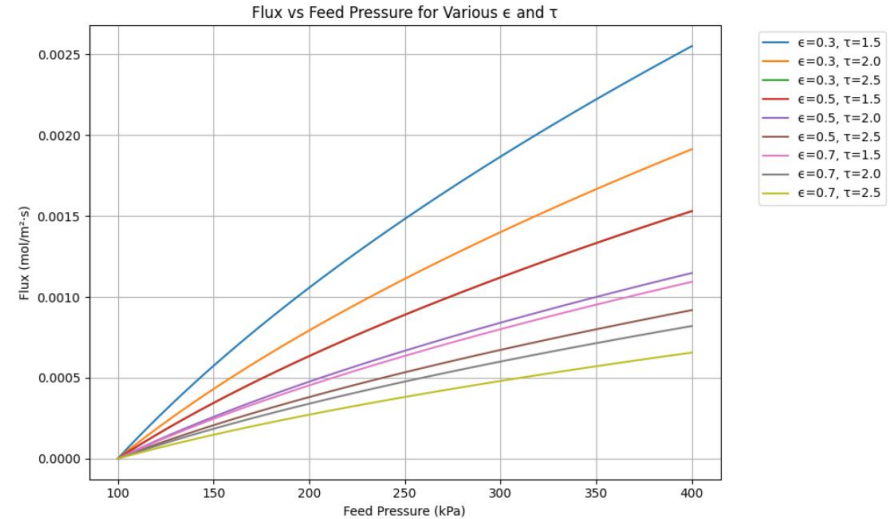


As the membrane thickness increases the flux decreases

# Steady state: Flux vs feed pressure @ temp. and $\epsilon, \tau$



Optimal membrane thickness = 5.00  $\mu\text{m}$   
Maximum hydrogen flux = 8.401e-03 mol/m<sup>2</sup>·s



Optimal Temperature = 450.0 K  
Maximum Flux = 8.401e-04 mol/m<sup>2</sup>·s



# Transient State Simulation in H2 Diffusion

**Governing equation:** Fick's Second Law of Diffusion

$$\frac{\partial C}{\partial t} = D \frac{\partial^2 C}{\partial x^2}$$

**Key parameters:**

- Membrane length:  $L = 0.75 \times 10^{-6} \text{ m}$
- Diffusion coefficient:  $D = 1 \times 10^{-8} \text{ m}^2/\text{s}$

**Boundary Conditions:**

- Left boundary ( $x = 0$ ):  $C = 1.0$  (constant concentration source)
- Right boundary ( $x = L$ ):  $C = 0.0$  (zero concentration)

**Initial Condition:**

- $C(x, t=0) = 0$  for all interior points
- $C(0, t=0) = 1.0$  and  $C(L, t=0) = 0.0$  at boundaries

# Numerical Method Implementation

## Discretization of the PDE

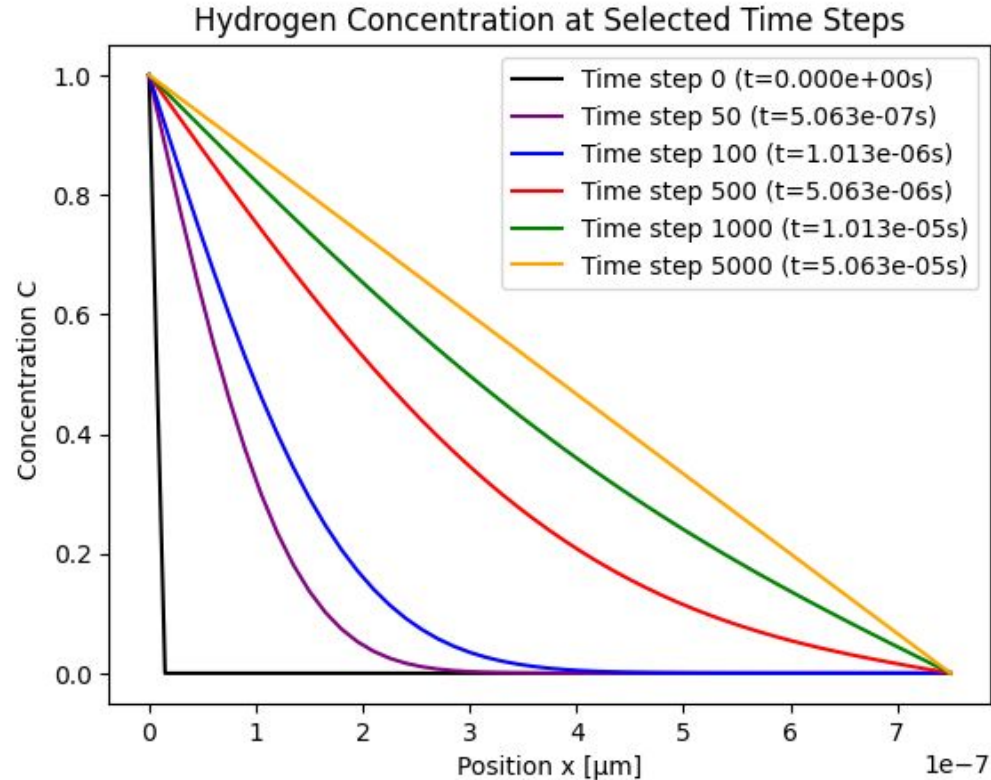
- The continuous PDE is converted to a discrete form using **Finite Difference Method**
- **Spatial discretization:**
  - Domain divided into  $N_x = 51$  points
  - Grid spacing:  $\Delta x = L/(N_x - 1)$

