$$\begin{split} & \underbrace{\beta(t)} = \underbrace{\sum_{i=0}^{n} \binom{n}{i} (1-t)^{n-i} t^{i} \underbrace{P_{i}}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 2000mm, 0mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 2000mm, 0000mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 13165 \cdot 2mm, 10080 \cdot 3mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 13165 \cdot 2mm, 10080 \cdot 3mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 13165 \cdot 2mm, 10080 \cdot 3mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 13165 \cdot 2mm, 10080 \cdot 3mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 13165 \cdot 2mm, 10080 \cdot 3mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 13165 \cdot 2mm, 10080 \cdot 3mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 13165 \cdot 2mm, 10080 \cdot 3mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 13165 \cdot 2mm, 10080 \cdot 3mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 13165 \cdot 2mm, 10080 \cdot 3mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 13165 \cdot 2mm, 10080 \cdot 3mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 13165 \cdot 2mm, 10080 \cdot 3mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 13165 \cdot 2mm, 10080 \cdot 3mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 13165 \cdot 2mm, 10080 \cdot 3mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 13165 \cdot 2mm, 10080 \cdot 3mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 13165 \cdot 2mm, 10080 \cdot 3mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 13165 \cdot 2mm, 10080 \cdot 3mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 13165 \cdot 2mm, 10080 \cdot 3mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 13165 \cdot 2mm, 10080 \cdot 3mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 13165 \cdot 2mm, 10080 \cdot 3mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 13165 \cdot 2mm, 10080 \cdot 3mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 13165 \cdot 2mm, 10080 \cdot 3mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 13165 \cdot 2mm, 10080 \cdot 3mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 13165 \cdot 2mm, 10080 \cdot 3mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 13165 \cdot 2mm, 10080 \cdot 3mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 13165 \cdot 2mm, 10080 \cdot 3mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 13165 \cdot 2mm, 10080 \cdot 3mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 13165 \cdot 2mm, 10080 \cdot 3mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 13165 \cdot 2mm, 10080 \cdot 3mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 13165 \cdot 2mm, 10080 \cdot 3mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \begin{bmatrix} 13165 \cdot 2mm, 10080 \cdot 3mm \end{bmatrix}}_{\text{control peak}} & \underbrace{P_{i}} = \underbrace{P_{i}} = \underbrace{P_{i}}$$

$$B(t) = \sum_{i=0}^{3} {3 \choose i} (i-t)^{3-i} t P_i$$

$$B(t) = {3 \choose 0} (i-t)^{3} P_0 + {3 \choose i} (i-t)^{2} t P_i + {3 \choose 2} (i-t) t^{2} P_2 + {3 \choose 3} (i-t)^{6} t^{2} P_3$$

$$B(t) = (i-t)^{3} P_0 + 3 (i-t)^{2} t P_i + 3 (i-t) t^{2} P_2 + (i-t)^{6} t^{2} P_3$$

$$B(t) = (i-t)^{3} P_0 + 3 (i-t)^{2} t P_i + 3 (i-t) t^{2} P_2 + (i-t)^{6} t^{2} P_3$$

$$B(t) = (i-t)^{3} P_0 + 3 (i-t)^{2} t P_1 + 3 (i-t)^{2} t P_2 + t^{2} P_3$$

$$E(t) = (i-t)^{3} P_0 + 3 (i-t)^{2} t P_1 + 3 (i-t)^{2} t P_2 + t^{2} P_3$$

$$E(t) = (i-t)^{3} P_0 + 3 (i-t)^{2} t P_1 + 3 (i-t)^{2} t P_2 + t^{2} P_3$$

$$E(t) = (i-t)^{3} P_0 + 3 (i-t)^{2} t P_1 + 3 (i-t)^{2} t P_2 + t^{2} P_3$$

$$E(t) = (i-t)^{3} P_0 + 3 (i-t)^{2} t P_1 + 3 (i-t)^{2} t P_2 + t^{2} P_3$$

$$E(t) = (i-t)^{3} P_0 + 3 (i-t)^{2} t P_1 + 3 (i-t)^{2} t P_2 + t^{2} P_3$$

$$E(t) = (i-t)^{3} P_0 + 3 (i-t)^{2} t P_1 + 3 (i-t)^{2} t P_2 + t^{2} P_3$$

$$E(t) = (i-t)^{3} P_0 + 3 (i-t)^{2} t P_1 + 3 (i-t)^{2} t P_2 + t^{2} P_3$$

$$E(t) = (i-t)^{3} P_0 + 3 (i-t)^{2} t P_1 + 3 (i-t)^{2} t P_2 + t^{2} P_3$$

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$$E(t) = (i-t)^{3} P_0 + 3 (i-t)^{2} t P_1 + 3 (i-t)^{2} t P_2 + t^{2} P_3$$

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$$E(t) = (i-t)^{3} P_0 + 3 (i-t)^{2} t P_1 + 3 (i-t)^{2} t P_2 + t^{2} P_3$$

$$E(t) = (i-t)^{3} P_0 + 3 (i-t)^{2} t P_1 + 3 (i-t)^{2} t P_2 + t^{2} P_3$$

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$$E(t) = (i-t)^{3} P_0 + 3 (i-t)^{2} P_1 + 3 (i-t)^{2} P_2 + t^{2} P_3$$

$$E(t) = (i-t)^{3} P_0 + 3 (i-t)^{2} P_1 + 3 (i-t)^{2} P_2 + t^{2} P_3$$

$$E(t) = (i-t)^{3} P_0 + 3 (i-t)^{2} P_1 + 3 (i-t)^{2} P_2 + t^{2} P_3$$

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$$E(t) = (i-t)^{3} P_0 + 3 (i-t)^{2} P_1 + 3 (i-t)^{2} P_2 + t^{2} P_3$$

$$E(t) = (i-t)^{3} P_0 + 3 (i-t)^{2} P_1 + 3 (i-t)^{2} P_2 + t^{2} P_3$$

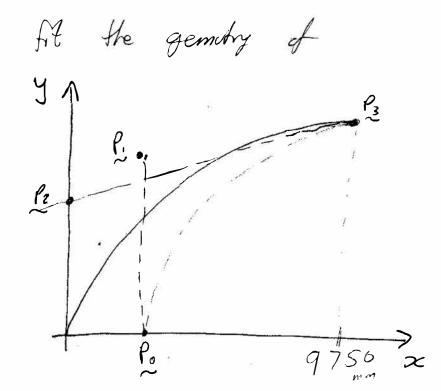
$$E(t) = (i-t)^{3$$

	9 July Part t (t) 15 0.7 39 680.4 0.75 46 999.4 0.8 55 183.4 0.85 64 279.0 0.9 74 332.64 0.95 85 390.8	9 676.6 9 761.1 9 809.4 9 822.7 9 808.1	
	91 1 97 500	9 772 · 7	
	This is not wor	king because it does not	fit the genutry of
	the Bear Core -	my this was	4 A
	4	12 1	P. o.
т		×	72
	G.	reen Blue Po	
	1 Po = [2	000mm, 0mm]	
	> 1011 0	000mm, 10,000mm]	
	and sint Po = [0	mm, 8 793mm]	Po
	end point $\hat{P}_3 = [\hat{q}]$	750mm; 9723.7mm	~
		4	
		from photograph.	
	7.4		

and the height of the contest point

9756

9ato Part t 15 0.7 0.75 0.85 0.85 0.9 0.95	(t) 39 680.4 46 999.4 55 183.4 64 279.0 74 332.64 85 390.8 97 500	61		Ç.
the Bear	one - D	ing because my this	A does	net •
		<u>[</u> 2)
v.	Gre	en Blue	Po	×
start point control point and control point	$P_1 = \begin{bmatrix} 200 \\ P_2 = \begin{bmatrix} 0 \\ 7 \end{bmatrix} \end{bmatrix}$ $P_3 = \begin{bmatrix} 9 \\ 7 \end{bmatrix}$	00mm, 0mm] 00mm, 10,000 m, 8793mm 50mm) 9723		
S. Sa	f	om photograph.		



