# **BLDC Motor Controller Design**

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# 1 Motor Parameters

The motor selection is the first step taken in order to design the motor controller. The motor was selected based on the application it was to be used in. The vehicles average and maximum speeds, and peak acceleration/deceleration was used as the criterion. The motor selected was the Turnigy G46 Brushless Outrunner.

Parameter	Value
Recommended Battery	4-5 Cells @ 14.4-18.5V
RPM	$670 \mathrm{kv}$
Max Current	40A
No Load Current	10V/3.9A
Current Capacity	55A/15sec
Internal Resistance	0.04  ohm
Weight	303g
Diameter of Shaft	$6\mathrm{mm}$
Dimensions	76x50mm

Figure 1: Motor Parameters

## 1.1 Motor Demands

The boundary parameters mentioned previously are also essential in selecting the components for the power stage of the motor controller. These parameters are as follows;

Parameter	Value
Average Speed	$30 \text{ km h}^{-1}$
Peak Speed	$52 \text{ km h}^{-1}$
Wheel diameter	$0.6 \mathrm{m}$
Wheel Reduction Ratio	1:10
Average RPM (for switching frequency)	2653  RPM
Peak RPM (for switching frequency)	4598  RPM
Peak Acceleration (for dv/dt FET capabilities)	$0.856~{ m RPM}~{ m s}^{-1}$

Figure 2: Motor Boundaries

## 2 MOSFETs

The selected MOSFET based on the motor parameters was the IRF1405 A summary of the MOSFETs parameters is below:

	Parameter	Value	Conditions
$V_{(BR)DSS}$	Drain-to-Source Breakdown Voltage	55V	$V_{GS} = 0V, \ I_D = 250\mu A$
$I_D$	Continuous Drain Current	169A	$V_{GS} = 10V, \ T_C = 25^{\circ}C$
$I_D$	Continuous Drain Current	118A	$V_{GS} = 10V, T_C = 100^{\circ}C$
$I_{DM}$	Pulsed Drain Current	680A	
$T_J$	Operating Junction Temperature Range	$-55^{\circ}C - 175^{\circ}C$	
$Q_G$	Total Gate Charge	170nC - 260nC	$I_D = 101A, \ V_{DS} = 44V, \ V_{GS} = 10V$
$Q_{gs}$	Gate-to-Source Charege	44nC - 66nC	$I_D = 101A, \ V_{DS} = 44V, \ V_{GS} = 10V$
$Q_{gd}$	Gate-to-Drain (Miller) Charge	62nC - 93nC	$I_D = 101A, \ V_{DS} = 44V, \ V_{GS} = 10V$
$t_r$	Rise time	190ns	$V_{DD} = 38V$ , $I_D = 101A$ , $R_G = 1.1\Omega$ , $V_{GS} = 10V$ ,
$t_f$	Fall time	110ns	$V_{DD} = 38V, I_D = 101A, R_G = 1.1\Omega, V_{GS} = 10V,$

Figure 3: IRF1405 Specifications

#### 2.1 Bootstrapping

The N-Channel MOSFET proposed to be used on the high side of the power stage requires a gate voltage above the source voltage by a minimum determined by the gate threshold voltage,  $V_{GS(Th)}$ . In order to reach these voltages, the simplest, and most widely used circuitry is the bootstrap charge circuit. <sup>1</sup>

The necessary calculations are:

$$\Delta V_{boot} \le V_{CC} - (V_{fbs} + V_{GS(min)}) \tag{1a}$$

$$C_{boot} = \frac{Q_{total}}{\Delta V_{boot}} \tag{1b}$$

## 3 Gate Driver

The N-Channel MOSFET gate driver is selected based on the MOSFET specifications. Additional criteria such as functionality and minimal power dissipation is secondary.

<sup>&</sup>lt;sup>1</sup>Fairchild AN9052: Design Guide for Selection of Bootstrap Components

### 3.1 Peak Current Drive Requirements

This is the primary criterion for the driver selection. This is primarly based on how fast the application (motor) requires the MOSFET to be turned on and off (rise and fall time of the gate voltage).

This turn on/off speed, dT, is in turn related to how fast the gate capacitance of the MOSFET can be charged and discharged.

$$dT = \frac{[dV \times C]}{I} = \frac{Q}{I} \tag{2}$$

Where;

- dV = Gate voltage
- $\bullet$  C = Gate capacitance
- $\bullet$  I = Peak drive current
- Q = Total gate charge

In the case of the IRF1405, the total gate charge is 260nC and a turn on/off time of  $t=t_r+t_f=300ns$ 

Thus we have a required average current draw of

not sure, used max total gate charge

$$I = \frac{Q}{dT} = \frac{260 \times 10^{-9}}{300 \times 10^{-9}} = 0.9A \tag{3}$$

### 3.2 Power Dissipation

There are three elements due to the charging and discharging of the gate capacitance of the MOSFET <sup>2</sup>:

- 1. Power dissipation due to the charging and discharging of the gate capacitance of the MOSFET,  $P_C$
- 2. Power dissipation due to quiescent current draw of the MOSFET driver,  $P_Q$
- 3. Power dissipation due to cross-conduction (shoot-through) current in the MOSFET driver,  $P_S$

<sup>&</sup>lt;sup>2</sup>Microchip AN799: Matching MOSFET Drivers to MOSFETs