### Parameters of Plastic Damage Concrete Model

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This documents gives a brief overview of the required input parameters of the plastic damage concrete model. Table 1 summarizes the parameters, which can be roughly categorized into 3 groups:

- (1) Parameters based on material properties: the Young modulus E, the Poisson ratio  $\nu$ , the tensile yield strength  $f_t$ , and the compressive yield strength  $f_c$
- (2) Plastic strain rate parameter: the plastic strain rate coefficient  $\beta$
- (3) Damage parameters: the parameters governing the damage evolution  $A_p$ ,  $A_n$ ,  $B_n$

Parameter	Description
$\overline{E}$	elastic modulus
u	Poission ratio
$f_t$	tensile yield strength
$f_c$	compressive yield strength
β	plastic strain rate parameter
$A_p$	positive damage parameter
$A_n$	negative damage parameter $\#1$
$B_n$	negative damage parameter $\#2$

Table 1: Model parameters

Parameters in the first group are directly based on properties of concrete material. It is noteworthy that in this model the tensile yield strength  $f_t$  assumes to coincide with the peak strength in uniaxial tension. The compressive yield strength  $f_c$  is the stress at the transition from elastic to plastic range in uniaxial compression and is typically less than the maximum compressive strength.

The following sections discuss the parameters in the second and the third group.

### 1 Plastic strain rate coefficient, $\beta$

The plastic strain rate coefficient  $\beta$  governs the post-yield hardening modulus in the effective (undamaged) space and the plastic strain rate. Fig. 1 shows sample stress-strain relation with complete load removal at strain value of  $5 \times 10^{-3}$  to illustrate the effect of  $\beta$ . A higher value of  $\beta$  increases the amount of plastic strain accumulated. A special case of  $\beta = 0$  represents elastic behavior with elastic unloading. Typical values of  $\beta$  are 0.3 - 0.6.

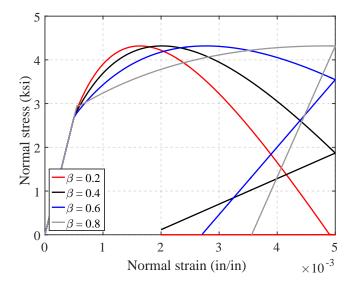


Figure 1: Effect of  $\beta$  on the stress-strain relation and damage evolution

### 2 Damage parameter $A_p$

Parameter  $A_p$  governs the tensile fracture energy and affects the "ductility" of the tensile response. Fig. 2 shows the effect of parameter  $A_p$  on the response in uniaxial tension for different values of  $A_p$ . A higher  $A_p$  results in a more "ductile" tensile response. Faria et al [1] suggests an expression to relate  $A_p$  to the characteristic length  $l_{ch}$  and fracture energy  $G_f$ :

$$A_p = \left(\frac{G_f E}{l_{ch}(f_t)^2} - \frac{1}{2}\right)^{-1} \ge 0 \tag{1}$$

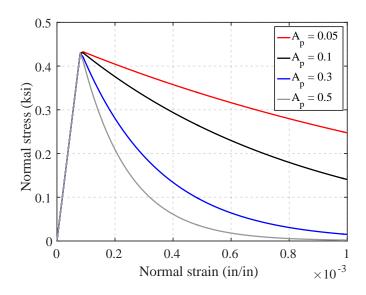


Figure 2: Effect of  $A_p$  on the stress-strain relation

## 3 Damage parameters $A_n$ and $B_n$

Parameters  $A_n$  and  $B_n$  govern the softening behavior of concrete in compression. Fig. 3 show the effect of parameters  $A_n$  and  $B_n$  on the response un uniaxial compression for different values of the parameters. Both parameters affect the ductility of the compressive response; however, parameter  $A_n$  changes the ductility but does not alter the peak strength significantly, whereas parameter  $B_n$  changes both the ductility and the peak strength. It is noteworthy that the numerical solution is rather sensitive to change in parameter  $B_n$ .

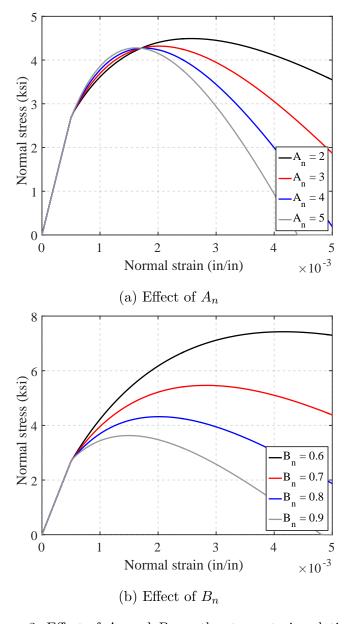


Figure 3: Effect of  $A_n$  and  $B_n$  on the stress-strain relation

# References

[1] Faria R, Oliver J, Cervera M. A strain-based plastic viscous-damage model for massive concrete structures. *International Journal of Solids and Structures* 1998; **35**(14):1533–1558.