@ differentate find gradient @ 7750mm Q. Find the height of the control point 3) use egn of struggly line and y = mx +c A. The cross section is elliptical up to P3, this is an assumption. egn of an ellipse $\frac{x^2}{q^2} + \frac{y^2}{b^2} = 1$ Need Translating S don't derrive it agom, use the egn for the tilted ellipse $\frac{2|500mn}{2} = |0.750mm$ from photograph of toriod 9770 mm 10750mm + 19770mm $y^2 = 9770^2 \left(1 - \frac{x^2}{10750mm}\right)$ $y = 9770mm \left(1 - \frac{x^2}{10.750mm^2}\right)^{\frac{1}{2}}$ positive result only

$$\frac{dy}{dx} = 9770 \text{mm} \times \frac{1}{x} \left(1 - \frac{x^2}{(10750 \text{mm})^2} \right)^{-\frac{1}{2}} \times -\frac{1}{(10750 \text{mm})^2}$$

$$\frac{dy}{dx} = \frac{9770 \text{mm}}{(10750 \text{mm})^2} \left(1 - \frac{x^2}{(10750 \text{mm})^2} \right)^{-\frac{1}{2}}$$

$$\frac{dy}{dx} = \frac{9770 \text{mm}}{(10750 \text{mm})^2} \left(1 - \frac{x^2}{(10750 \text{mm})^2} \right)^{-\frac{1}{2}}$$

(2) differentiate find graviant (w 7 150mm (). Lind the height of the control point egn of straight line and yemx to A. The cross section is elliptical up to is an assumption egn of an ellipse $\frac{x^2}{q^2} + \frac{y^2}{b^2} = 1$ Need Need Translating don't derrive it agam, use the egn for the tilted ellase $\frac{21500mn}{2} = 10750mm$ from photograph of toriod 9770 mm $y^{2} = 4770^{2} \left(1 - \frac{x^{2}}{10.750 \text{ m/m}} \right)$ $y = 9770mm \left(1 - \frac{x^2}{10.750mm^2}\right)^{\frac{1}{2}}$ positive result only

 $\frac{dy}{dx} = 9770 \text{mm} \left(1 - \frac{10750 \text{mm}^2}{10750 \text{mm}^2}\right)^{-\frac{1}{2}} \times \frac{4x}{(10750 \text{mm})^2}$

$$\frac{dy}{dx} = \frac{9770 \text{mm}}{(10750 \text{mm})^2} \left(1 - \frac{36}{(10750 \text{mm})^2}\right)^{\frac{1}{2}}$$

$$\frac{dy}{dx} = \frac{-9770 \, \text{mm}}{(10750 \, \text{mm})^2} \propto \left(1 - \frac{x^2}{(10750 \, \text{mm})^2}\right)^{-\frac{1}{2}}$$

$$\frac{dy}{dx} = \frac{-9770 \, \text{mm}}{(10750 \, \text{mm})^2} \propto \left(1 - \frac{9750 \, \text{mm}}{(10750 \, \text{mm})^2}\right)^{-\frac{1}{2}}$$

$$\frac{dy}{dx} = \frac{9770 \, \text{mm} \times 9750 \, \text{mm}}{(10750 \, \text{mm})^2} \times \left(1 - \frac{9750 \, \text{mm}}{(10750 \, \text{mm})^2}\right)^{-\frac{1}{2}}$$

$$\frac{dy}{dx}\Big|_{X=9750\,\text{mm}} = \frac{-9520\,\text{mm}}{(10750\,\text{mm})^2} \times \left(1-\left(\frac{39}{43}\right)^2\right)^{-\frac{1}{2}}$$

$$\frac{dy}{dx}\Big|_{x=9750mm} = \frac{95\ 257\ 500mm}{115\ 562\ 500mm} \times \left(1 - \left(\frac{39}{43}\right)^2\right)^{-\frac{1}{2}}$$

$$190\ 515mm \times \left(1 - \left(\frac{39}{43}\right)^2\right)^{-\frac{1}{2}}$$

$$= -\frac{196 \ 515 \text{ mm}}{231 \ 125 \text{ mm}} \times \left(1 - \left(\frac{39}{43}\right)^{2}\right)^{-\frac{1}{2}}$$

$$= -\frac{38 \ 103 \text{ m/s}}{46 \ 225 \text{ m/s}} \times \left(1 - \left(\frac{39}{43}\right)^{2}\right)^{-\frac{1}{2}}$$

$$= -\frac{38 \ 103}{(215)^{2}} \times \left(1 - \left(\frac{39}{43}\right)^{2}\right)^{-\frac{1}{2}}$$

$$\frac{dy}{dz} = \frac{-9770 \, \text{mm}}{(10750 \, \text{mm})^2} \, \text{DC} \left(1 - \frac{x^2}{(10750 \, \text{mm})^2} \right)^{-\frac{1}{2}}$$

$$\frac{dy}{dz} = \frac{9770 \, \text{mm}}{(10750 \, \text{mm})^2} \, \text{DC} \left(1 - \frac{(9750 \, \text{mm})^2}{(10750 \, \text{mm})^2} \right)^{-\frac{1}{2}}$$

$$\frac{dy}{dz} = \frac{9750 \, \text{mm}}{(10750 \, \text{mm})^2} \, \times \left(1 - \left(\frac{9750 \, \text{mm}}{10750 \, \text{mm}} \right)^2 \right)^{-\frac{1}{2}}$$

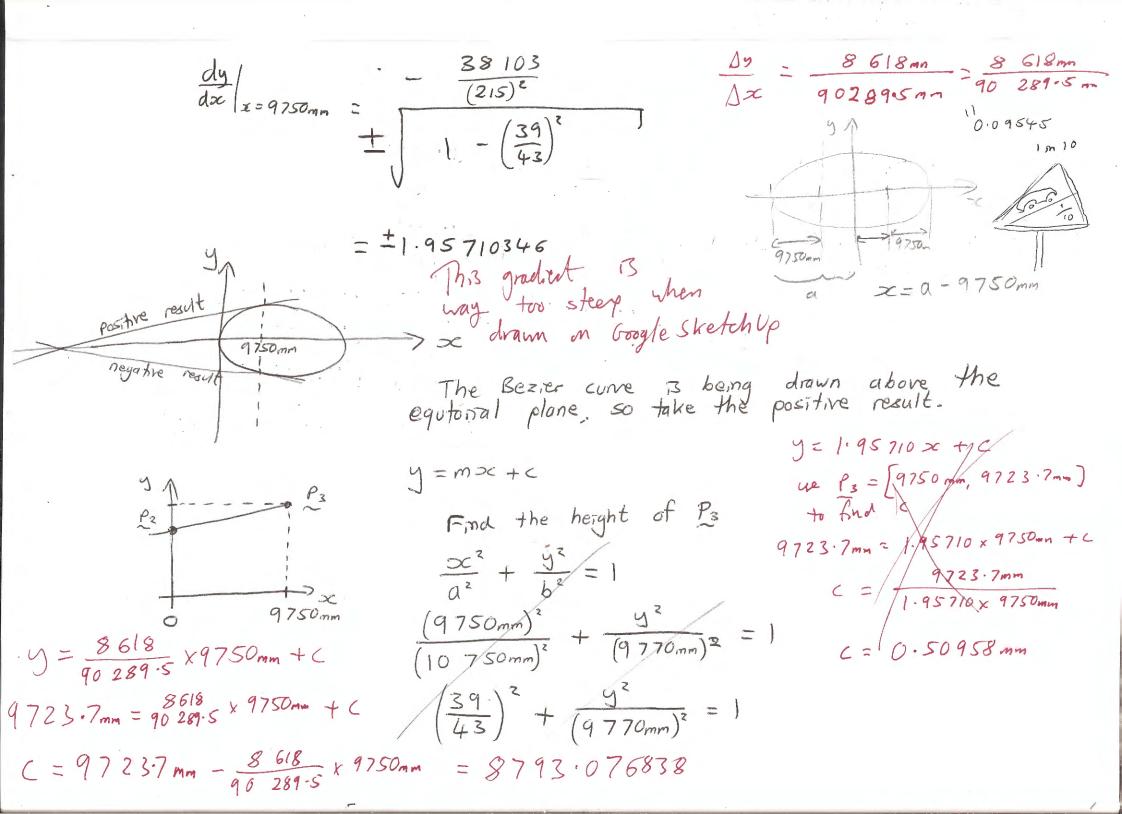
$$\frac{d9}{dx}\Big|_{X=9750_{mm}} = \frac{95\ 257\ 500\ mm}{(10\ 750_{mm})^2} \times \left(1-\left(\frac{39}{43}\right)^2\right)^{-\frac{1}{2}}$$

