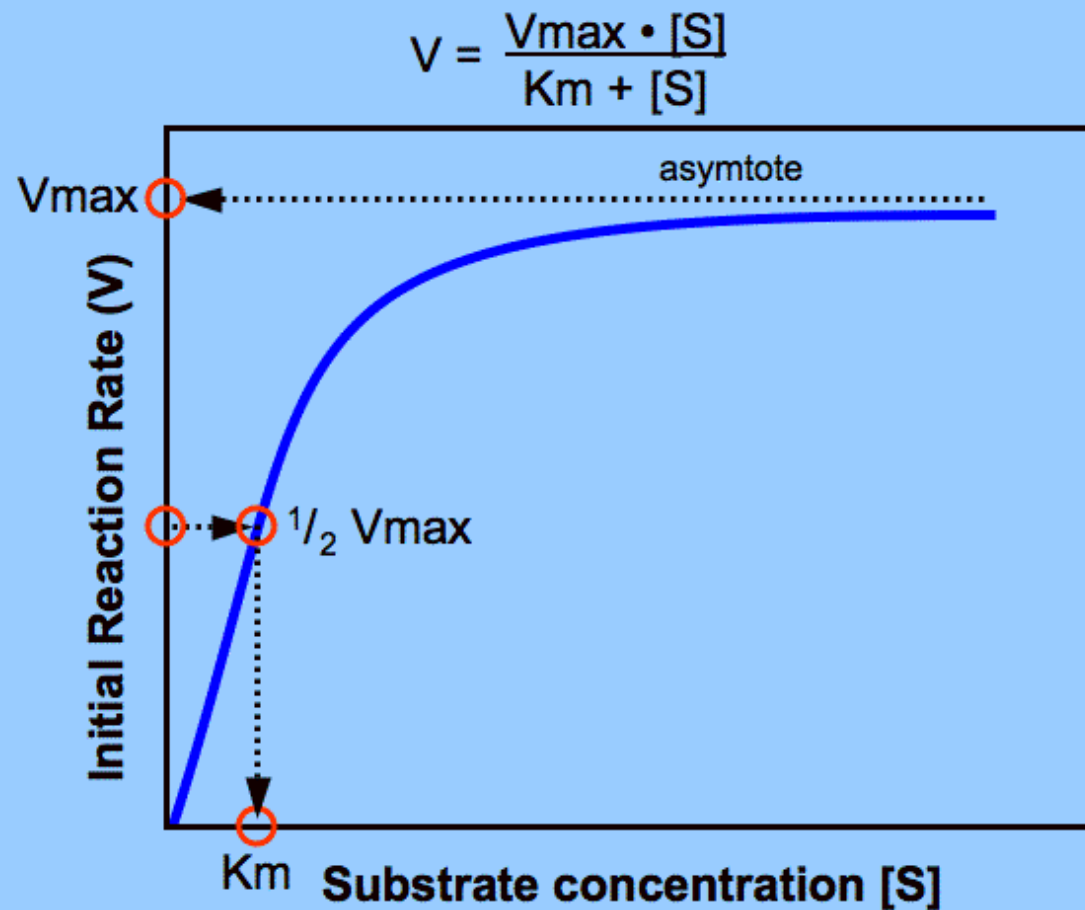


Lecture #3: Michaelis-Menten Kinetics

- (1) Introduction
- (2) Assumptions
- (3) Derivation
- (4) Description of v_o versus $[S]$ curves
- (5) Michaelis constant (K_M)
- (6) Specificity/Substrate constant (SpC)
- (7) Appendix

