

The 2^k Factorial Design

- Montgomery, chap 6; BHH (2nd ed), chap 5
- **Special case** of the general factorial design; k factors, all at two levels
- Require relatively few runs per factor studied
- Very widely used in industrial experimentation
- Interpretation of data can proceed largely by common sense, elementary arithmetic, and graphics
- For quantitative factors, can't explore a wide region of factor space, but determine promising directions
- Designs can be suitably augmented---sequential assembly
- Basis for 2-level fractional factorial designs, especially useful for screening.

The Simplest Case: The 2^2

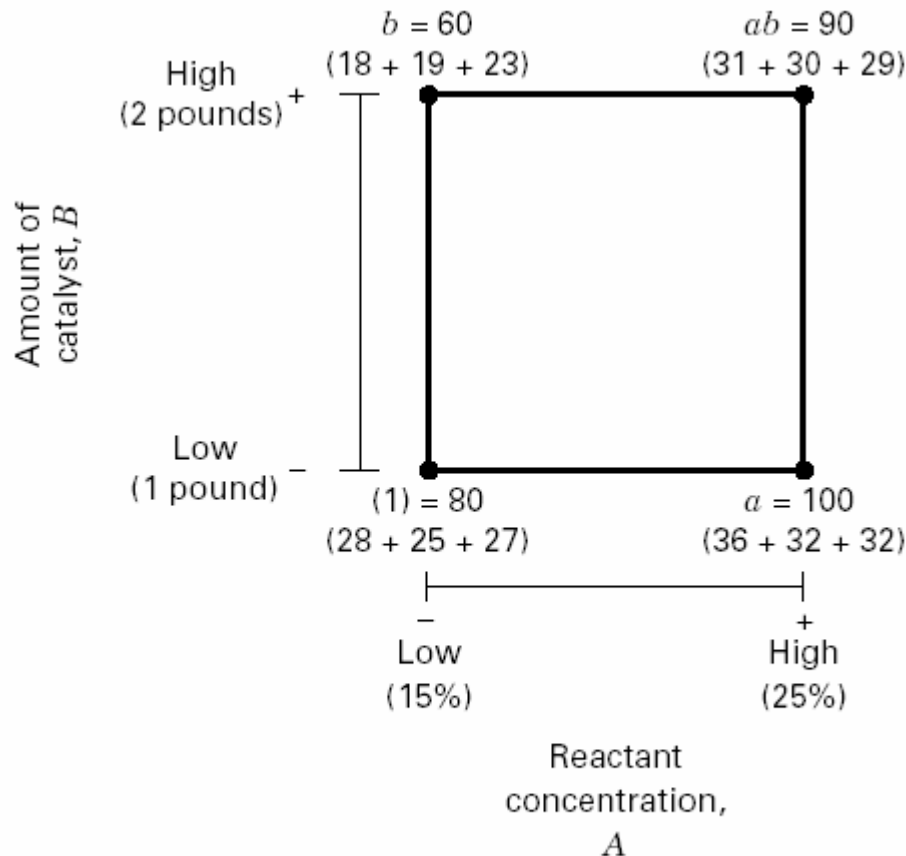


Figure 6-1 Treatment combinations in the 2^2 design.

“-” and “+” denote the low and high levels of a factor, respectively.

Note names of treatment combinations: (1), a , b , ab

Low and high are arbitrary terms

Geometrically, the four runs form the corners of a square

Factors: quantitative or qualitative; interpretation in the final model will be different

Chemical Process Example

| Factor | | Treatment Combination | Replicate | | | Total |
|----------|----------|------------------------------|-----------|----|-----|-------|
| <i>A</i> | <i>B</i> | | I | II | III | |
| – | – | <i>A</i> low, <i>B</i> low | 28 | 25 | 27 | 80 |
| + | – | <i>A</i> high, <i>B</i> low | 36 | 32 | 32 | 100 |
| – | + | <i>A</i> low, <i>B</i> high | 18 | 19 | 23 | 60 |
| + | + | <i>A</i> high, <i>B</i> high | 31 | 30 | 29 | 90 |

A = reactant concentration, B = catalyst amount,
 y = recovery

Analysis Procedure for a Factorial Design

- Estimate factor **effects**
- **Formulate** model
 - With replication, use full model
 - With an unreplicated design, use normal probability plots
- Statistical **testing** (ANOVA)
- **Refine** the model
- Analyze **residuals** (graphical)
- **Interpret** results

Estimation of Factor Effects

$$\begin{aligned} A &= \bar{y}_{A^+} - \bar{y}_{A^-} \\ &= \frac{ab + a}{2n} - \frac{b + (1)}{2n} \\ &= \frac{1}{2n} [ab + a - b - (1)] \end{aligned}$$

$$\begin{aligned} B &= \bar{y}_{B^+} - \bar{y}_{B^-} \\ &= \frac{ab + b}{2n} - \frac{a + (1)}{2n} \\ &= \frac{1}{2n} [ab + b - a - (1)] \end{aligned}$$

$$\begin{aligned} AB &= \frac{ab + (1)}{2n} - \frac{a + b}{2n} \\ &= \frac{1}{2n} [ab + (1) - a - b] \end{aligned}$$

Computation: difference between averages of “+” and “-” sign observations

The effect estimates are:

$$A = 8.33, \quad B = -5.00, \quad AB = 1.67$$

Practical interpretation?

- Increasing reactant concentration increases yield
- Catalyst effect is negative
- Interaction effect is relatively smaller

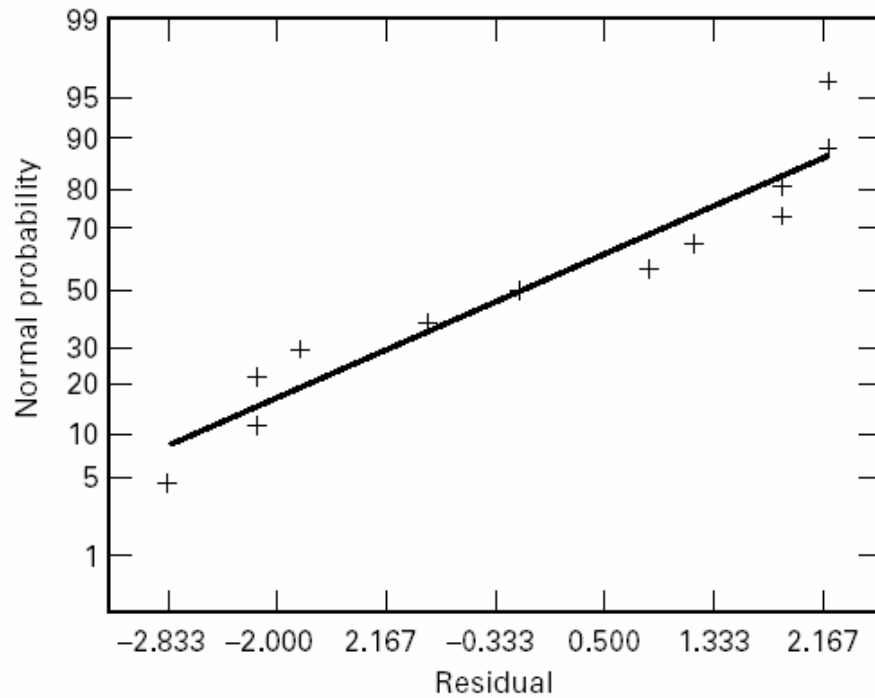
Statistical Testing - ANOVA

Table 6-1 Analysis of Variance for the Experiment in Figure 6-1

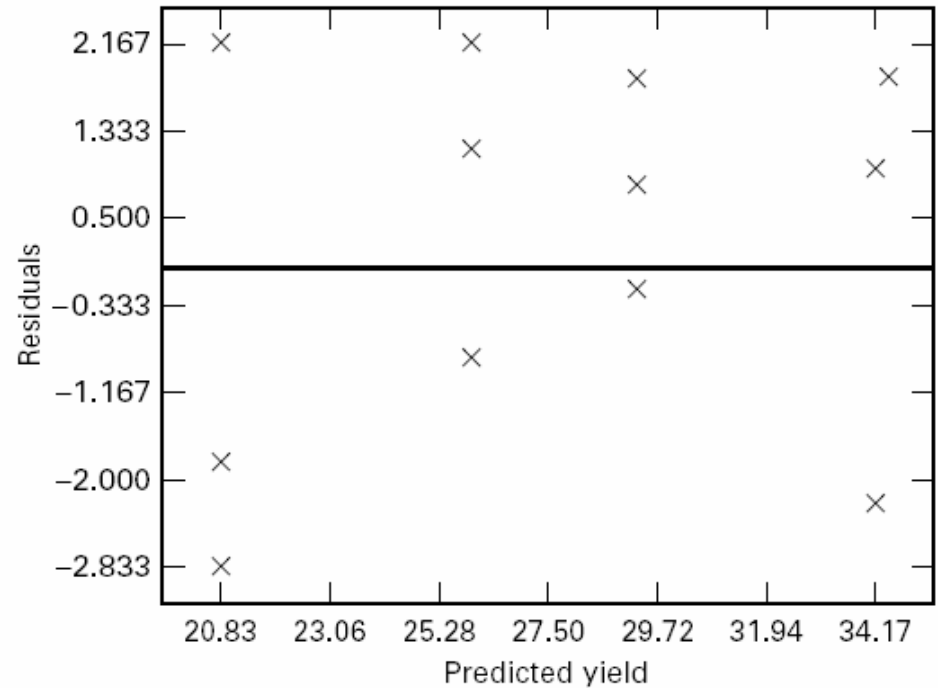
| Source of Variation | Sum of Squares | Degrees of Freedom | Mean Square | F_0 | P -Value |
|---------------------|----------------|--------------------|-------------|-------|------------|
| <i>A</i> | 208.33 | 1 | 208.33 | 53.15 | 0.0001 |
| <i>B</i> | 75.00 | 1 | 75.00 | 19.13 | 0.0024 |
| <i>AB</i> | 8.33 | 1 | 8.33 | 2.13 | 0.1826 |
| Error | 31.34 | 8 | 3.92 | | |
| Total | 323.00 | 11 | | | |