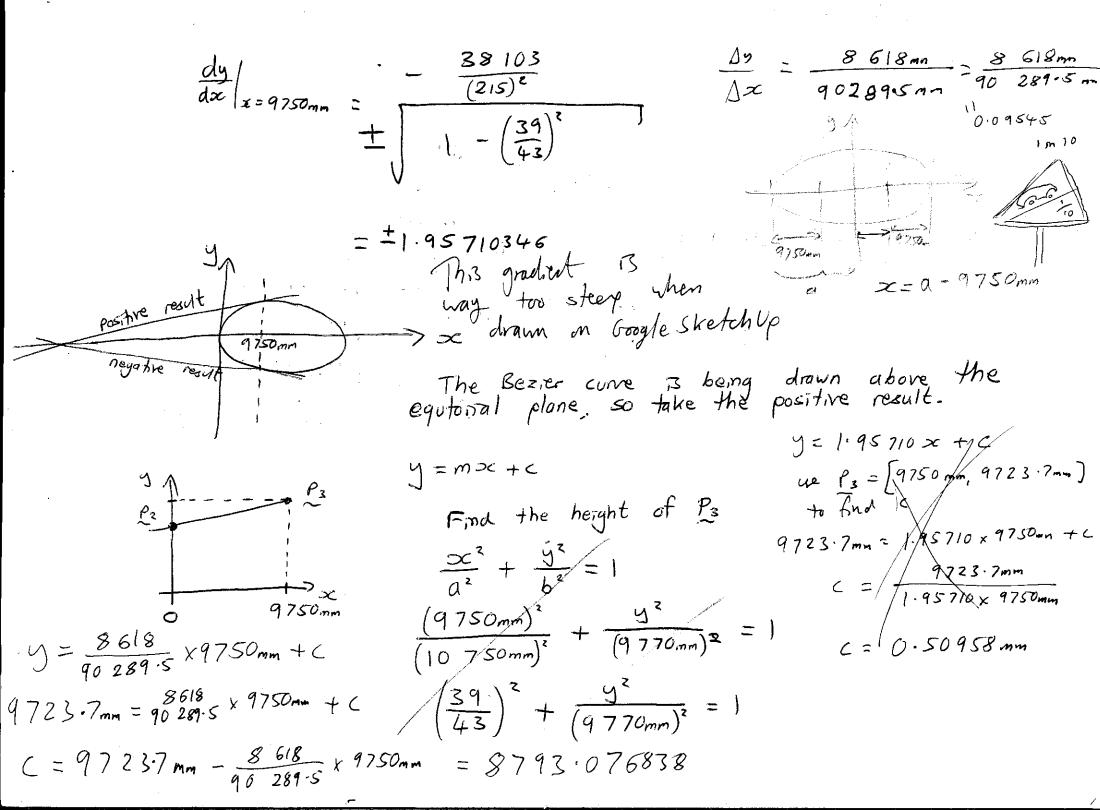
$$\frac{dy}{dx}\Big|_{x=9750\text{mm}} = \frac{95\ 257\ 500\text{mm}}{115\ 562\ 500\text{mm}} \times \left(1 - \left(\frac{39}{43}\right)^2\right)^{-\frac{1}{2}}$$

$$= -\frac{196 \ 515 \text{ mm}}{231 \ 125 \text{ mm}} \times \left(1 - \left(\frac{39}{43}\right)^{2}\right)^{-\frac{1}{2}}$$

$$= -\frac{38 \ 103 \text{ mm}}{46 \ 225 \text{ mm}} \times \left(1 - \left(\frac{39}{43}\right)^{2}\right)^{-\frac{1}{2}}$$

$$= -\frac{38 \ 103}{(215)^{2}} \times \left(1 - \left(\frac{29}{43}\right)^{2}\right)^{-\frac{1}{2}}$$





$$\left(\frac{39}{43}\right)^{2} + \frac{y^{2}}{(9770m)^{2}} = 1$$

$$\frac{y^{2}}{(9770m)^{2}} = 1 - \left(\frac{39}{43}\right)^{2}$$

$$y^{2} = (9770m)^{2} \left[1 - \left(\frac{39}{43}\right)^{2}\right]$$

$$y^{2} = 16 \quad 932 \quad 694 \quad mm^{2}$$

$$y^{2} = 4114 - 935479 \quad mm$$

$$7 = 1 - \frac{y^{2}}{(9770m)^{2}} = 1$$

$$1 = \frac{y^{2}}{(9770m)^{2}} = 1 - \frac{1521}{16}$$

y=x y=x-1

 $y^2 = (9770 \text{mm})^2 \left[-\frac{1521}{16} \right]$ y = 9770mm / 1 - 98.0625 the mendian it is plannar of translated elipse Equation $(a-9.750mm)^2 + \frac{y^2}{b^2} = 1$ Use the co-ordinate of the end point you have already calculated (Holed ellipse calc) Jut read from Google 9723.7 mm 9723.7mm $y^{2} = 9770m^{2} \left(1 - \left(\frac{4}{43}\right)^{2}\right)$ $y = 9770 \text{ mm x} / 1 - \left(\frac{4}{43}\right)^{3}$ $\left(\frac{1}{2} - \frac{21500}{2} + \frac{y^2}{4^2} = 1 \right)$ 9 = 9364.491414

$$B(t) = {3 \choose 0} (1-t)^{3} P_{0} + {3 \choose 1} (1-t)^{2} t P_{1} + {3 \choose 2} (1-t) t^{3} P_{2} + {3 \choose 3} (1-t)^{4} P_{3}$$

$$= (1-t)^{3} P_{0} + 3 (1-t)^{2} t P_{1} + 3 (1-t) t^{2} P_{2} + t^{3} P_{3}$$

$$= (1-t)^{3} P_{0} + 3 (1-t)^{2} t P_{1} + 3 (1-t)^{2} P_{2} + t^{3} P_{3}$$

$$= 2000_{\text{am}} (1-t)^{3} + 2000_{\text{am}} \times 3 (1-t)^{2} t + 0 + t^{3} 9750_{\text{am}}$$

$$= 2000_{\text{am}} (1-t)^{3} + 6000_{\text{am}} (1-t)^{2} t + 9750_{\text{am}} t^{3}$$

$$= 0 + 10.000_{\text{am}} \times 3 \times (1-t)^{2} t \text{ as } t \times 3793_{\text{am}} \times 3 \times (1-t)^{2} t \times 9723_{\text{am}} t^{3}$$

$$= 30,000_{\text{am}} t (1-t)^{2} + 26379_{\text{am}} t^{2} (1-t) + 9723_{\text{am}} t^{3}$$

data Pont	t	green/t)/mm	blue (t)	mm	•	
(0	2000	0	·	5	
	0.05	1985.7	1417-6			
	0.1	19451.7	26 77.1			. *
	0.15	1911.4	3788.5		/x	
	0.20	1870-0	4761.9		. 91	
	0.35	1839.4	5607.2			locks like this
	0 - 30	1831-3	6334.4		1400	
	J. 35	1854.5	6953.6		χ Λ	
	p 0-40	1920	7474.7		9	
	0.45	2638.0	7907.8	-		
	0.50	2218.8	8262.8	•	3(

0-53 0-60	2472·7 2810	8549.9 8778.9	This table of results will plot a
0-65 0-70 0-75 0-80 0-85 0-90 0-95	3241·1 3776·3 4425·8 5200 6109·2 7163·8 8373·9 9750	8959.9 9102.9 9218.0 9315.0 9404.1 9495.3 9598.5 9723.7	the median plane green & blue axis to give a visually smothe Beziver Circles are to be drawn from the r=2000mm ring in the equator. Then take verticals from the spiral on the median plane and then join the
C	<u> </u>		dots with straight line

lines.