Michaelis Menten Plot



Michaelis-Menten Kinetics

(1) Introduction



Leonor Michaelis
1875–1949

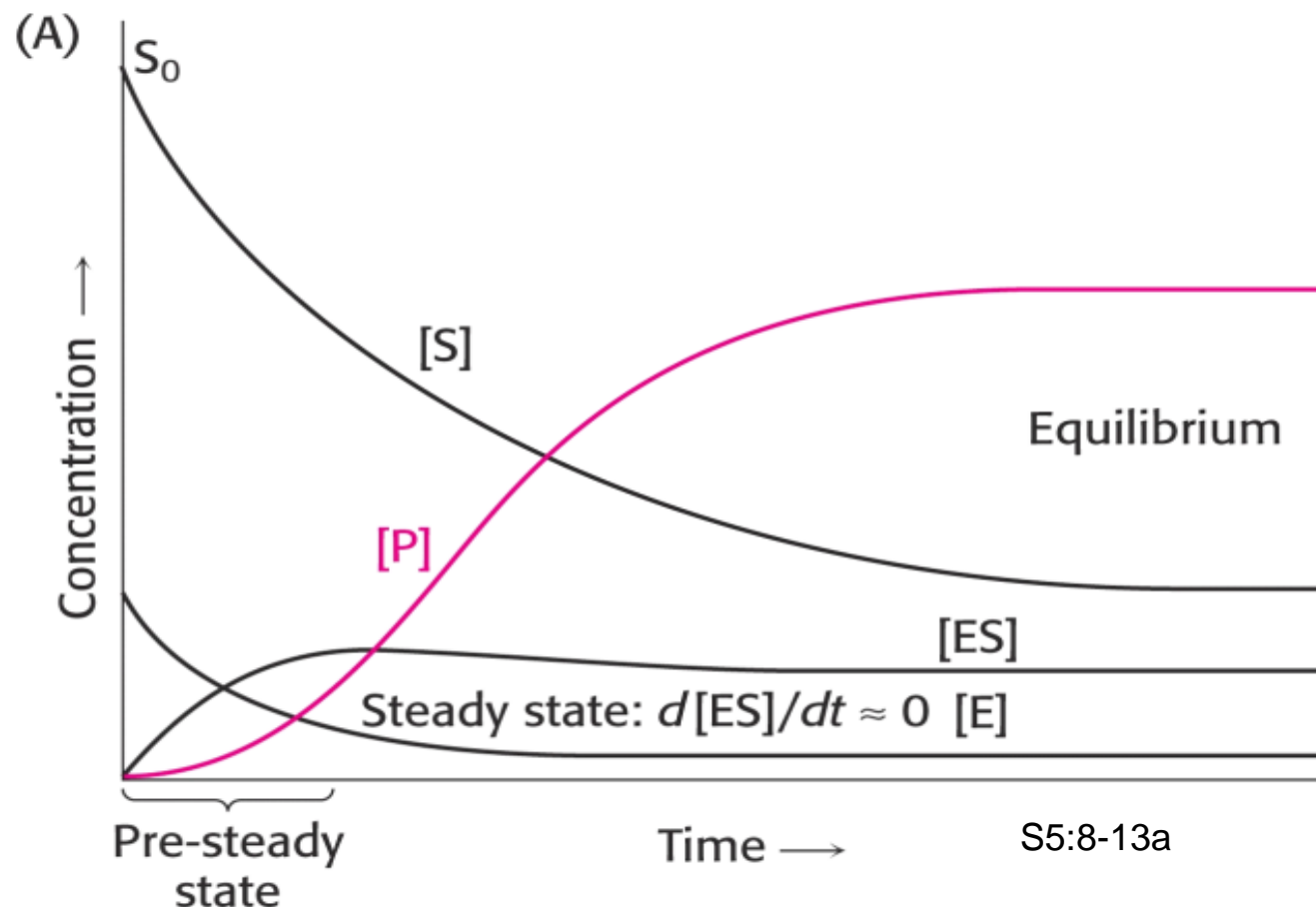


Maud Menten
1879–1960

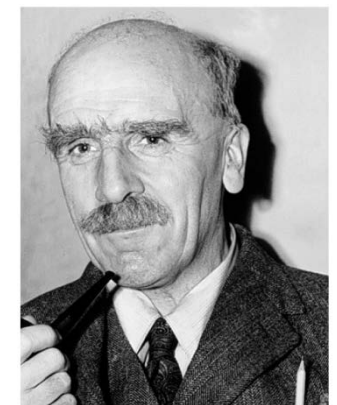
-The M-M treatment (rapid equilibrium approximation \equiv 1913) is unsuitable for many biochemical systems because:

- (a) Many intermediates in enzyme reactions are reactive intermediates
- (b) True equilibrium likely doesn't exist
- (c) Biochemical systems are often a chain of reactions

-apply the steady-state treatment to assume that **the rate of ES formation is equal to the rate of ES consumption** over the short time interval defined by the initial velocity



-in 1925 Briggs and Haldane developed the steady-state treatment



J. B. S. Haldane
1892–1964

2. Assumptions:



(a) the E-S complex is in a **steady-state**

-the rate at which the complex is being formed from E_f and S is equal to the rate at which it is consumed by being broken down to $E + P$ or $E + S$

$$d[ES]/dt = 0$$

(b) The formation of P \propto the concn of ES complex

-the reverse reaction can be ignored (k_{-2} rate)