Residuals and Diagnostic Checking



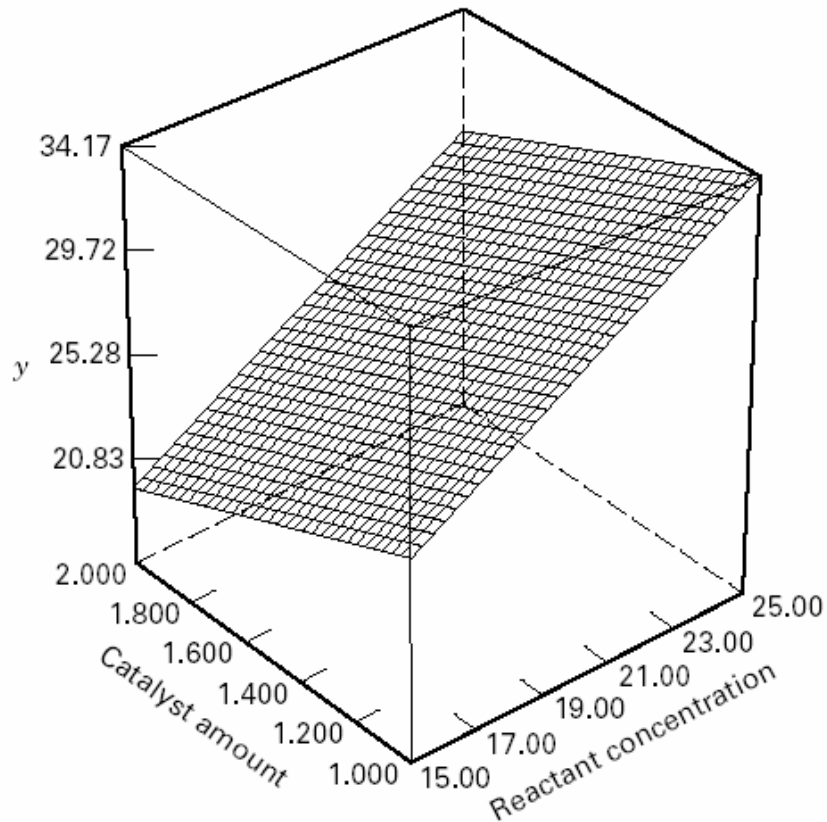
(a) Normal probability plot



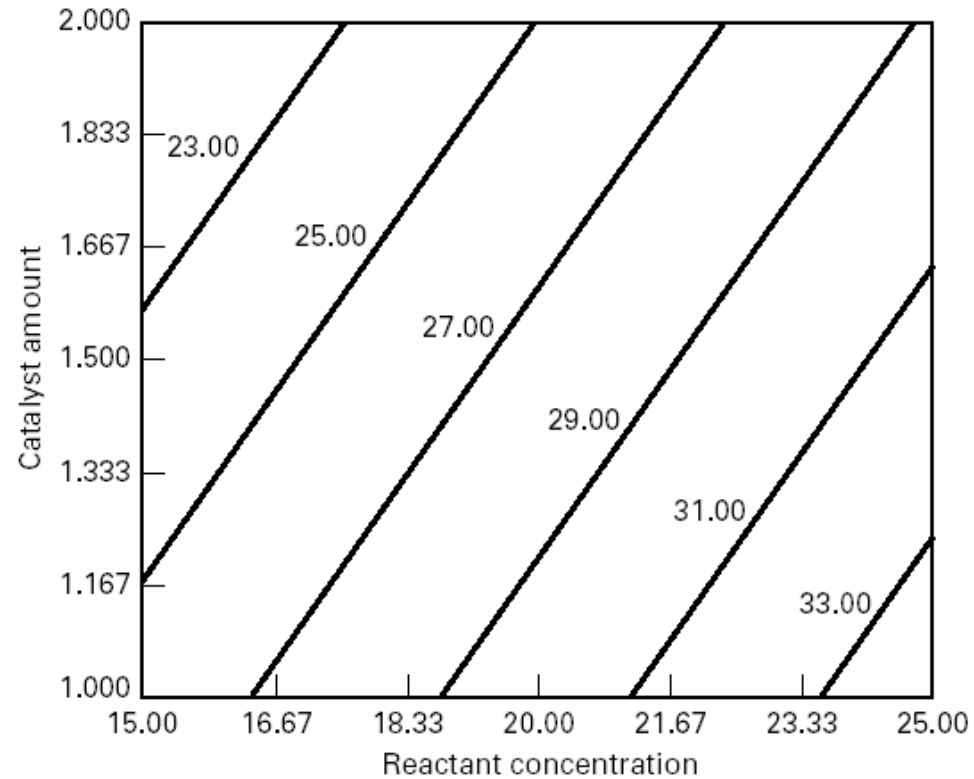
(b) Residuals versus predicted yield

Figure 6-2 Residual plots for the chemical process experiment.

The Response Surface (for the additive model)



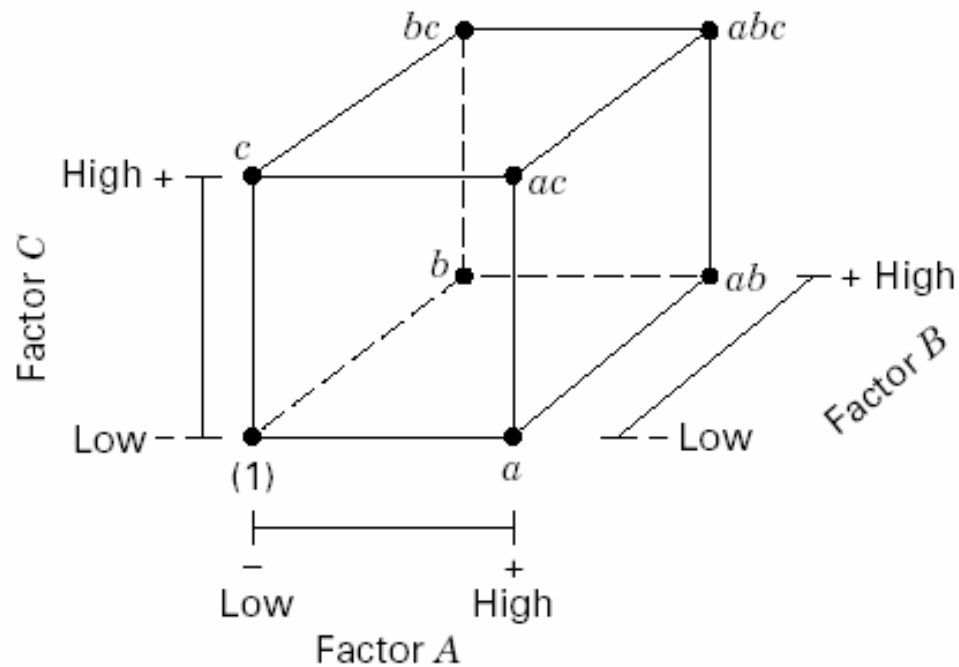
(a) Response surface



(b) Contour plot

Figure 6-3 Response surface plot and contour plot of yield from the chemical process experiment.