Eqn of an ellipse
$$\frac{x^{2}}{a^{2}} + \frac{y^{2}}{b^{2}} = 1$$

Franslated
$$\frac{\left[x - \frac{21500}{2}\right]^{2}}{\left[x - \frac{21500}{2}\right]^{2}} + \frac{y^{2}}{H^{2}} = 1$$

$$\frac{y^{2}}{H^{2}} = 1 - \frac{\left[x - \frac{21500}{2}\right]^{2}}{\left[x - \frac{21500}{2}\right]^{2}}$$

$$y^{2} = H^{2} \left(1 - \frac{\left[x - \frac{21500}{2}\right]^{2}}{\left(\frac{21500}{2}\right)^{2}}\right)$$

$$y = H \left(1 - \frac{\left[x - \frac{21500}{2}\right]^{2}}{\left(\frac{215000}{2}\right)^{2}}\right)$$

$$y = 9.770 \text{ mm} \left(1 - \frac{\left[x - \frac{215000}{2}\right]^{2}}{\left(\frac{215000}{2}\right)^{2}}\right)$$

$$y = 4.9770 \text{ mm} \left(1 - \frac{x}{10.750 \text{ mm}}\right)^{2}$$

$$y = 4.9770 \text{ mm} \left[1 - \frac{x}{10.750 \text{ mm}}\right]^{2}$$



INVOLUTE OF CIRCLE

FOLIUM 0 + egns DESCARIES

Rarametriz eqns
$$x = \frac{3at}{1+t^3}$$

$$y = \frac{3at^2}{1+t^3}$$
Area $t \log = \frac{3a}{2}$

$$Equation of asymptote: x + y + a = 0$$

$$\frac{21500}{2} = 250 \\
+ 500 \\
+ 10,000 \\
\hline
10,750$$

Height of end point
$$P_3$$

from photo ratio 9 750mm
 $y = 9770 \text{ mm}$ $1 - \frac{(9750 \text{ mm} - 10750 \text{ mm})^2}{(10.750 \text{ mm})^2}$
 $y = 9770 \text{ mm}$ $1 - \frac{4000 \text{ mm}}{43}$ $y = 9770 \text{ mm}$ $1 - \frac{10000000 \text{ mm}^2}{115.562.500 \text{ mm}^2}$
 $y = 9770 \text{ mm}$ $1 - \frac{16}{1849}$
 $y = 9727.636657 \text{ mm}$ $\frac{16}{1849}$

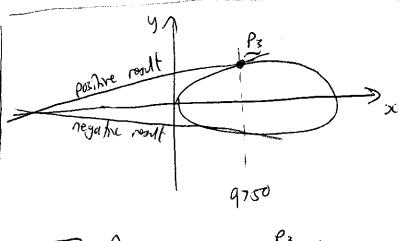
very close to the measuret 30. taken from the 30-model

diffrentiate $y = \pm 9770 \text{ mm} \left[1 - \frac{(\infty - 10.750 \text{ nm})^2}{(10.750 \text{ nm})^2} \right]$ with ∞ using the product rule $\frac{dy}{dx} = \frac{1}{dx} = \frac{10750 \, \text{mm}}{dx} \left[1 - \left(\frac{x - 10750 \, \text{mm}}{10750 \, \text{mm}} \right)^2 \right]^{\frac{1}{2}}$ $= \pm 9770_{mm} \times \frac{1}{2} \left[1 - \left(\frac{2C - 10750_{mm}}{10750_{mm}} \right)^{-\frac{1}{2}} \cdot \left[2 \left(\frac{2C - 10750_{mm}}{10750_{mm}} \right) \cdot \sqrt{\frac{1}{2000_{mm}}} \right]^{-\frac{1}{2}} = 0$ H = X-10750 $= +9770mn \times \frac{1}{2} \left[1 - \left(\frac{x - 10750mn}{10750mn}\right)^{2}\right]^{\frac{1}{2}} \left(\frac{x - 10750mn}{10750mn}\right)^{\frac{1}{2}}$ 1022017 = DC -10220 $Q = \frac{1}{10^{240}} \times -\frac{10^{210}}{10^{210}}$ $\frac{dv}{dx} = \pm 9700_{mm} \times \left[1 - \left(\frac{3C - 10750m}{10750m}\right)^{2}\right]^{\frac{3}{2}} \times \frac{-10750m}{(10750m)^{2}}$ H= 10750 >c - 1 $\frac{du}{dz} = \frac{1}{10750}$ $= \pm 9700 \text{ mm} \times \left[1 - \frac{3c - 10750 \text{ mm}}{10750^2} \right]^2 \left(\frac{3c - 10750 \text{ mm}}{10750^2} \right)$ $= +9700 \left[1 - \left(\frac{5C - 10750 \, \text{mm}}{10750 \, \text{mn}} \right)^2 \right]^{\frac{2}{3}} \left[\frac{\times -10750 \, \text{mm}}{10750^2 \, \text{mm}} \right]$

201/2

Solve this at x = 9750mm, the ratio measurement taken from the photo. $\frac{dy}{dx}\Big|_{x=9750mm} = \frac{\pm 9700 \text{ Mm}}{10750 \text{ mm}} \times \Big[- \frac{(9750 \text{ mm} - 10750 \text{ mm})^2}{10750 \text{ mm}} \Big] \frac{9750 \text{ mm} - 10750 \text{ mm}}{(10750 \text{ mm})^2} \Big]$ $= \pm 9700 \text{ max} \times \left[1 - \left(\frac{-4}{43}\right)^{2}\right] - \frac{2}{231125}$ = + 9700 xx x 1833 x (-27) $= + \frac{9700 \times 1833 \times 2}{1849 \times 231125}$ = 7 0.08321092687 MBA

close to 0.09545 measted from the 3D model



Take the result of graduat and one the co-ordinates of P3 within y=mx+c egn of stright line to find the co-ordinate of P2; i.e. when gradual to X=0.

$$J = \frac{35}{427} \frac{560}{350} \frac{200}{125} SC + C$$

$$C = y - \frac{35}{427} \frac{560200}{350125}$$

at $P_3 = \left[9750_{mm}, 9770_{mm} \right] \frac{16}{1849}$

$$C = 9770 \text{mm} \int 1 - \frac{16}{1849} - \frac{35}{427} \frac{560200}{350125} \times 9750 \text{mm}$$

very close to the value measured on the 30 model

$$C = 9770 \text{mm} \times \left(\sqrt{1 - \frac{16}{1849}} - \frac{35}{427} \frac{560200}{350125} \right)$$

Use the Bezier cine function where n=3 to that describe the parametric egn for green (t) a blue (t) start point Po = 2000mm, Omm] P. = [2000mm, 10,000mm] THIS VALUE. $P_2 = \left[O_{mm}, 8916.33012 \text{ mar} \left(\sqrt{1 - \frac{16}{1849}} - \frac{35560200}{427350125} \right) \right]$ $P_3 = \left[(9.750 \text{mm}), 9770 \text{mm} \right] \frac{16}{1849}$ 0< 6 < 1 $\mathbb{E}(t) = \sum_{i=1}^{3} {3 \choose i} (i-t)^{3-i} t^{i} P_{i}$ $B(t) = (1-t)^{2} P_{0} + 3(1-t)^{2} t P_{1} + 3(1-t)t^{2} P_{2} + t^{2} P_{3}$ green(t) = $(1-t)^3 - 2000 \text{ mm} + 3(1-t)^2 t - 2000 \text{ mm} + 3(1-t)t^2 \cdot 0 \text{ mm} + t^3 \cdot 9750 \text{ mm}$ = $2000mm(1-t)^3 + 6000mm + (1-t)^2 + 9750mm + 3$ blue $(t) = (1-t)^3$. $O_{mm} + 3(1-t)^2 + 10000 mm + 3(1-t)t^2 = 9770 mm = <math>\sqrt{1-\frac{16}{1849}} - \frac{35560200}{427350125} + t^3 = 1$

plut the	table number data point	scal valvos	to 2d.p or 4 or green(t)/mm	Who blue (t) /mm	
	÷ 4 5 6 7 8	0 0 0 5	2000 1986.71875 1983.75 1911.40625 1870 1839.84375 1831.25 1834.53125 1920 2037.96875 2218.75 2472.65625 2810 3241.09375 3776.25 4425.78125 5200 6109.21875		blue(f)/mn requires for muly memory for the CASIO fx-85ES retype egn m MATHIAB form.
	19	0.90	7163-75		

