# Q4001 Thermodynamics of Materials Midterm Exam. Part I

Antonio Osamu Katagiri Tanaka - A01212611@itesm.mx

```
In [1]: from IPython.display import display, Image
display(Image(filename='./img/part1_directions.jpg'));
display(Image(filename='./img/1_0.jpg'));
display(Image(filename='./img/1_1.jpg'));
display(Image(filename='./img/1_2.jpg'));
display(Image(filename='./img/1_3.jpg'));
```

### Q4001 Thermodynamics of Materials Midterm Exam. Part I

Please turn in the exam Tuesday, october 8th, before 6:00pm.

- 1. An ideal gas is originally confined to a volume  $V_1$  in an insulated container of volume  $V_1 + V_2$ . The remainder of the container is evacuated. The partition is then removed and the gas expands to fill the entire container. If the initial temperature of the gas was T, what is the final temperature? What is the change in entropy? Justify your answer.
- 2. Demonstrate the following thermodynamic relations:

(a) 
$$\left(\frac{\partial T}{\partial P}\right)_S = \frac{\alpha V T}{C_P}$$

(b) 
$$\left(\frac{\partial T}{\partial P}\right)_{H} = -\frac{V}{C_{P}}\left(1 - \alpha T\right)$$

(c) 
$$\left(\frac{\partial H}{\partial S}\right)_{V} = T\left[1 + \frac{\alpha V}{\kappa_{T}C_{V}}\right]$$

3. A certain system is found to have a Gibbs free energy given by

$$\overline{G} = RT \ln \left[ \frac{aP}{(RT)^{5/2}} \right]$$

where a and R are constants. Find the specific heat at constant pressure,  $\overline{C}_P$ .

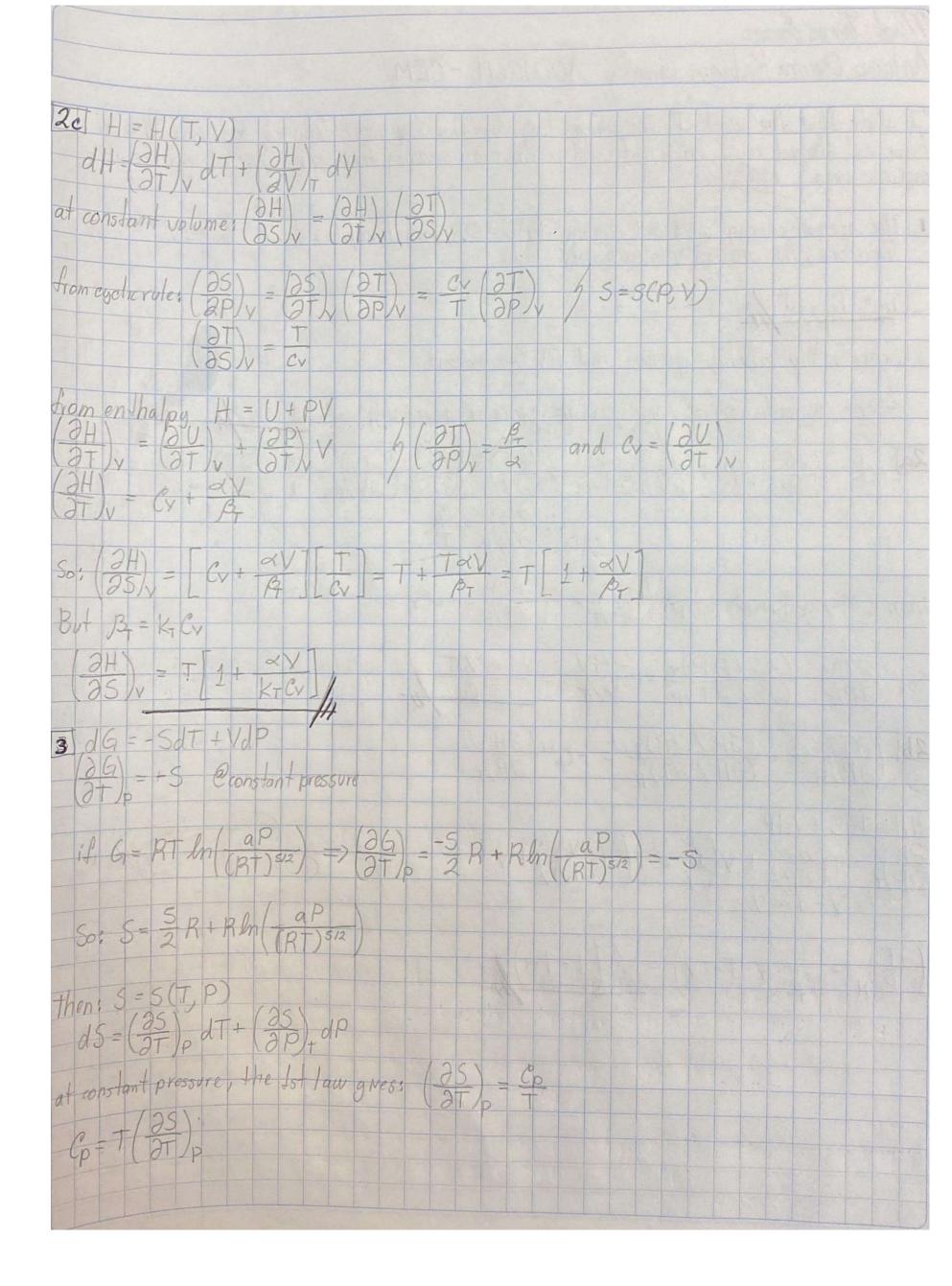
4. For a system whose internal energy is given by:

$$U = k \frac{S^3}{V}$$

where k is a constant.

- (a) What are the units of k?
- (b) Find the equation of the adiabats in the P vs. V plane.
- (c) Find the derived expressions for P and T.
- (d) Write the equation of state for the system in terms of P, V and T.
- 5. The heat of melting of ice at 1 atm and  $0^{\circ}$ C is  $6.01 \,\mathrm{kJ/mol}$ . The density of ice under these conditions is  $0.917 \,\mathrm{g/cm^3}$  and the density of water is  $0.9998 \,\mathrm{g/cm^3}$ . If 1 mole of ice is melted under these conditions, what will be
  - (a) the work done?
  - (b) the change in internal energy?
  - (c) the change in entropy?

Mid-Term Eyam
Antonio Osamo Katagiri Tanaka A01212611 - CEM "I state that the work I am submitting for this exam is solely my own and that I have not shared it. I have not used morm of non coming from any uncited source in my answers" May. 1 The internal energy does not change (DU=0), which implies that DT=0.
Therefore, the process is adiabatical. Since it's adiabatic, q=0 and  $PV^{p}=constant$ 4> no degradation of energy occurs, since it's reversible : 15 = 0/1 2a ds = (35) dP + (35) dV 125) (25) (2T) = CD (2T) From a Maxwell relationship (25) = (21) = So: (at) = (as/aP)+ = - <V = 2b (aT) = (aH/aP) = -6-1 (aH) aP)  $\frac{dH = TdS + VdP}{\left(\frac{\partial H}{\partial P}\right) = \frac{1}{3}\left(\frac{\partial S}{\partial P}\right) + V\left(\frac{1}{3}\right) = T\left(\frac{\partial V}{\partial T}\right) + V$   $= V - T\alpha V$ 



25	) =	R 3											V										14		131		BT.		I.
: 6	P	1/R.	5	) =	52	R	1														SIL								
		(3	K.I		7	1	/#		A				4.0							NA Ba									
0=	11 =	V	1							1																			
U=(	20 at	d	T+	12	1)	C	V	+	(2)	2)																			
ų -		(JK	1/3	(0)	///	n			0	(1)	BT		S			J		V											
	7 3	m	3	K-01	11/5		13	3	1		a.	5	Y	is	m	m	per 3	r K	elvi										
k	-unit	8 2	J	m 3		K	3 n	1	4		013		U	in	V	sule	es.												12
27 (	1= 1	53	1	w	Hre	0	1=1	100	M		X													T.					
nG	Ta	KS	3 /																										
nB	T -	KS	3	for	an	de	al o	05		4	P	V:	n)	RT	5	C	y =	1	R		5	CK		R	C				
PI	2=	KS	3								MX	A						1	0	10		-6	0 =	1	-2				The second
P	= (	1-2	) K	S3	/																		9						1
	V	<3		-	1																Yes								
U=			1		no						10	<b>Y</b>	(										Au						1
1-2	- 2	10	Cp		2	3	WI	n	Cp	= -	1-0												) \ .						
100	-	X (-	1-38	7 3 7 3	1																								
7	= <u>K</u>	N 1	-2	3	T 3	100	N.		Ų U				2)	2 \	A					13			axi			A			1
RV -g)	Kn	3 R3	73	3 -	#		=	>	F	2 =	n's	1-	8) R2		3	A		31				1	1/1	ei	40	(8)	WE		-
=	V		12	7/				100	B	131		101	1820				101						121			170	633		
+	m21	22 K	y3	111	1		13	Au		V							1113				10				3	1		M	1
						10	1				D		as	16		3	10	110	N	A.	No.	Y	(33)				- 1		-