The 2^3 Factorial Design



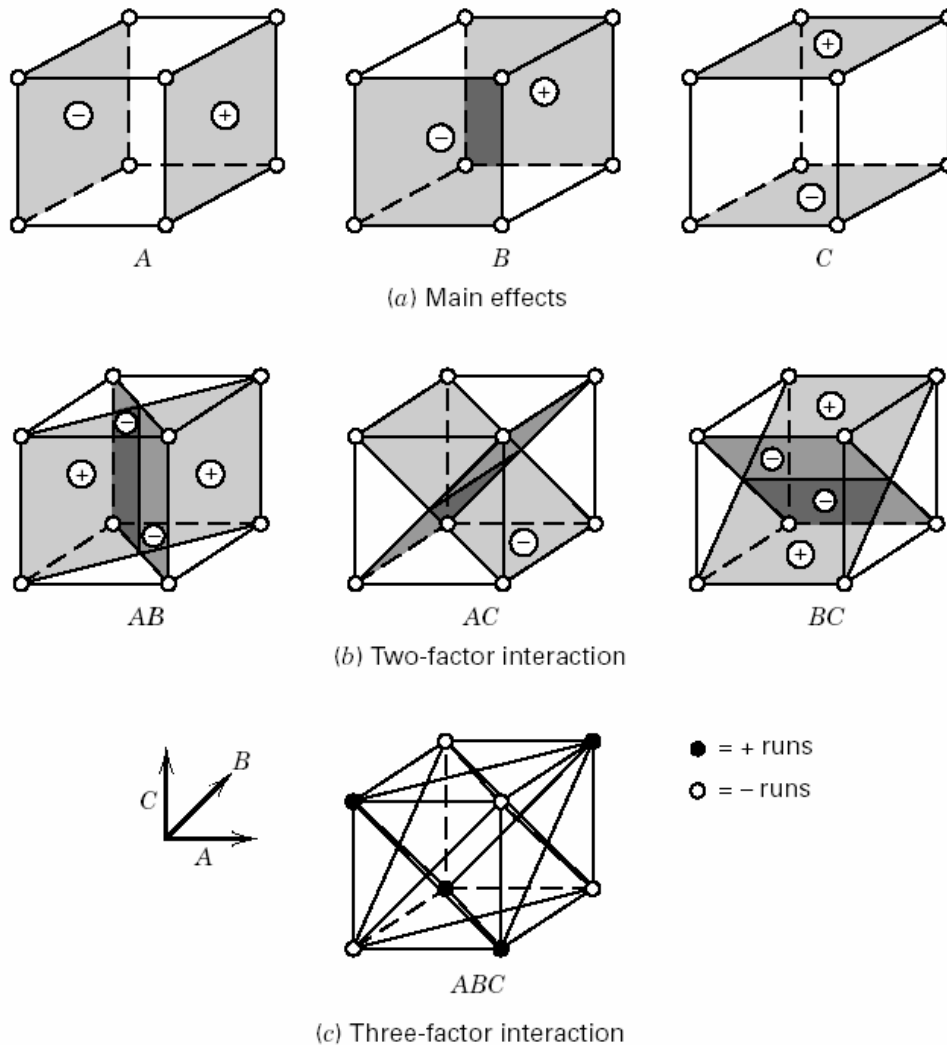
(a) Geometric view

| Run | Factor | | |
|-----|----------|----------|----------|
| | <i>A</i> | <i>B</i> | <i>C</i> |
| 1 | – | – | – |
| 2 | + | – | – |
| 3 | – | + | – |
| 4 | + | + | – |
| 5 | – | – | + |
| 6 | + | – | + |
| 7 | – | + | + |
| 8 | + | + | + |

(b) The design matrix

Figure 6-4 The 2^3 factorial design.

Effects in The 2^3 Factorial Design



$$A = \bar{y}_{A^+} - \bar{y}_{A^-}$$

$$B = \bar{y}_{B^+} - \bar{y}_{B^-}$$

$$C = \bar{y}_{C^+} - \bar{y}_{C^-}$$

etc, etc, ...

Interaction effects are also differences between averages of 4 runs.

Figure 6-5 Geometric presentation of contrasts corresponding to the main effects and interactions in the 2^3 design.

An Example of a 2^3 Factorial Design

Table 6-4 The Plasma Etch Experiment, Example 6-1

| Run | Coded Factors | | | Etch Rate | | Total | Factor Levels | | |
|-----|---------------|----|----|-------------|-------------|--------------|--|-----------|------|
| | A | B | C | Replicate 1 | Replicate 2 | | Low (-1) | High (+1) | |
| 1 | -1 | -1 | -1 | 550 | 604 | (1) = 1154 | A (Gap, cm) | 0.80 | 1.20 |
| 2 | 1 | -1 | -1 | 669 | 650 | $a = 1319$ | B (C ₂ F ₆ flow, SCCM) | 125 | 200 |
| 3 | -1 | 1 | -1 | 633 | 601 | $b = 1234$ | C (Power, W) | 275 | 325 |
| 4 | 1 | 1 | -1 | 642 | 635 | $ab = 1277$ | | | |
| 5 | -1 | -1 | 1 | 1037 | 1052 | $c = 2089$ | | | |
| 6 | 1 | -1 | 1 | 749 | 868 | $ac = 1617$ | | | |
| 7 | -1 | 1 | 1 | 1075 | 1063 | $bc = 2178$ | | | |
| 8 | 1 | 1 | 1 | 729 | 860 | $abc = 1589$ | | | |

$A = \text{gap}, B = \text{Flow}, C = \text{Power}, y = \text{Etch Rate}$

Table of – and + Signs for the 2³ Factorial Design (pg. 214)

Table 6-3 Algebraic Signs for Calculating Effects in the 2³ Design

| Treatment Combination | Factorial Effect | | | | | | | |
|--------------------------|------------------|----------|----------|-----------|----------|-----------|-----------|------------|
| | <i>I</i> | <i>A</i> | <i>B</i> | <i>AB</i> | <i>C</i> | <i>AC</i> | <i>BC</i> | <i>ABC</i> |
| (1) | + | – | – | + | – | + | + | – |
| <i>a</i> | + | + | – | – | – | – | + | + |
| <i>b</i> | + | – | + | – | – | + | – | + |
| <i>ab</i> | + | + | + | + | – | – | – | – |
| <i>c</i> | + | – | – | + | + | – | – | + |
| <i>ac</i> | + | + | – | – | + | + | – | – |
| <i>bc</i> | + | – | + | – | + | – | + | – |
| <i>abc</i> | + | + | + | + | + | + | + | + |

Properties of the Table

- Except for column I , every column has an equal number of + and – signs
- The sum of the product of signs in any two columns is zero: **orthogonal** design
- Multiplying any column by I leaves that column unchanged (identity element)
- The product of any two columns yields a column in the table:

$$A \times B = AB$$

$$AB \times BC = AB^2C = AC$$

- Orthogonality is an important property shared by all factorial designs

R computation

```
> etch.rate <- matrix(c(550,604,669,650,633,601,642,635,  
+ 1037,1052,749,868,1075,1063,729,860),byrow=T,ncol=2)  
> dimnames(etch.rate) <- list(  
+ c("(1)", "a", "b", "ab", "c", "ac", "bc", "abc"), c("Rep1", "Rep2"))  
>  
> A <- rep(c(-1,1),4)  
> B <- rep(c(-1,-1,1,1),2)  
> C <- c(rep(-1,4),rep(1,4))  
>  
> Total <- apply(etch.rate,1,sum)  
>  
> cbind(A,B,C,etch.rate>Total)
```

| | A | B | C | Rep1 | Rep2 | Total |
|-----|----|----|----|------|------|-------|
| (1) | -1 | -1 | -1 | 550 | 604 | 1154 |
| a | 1 | -1 | -1 | 669 | 650 | 1319 |
| b | -1 | 1 | -1 | 633 | 601 | 1234 |
| ab | 1 | 1 | -1 | 642 | 635 | 1277 |
| c | -1 | -1 | 1 | 1037 | 1052 | 2089 |
| ac | 1 | -1 | 1 | 749 | 868 | 1617 |
| bc | -1 | 1 | 1 | 1075 | 1063 | 2138 |
| abc | 1 | 1 | 1 | 729 | 860 | 1589 |

R computation (cont)

```
> # #reps: n=2
> n <- 2
> # Effect estimates are differences of averages of 4 means ("runs")
> # Effect estimates:
> Aeff <- (Total %*% A) / (4*n)
> Beff <- (Total %*% B) / (4*n)
> Ceff <- (Total %*% C) / (4*n)
>
> # Interaction effects
> AB <- A*B
> AC <- A*C
> BC <- B*C
> ABC <- A*B*C
> cbind(A,B,C,AB,AC,BC,ABC,Total)
      A  B  C AB AC BC ABC Total
(1) -1 -1 -1  1  1  1  -1  1154
a     1 -1 -1 -1 -1  1   1  1319
b    -1  1 -1 -1  1 -1   1  1234
ab     1  1 -1  1 -1 -1  -1  1277
c    -1 -1  1  1 -1 -1   1  2089
ac     1 -1  1 -1  1 -1  -1  1617
bc    -1  1  1 -1 -1  1  -1  2138
abc     1  1  1  1  1  1   1  1589
>
> ABeff <- (Total %*% AB) / (4*n)
> ACeff <- (Total %*% AC) / (4*n)
> BCeff <- (Total %*% BC) / (4*n)
> ABCeff <- (Total %*% ABC) / (4*n)
```

R computation (cont)

```
> # Summary
> Effects <- t(Total) %*% cbind(A,B,C,AB,AC,BC,ABC) / (4*n)
> Summary <- rbind( cbind(A,B,C,AB,AC,BC,ABC),Effects )
> dimnames(Summary)[[1]] <- c(dimnames(etch.rate)[[1]],"Effect")
> Summary
```

| | A | B | C | AB | AC | BC | ABC |
|--------|----------|--------|---------|---------|----------|--------|--------|
| (1) | -1.000 | -1.000 | -1.000 | 1.000 | 1.000 | 1.000 | -1.000 |
| a | 1.000 | -1.000 | -1.000 | -1.000 | -1.000 | 1.000 | 1.000 |
| b | -1.000 | 1.000 | -1.000 | -1.000 | 1.000 | -1.000 | 1.000 |
| ab | 1.000 | 1.000 | -1.000 | 1.000 | -1.000 | -1.000 | -1.000 |
| c | -1.000 | -1.000 | 1.000 | 1.000 | -1.000 | -1.000 | 1.000 |
| ac | 1.000 | -1.000 | 1.000 | -1.000 | 1.000 | -1.000 | -1.000 |
| bc | -1.000 | 1.000 | 1.000 | -1.000 | -1.000 | 1.000 | -1.000 |
| abc | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| Effect | -101.625 | 7.375 | 306.125 | -24.875 | -153.625 | -2.125 | 5.625 |

```
>
> # Fit as an ANOVA model
> etch.vec <- c(t(etch.rate))
> Af <- rep(as.factor(A),rep(2,8))
> Bf <- rep(as.factor(B),rep(2,8))
> Cf <- rep(as.factor(C),rep(2,8))
> options(contrasts=c("contr.sum","contr.poly"))
> etch.lm <- lm(etch.vec ~ Af*Bf*Cf)
```