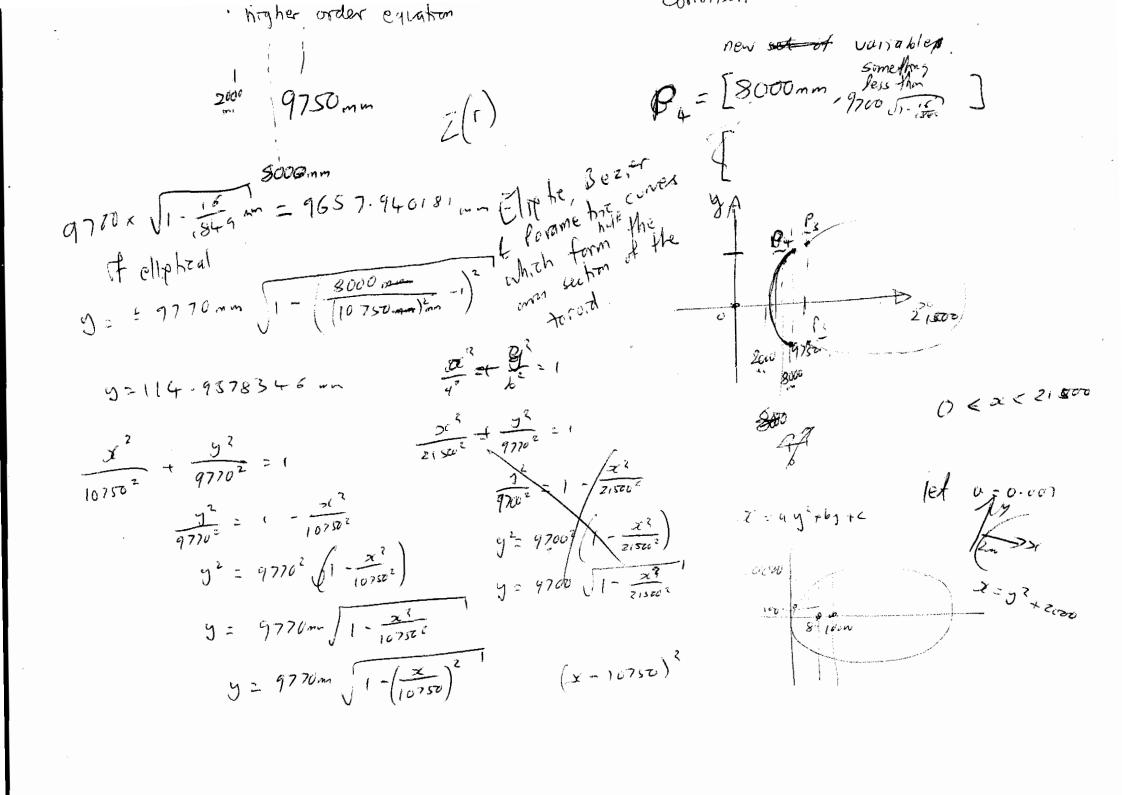
9750 In Bezier Come, now we have point stat part 4 and point and 3-gradient y=moc+c => Z=moc+ny+c ? Where the 3-grant combe find from n 4 pm. How would me find the 3-gradient from the egn of the titled ellipse? Do we have a what 13 (3) ? ? ? 3-space egn for the tilted ollipse ? mondian do we read this gradient from the Photo? This spect the Bezzer Circ egn $\mathcal{B}(t) = \sum_{i=1}^{3} {\binom{3}{i} (i-t)^{3-i} t^{i} P_{i}}$ i.e. $[x_{a} y_{a}^{2}] = \sum_{i=1}^{3} {3 \choose i} (1-t)^{3-i} + [x_{p} y_{p}^{2} z_{p}]$ So it is 3D! - D Make something up. have not plated

looks like this I Try using start and So the Bezier cuive with the correct gradient and see what the eg x intercept frah ponts of 13 Po = 9750 mm, 9700 mm 1 - 16 stat pont P1 = [0,700, 1-16] - 35 600 200] Pe = [Omn, -9770mm x JI-1849 - 35 600 220] P3 = 9750mm, - 9700mm /1-15 end point This is a chance and nort per the own at [2000mm, om) - will have to use more than one Beever 10,000 J= Gx + bx + c By oc co-ordinate. 0 < y ≤ 8000mn

Quadratic

condition

c - 2000 mm



Bad Parametric Space Come. - What is the correct term for equations of higher orders? Bez, er (me Dodechaledn Pim Con Sphere whe mesh torrod 1 spiral ny vortex Torrod y=a>ci+b>c+c r = 02 2 + 62 + c rearrage for 2(1) imporsible! r= a2 2 + 62 + C conditions @ Ight salong a quadrate. $coc = a \frac{q \cos t}{t} + b \frac{q \cos t}{t} - \frac{Goot}{t} \Rightarrow 6000 = q \cos^2 a + q \cos d$ booding 8000 = 9 9500 -6 + 162-4ac n' beAr! 62 - 12000 a

6 - yezz. 6000 = 9500 2 a + 9500 b (19 000 a + 6) = 62-8000 a
AHHHHHHHH 6 = 90 250 9 + 9.56 6 = 6 - 90250 a O -9499 -18999 - b = J62 - 4 a 2000 - 28 441 37019 2 × a -94949.

A100 -

plot (x,l,y) Beger on pormetic. Parametric are not ? Bit there want 60. Altel ellipses can be 20 plot 2 (r. 0) How will me get become to not z(r, 0) Wildge at rim? Plotting torios in 3D using MATLAB Bezier curves are Parametric Search the MATLAB help for 3D space curves. Write the script for the ellipse then tilt it. plot (x,y,'r', x, z, 'b--') Types This This means a blue real Like I was dolled line. Both Excel and Matlat is good, will need another day. What MATLAB would be good for is repeativly drawing the parametre and changeing the values of a 4 b this is scary because a 4 b are both any real numbers from - so to + so so any poss, blity of getting close would be to try them all which would take so amount of time. But you don't know it you don't try & so start from I for both and See Mut hoppen. We have the ellipse, - good. Need to draw a vertel- for r= 8000mm

MALINE TO THE TOP OF THE PROPERTY OF THE PROPE

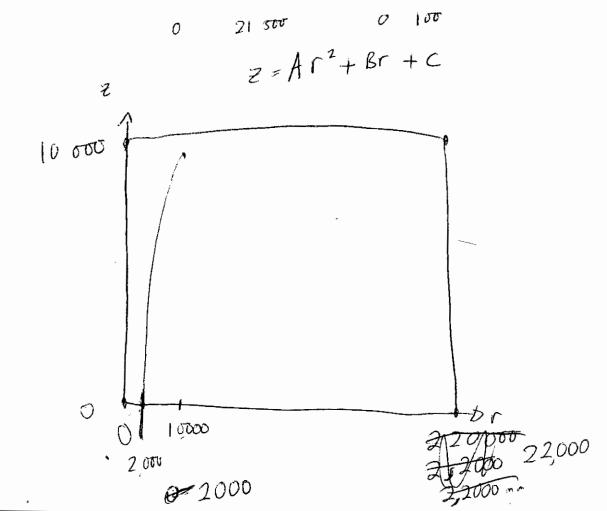
The Bezzer come egn is too much for MATLAB to take, so as with Excel, enter the equation term by term. just reading out the table of results first, plotting, add a term, read out ect until the whole equation works.

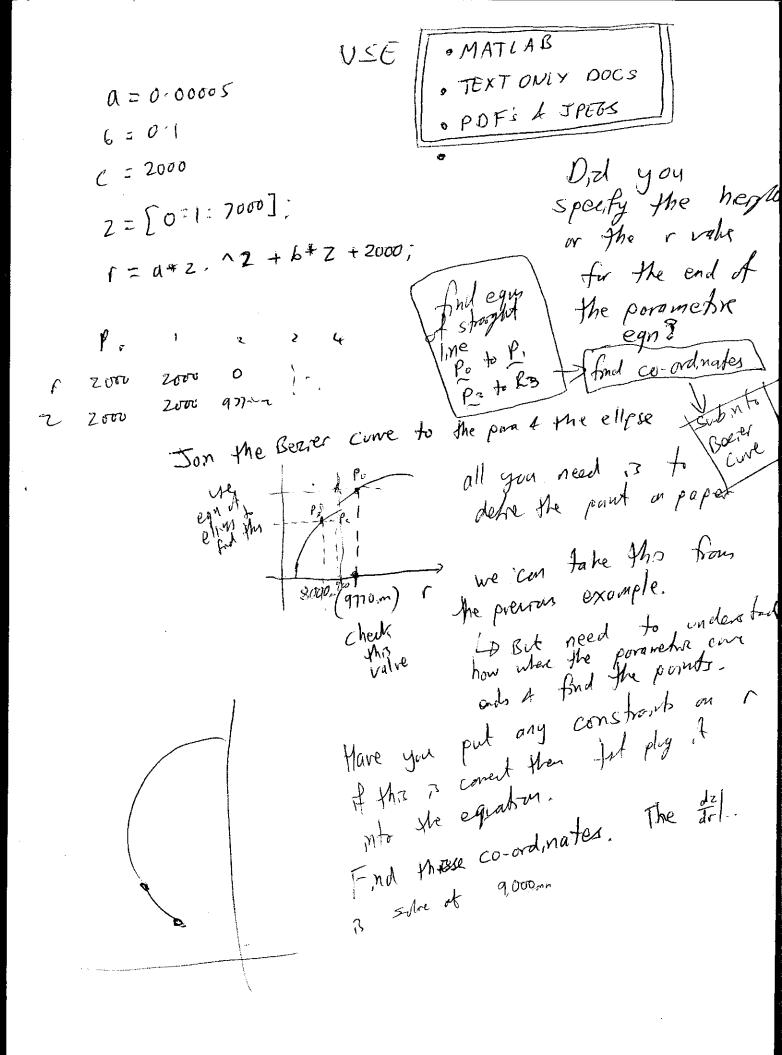
. Find the syntax for plotting multiple graphes on one axis, this is agreed for this e.g. because I like to Keep the oxis of the model. z - vertically up from the equatoral plane and r. radially outwards

· How can I more all the scripts together?

