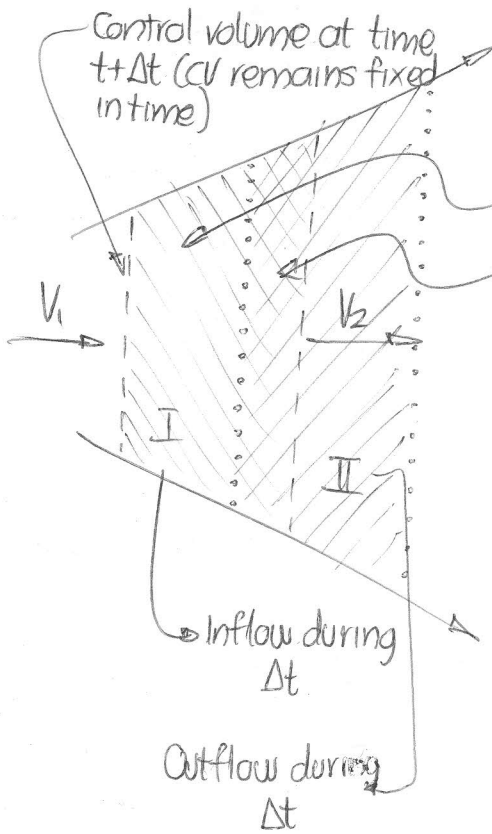


THE REYNOLDS TRANSPORT THEOREM



System (material volume) and control volume at time t

System at time $t + \Delta t$

$B \rightarrow$ any extensive property

$b = B/m \rightarrow$ corresponding intensive property

$\dot{B} \rightarrow$ flow rate

$$B_{sys,t} = B_{cv,t}$$

$$B_{sys,t+\Delta t} = B_{cv,t+\Delta t} - B_{I,t+\Delta t} + B_{II,t+\Delta t}$$

$$\frac{\Delta B_{sys}}{\Delta t} = \frac{B_{sys,t+\Delta t} - B_{sys,t}}{\Delta t}$$

$$= \frac{B_{cv,t+\Delta t} - B_{I,t+\Delta t} + B_{II,t+\Delta t} - B_{cv,t}}{\Delta t}$$

$$= \frac{B_{cv,t+\Delta t} - B_{cv,t}}{\Delta t} - \frac{B_{I,t+\Delta t}}{\Delta t} + \frac{B_{II,t+\Delta t}}{\Delta t}$$

$$\frac{dB_{sys}}{dt} = \lim_{\Delta t \rightarrow 0} \frac{\Delta B_{sys}}{\Delta t} = \frac{dB_{cv}}{dt} - \dot{B}_{in} + \dot{B}_{out}$$

$$B_{I,t+\Delta t} = b_1 m_{I,t+\Delta t} = b_1 \rho_1 V_{I,t+\Delta t} = b_1 \rho_1 V_1 \Delta t A_1$$

$$B_{II,t+\Delta t} = b_2 m_{II,t+\Delta t} = b_2 \rho_2 V_{II,t+\Delta t} = b_2 \rho_2 V_2 \Delta t A_2$$

$$\dot{B}_{in} = \dot{B}_I = \lim_{\Delta t \rightarrow 0} \frac{B_{I,t+\Delta t}}{\Delta t} = \lim_{\Delta t \rightarrow 0} \frac{b_1 \rho_1 V_1 \Delta t A_1}{\Delta t} = b_1 \rho_1 V_1 A_1$$

$$\dot{B}_{out} = \dot{B}_{II} = \lim_{\Delta t \rightarrow 0} \frac{B_{II,t+\Delta t}}{\Delta t} = \lim_{\Delta t \rightarrow 0} \frac{b_2 \rho_2 V_2 \Delta t A_2}{\Delta t} = b_2 \rho_2 V_2 A_2$$

$$\therefore \frac{dB_{sys}}{dt} = \frac{dB_{cv}}{dt} - b_1 \rho_1 V_1 A_1 + b_2 \rho_2 V_2 A_2$$

if velocities are normal to the areas

$$\dot{B}_{\text{net}} = \dot{B}_{\text{out}} - \dot{B}_{\text{in}} = \int_{\text{cs}} \rho b \vec{V} \cdot \vec{n} dA \quad (\text{inflow if negative})$$

$$\dot{B}_{\text{cv}} = \int_{\text{cv}} \rho b dV$$

$$\therefore \frac{d\dot{B}_{\text{sys}}}{dt} = \frac{d}{dt} \int_{\text{cv}} \rho b dV + \int_{\text{cs}} \rho b \vec{V} \cdot \vec{n} dA //$$

if CV is not moving or deforming with time

$$\frac{d\dot{B}_{\text{sys}}}{dt} = \int_{\text{cv}} \frac{\partial}{\partial t} (\rho b) dV + \int_{\text{cs}} \rho b \vec{V} \cdot \vec{n} dA //$$