46 The adiabats of the ideal gas is PV = constant	
50, from P and V from [4e]  [1-8) k53] V(1-8)2 138 = constant 1  [1] 12	
4d dU = da + dw dU = TdS - PdV dU = TdS - (1-8)KS3 dV /	400
5au the work is defined by $\frac{18.015}{w = PdV}$ $\frac{18.015}{0.999890m^3}$ $\frac{18.015}{0.9179/cm^3}$ $\frac{10.0012}{0.9012}$ $\frac{18.015}{0.9179/cm^3}$	.015
$5c$ $q = 6.01$ kJ $\rightarrow$ as 1+3 the heat of melting. $AS = \frac{q}{7} = \frac{6.01}{0.00} = \frac{32.002}{1.00} = \frac{3}{1.00} = \frac{3}{1$	
5b $\Lambda U = q - w = 6.01 \text{ KJ} - (-0.165)$ $\Delta U = 6010.16 \text{ J/p}$	
References:  Stolen, S., Grande, T., & Neil L., A. (2004). Chemical Them Macroscopic and Microscopic Aspects. (J. W. & S. Inc., Ed.  B. Gaskell, D., & E. Laughlin, D. (2018). Introduction to Jh. Materials. (C. Piress Ed.). Taylor & Framois Group	noclynamics of Materials - 1) John Wiley & Sons Utd
Materials. (C. Press Ed.). laylor & Frameis Group  [3] Mortimer G., R. (2013) Mathematics for Physical Chemistry. ( ad.) Amsterdam: British Library Catologuing in Publication Da	

## **Q4001 Thermodynamics of Materials Midterm Exam. Part II**

### Antonio Osamu Katagiri Tanaka - A01212611@itesm.mx

"I state that the work I am submitting for this exam is solely my own and that I have not shared it. I have not used information coming from any uncited source in my answers."

### Q4001 Thermodynamics of Materials Midterm Exam. Part II

October, 2019

Please turn in the exam Tuesday, october 9th, before 4:00pm.

6. The state equation of a new material is

$$P = \frac{aT^3}{V}$$

where a is a constant. The internal energy of the matter is

$$U = BT^n \ln \frac{V}{V_o} + f(T)$$

where B, n and  $V_o$  are all constants, f(T) only depends on the temperature. Find B and n.

7. The molar entropy of an gas is given by

$$\overline{S} = \frac{1}{2} \left[ \sigma + 5R \ln \overline{U} + 2R \ln \overline{V} \right]$$

- (a) Find  $\overline{C}_V$  and  $\overline{C}_P$ .
- (b) Find  $\alpha$  and  $\kappa_T$ .
- 8. A paramagnetic system in an uniform magnetic field  $\mathcal{H}$  is thermally insulated from the surroundings. It has an induced magnetization  $M = a\mathcal{H}/T$  and a heat capacity  $C_{\mathcal{H}} = b/T^2$  at constant  $\mathcal{H}$ , where a and b are constants and T is the temperature. How will the temperature of the system change when  $\mathcal{H}$  is quasi-statically reduced to zero? In order to have the final temperature change by a factor of 2 from the initial temperature, how strong should be the initial  $\mathcal{H}$ ?
- 9. Demonstrate that

$$\overline{C}_P - \overline{C}_V = \left[ P + \left( \frac{\partial U}{\partial V} \right)_T \right] \left( \frac{\partial V}{\partial T} \right)_P \quad \text{and that} \quad P + \left( \frac{\partial U}{\partial V} \right)_T = T \left( \frac{\partial P}{\partial T} \right)_V$$

and calculate  $\overline{C}_P - \overline{C}_V$  for a van der Waals gas. Compare how much these values differ for He and  $CO_2$  at  $T = 200 \,\mathrm{K}$  and  $\overline{V} = 0.2 \,\mathrm{L} \,\mathrm{mol}^{-1}$ .