Estimation of Factor Effects

Table 6-5 Effect Estimate Summary for Example 6-1

| Factor | Effect Estimate | Sum of Squares | Percent Contribution |
|------------|-----------------|----------------|----------------------|
| <i>A</i> | -101.625 | 41,310.5625 | 7.7736 |
| <i>B</i> | 7.375 | 217.5625 | 0.0409 |
| <i>C</i> | 306.125 | 374,850.0625 | 70.5373 |
| <i>AB</i> | -24.875 | 2475.0625 | 0.4657 |
| <i>AC</i> | -153.625 | 94,402.5625 | 17.7642 |
| <i>BC</i> | -2.125 | 18.0625 | 0.0034 |
| <i>ABC</i> | 5.625 | 126.5625 | 0.0238 |

Model Coefficients – Full Model

| Factor | Coefficient Estimated | DF | Standard Error | 95% CI Low | 95% CI High | VIF |
|---------------|----------------------------------|-----------|---------------------------|-----------------------|------------------------|------------|
| Intercept | 776.06 | 1 | 11.87 | 748.70 | 803.42 | |
| A-Gap | −50.81 | 1 | 11.87 | −78.17 | −23.45 | 1.00 |
| B-Gas flow | 3.69 | 1 | 11.87 | −23.67 | 31.05 | 1.00 |
| C-Power | 153.06 | 1 | 11.87 | 125.70 | 180.42 | 1.00 |
| AB | −12.44 | 1 | 11.87 | −39.80 | 14.92 | 1.00 |
| AC | −76.81 | 1 | 11.87 | −104.17 | −49.45 | 1.00 |
| BC | −1.06 | 1 | 11.87 | −28.42 | 26.30 | 1.00 |
| ABC | 2.81 | 1 | 11.87 | −24.55 | 30.17 | 1.00 |

R computation (cont)

```
> options(contrasts=c("contr.sum", "contr.poly"))
> etch.lm <- lm(etch.vec ~ Af*Bf*Cf)
> summary(etch.lm)
```

Call:

```
lm(formula = etch.vec ~ Af * Bf * Cf)
```

Residuals:

| | Min | 1Q | Median | 3Q | Max |
|--|------------|------------|-----------|-----------|-----------|
| | -6.550e+01 | -1.113e+01 | 8.882e-16 | 1.113e+01 | 6.550e+01 |

Coefficients:

| | Estimate | Std. Error | t value | Pr(> t) | |
|-------------|----------|------------|---------|----------|-----|
| (Intercept) | 776.062 | 11.865 | 65.406 | 3.32e-12 | *** |
| Af1 | 50.813 | 11.865 | 4.282 | 0.002679 | ** |
| Bf1 | -3.687 | 11.865 | -0.311 | 0.763911 | |
| Cf1 | -153.062 | 11.865 | -12.900 | 1.23e-06 | *** |
| Af1:Bf1 | -12.437 | 11.865 | -1.048 | 0.325168 | |
| Af1:Cf1 | -76.812 | 11.865 | -6.474 | 0.000193 | *** |
| Bf1:Cf1 | -1.063 | 11.865 | -0.090 | 0.930849 | |
| Af1:Bf1:Cf1 | -2.812 | 11.865 | -0.237 | 0.818586 | |

Signif. codes: 0 '***' 0.001 '**' 0.01 '*' 0.05 '.' 0.1 ' ' 1

Residual standard error: 47.46 on 8 degrees of freedom

Multiple R-Squared: 0.9661, Adjusted R-squared: 0.9364

F-statistic: 32.56 on 7 and 8 DF, p-value: 2.896e-05

Review question:

**Why are the anova
model coefficients ½
the “effect estimates”?**

ANOVA Summary – Full Model

Table 6-6 Analysis of Variance for the Plasma Etching Experiment

| Source of Variation | Sum of Squares | Degrees of Freedom | Mean Square | F_0 | P -Value |
|---------------------|----------------|--------------------|--------------|--------|------------|
| Gap (A) | 41,310.5625 | 1 | 41,310.5625 | 18.34 | 0.0027 |
| Gas flow (B) | 217.5625 | 1 | 217.5625 | 0.10 | 0.7639 |
| Power (C) | 374,850.0625 | 1 | 374,850.0625 | 166.41 | 0.0001 |
| AB | 2475.0625 | 1 | 2475.0625 | 1.10 | 0.3252 |
| AC | 94,402.5625 | 1 | 94,402.5625 | 41.91 | 0.0002 |
| BC | 18.0625 | 1 | 18.0625 | 0.01 | 0.9308 |
| ABC | 126.5625 | 1 | 126.5625 | 0.06 | 0.8186 |
| Error | 18,020.5000 | 8 | 2252.5625 | | |
| Total | 531,420.9375 | 15 | | | |

R computation (cont)

```
> anova(etch.lm)
```

Analysis of Variance Table

Response: etch.vec

| | Df | Sum Sq | Mean Sq | F value | Pr(>F) | |
|-----------|----|--------|---------|----------|-----------|-----|
| Af | 1 | 41311 | 41311 | 18.3394 | 0.0026786 | ** |
| Bf | 1 | 218 | 218 | 0.0966 | 0.7639107 | |
| Cf | 1 | 374850 | 374850 | 166.4105 | 1.233e-06 | *** |
| Af:Bf | 1 | 2475 | 2475 | 1.0988 | 0.3251679 | |
| Af:Cf | 1 | 94403 | 94403 | 41.9090 | 0.0001934 | *** |
| Bf:Cf | 1 | 18 | 18 | 0.0080 | 0.9308486 | |
| Af:Bf:Cf | 1 | 127 | 127 | 0.0562 | 0.8185861 | |
| Residuals | 8 | 18020 | 2253 | | | |

Signif. codes: 0 '***' 0.001 '**' 0.01 '*' 0.05 '.' 0.1 ' ' 1

```
> model.matrix(etch.lm)
```

| | (Intercept) | Af1 | Bf1 | Cf1 | Af1:Bf1 | Af1:Cf1 | Bf1:Cf1 | Af1:Bf1:Cf1 |
|----|-------------|-----|-----|-----|---------|---------|---------|-------------|
| 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 2 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 3 | 1 | -1 | 1 | 1 | -1 | -1 | 1 | -1 |
| 4 | 1 | -1 | 1 | 1 | -1 | -1 | 1 | -1 |
| 5 | 1 | 1 | -1 | 1 | -1 | 1 | -1 | -1 |
| 6 | 1 | 1 | -1 | 1 | -1 | 1 | -1 | -1 |
| 7 | 1 | -1 | -1 | 1 | 1 | -1 | -1 | 1 |
| 8 | 1 | -1 | -1 | 1 | 1 | -1 | -1 | 1 |
| 9 | 1 | 1 | 1 | -1 | 1 | -1 | -1 | -1 |
| 10 | 1 | 1 | 1 | -1 | 1 | -1 | -1 | -1 |
| 11 | . | . | . | . | . | . | . | . |

BHH sect 5.10: “Misuse of the ANOVA for 2^k Factorial Experiments”

- For 2^k designs, the use of the ANOVA is confusing and makes little sense. $N=n \times 2^k$ observations. $2^k - 1$ d.f. partitioned into individual “SS” for effects, each equal to $N(\text{effect})^2/4$, divided by $df=1$, and turned into an F-ratio. Experimenter wants magnitude of effect, $\bar{y}_+ - \bar{y}_-$, and t ratio = effect/se(effect).
- P-values should not be used mechanically for yes-or-no decisions on what effects are real. Information about the size of an effect and its possible error must be allowed to interact with experimenter’s subject matter knowledge. Graphical methods (coming) provide a valuable means of allowing information in the data and in the mind of the experimenter to interact properly.

Refine Model – Remove Nonsignificant Factors

Table 6-7 (continued)

Response: Etch rate

ANOVA for Selected Factorial Model

Analysis of variance table [Partial sum of squares]

| Source | Sum of Squares | DF | Mean Square | F Value | Prob > F |
|---------------|-----------------------|-----------|--------------------|----------------|--------------------|
| Model | 5.106E+005 | 3 | 1.702E+005 | 97.91 | <0.0001 |
| A | 41310.56 | 1 | 41310.56 | 23.77 | 0.0004 |
| C | 3.749E+005 | 1 | 3.749E+005 | 215.66 | <0.0001 |
| AC | 94402.56 | 1 | 94402.56 | 54.31 | <0.0001 |
| Residual | 20857.75 | 12 | 1738.15 | | |
| Lack of Fit | 2837.25 | 4 | 709.31 | 0.31 | 0.8604 |
| Pure Error | 18020.50 | 8 | 2252.56 | | |
| Cor Total | 5.314E+005 | 15 | | | |

| | | | |
|-----------|----------|----------------|--------|
| Std. Dev. | 41.69 | R-Squared | 0.9608 |
| Mean | 776.06 | Adj R-Squared | 0.9509 |
| C.V. | 5.37 | Pred R-Squared | 0.9302 |
| PRESS | 37080.44 | Adeq Precision | 22.055 |

Note that Sums of Squares for A, C, AC did not change.

Model Coefficients – Reduced Model

| Factor | Coefficient Estimate | DF | Standard Error | 95% CI Low | 95% CI High | VIF |
|-----------|----------------------|----|----------------|------------|-------------|------|
| Intercept | 776.06 | 1 | 10.42 | 753.35 | 798.77 | |
| A-Gap | −50.81 | 1 | 10.42 | −73.52 | 28.10 | 1.00 |
| C-Power | 153.06 | 1 | 10.42 | 130.35 | 175.77 | 1.00 |
| AC | −76.81 | 1 | 10.42 | −99.52 | −54.10 | 1.00 |

What has changed from the previous larger table of coefficient estimates?