-implies that the **breakdown of ES to E + P** is *RDS* of reaction

$$v_o = k_2[ES]$$

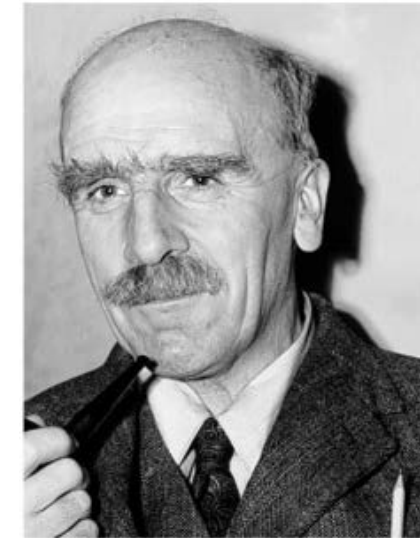
-implies that reverse reaction ($E + P \rightarrow EP \rightarrow ES$) is negligible (true if use **initial velocity!**)

(c) The S concn is much larger than E_T concn

-change in [S] as a result of the formation of ES complex is negligible

-the substrate concn is taken to be a constant

-assumptions (b) and (c) are identical to those of M-M treatment



J. B. S. Haldane
1892–1964

- **Deviation from M-M kinetics happens when:**

- There are multiple catalytic steps ($k_2 \neq k_{cat}$)

- [ES] is not at steady state

- The enzyme displays cooperativity

- There are multiple substrates

- Substrate binding is irreversible

3. Derivation



-assumption (a): $d[ES]/dt = 0$ {K-1}

Rate of formation of ES = Rate of consumption of ES

Rate of formation = $k_1[E_f][S] + \cancel{k_{-2}[E_f][P]}$ {K-2}

-based on assumption (b) the second term can be ignored (reverse reaction) so:

Rate of ES formation = $k_1[E_f][S]$ {K-3}

Rate of ES consumption = $k_{-1}[ES] + k_2[ES] = (k_{-1} + k_2)[ES]$ {K-4}

$d[ES]/dt = k_1[E_f][S] - (k_{-1} + k_2)[ES] = 0$ {K-5}

$k_1[E_f][S] = (k_{-1} + k_2)[ES]$ {K-6}

Mass Conservation Equation for $[E_T]$ at constant $[S]$

$[E_T] = [E_f] + [ES]$ {K-7}

and $[E_f] = [E_T] - [ES]$ {K-8}

-substitute $[E_T] - [ES]$ from {K-8} into {K-6} for $[E_f]$

$$k_1([E_T] - [ES])[S] = (k_{-1} + k_2)[ES] \quad \text{{K-9} group rate constants}$$

$$([E_T] - [ES])[S] = \{(k_{-1} + k_2)/k_1\}[ES] \quad \text{{K-10}}$$

-define a new constant, K_M , such that: $K_M = (k_{-1} + k_2)/k_1$ {K-11}

-called the "**Michaelis constant**"

-substituting K_M into {K-10} yields:

$$([E_T] - [ES])[S] = K_M[ES] \quad \text{or}$$

$$[E_T][S] - [ES][S] = K_M[ES] \quad \text{{K-12} get [ES] out of eq.}$$

-velocity of reaction based on assumption (b) and so:

$$v_o = k_2[ES] \quad \text{{K-13}}$$

or

$$[ES] = v_o/k_2$$

-substituting for $[ES]$ into {K-12} gives the rate equation:

$$[E_T][S] - v_o/k_2 * [S] = K_M * v_o/k_2 \quad \text{{K-14}}$$

-rearranging {K-14} gives: (multiply by k_2)

$$k_2[E_T][S] - v_o[S] = K_M v_o \quad \text{{K-15}}$$

At **saturation** conditions: $k_2 = k_{\text{cat}}$

-recall: $\text{TN } (k_{\text{cat}}) = V_{\text{max}}/[E_T]$ so:

$$k_2 = V_{\text{max}}/[E_T] \quad \{\text{K-16}\}$$

$$V_{\text{max}} = k_2[E_T] \quad \{\text{K-17}\}$$

-substitute V_{max} into {K-15}

$$k_2[E_T][S] - v_o[S] = K_M v_o \quad \{\text{K-15}\}$$

$$V_{\text{max}}[S] - v_o[S] = K_M v_o \quad \text{and rearrange}$$

$$V_{\text{max}}[S] = K_M v_o + v_o[S] \quad \text{group terms}$$

$$V_{\text{max}}[S] = v_o(K_M + [S]) \quad \text{solve for } v_o$$

$$v_o = V_{\text{max}}[S]/(K_M + [S]) \quad \{\text{K-18}\}$$

Michaelis-Menten Equation!