gas	$a/\mathrm{atm}\mathrm{L}^2\mathrm{mol}^{-2}$	$b/{ m L}{ m mol}^{-1}$
Не	0.0346	0.0238
$CO_2$	3.64	0.0427

- 10. A thermally conducting, uniform and homogeneous bar of length L, cross section A, density  $\rho$  and specific heat at constant pressure  $c_P$  is brought to a nonuniform temperature distribution by contact at one end with a hot reservoir at a temperature  $T_h$  and at the other end with a cold reservoir at a temperature  $T_c$ . The bar is removed from the reservoirs, thermally insulated and kept at constant pressure.
  - (a) Determine the final temperature of the bar.
  - (b) Show that the change in entropy of the bar is

$$\Delta S = c_P \rho A L \left[ 1 + \ln T_f + \frac{T_c}{T_h - T_c} \ln T_c - \frac{T_h}{T_h - T_c} \ln T_h \right]$$

#### Q 6

The 1st law gives,

$$egin{aligned} dU &= TdS - PdV \ dS &= rac{dU + PdV}{T} \ dS &= rac{dU}{T} + rac{PdV}{T} \ dS &= \left[rac{1}{T} \left(rac{\partial U}{\partial V}
ight)_T + rac{P}{T}
ight] dV + rac{1}{T} \left(rac{\partial U}{\partial T}
ight)_V dT \end{aligned}$$

$$\left(rac{\partial U}{\partial V}
ight)_T = rac{BT^n}{V} ext{ and } \left(rac{\partial U}{\partial T}
ight)_V = f'(T) + BnT^{n-1}ln\left(rac{V}{V_0}
ight)$$

So,

$$dS = \left[\frac{1}{T}\frac{BT^{n}}{V} + \frac{\frac{aT^{3}}{V}}{T}\right]dV + \frac{1}{T}\left[f'(T) + BnT^{n-1}ln\left(\frac{V}{V_{0}}\right)\right]dT$$

$$dS = \frac{BT^{n-1} + aT^{2}}{V}dV + \left[\frac{f'(T)}{T} + nBT^{n-2}ln\left(\frac{V}{V_{0}}\right)\right]dT$$

$$\frac{\partial}{\partial T}\left(\frac{BT^{n-1} + aT^{2}}{V}\right) = \frac{\partial}{\partial V}\left(\frac{f'(T)}{T} + nBT^{n-2}ln\left(\frac{V}{V_{0}}\right)\right)$$

$$\frac{2aT + B(n-1)T^{n-2}}{V} = \frac{BnT^{n-2}}{V}$$

$$2aT = BbT^{n-2} - B(n-1)T^{n-2}$$

$$2aT = BT^{n-2}$$

$$B = 2aT^{3-n}$$

[1] Lim, Y.-K. (2019). Problems and Solutions on Thermodynamics and Statistical Mechanics. Journal of Chemical Information and Modeling, 53(9), 1689–1699. https://doi.org/10.1017/CBO9781107415324.004

### Q 7

@ constant volume

$$dU = TdS - PdV \ \left(rac{\partial S}{\partial U}
ight)_V = rac{1}{T}$$

From:

$$S = rac{1}{2}[\sigma + 5RlnU + 2RlnV] \ \left(rac{\partial S}{\partial U}
ight)_V = rac{5R}{2U} \ U = rac{5}{2}RT$$

From the  $c_{v}$  definition,

$$c_v = \left(rac{\partial U}{\partial T}
ight)_V = rac{\partial}{\partial T}rac{5}{2}RT = rac{5R}{2}$$

From the  $c_p$  definition,

$$c_p = c_v + R = rac{5R}{2} + R = rac{7R}{2}$$

From Problem 9,

$$c_p - c_v = \left(rac{\partial V}{dT}
ight)_P \left[\left(rac{\partial U}{\partial V}
ight)_T + P
ight]$$

with:

$$egin{aligned} lpha &= rac{1}{v}igg(rac{\partial V}{\partial T}igg)_P \ P &= -igg(rac{\partial A}{\partial V}igg)_T \ c_p - c_v &= lpha V\left[igg(rac{\partial U}{\partial V}igg)_T - igg(rac{\partial A}{\partial V}igg)_T
ight] \end{aligned}$$

$$\begin{split} A &= U - TS \\ \left(\frac{\partial A}{\partial V}\right)_T &= \left(\frac{\partial U}{\partial V}\right)_T - T \left(\frac{\partial S}{\partial V}\right)_T \\ - \left(\frac{\partial A}{\partial V}\right)_T &= - \left(\frac{\partial U}{\partial V}\right)_T + T \left(\frac{\partial S}{\partial V}\right)_T \end{split}$$