Model Summary Statistics for Reduced Model (pg. 222)

- R^2 and adjusted R^2

$$R^2 = \frac{SS_{Model}}{SS_T} = \frac{5.106 \times 10^5}{5.314 \times 10^5} = 0.9608$$

$$R^2_{Adj} = 1 - \frac{SS_E / df_E}{SS_T / df_T} = 1 - \frac{20857.75 / 12}{5.314 \times 10^5 / 15} = 0.9509$$

- R^2 for prediction (based on PRESS)

$$R^2_{Pred} = 1 - \frac{PRESS}{SS_T} = 1 - \frac{37080.44}{5.314 \times 10^5} = 0.9302$$

Model Summary Statistics (pg. 222)

- **Standard error** of model coefficients (full model)

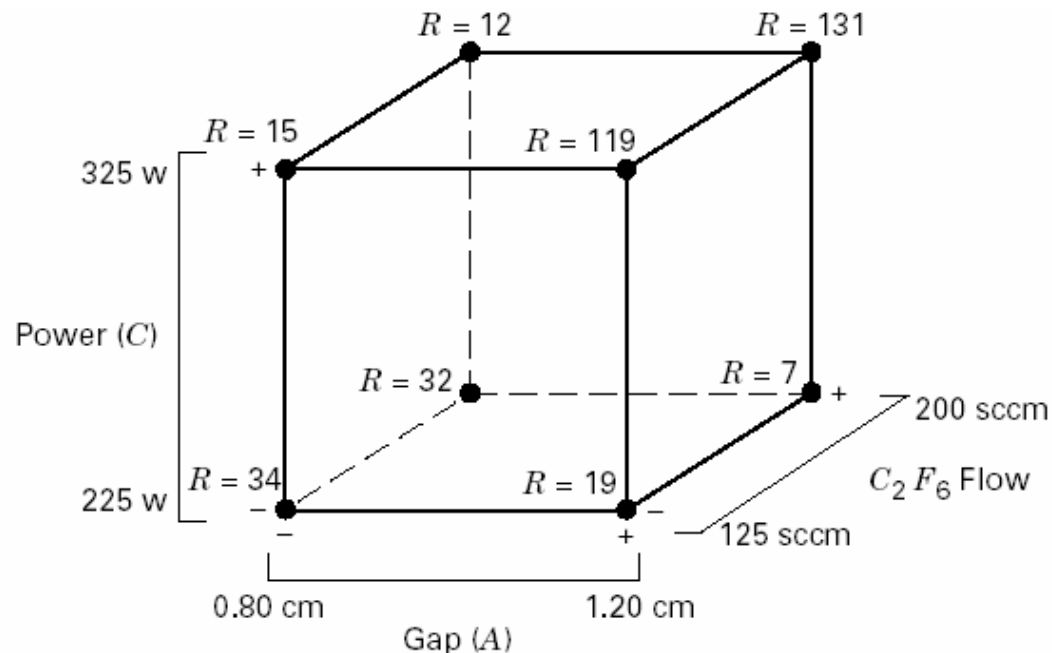
$$se(\hat{\beta}) = \sqrt{V(\hat{\beta})} = \sqrt{\frac{\sigma^2}{n2^k}} = \sqrt{\frac{\hat{\beta} MS_E}{n2^k}} = \sqrt{\frac{2252.56}{2(8)}} = 11.87$$

- **Confidence interval** on model coefficients

$$\hat{\beta} - t_{\alpha/2, df_E} se(\hat{\beta}) \leq \beta \leq \hat{\beta} + t_{\alpha/2, df_E} se(\hat{\beta})$$

Exercise: derive the above expression for $se(\hat{\beta})$

Model Interpretation



Cube plots are often useful visual displays of experimental results

Figure 6-8 Ranges of etch rates for Example 6-1.

Assessing “error” or residual variation

Often there are more factors to be investigated that can conveniently be accommodated with the time and budget available. Rather than make 16 runs for a replicated 2^3 factorial, it might be preferable to introduce a 4th factor and run an *un*-replicated 2^4 design.

Options:

1. With replication, use the usual pooled variance computed from the replicates.
2. Assume that higher order interaction effects are noise and construct an internal reference set.
3. Assess meaningful effects, including possibly meaningful higher order interactions, using Normal and “Lenth” plots.

Example: Process development experiment.

| Factor | Level 1 | Level 2 |
|----------------------------|---------|---------|
| Catalyst charge (lb) | 10 | 15 |
| Temperature © | 220 | 240 |
| Pressure (psi) | 50 | 80 |
| Reactant concentration (%) | 10 | 12 |

Response: “percent conversion”

```
> # Read in process development data of BHH2 Table 5.10a
> tab5.10.dat <- read.table(file.choose(),header=T)
> dimnames(tab5.10.dat)[[2]][2:5] <- c("A", "B", "C", "D")
> tab5.10.dat
```

| | yatesOrd | A | B | C | D | conversion | randomOrd |
|----|----------|----|----|----|----|------------|-----------|
| 1 | 1 | -1 | -1 | -1 | -1 | 70 | 8 |
| 2 | 2 | 1 | -1 | -1 | -1 | 60 | 2 |
| 3 | 3 | -1 | 1 | -1 | -1 | 89 | 10 |
| 4 | 4 | 1 | 1 | -1 | -1 | 81 | 4 |
| 5 | 5 | -1 | -1 | 1 | -1 | 69 | 15 |
| 6 | 6 | 1 | -1 | 1 | -1 | 62 | 9 |
| 7 | 7 | -1 | 1 | 1 | -1 | 88 | 1 |
| 8 | 8 | 1 | 1 | 1 | -1 | 81 | 13 |
| 9 | 9 | -1 | -1 | -1 | 1 | 60 | 16 |
| 10 | 10 | 1 | -1 | -1 | 1 | 49 | 5 |
| 11 | 11 | -1 | 1 | -1 | 1 | 88 | 11 |
| 12 | 12 | 1 | 1 | -1 | 1 | 82 | 14 |
| 13 | 13 | -1 | -1 | 1 | 1 | 60 | 3 |
| 14 | 14 | 1 | -1 | 1 | 1 | 52 | 12 |
| 15 | 15 | -1 | 1 | 1 | 1 | 86 | 6 |
| 16 | 16 | 1 | 1 | 1 | 1 | 79 | 7 |

```
> # Full design matrix with interactions
> des4 <- ffFullMatrix(X,x=c(1,2,3,4),maxInt=4)
> des4
```

\$Xa

| | one | x1 | x2 | x3 | x4 | x1*x2 | x1*x3 | x1*x4 | x2*x3 | x2*x4 | x3*x4 | x1*x2*x3 | x1*x2*x4 |
|----|-----|----|----|----|----|-------|-------|-------|-------|-------|-------|----------|----------|
| 1 | 1 | -1 | -1 | -1 | -1 | 1 | 1 | 1 | 1 | 1 | 1 | -1 | -1 |
| 2 | 1 | 1 | -1 | -1 | -1 | -1 | -1 | -1 | 1 | 1 | 1 | 1 | 1 |
| 3 | 1 | -1 | 1 | -1 | -1 | -1 | 1 | 1 | -1 | -1 | 1 | 1 | 1 |
| 4 | 1 | 1 | 1 | -1 | -1 | 1 | -1 | -1 | -1 | -1 | 1 | -1 | -1 |
| 5 | 1 | -1 | -1 | 1 | -1 | 1 | -1 | 1 | -1 | 1 | -1 | 1 | -1 |
| 6 | 1 | 1 | -1 | 1 | -1 | -1 | 1 | -1 | -1 | 1 | -1 | -1 | 1 |
| 7 | 1 | -1 | 1 | 1 | -1 | -1 | -1 | 1 | 1 | -1 | -1 | -1 | 1 |
| 8 | 1 | 1 | 1 | 1 | -1 | 1 | 1 | -1 | 1 | -1 | -1 | 1 | -1 |
| 9 | 1 | -1 | -1 | -1 | 1 | 1 | 1 | -1 | 1 | -1 | -1 | -1 | 1 |
| 10 | 1 | 1 | -1 | -1 | 1 | -1 | -1 | 1 | 1 | -1 | -1 | 1 | -1 |
| 11 | 1 | -1 | 1 | -1 | 1 | -1 | 1 | -1 | -1 | 1 | -1 | 1 | -1 |
| 12 | 1 | 1 | 1 | -1 | 1 | 1 | -1 | 1 | -1 | 1 | -1 | -1 | 1 |
| 13 | 1 | -1 | -1 | 1 | 1 | 1 | -1 | -1 | -1 | -1 | 1 | 1 | 1 |
| 14 | 1 | 1 | -1 | 1 | 1 | -1 | 1 | 1 | -1 | -1 | 1 | -1 | -1 |
| 15 | 1 | -1 | 1 | 1 | 1 | -1 | -1 | -1 | 1 | 1 | 1 | -1 | -1 |
| 16 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |

[. . . additional columns of 1's and -1's . . .]