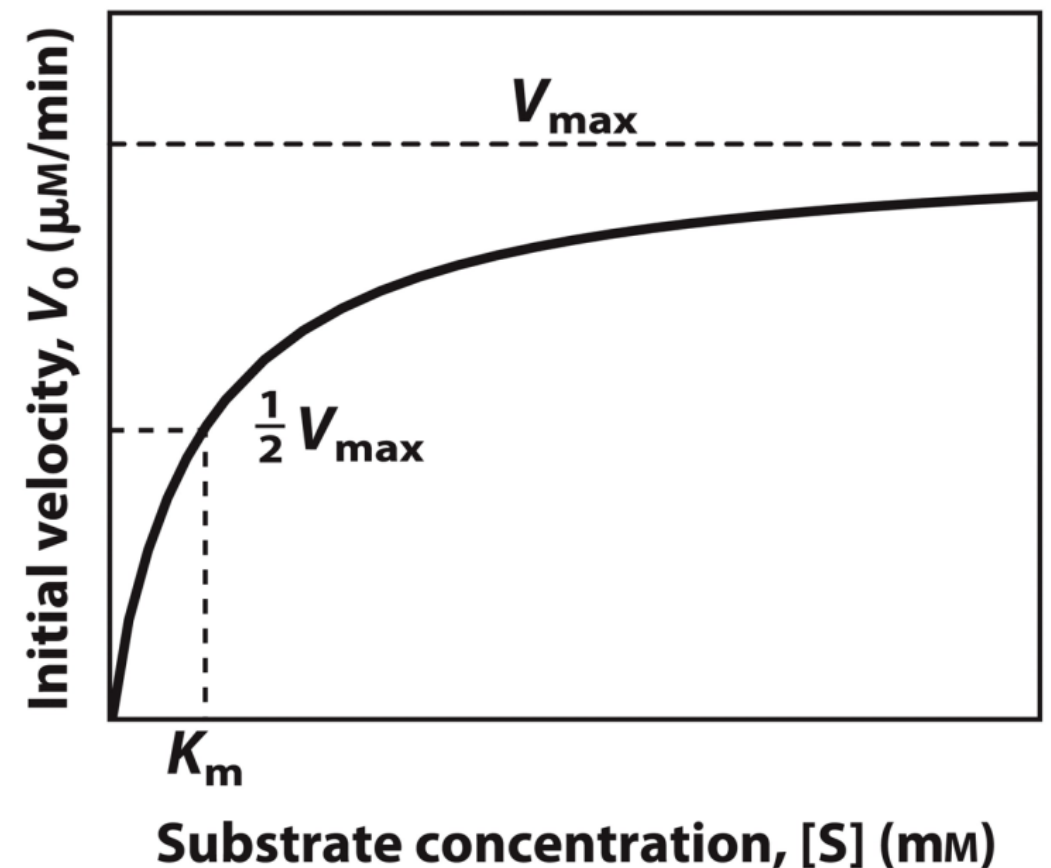
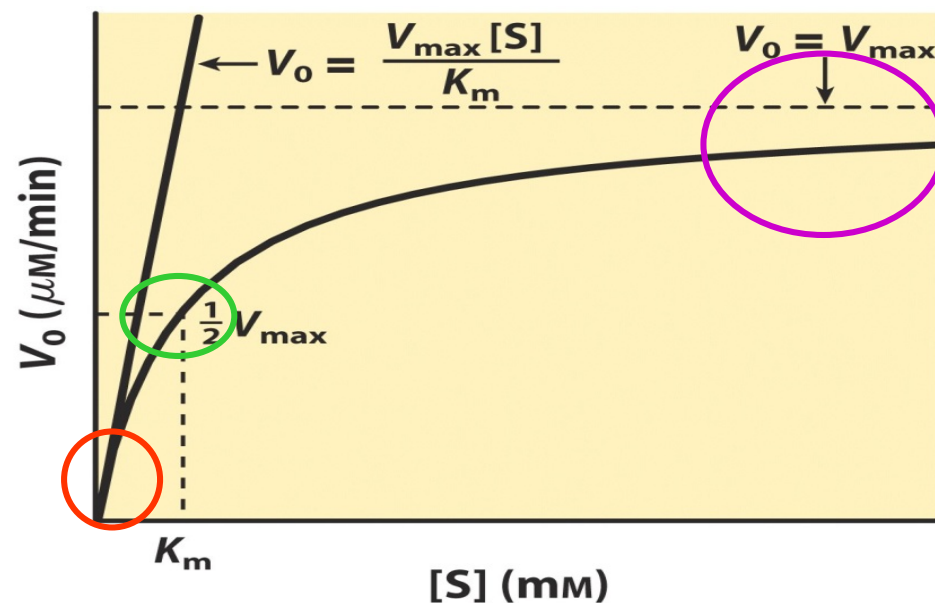