CONSERVATION OF MASS

$$\beta = m$$

$$b = m/m = 1$$

$$\left(\frac{dm}{dt}\right)_{\text{sys}} = 0$$

Using RTT

$$0 = \frac{d}{dt} \left(\int_{\text{cv}} \rho dV \right) + \int_{\text{cs}} \rho (\vec{V} \cdot \vec{n}) dA$$

$$\int_{\text{cv}} \frac{\partial \rho}{\partial t} dV + \int_{\text{cs}} \rho (\vec{V} \cdot \vec{n}) dA = 0 //$$

$$\int_{\text{cv}} \frac{\partial \rho}{\partial t} dV + \sum_i (\rho_i A_i V_i)_{\text{out}} - \sum_i (\rho_i A_i V_i)_{\text{in}} = 0 //$$

THE LINEAR MOMENTUM EQUATION

$$\vec{B} = m\vec{V}$$

$$\vec{b} = m\vec{V}/m = \vec{V}$$

Using RIT

$$\frac{d}{dt}(m\vec{V})_{\text{sys}} = \sum \vec{F} = \frac{d}{dt} \left(\int_{\text{cv}} \vec{T} \rho dV \right) + \int_{\text{cs}} \vec{T} \rho (\vec{V} \cdot \vec{n}) dA$$

$$\sum \vec{F} = \frac{d}{dt} \left(\int_{\text{cv}} \vec{T} \rho dV \right) + \sum (\dot{m}_i \vec{V}_i)_{\text{out}} - \sum (\dot{m}_i \vec{V}_i)_{\text{in}}$$

THE ENERGY EQUATION

$$\dot{Q} - \dot{W} = \frac{dE}{dt}$$

$\dot{Q} \rightarrow \text{heat}$
 $\dot{W} \rightarrow \text{work}$

$$B = E$$

$$b = \frac{E}{m} = e$$

Using RIT

$$\frac{dQ}{dt} - \frac{dW}{dt} = \frac{dE}{dt} = \frac{d}{dt} \left(\int_{cv} e \rho dV \right) + \int_{cs} e \rho (\vec{V} \cdot \vec{n}) dA$$

$$e = e_{\text{internal}} + e_{\text{kinetic}} + e_{\text{potential}} + e_{\text{other}}$$

$$e = \hat{u} + \frac{1}{2} V^2 + gz$$

$$\dot{W} = \dot{W}_{\text{shaft}} + \dot{W}_{\text{press}} + \dot{W}_{\text{viscous stresses}} = \dot{W}_s + \dot{W}_p + \dot{W}_v$$

$$d\dot{W}_p = -(p dA) V_{n, \text{in}} = -p (-\vec{V} \cdot \vec{n}) dA$$

↑
because it goes in

$$\dot{W}_p = \int_{cs} p (\vec{V} \cdot \vec{n}) dA //$$

$$d\dot{W}_v = -\vec{\tau} \cdot \vec{V} dA$$

$\vec{\tau} \rightarrow \text{stress vector}$

$$\dot{W}_v = - \int_{cs} \vec{\tau} \cdot \vec{V} dA //$$

$$\dot{W} = \dot{W}_s + \int_{cs} p (\vec{V} \cdot \vec{n}) dA - \int_{cs} (\vec{\tau} \cdot \vec{V})_{ss} dA$$

$$\dot{Q} - \dot{W}_s - \int_{cs} p (\vec{V} \cdot \vec{n}) dA - \dot{W}_v = \frac{d}{dt} \left(\int_{cv} e \rho dV \right) + \int_{cs} e \rho (\vec{V} \cdot \vec{n}) dA$$

$$\dot{Q} - \dot{W}_s - \dot{W}_v = \frac{d}{dt} \left(\int_{cv} e \rho dV \right) + \int_{cs} e \rho (\vec{V} \cdot \vec{n}) dA + \int_{cs} p (\vec{V} \cdot \vec{n}) dA$$

$$\dot{Q} - \dot{W}_s - \dot{W}_v = \int_{cv} \frac{\partial}{\partial t} (e \rho) dV + \int_{cs} (e + p) \rho (\vec{V} \cdot \vec{n}) dA //$$