\$x

[1] 1 2 3 4

\$maxInt

[1] 4

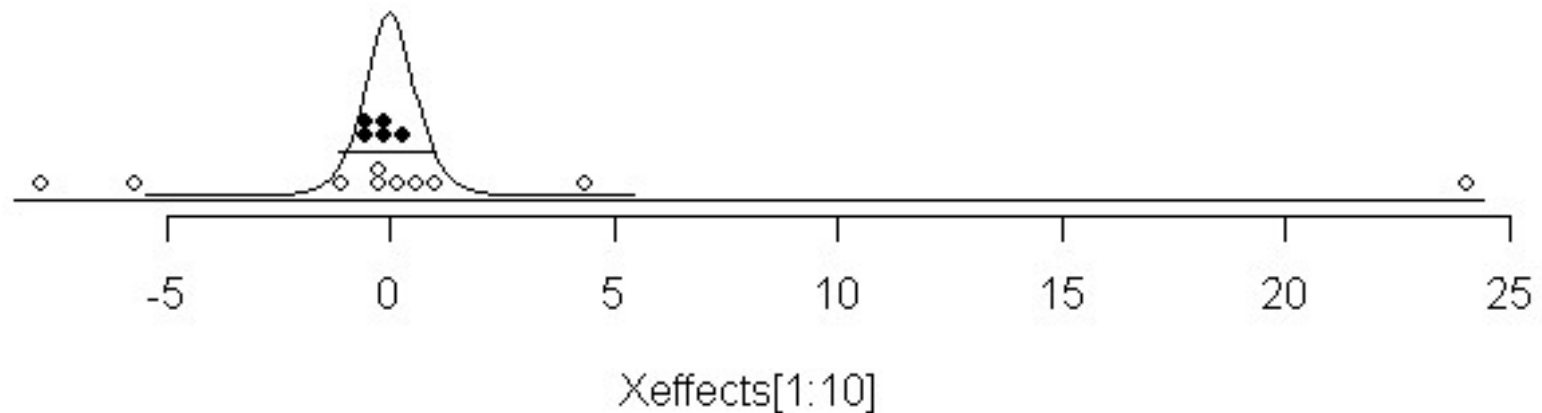
\$nTerms

| blk | main | int.2 | int.3 | int.4 |
|-----|------|-------|-------|-------|
| 0 | 4 | 6 | 4 | 1 |

```

> # Use the higher order interaction effects as the reference set of
> # (independent) effects that represent noise. The standard
> # deviation of these (about zero) provides a relevant se for
> # the rest of the effects.
>
> Xeffects <- matrix(tab5.10.dat$conversion,nrow=1) %*% des4$Xa[,-1]/8
> dotPlot(Xeffects[1:10])
> dots(Xeffects[11:15],y=0.1,stacked=T,pch=19) # add the higher order effects
> SEeffect <- sqrt(sum(Xeffects[11:15]^2)/5)
> SEeffect
[1] 0.5477226
> lines(SEeffect*seq(-10,10,.11),dt(seq(-10,10,.11),df=5)) # add t(df=5)
reference density
> t.ratios <- Xeffects[11:15]/SEeffect
> round(t.ratios,2)
[1]

```



```

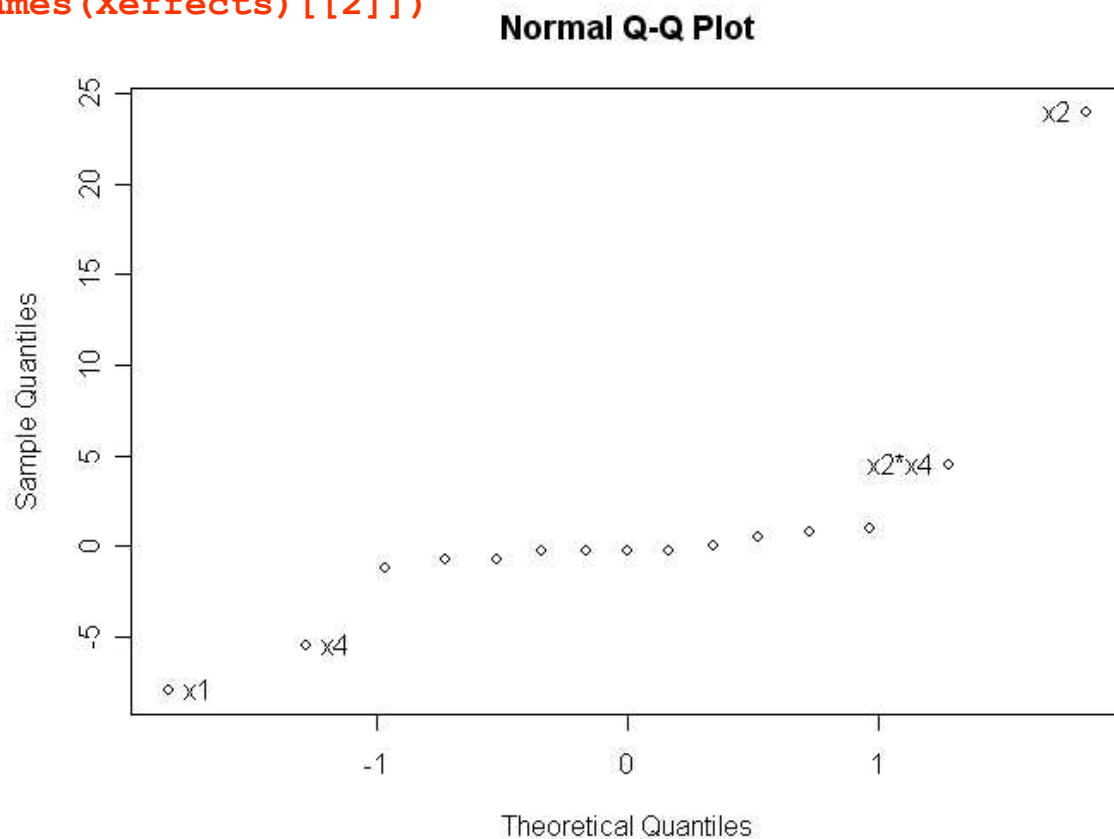
> # The "significant" design effects relative to the higher
> # order interactions as a reference set are clear. 31

```

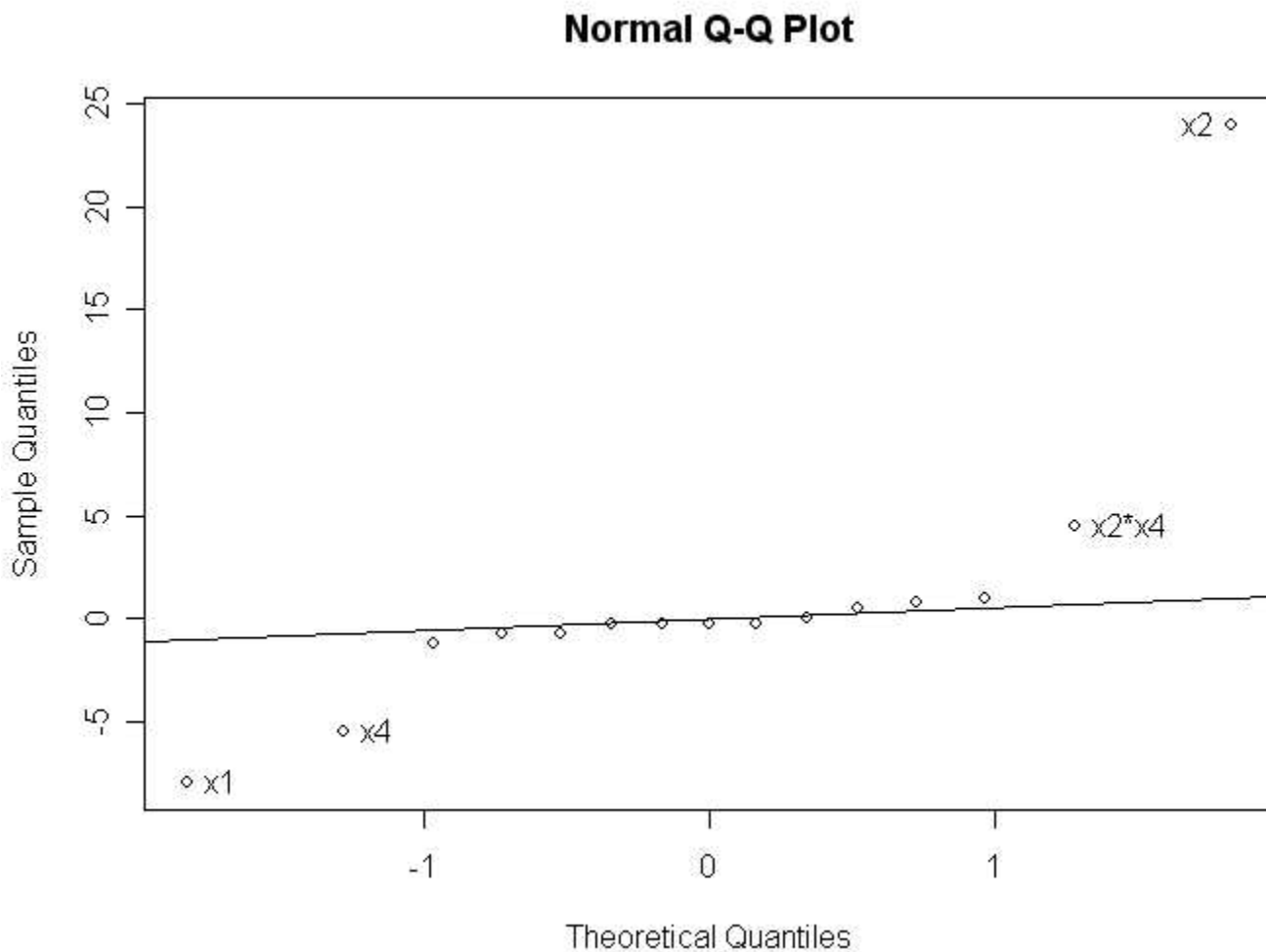
```

> # Two problems arise in the assessment of effects from unreplicated
> # factorials:
> # (a) occasionally meaningful high-order interactions do occur,
> # (b) it is necessary to allow for selection.
> # Daniel (1959) suggested "normal probability" (or, effectively, QQ) plots.
> # Idea: if none of the effects are "real", the estimated effects, which all
> # have the same std error, should look like a sample from a normal distr.
> # There will always be a largest computed effect, so the question is:
> # Are the largest (smallest) effects bigger (smaller) than expected for a
> # normal distribution?
> temp <- qqnorm(Xeffects)
> identify(temp$x, temp$y, dimnames(Xeffects)[[2]])
[1] 1 2 4 9
>