If I can plat what I have plotted on Excel I will be happy. — I've do not use the semi colon, term by term and

0-8×104 2.2×104 0 10000 8,000 2 2000 0 10000





8000 mn

4

$$P_{0} = \left[9750_{mm}, 9770_{mm} \right] - \frac{16}{1849}
 P_{1} = \left[8000_{mm}, 9770_{mm} \right] - \frac{16}{1849}
 P_{2} = \left[8000_{mm}, 9770_{mm} \right] - \frac{16}{1849}
 P_{3} = \left[8000_{mm}, 9770_{mm} \right] - \frac{16}{1849}$$

Use results from before

$$P_0 = \begin{bmatrix} P_1 & P_2 & P_3 \\ P_4 & P_4 \end{bmatrix}$$
 $P_1 = \begin{bmatrix} 9 & P_4 & P_4 \\ P_5 & P_5 \end{bmatrix}$

2000 m $P_2 = \begin{bmatrix} 9 & P_5 & P_5 \\ P_7 & P_7 \end{bmatrix}$

$$P_{0} = \begin{bmatrix} 9750 \text{ mm} \\ -\frac{16}{1849} - \frac{356000}{427350125} \end{bmatrix}$$

$$P_{2} = \begin{bmatrix} 0,9770 \text{ mm} \times \sqrt{1 - \frac{16}{1849}} - \frac{356000}{427350125} \\ -\frac{16}{1849} - \frac{16}{1849} \end{bmatrix}$$

Parmetric Cure $r = az^{2} + bz + c$ $\frac{dr}{dz} = 2az + b$ $\frac{dr}{dz} = 2az + b$ $\frac{dr}{dz} = 2az + b$ $= 4000 \text{ mm} \times z + b$

Would it not be better to read co-ordinates from the photo of how the shape curves then do a curve fit?

Tongent need tales of a 4 b.

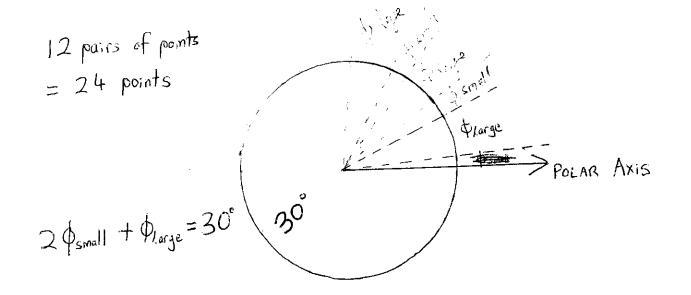
Yea but can still type up what you have done.

cylindrial polar-coordinades

(Z = =

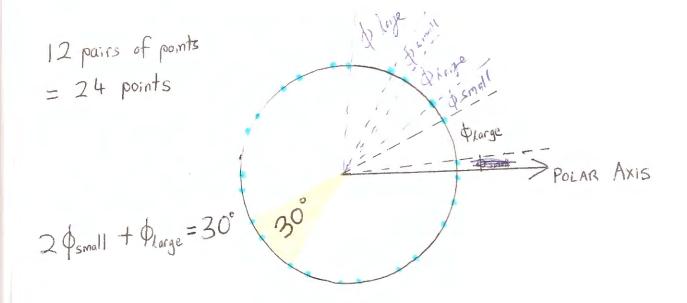
MATLAB ezplot(d) s = solve(eq) eq =x? (matlob ossumes it is equal to zero) double (sti) gives a numerical result. Symst defines a symbolic conable, the dependent works Simplify (cos(x)^2 + 2+sin(x)^2) S= taylor(sin(sc)) 4mit (x+5,3) czplot f.He () = 63.95436206 degra:

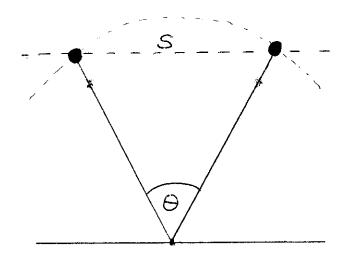
CO-ORDINATES OF END OF ELLIPSES



MATLAB ezplot(d) s = solve(eq) eq = x? (Matlabossumes it is equal to zero) double (sti) gives a numerical result. syms t defines a symboliz conable, the dependent who Simplify (cos(x)^2 + 2+sin(x)^2) Sz fajlor (sin(sc)) 4m/t (x+5,3) czplat fifte 0 = 63.95436206 degrees

CO-ORDINATES OF END OF ELLIPSES



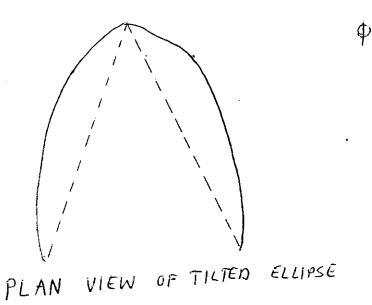


SIDE VIEW OF TILTED ELLIPSE

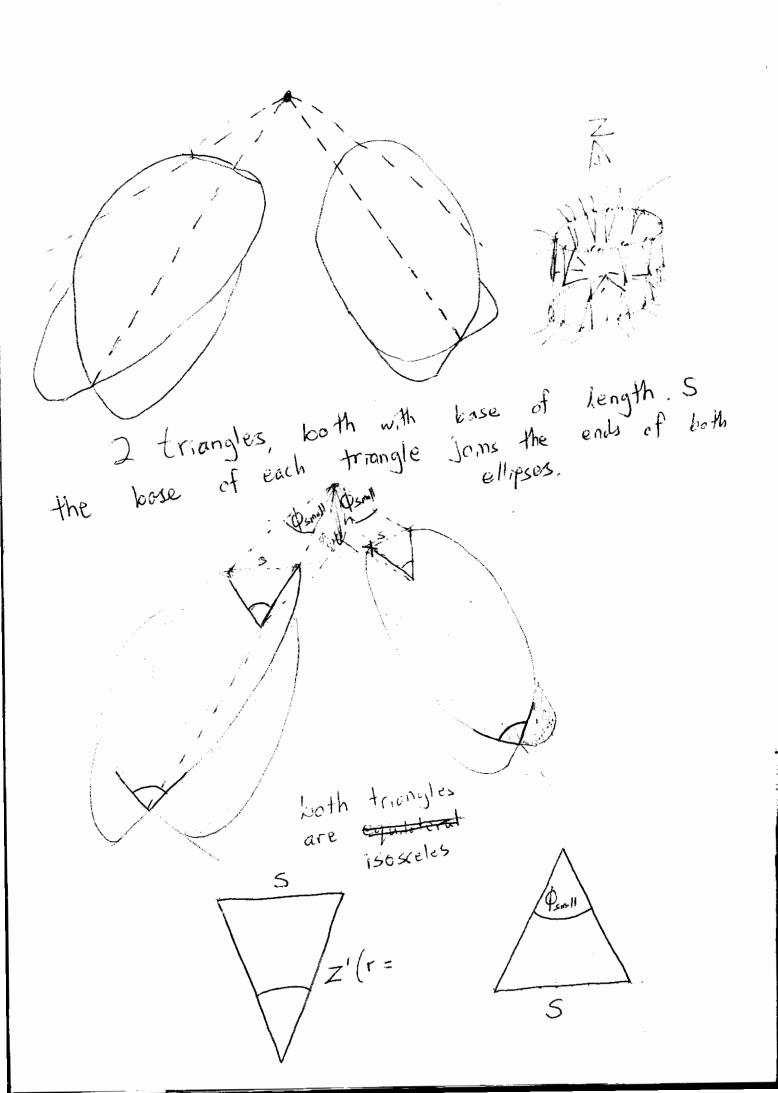
S = seperation

point where tilted ellipse ends.