Figure 6-11
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4. Description of v_o versus $[S]$ curve:

i. When $[S] \ll K_M$ then {K-18} becomes:

$$v_o = V_{\max}[S]/(K_M + [S]) = V_{\max}[S]/K_M = k''[S] \quad \{K-19\}$$

where $k'' = V_{\max}/K_M = \text{constant}$

-{K-19} is rate equation for first order reaction with $v_o \propto [S]$

-low concn range of v versus $[S]$ curve

ii. When $[S] \gg K_M$ then {K-18} becomes: (drop K_M)

$$v_o = V_{\max}[S]/(K_M + [S]) = V_{\max}[S]/[S] = V_{\max} \quad \{K-20\}$$

-{K-20} is rate equation for a **zero order reaction** with v_o independent of $[S]$

-high end of v_o versus $[S]$ curve

iii. Central part of v_o versus $[S]$ curve is described by intermediate range of $[S]$

-**special case:** when $[S] = K_M$

$$v_o = V_{\max}[S]/(K_M + [S]) = V_{\max}[S]/([S] + [S]) = V_{\max}/2$$

- K_M defined as being **equal to that substrate concn which gives one half of the maximum velocity of reaction**

- K_M has units of concn (M)

5. Michaelis Constant (K_M)

(a) K_M is $[S]$ at which one half of V_{\max} of a reaction is observed

(b) K_M has units of concn

(c) K_M is a constant only under rigorously defined conditions of pH, T, ionic strength, etc

-if reaction has 2 or more substrates, the true K_M for a given substrate is when all other $[S]$ are at saturation

- V_{\max} is that observed when all substrates are at sat'n concn

(d) Values for K_M vary greatly from E to E

-generally range 10^{-8} to 1.0 M

-large K_M : **means that one half of V_{\max} is achieved at a relatively large S concn**

-small K_M : **means that 1/2 of V_{\max} occurs at relatively low S concn**

(e) K_M is **not** an equilibrium constant, but rather a complex constant, composed of various rate constants

$$K_M = (k_{-1} + k_2)/k_1 \text{ for simple reaction}$$



(f) K_M is **not** a dissociation constant of the ES complex

Numerical values of K_M

(a) K_M relates reaction velocity to $[S]$ and indicates the **approximate level of the intracellular $[S]$**

-unlikely that intracellular $[S]$ would be significantly higher or lower than the K_M

(b) K_M is a **characteristic constant** for a given E under defined conditions

-useful to help identify an enzyme

(c) K_M is useful for comparing the activity of different E and for comparing the "suitability" of alternate substrates for the same E

-a substrate with a lower K_M is a better substrate

(d) best S of an E is one which leads to the **highest V_{max} and the lowest K_M**

-a substrate which yields the highest V_{max}/K_M ratio

TABLE 6-6 K_m for Some Enzymes and Substrates

Enzyme	Substrate	K_m (mM)
Hexokinase (brain)	ATP	0.4
	D-Glucose	0.05
	D-Fructose	1.5
Carbonic anhydrase	HCO_3^-	26
Chymotrypsin	Glycyltyrosinylglycine	108
	N-Benzoyltyrosinamide	2.5
β -Galactosidase	D-Lactose	4.0
Threonine dehydratase	L-Threonine	5.0

Table 6-6
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(e) Knowing the K_M value permits adjustment of assay conditions, one can vary $[S]$ according to the needs of assay

-can then measure total $[E]$ or $[S]$

(f) K_M values useful in evaluating the relative roles of forward and reverse reactions in metabolism

6. Specificity Constant (SpC)

- recall: (V_{max} or k_{cat}) is the maximum number of moles of substrate that are converted to product each second per mole of enzyme

- k_{cat} is a measure of **how rapidly an enzyme can operate once the active site is filled**

$$\bullet k_{cat} = V_{max}/[E]$$

-under physiological conditions, enzymes **do not operate** at saturating S conditions

-usually the ratio of $[S]:K_M$ is in the range of 0.01 to 1.0.

-previously determined that at low $[S]$ then:

$$v_o = V_{max}[S]/K_M$$

- the number of moles of S converted to P per second per mole of enzyme = $(V_{max}[S]/K_M)/[E] = (k_{cat}/K_M)[S]$

-the ratio k_{cat}/K_M is therefore a measure of **how rapidly an enzyme can work at low $[S]$**

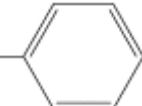
-known as the "**specificity constant**" (SpC)

$-k_{\text{cat}}/K_M$ compares the relative abilities of different compounds to serve as a substrate for a given enzyme

- SpC: compares the rate of an enzyme-catalyzed reaction with the rate of random diffusion of the enzyme and substrate

-if every collision between a protein and a small molecule resulted in a reaction, the max possible value of the second-order rate constant would be 10^8 to $10^9 \text{ M}^{-1}\text{s}^{-1}$