```

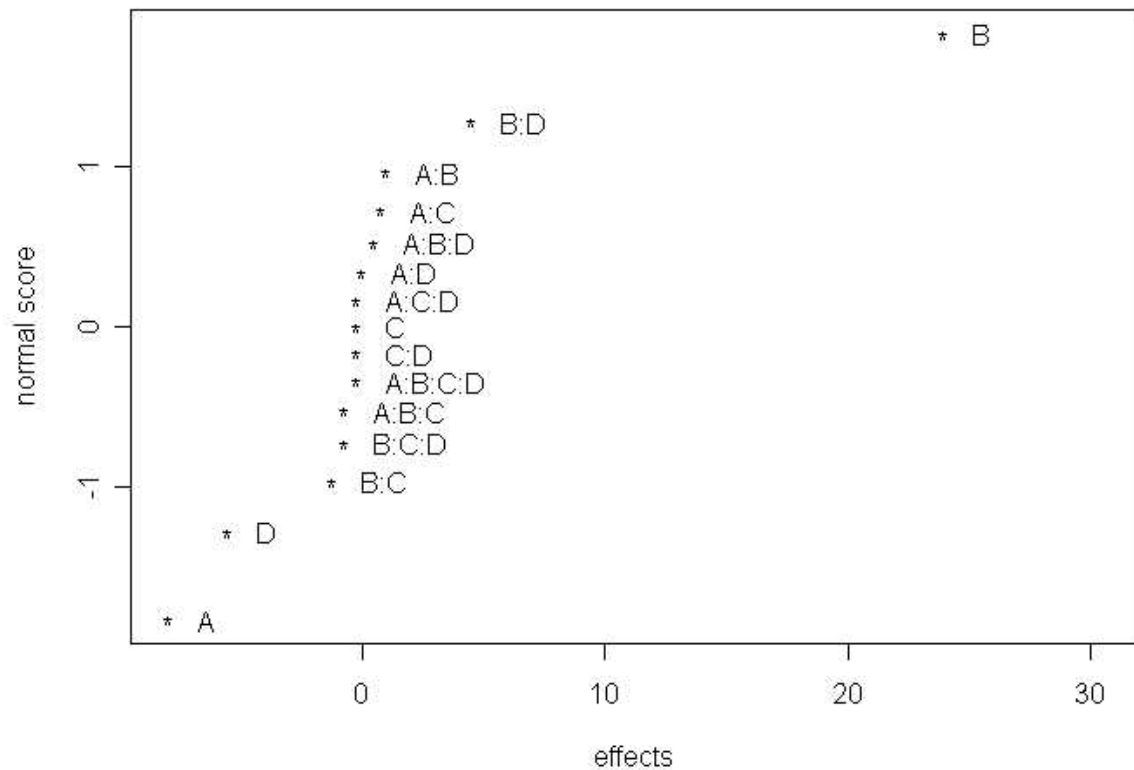



```
> # If we were correct in assessing the standard error of the effects from the  
> # higher order interactions, as above, then the a line with slop SEeffect  
> # should characterize the appropriate std dev (slope of the qqplot)  
> # for the majority of the effects.  
> abline(0,.55)
```



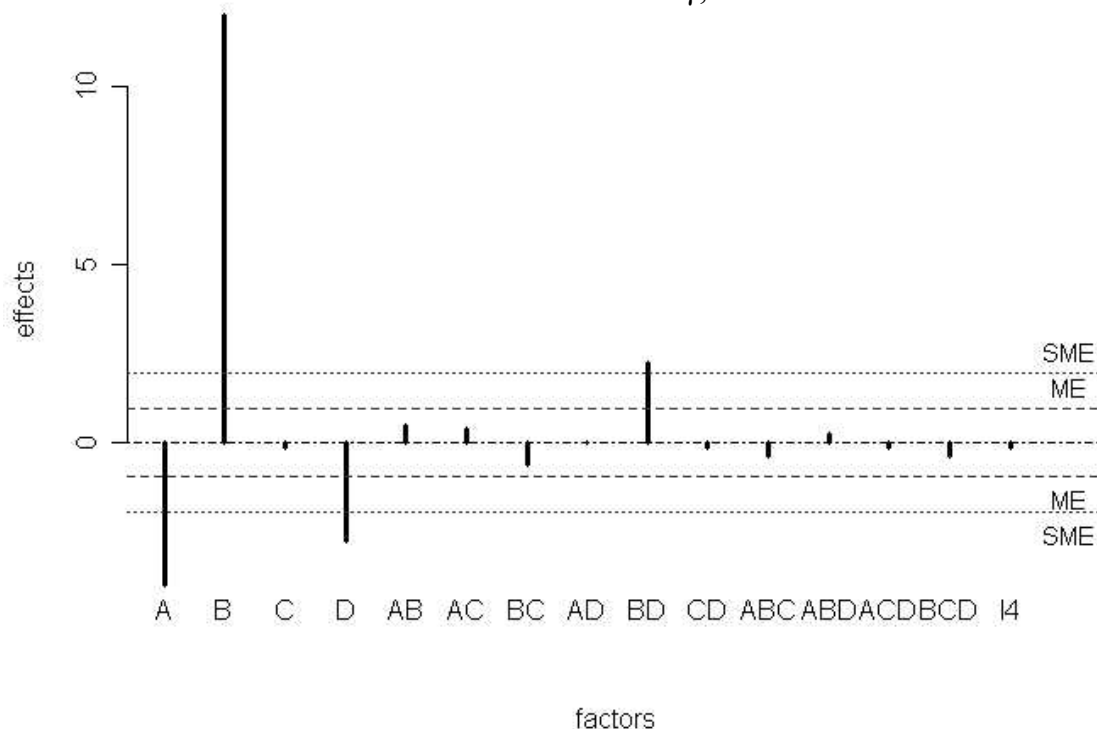
```
> # Or try the DanielPlot function in the BHH2 library
> # Ref: C. Daniel (1976). Application of Statistics to
> # Industrial Experimentation. Wiley.
```

```
> attach(tab5.10.dat)
> options(contrasts=c("contr.sum", "contr.poly"))
> A <- as.factor(-X[,1])
> B <- as.factor(-X[,2])
> C <- as.factor(-X[,3])
> D <- as.factor(-X[,4])
> lm.conversion <- lm( conversion ~ A*B*C*D )
> DanielPlot(lm.conversion)
>
```



Lenth plots

- Lenth (1989) defined an alternative (“robust”) procedure that identifies “significant” effects.
- m is median of k effects.
- *pseudo s.e* is $s_0 = 1.5m$. Exclude effects exceeding $2.5s_0$ and recompute m and s_0 .
- *Margin of error*, $ME = t_{0.975,d} \times s_0$, $d=k/3$ (approx 95% CI).
- *Simultaneous margin of error*, $SME = t_{\gamma,d} \times s_0$, $\gamma=(1+0.95^{1/k})/2$.

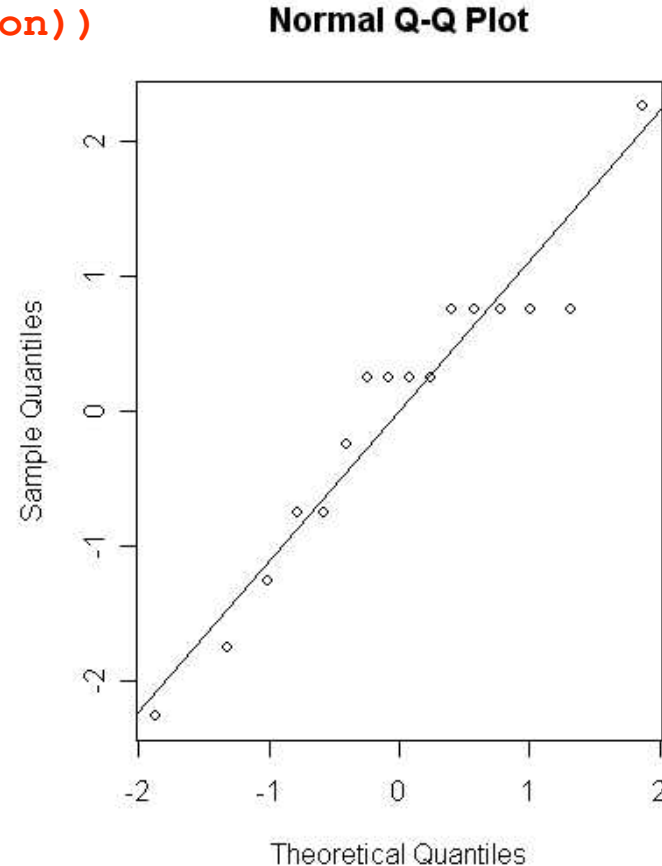
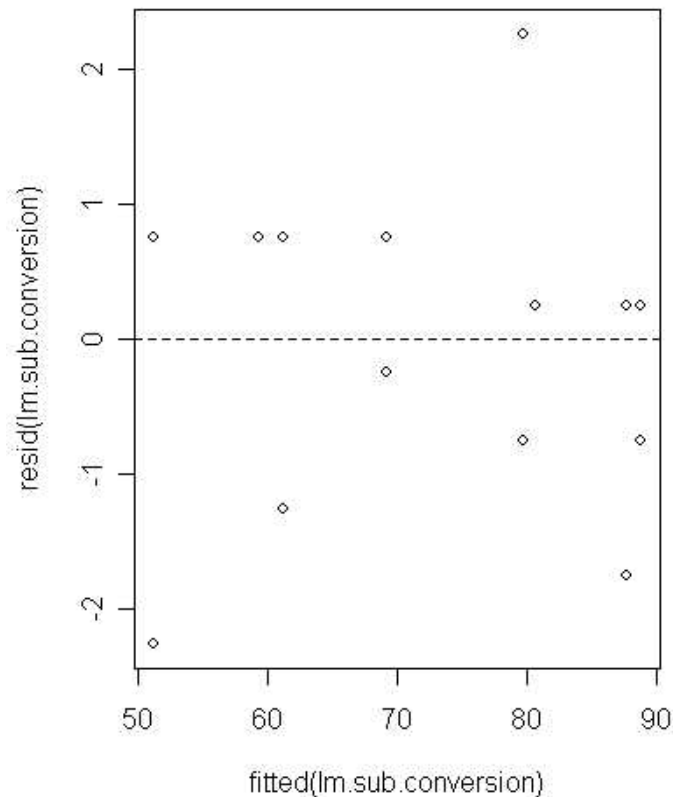


```

> # Diagnostic plotting of residuals
> # Fit without identified "significant" effects

> lm.sub.conversion <- lm(conversion ~
    des4$Xa[,c("x1","x2","x4","x2*x4")])
> par(mfrow=c(1,2))
> plot(fitted(lm.sub.conversion), resid(lm.sub.conversion))
> abline(h=0,lty=2)
> qqnorm(resid(lm.sub.conversion))
> qqline(resid(lm.sub.conversion))

