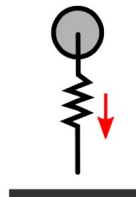
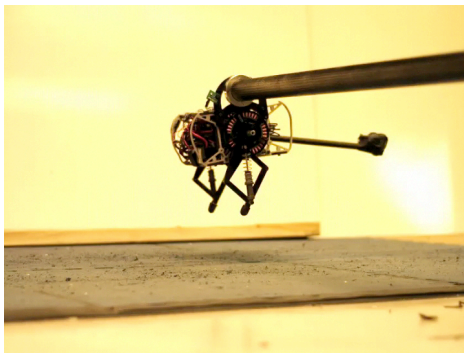


# Controlled IDOF vertical hopper (VH)

- From De and Koditschek [2015b],



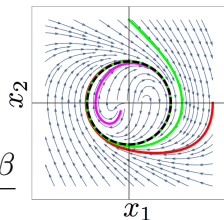
- Phase-energy EoM (De and Koditschek [2015a])

$$\dot{a} = \cos(\psi)u, \quad \dot{\psi} = \omega - \frac{1}{\omega a} \sin(\psi)u$$

- Oscillatory energization, natural damping

$$u = (\textcolor{red}{k} - \textcolor{blue}{a}\beta) \cos(\psi)$$

- On average (De and Koditschek [2015a])  $\frac{da}{d\psi} \stackrel{\text{avg}}{=} \frac{k - a\beta}{2}$



# Controlled IDOF Active Rimless Wheel

- Rimless wheel (McGeer [1990])
- Add liftoff impulse
- *Simplistic view:*

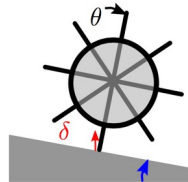
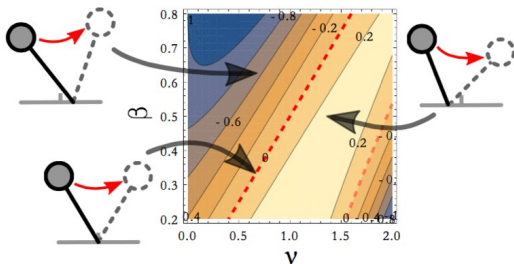
$$F(a_{LO}) = a_{LO} + \gamma$$

$$R(a_{TD}) = \delta a_{TD}, \quad 0 < \delta < 1$$

$$P(a) = \delta(a + \gamma)$$

- Equivalent to stepping (Raibert [1986])

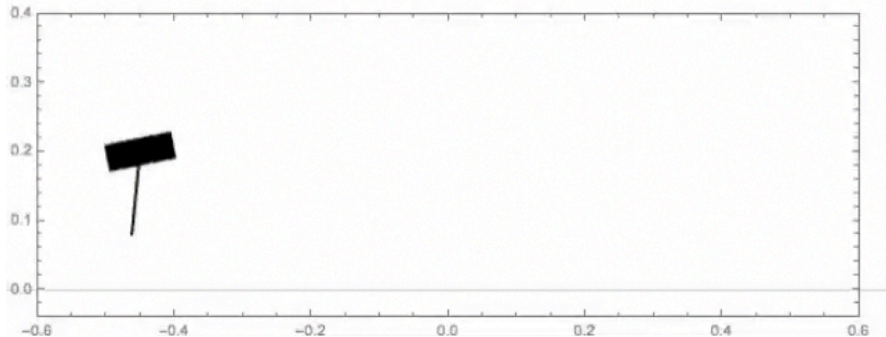
From De and Koditschek [2015a],



Bhounsule et al. [2012]

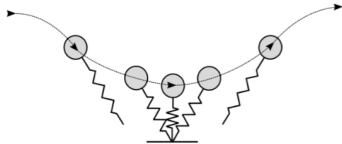
# SLIP as a composition

Clearly works in practice



# SLIP as a composition—verification

- Does SLIP anchor a VH?
- i.e. the dynamics are “the same” on an invariant (attracting) submanifold—Full and Koditschek [1999]



- Radial stance dynamics:  $m\ddot{r} = -\nabla\varphi(r) - g \cos \theta - r\dot{\theta}^2$

- Say  $\begin{bmatrix} x_1 \\ x_2 \end{bmatrix} := \begin{bmatrix} r \\ \dot{r} \end{bmatrix}$

- Then

$$f(x) = \begin{bmatrix} x_2 \\ -\nabla\varphi(x_1) - g \cos \theta - x_1\dot{\theta}^2 \end{bmatrix} \quad f_{\text{VH}}(x) = \begin{bmatrix} x_2 \\ -\nabla\varphi(x_1) - g \end{bmatrix}$$

- Clearly  $f|_{\theta=0, \dot{\theta}=0} = f_{\text{VH}}$   
...but not otherwise

- New research:  $\bar{f} \sim \bar{f}_{\text{VH}}$  —De and Koditschek [2015a]

# Summary

- SLIP can be decomposed
- A vertical hopper can be controlled by active damping
- A rimless wheel can be controlled with active liftoff impulse
- SLIP as a composition empirically works
- But exact anchoring cannot be shown in general