· Height of tilted



 $\phi = \phi(r)$

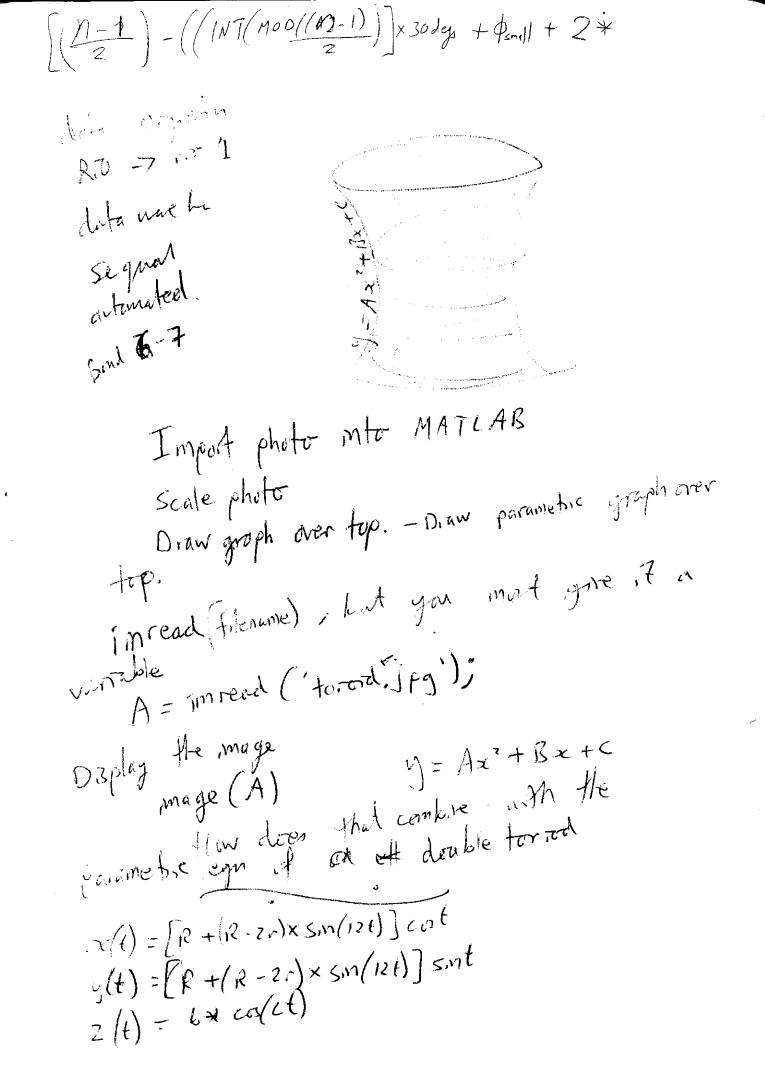


toroid

a Surface of revolution generated by revolving any 2D shape in 3D space about an axis coplanar with the 2D shape.

torus

a special case of the toroid where the 2D shape is a circle.



X=rint How much does the pitch y=rsint Change by? z = ctQ, How do we the wast is r->r(1)->r(2) change I firm 716 2 A. Just than shoten or lengthen the range of t. -> Lt (= AZ+BZ+C this will charge the Lt 2 =ct ef C height r = Acili+ Bc++ C x = (Acili+ Bol+ 6) * cost y = (Ac2(2 + Bct + C) * sint 2(4) Try this -> does I make the heli kilge? cylindrical co-ordinates (r, 0, h) r= Ah'+Bh+C r(t)=1 $\rightarrow e(0) = t$ $\theta(t) = t$ h(t) = tfrom the with post h(t)=t Copy the data from the parametric equation by not Can you plot It raw data? If so plot or a scotter groph. This will look like the glass paper weight with pattern in. LISMIA J h= #if revs * 27 e = ingett h= 27 C x # frevs pAtch = 27e --TÝC (= 2Ã tom-thm = 21 # of res 7 = 21 C

DSMII + 27 (1+12) = 4770MM + JI-15 + 2 x 2/1 SM Smill = 2 xr \$ ingl Finding 4 small calculations ! Z/(r=9750,mm) $\frac{16}{2700} \left[\frac{16}{1849} - 20 \right] = \frac{\frac{1}{2}}{970} \left[\frac{1}{1849} + \frac{1}{2} \left(180^{2} - 20 \right) \right] = \frac{\frac{1}{2}}{970} \left[\frac{1}{1849} + \frac{1}{2} \left(180^{2} - 20 \right) \right] = \frac{\frac{1}{2}}{970} \left[\frac{1}{1849} + \frac{1}{2} \left(180^{2} - 20 \right) \right] = \frac{1}{2}$ Sin Grad = \frac{2}{1750... 2x 9750m Sm (sm) = 5 2/x 9770 JI-15 ton = (180-20) = \$x 9750 - 5,4 9,4 9770 JI-16 tan (180-26) = Sin P. M asmil = aizsin (9750) 1 1849 (180-20)

PS41 =

Sir 2 = 3-50 m Envete for 9750 ... 2 arsm (977 x **b**small = O= 63.95456206

H

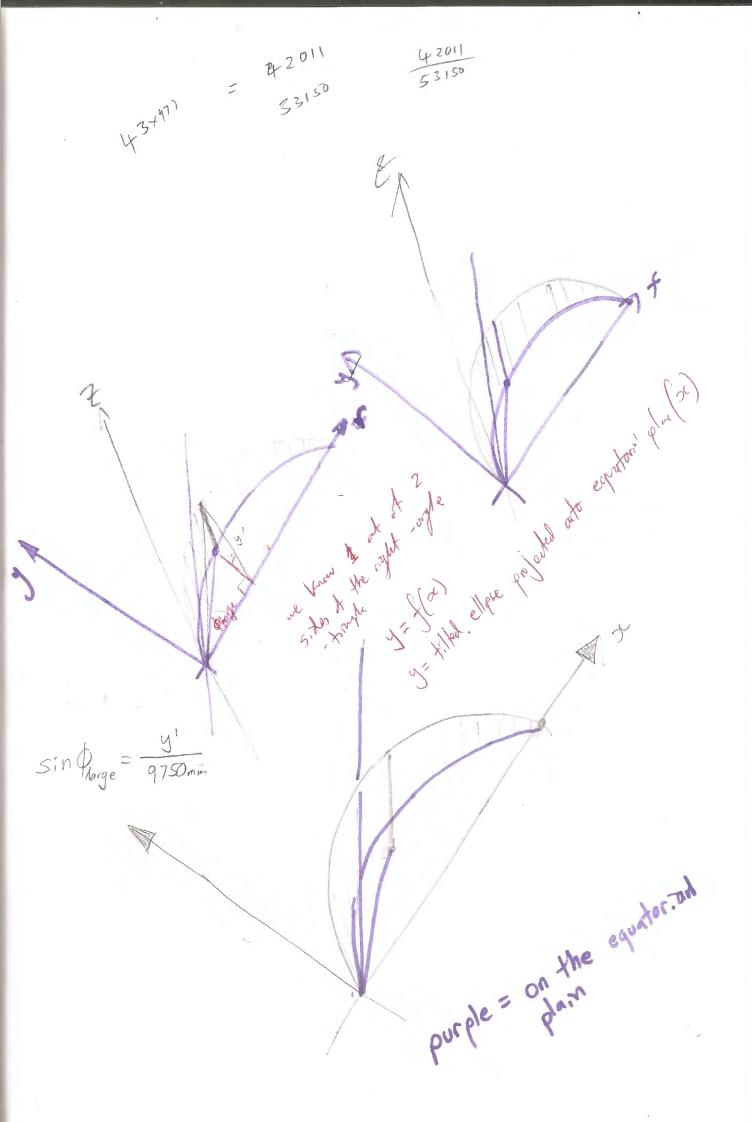
9770m 1-16 $Sin\left(\frac{\phi_{snall}}{2}\right) = \frac{L}{9750m}$ L = 9750.mm x sin (4 small) equate for L 9770mm 11-16 9750mm x sin (\$\phi_small) = rearange for Psmall Sm (4 small) = 9770 JI - 1849 9750 ton 8 Psmall = 2 arcsin (977 1- 16 49 75 x tan 0 0= 63.95456206