```



Blocking the 2^k factorial design

- May be interested in a 2^3 design, but batches of raw material (or periods of time) only large enough to make 4 runs.
- Define blocks so that all runs in which 3-factor interaction “123” is minus are in one block and all other runs in the other block.
- Note: due if all observations in 2nd block were increased by some value d , this would affect only the 123 interaction; because of orthogonality it would *sum out* in the calculation of the main and 2-way effects: 1, 2, 3, 12, 13, 23. *Systematic differences* between blocks are eliminated from main effects and 2-factor interactions.
- Think of block as a 4th factor. We are considering a half fraction of a 2^4 design for all 4 factors.

| Run | 1 | 2 | 3 | 12 | 13 | 23 | 123 | Block | | 1 | 2 | 3 | Run |
|-----|---|---|---|----|----|----|-----|-------|----------|---|---|---|-----|
| 1 | - | - | - | + | + | + | - | I | Block I | - | - | - | 1 |
| 2 | + | - | - | - | - | + | + | II | | + | + | - | 4 |
| 3 | - | + | - | - | + | - | + | II | | + | - | + | 6 |
| 4 | + | + | - | + | - | - | - | I | | - | + | + | 7 |
| 5 | - | - | + | + | - | - | + | II | Block II | + | - | - | 2 |
| 6 | + | - | + | - | + | - | - | I | | - | + | - | 3 |
| 7 | - | + | + | - | - | + | - | I | | - | - | + | 5 |
| 8 | + | + | + | + | + | + | + | II | | + | + | + | 8 |

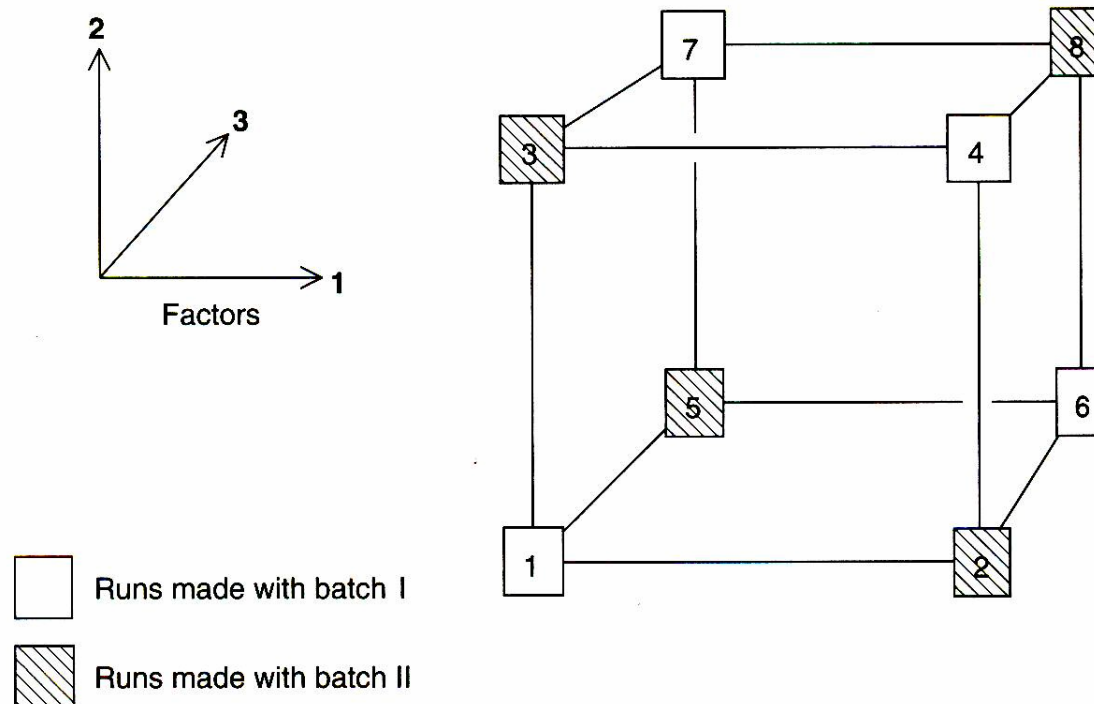


Figure 5.16. Arranging a 2^3 factorial design in two blocks of size 4.

Blocks of size 2

- Want to conduct experiment in blocks of size 2 so as to do no damage to estimates of main effects.
- Define 4 blocks of size 2 by the combinations of two blocking factors, which we may call 4 and 5.
- For example, we might start with “4” = “123”, as before, and confound some other expendible 2-factor interaction with the other, say “5” = “23”

Table 5.14. (a) An Undesirable Arrangement: A 2^3 Design in Blocks of Size 2
(b) Allocation to Blocks (Variables 4 & 5)

| Run Number | Experimental Variable | | | Block Variable | | | Experiment Arranged in Four Blocks | | | | |
|---------------|--------------------------|---|---|-------------------|--------|--------|---------------------------------------|---|---|---|-----|
| | 1 | 2 | 3 | 4 = 123 | 5 = 23 | 45 = 1 | Block | 1 | 2 | 3 | Run |
| (a) | | | | | | | | | | | |
| 1 | — | — | — | — | + | — | I | + | + | — | 4 |
| 2 | + | — | — | + | + | + | | + | — | + | 6 |
| 3 | — | + | — | + | — | — | II | — | + | — | 3 |
| 4 | + | + | — | — | — | + | | — | — | + | 5 |
| 5 | — | — | + | + | — | — | III | — | — | — | 1 |
| 6 | + | — | + | — | — | + | | — | + | + | 7 |
| 7 | — | + | + | — | + | — | IV | + | — | — | 2 |
| 8 | + | + | + | + | + | + | | + | + | + | 8 |

(b)

| | | Runs | |
|------------|---|------------|-----|
| Variable 5 | + | 1,7 | 2,8 |
| | — | 4,6 | 3,5 |
| | | — | + |
| | | Variable 4 | |

Generators and defining relations

- We write **I** for the vector of 1's, and the product of any design column with itself is **I=11=22=33=44=55**
- Take the two specifications for the blocking variables, **4=123** and **5=23**. Multiply 1st expression by **4** and 2nd by **5**: **I=1234** and **I=235**. These are called the *generators* of the blocking arrangements.
- Multiply these two together and to get **1223345=145** to complete the *defining relation* **I=1234=235=145**.
- The third generator shows that the main effect **1** is confounded with the **45** block effect, which we don't want.
- Better: confound the two block variables **4** and **5** with any two of the 2-factor interactions, say **4=12**, **5=13**

Table 5.15. A 2^3 Design in Blocks of Size 2, a Good Arrangement

| Run Number | Experimental Variable | | | Block Variable | | Experiment Arranged in Four Blocks | | | | |
|---------------|--------------------------|---|---|-------------------|--------|---------------------------------------|---|---|---|-----|
| | 1 | 2 | 3 | 4 = 12 | 5 = 13 | Block | 1 | 2 | 3 | Run |
| 1 | — | — | — | + | + | I | + | — | — | 2 |
| 2 | + | — | — | — | — | | — | + | + | 7 |
| 3 | — | + | — | — | + | | | | | |
| 4 | + | + | — | + | — | II | — | + | — | 3 |
| 5 | — | — | + | + | — | | + | — | + | 6 |
| 6 | + | — | + | — | + | III | | | | |
| 7 | — | + | + | — | — | | + | + | — | 4 |
| 8 | + | + | + | + | + | | — | — | + | 5 |
| | | | | | | IV | | | | |
| | | | | | | | — | — | — | 1 |
| | | | | | | | + | + | + | 8 |

5.17. LEARNING BY DOING

Fractional Factorial Designs

- Chapter 6 of BHH (2nd ed) discusses fractional factorial designs.
- Example: full 2^5 factorial would require 32 runs. An experiment with only 8 runs is a $1/4^{\text{th}}$ (quarter) fraction. Because $1/4 = (1/2)^2 = 2^{-2}$, this is referred to as a 2^{5-2} design.
- In general, 2^{k-p} design is a $(1/2)^p$ fraction of a 2^k design using 2^{k-p} runs.
- Note that the first blocked design we considered was a half fraction: 2^{4-1} defined by the generating relation **I=1234**, which provides all the confounded (“aliased”) relationships. E.g. **1=1I=11234=234**.