TABLE 8.7 Substrate preferences of chymotrypsin

Amino acid in ester	Amino acid side chain	$k_{\text{cat}}/K_M (\text{s}^{-1} \text{M}^{-1})$
Glycine	—H	1.3×10^{-1}
Valine	$\begin{array}{c} \text{CH}_3 \\ \\ \text{—CH} \\ \\ \text{CH}_3 \end{array}$	2.0
Norvaline	—CH ₂ CH ₂ CH ₃	3.6×10^2
Norleucine	—CH ₂ CH ₂ CH ₂ CH ₃	3.0×10^3
Phenylalanine	—CH ₂ — 	1.0×10^5

Source: After A. Fersht, *Structure and Mechanism in Protein Science: A Guide to Enzyme Catalysis and Protein Folding* (W. H. Freeman and Company, 1999), Table 7.3.

TABLE 6–8 Enzymes for Which k_{cat}/K_m Is Close to the Diffusion-Controlled Limit (10^8 to $10^9 \text{ M}^{-1}\text{s}^{-1}$)

Enzyme	Substrate	$K_{\text{cat}} (\text{s}^{-1})$	$K_m (\text{M})$	$K_{\text{cat}}/K_m (\text{M}^{-1}\text{s}^{-1})$
Acetylcholinesterase	Acetylcholine	1.4×10^4	9×10^{-5}	1.6×10^8
Carbonic anhydrase	CO ₂	1×10^6	1.2×10^{-2}	8.3×10^7
	HCO ₃ [−]	4×10^5	2.6×10^{-2}	1.5×10^7
Catalase	H ₂ O ₂	4×10^7	1.1×10^0	4×10^7
Crotonase	Crotonyl-CoA	5.7×10^3	2×10^{-5}	2.8×10^8
Fumarase	Fumarate	8×10^2	5×10^{-6}	1.6×10^8
	Malate	9×10^2	2.5×10^{-5}	3.6×10^7
β-Lactamase	Benzylpenicillin	2.0×10^3	2×10^{-5}	1×10^8

Source: Fersht, A. (1999) *Structure and Mechanism in Protein Science*, p. 166, W. H. Freeman and Company, New York.

Table 6-8
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-some enzymes have achieved an **astounding state** of perfection!

-only way to **increase rate** is to (i) generate substrate at the active site or (ii) decrease the size of the E moiety

-first possibility arises when two or more E are combined in a multi-enzyme complex

-the product of one reaction can then be released close to the active site of the next E

-second possibility is difficult since the sizes of E are limited by the need for tertiary structure to create the proper active site geometry

-large sizes of E are dictated by the need for secondary binding sites for effector molecules that regulate enzymatic activity