O is correct, the colculations have been cheeked and it looks correct when looking at the photograph. Just need of in radians for MATLAB. r in this case is the radial $a = rsm(\frac{\pi}{n})$ distance to the first join above $\tan \Theta = \frac{H_i}{a}$ the equator. (not the end of the ellipse) =) can we use the other triangle formed by tan 0 = 8,500 mm (sin√1) the top of the ellipse and the orgin? Yes but we want. $\Gamma = \frac{21,500 \text{ arm}}{2} \left(1 + \sqrt{1 - \frac{8-5}{9-77}}^2 \right)$ 0 = arctan 8,500mm This was calculated using MATERIE very quickly or r= 10750m (1+)1-(8.5). Check that the height is correct not height of join 7 sit 2 (975) Is height of end of tilted ellipse $Z(r) = H \sqrt{1 - \left(\frac{r \cdot R}{R}\right)^2}$ $Z(r=9.75)=9.77/1-(\frac{9.75-10.75}{10.75})^2$ Z(r=9.75) = 9.727636657or 9,728 mm /es! osbafor :- H=9.77 R=10.75 Ps.11 < 30° Pm < 30° 2 /small + Plage = 30° From Sketch up Model Psmall 22-4°

radeal dhe

height $a^2 = r^2 + h^2$

add differ

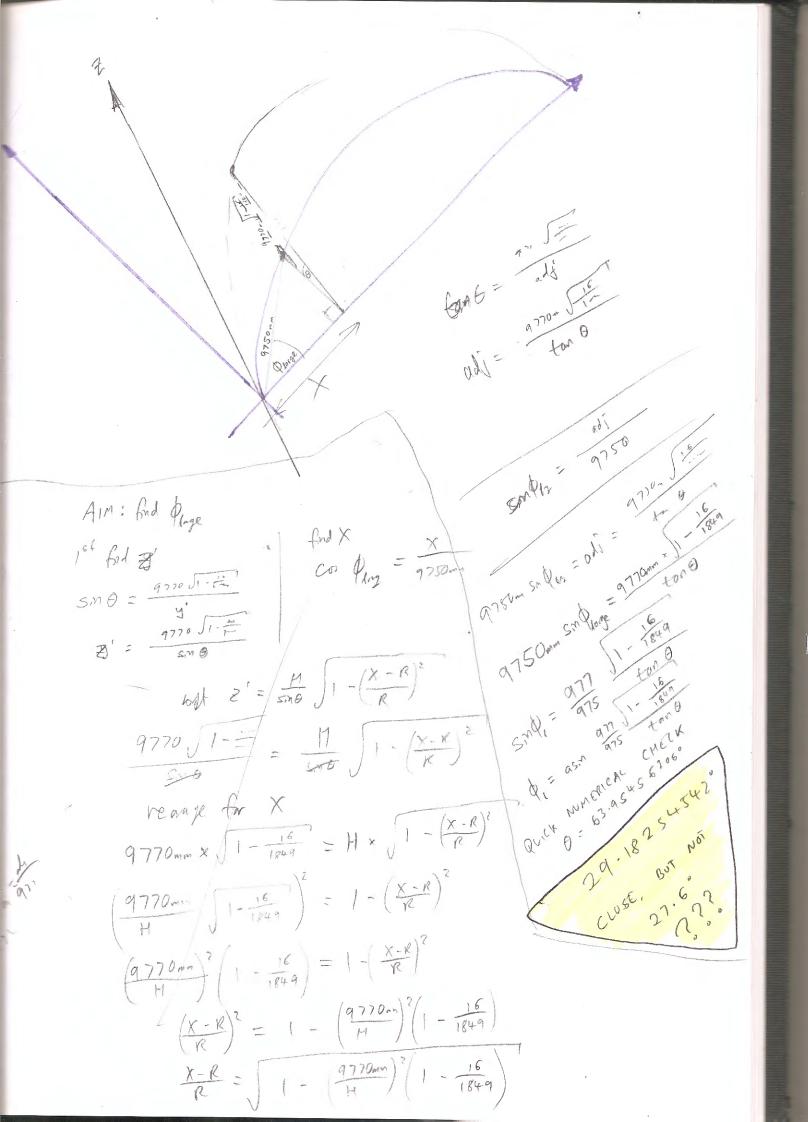


$$Z' = \frac{H}{s_M \theta} \int \left[-\left(\frac{r \cdot R}{R}\right)^2 \right]$$

$$\frac{2' \cos \theta = y'}{\sin \theta} \int_{-\infty}^{\infty} \frac{1 - \left(\frac{r - R}{R}\right)'}{\cos \theta} \cos \theta = y'$$

Equate for (
$$y'\left(r = 9750.6 \text{ for } \psi_{ene}\right) = H \frac{\cos \theta}{\sin \theta} \int \left[-\frac{r \cdot R}{R}\right]^{2}$$

$$= H \frac{\cos \theta}{\sin \theta} \int \left[-\frac{\left(9750...4 \mu_{ene} - R\right)^{2}}{R}\right]^{2}$$



$$\begin{array}{lll}
X - R &= R & 1 - \left(\frac{9770 \text{ mm}}{H}\right)^{2} \left(1 - \frac{16}{1849}\right) \\
X - R &= R & 1 - \left(\frac{9770 \text{ mm}}{H}\right)^{2} \left(1 - \frac{16}{1849}\right) \\
X &= R & 1 - \frac{9770 \text{ mm}}{9775 \text{ m}} \left(1 - \frac{16}{1849}\right) \\
X &= R & 1 - \left(1 - \frac{16}{1849}\right) \\
X &= R & 164 \\
X &= R &$$

$$\Theta = \arctan \frac{8.5}{c \cdot sm} \frac{5}{fr}$$

$$\frac{\sqrt{1 - \frac{16}{1849}}}{\sqrt{1 - \frac{16}{1849}}}$$

$$\frac{\sqrt{1 - \frac{16}{1849}}}{\sqrt{1 - \frac{16}{1849}}}$$

$$= \arcsin \left(\frac{977}{975} \times \frac{\sqrt{1 - \frac{16}{1849}}}{\sqrt{1 - \frac{16}{1849}}}\right)$$

$$= -\frac{1}{2} - \arctan \left(\frac{\sqrt{1 - \frac{16}{1849}}}{\sqrt{1 - \frac{16}{1849}}}\right)$$

$$= \left(\frac{\sqrt{1 - \frac{1}{2}}}{\sqrt{1 - \frac{16}{1849}}}\right)$$

$$= -\frac{1}{2} - \arctan \left(\frac{\sqrt{1 - \frac{16}{1849}}}{\sqrt{1 - \frac{16}{1849}}}\right)$$

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$$= -\frac{1}{2} - \arctan \left(\frac{\sqrt{1 - \frac{16}{1849}}}{\sqrt{1 - \frac{1$$

Freq dist wt + pt.m w = 2nt we ynt we ynt wt + pt.m wt + pt.m

27+ Psmall + 8 = angle in radians through which the Space curve rotates from the end of one ellipse at the top of the toroid to an end of another ellipse at the of bottom of the toroid. of (2) = r co (2) oz r snt $y(z) = r \cos\left(\frac{z}{c}\right)$ $z(z) = r \cos\left(\frac{z}{c} + \frac{displainent}{might}\right)$ zzet +=== helites on so $z(z) = r \cos(\frac{z}{c} + \frac{\rho hose constant}{c})$ To. Loh $c(z) = r cos \left(\frac{2\pi}{pitch} Z + \frac{phose constant}{displacement}\right)$ Pitch pach = 27E C= P./N A displorement

 $\chi(z) = r\cos\left(\frac{z}{c} + dspharement\right)$ But you can't have a ces of a Sub in $C = \frac{2 \times 9770 \text{mm} \times \sqrt{1 - \frac{16}{1849}}}{2\pi + \phi_{\text{small}} + \frac{8\pi}{6}}$

 $\chi(z) = r \cos \left(\frac{2\pi + \phi_{\text{smell}} + \frac{8\pi}{6}}{2 \times 9770 \text{ mm}} \times \sqrt{1 - \frac{16}{18449}} \right) + d \frac{\text{sphote constant}}{2}$

chare length 2th trave length = 2th Phone constant constant pitch = 2th

phase constant = 27 displacent

xy plane at height 9770mm 1 - 15 16 1894 n=9 n=8 -0 -n=6 \$ locase n=10 *n=2 n=11 n=1 on=12 ·n=24 4 Small 12

V COS [2 - Phue m2] r co = phose cont m z x(t) = r cos t - phose cont, n ? 9(4)= rsin (t - phose cont in 2) 2(f)=ct This is the real meand distur Humph

What if the stellorator and the tocomac are both non optimal, example of General Fistons 30 paton model 13 aphinal 2 Only measurement and data collection acurate will decide. 9750mm 9770mm [1r = 9770 m /1- 1549 + (9750 mm) [9770m] 1-15/19) + (9750m))