$$\frac{\partial^2 C}{\partial x^2} \approx \frac{C_{i+1} - 2C_i + C_{i-1}}{(\Delta x)^2}$$

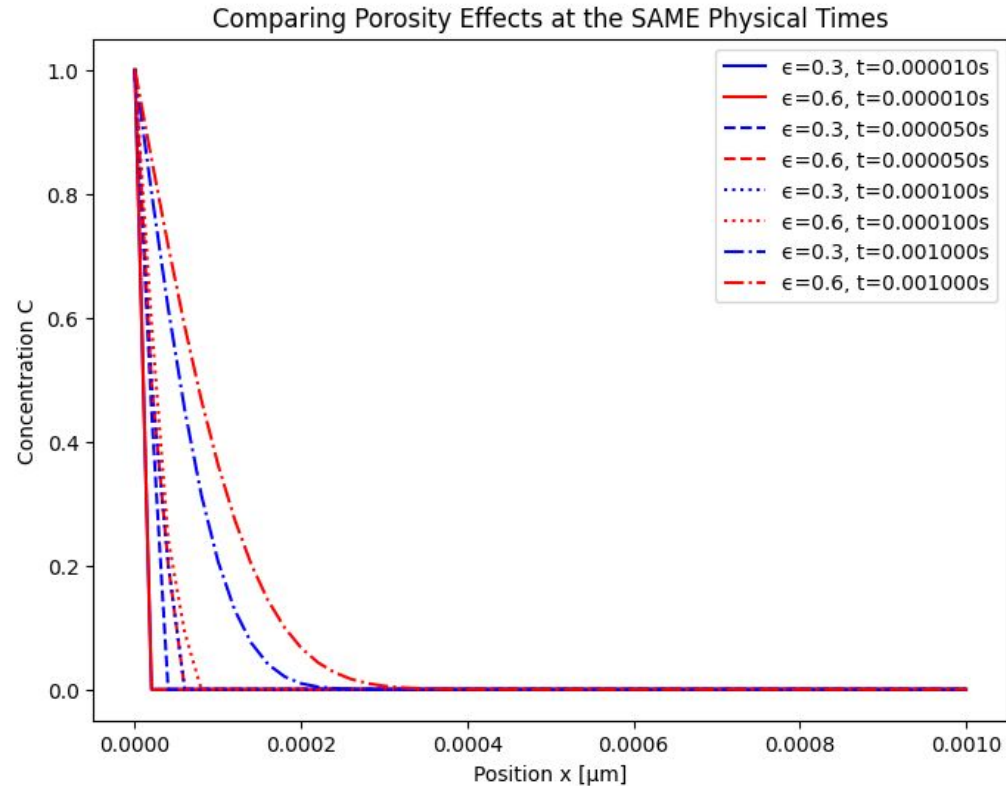
- Second derivative approximation:

$$\frac{C_i^{n+1} - C_i^n}{\Delta t} \approx D \frac{C_{i+1}^n - 2C_i^n + C_{i-1}^n}{(\Delta x)^2} \xrightarrow{\text{rearrange}} C_i^{n+1} \approx C_i^n + \frac{D \Delta t}{(\Delta x)^2} (C_{i+1}^n - 2C_i^n + C_{i-1}^n)$$

# Result Demo: Vanilla Finite Difference method



# Result Demo: Finite Difference + Porosity



# Future Work

- Add temperature-dependence and permeability gradients
- Include non-Fick transport to simulate real membrane data
- Integrate experimental validation

Backup slides