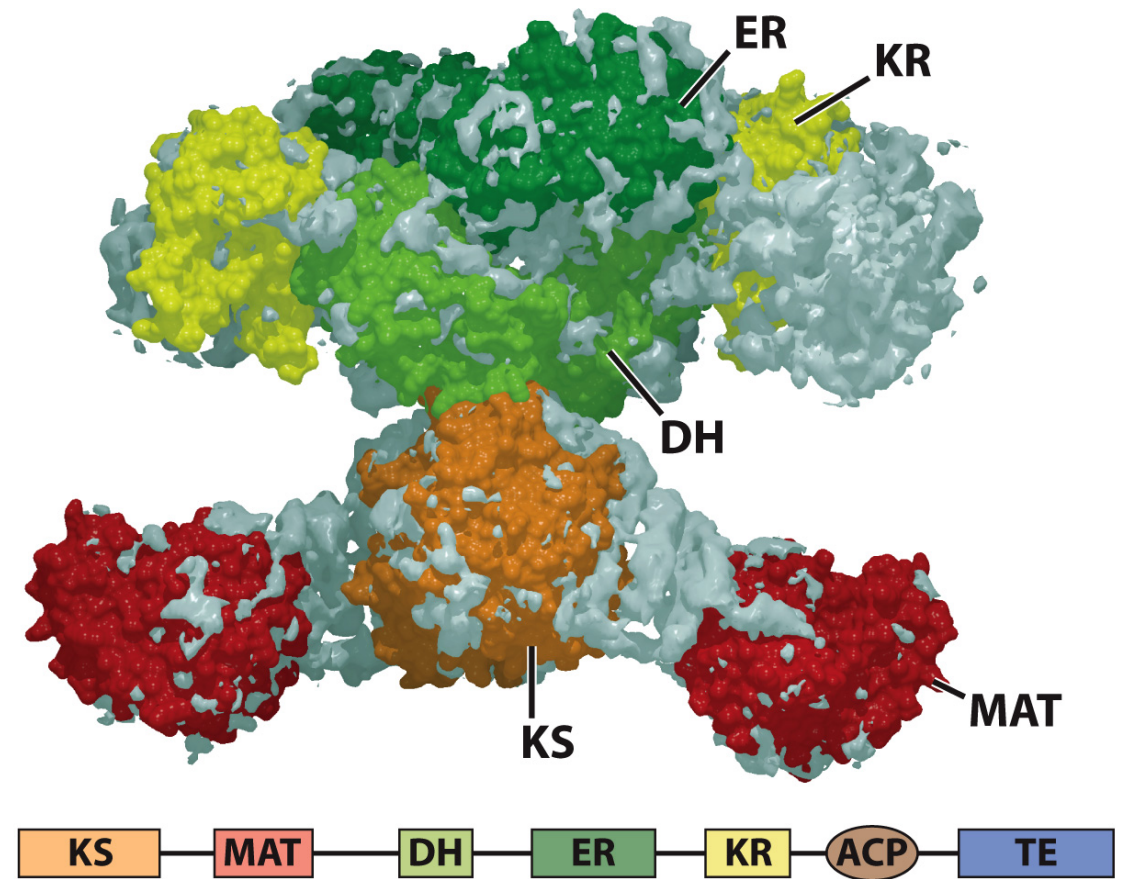
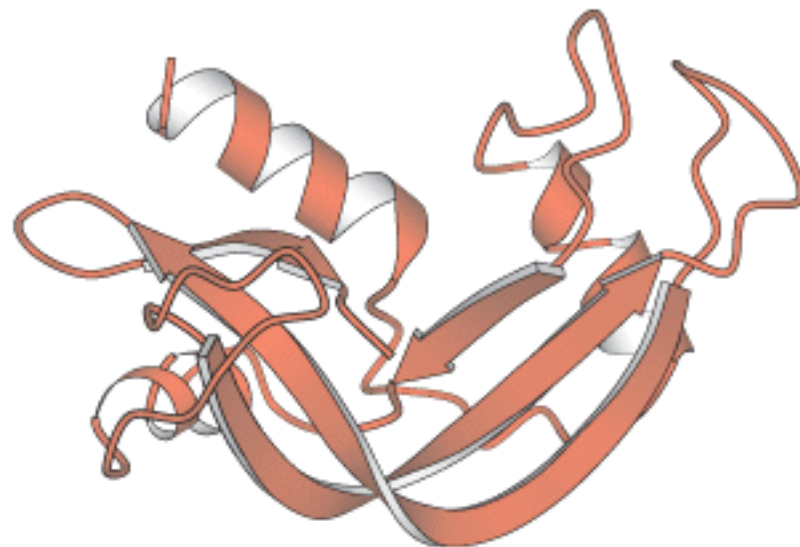
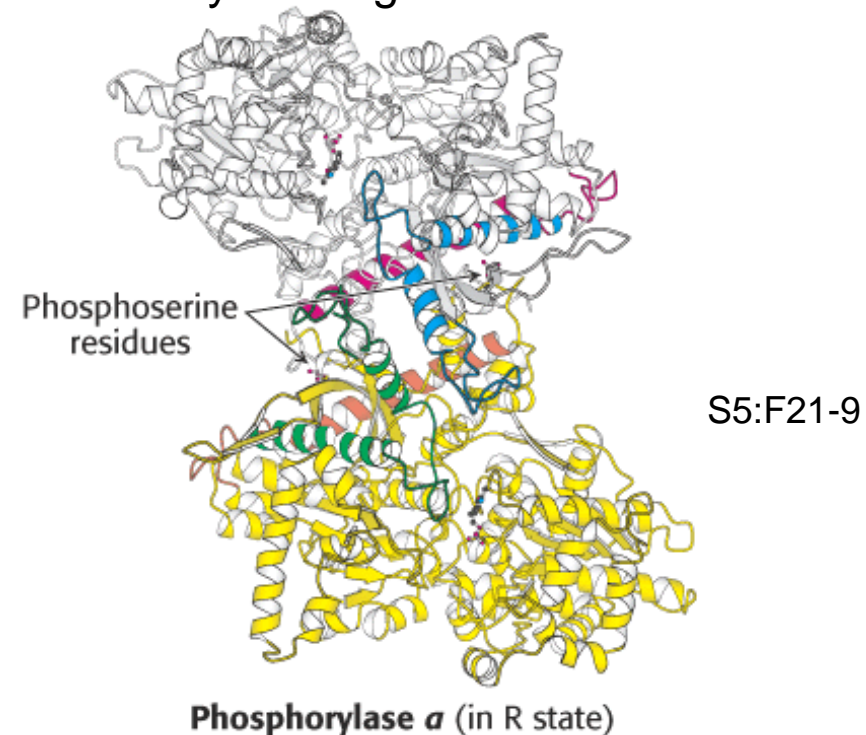


Figure 21-3a
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S5:F7-1

Human ribonuclease



Phosphorylase α (in R state)

Appendix

Michaelis-Menten Equation (Integrated Form)

Comment: You may wish to use the integrated Michaelis-Menten equation to determine the precise changes in [S] during an enzyme-catalyzed reaction or to determine how long it will take to form a certain amount of product, etc. This derivation is for your reading pleasure only and is meant to be background information to support some questions found in Problem Set#2 (e.g., Question #8).

(1) Derivation

- for calculations involving changes as a function of reaction time, the integrated form of the Michaelis-Menten equation must be used
- the Michaelis-Menten equation is a differential equation since velocity is the rate of change of either substrate consumption or product formation

thus, $v = -d[S]/dt = d[P]/dt$

the M-M equation can be written as: $-d[S]/dt = V_{\max}[S]/(K_M + [S])$ **[M-1]**

separating variables: $-V_{\max}dt = (K_M/[S] + 1)d[S]$ **[M-2]**

equation can be integrated between an initial time (t_0) and a final time (t) for which the corresponding substrate concns are $[S]_0$ and $[S]_t$, respectively.

$$-1 \int_{t_0}^t V_{\max} dt = \int_{t_0}^t \left(\frac{K_M}{[S]} + 1 \right) d[S] \quad \text{[M-3]}$$

$$V_{\max}(t-t_0) = K_M \ln([S]_0/[S]_t) + ([S]_0 - [S]_t) \quad \text{[M-4]}$$

If we let $t_0 = 0$ and $y = ([S]_0 - [S]_t)$ and substituting for $[S]_t$

where $[S]_t = [S]_0 - y$

$$\text{then, } V_{\max}t = K_M \ln([S]_0/[S]_0 - y) + y \quad \text{[M-5]}$$

$$\text{converting to ordinary logs: } V_{\max}(t) = 2.303 K_M \log([S]_0/([S]_0 - y)) + y \quad \text{[M-6]}$$

$$\text{rearranging yields: } V_{\max} = 2.303 K_M (1/t) \log([S]_0/([S]_0 - y)) + (y/t) \quad \text{[M-7]}$$

$$2.303 K_M (1/t) \log([S]_0/([S]_0 - y)) = V_{\max} - (y/t) \quad \text{[M-8]}$$

$$2.303/t \log([S]_0/([S]_0 - y)) = -1/K_M (y/t) + V_{\max}/K_M \quad \text{[M-9]}$$

(2) Simplified forms

-Equation M-9 (above) reduces to simpler forms when the substrate concn is either very large or small compared to K_M and y
-if $[S]_0 \gg K_M$ and much larger than the change in substrate concn (y) then equation M-9 reduces to:

$$2.303/t \log([S]_0/[S]_t) = -1/K_M (y/t) + V_{\max}/K_M \quad [\mathbf{M-10}]$$

that is, $y/t = V_{\max}$ **[M-11]**

but, y/t is the change in $[S]$ per unit time, i.e., the velocity of the reaction

$$v = y/t = V_{\max} \quad [\mathbf{M-12}]$$

likewise, if $[S]_0$ (and hence y) is $\ll K_M$ then equation M-9 reduces to:

$$2.303/t \log([S]_0/([S]_0 - y)) = V_{\max}/K_M \quad [\mathbf{M-13}]$$

which describes a first order reaction (initial part of v versus $[S]$ curve)

V_{\max}/K_M is the first order rate constant (k) and thus equation M-13 can be rewritten:

$$2.303 \log([S]_0/[S]_t) = kt \quad [\mathbf{M-14}]$$

$$\log([S]_0/[S]_t) = kt/2.303 \quad [\mathbf{M-15}]$$

$$\log[S]_0 - \log[S]_t = kt/2.303 \quad [\mathbf{M-16}]$$

$$-\log[S]_t = kt/2.303 - \log[S]_0 \quad [\mathbf{M-17}]$$

$$\log[S]_t = -kt/2.303 + \log[S]_0 \quad [\mathbf{M-18}]$$

$$[S]_t = [S]_0 e^{-kt} \quad [\mathbf{M-19}]$$

the half-life for this first order reaction: at $t_{1/2}$ then $[S]_t/[S]_0 = 0.5$
so: $[S]_t/[S]_0 = e^{-kt}$ **[M-20]**

$$0.5 = e^{-kt} \quad [\mathbf{M-21}]$$

$$\ln(0.5) = -kt_{1/2} \quad [\mathbf{M-22}]$$

$$t_{1/2} = 0.693/k = 0.693K_M/V_{\max} \quad [\mathbf{M-23}]$$