$$c_p - c_v = lpha V \left[ T igg( rac{\partial S}{\partial V} igg)_T 
ight] = T lpha V igg( rac{\partial P}{\partial T} igg)_V$$

$$\left(\frac{\partial P}{\partial T}\right)_V = -\left(\frac{\partial P}{\partial V}\right)_T \left(\frac{\partial V}{\partial T}\right)_P$$

$$egin{aligned} c_p - c_v &= Tlpha V \left[ -\left(rac{\partial P}{\partial V}
ight)_T \left(rac{\partial V}{\partial T}
ight)_P 
ight] \ c_p - c_v &= \left(Tlpha V
ight) \left(rac{1}{Vk_T}
ight) \left(Vlpha
ight) \ c_p - c_v &= rac{VTlpha^2}{k_T} \ rac{lpha}{k_T} &= rac{R}{TVlpha} \end{aligned}$$

Since

$$rac{lpha}{k_T} = rac{R}{V} = rac{R}{TVlpha}$$

$$\alpha = \frac{1}{T}$$

$$k_T = rac{VTlpha^2}{c_p - c_v} \ k_T = rac{VTlpha^2}{R}$$

$$k_T = rac{V}{RT}$$

[1] Lim, Y.-K. (2019). Problems and Solutions on Thermodynamics and Statistical Mechanics. Journal of Chemical Information and Modeling, 53(9), 1689–1699. https://doi.org/10.1017/CBO9781107415324.004

[2] R. Gaskell, D., & E. Laughlin, D. (2018). Introcuction to the Thermodynamics of Materials. (C. Press, Ed.). Taylor & Francis Group.

Q 8

dU = TdS + HdM

gives:

 $\left(\frac{\partial T}{\partial M}\right)_S = \left(\frac{\partial H}{\partial S}\right)_M$ 

From a Maxwell relation:

 $\left(rac{\partial T}{\partial S}
ight)_H \left(rac{\partial M}{\partial H}
ight)_H = -1$ 

Also:

 $c_H = T igg(rac{\partial S}{\partial T}igg)_H \ igg(rac{\partial T}{\partial S}igg)_H = rac{T}{c_H}$ 

Recall:

$$M = rac{aH}{T} \ \left(rac{\partial M}{\partial T}
ight)_H = -rac{aH}{T^2}$$

$$\begin{split} \left(\frac{\partial T}{\partial H}\right)_S &= \left(\frac{\partial T}{\partial S}\right) \left(\frac{\partial S}{\partial H}\right) = \left(\frac{\partial H}{\partial S}\right) \left(\frac{\partial T}{\partial H}\right) \cdot \left(\frac{\partial H}{\partial T}\right) \left(\frac{\partial M}{\partial H}\right) \cdot \left(\frac{\partial T}{\partial S}\right) \left(\frac{\partial M}{\partial H}\right) \\ & \left(\frac{\partial T}{\partial H}\right)_S = \left(\frac{\partial T}{\partial S}\right)_H \left(\frac{\partial M}{\partial T}\right)_H (-1) \\ & \left(\frac{\partial T}{\partial H}\right)_S = -\frac{T}{c_H} \frac{aH}{T^2} \\ & \left(\frac{\partial T}{\partial H}\right)_S = \frac{aTH}{b} \end{split}$$

$$\int rac{aHT}{b}\,dH = rac{aH^2T}{2b} = ln\left(rac{T}{T_f}
ight)$$

$$T=T_f\left(e^{rac{aH^2T}{2b}}
ight)$$

T approaches  $T_f$  when H approaches 0. If

$$T_f = \frac{T_i}{2}$$

Then

$$H_i = \left(rac{2b}{a}ln(2)
ight)^{rac{1}{2}}$$

[1] Lim, Y.-K. (2019). Problems and Solutions on Thermodynamics and Statistical Mechanics. Journal of Chemical Information and Modeling, 53(9), 1689–1699. https://doi.org/10.1017/CBO9781107415324.004

[3] R.L., C. (1986). Thermodynamics, Magnetoche(Springer), 3-4. Retrieved from https://link.springer.com/chapter/10.1007%2F978-3-642-70733-9\_3

#### Q 9

Let's demonstrate:  $ar{C_P} - ar{C_V} = \left[P + \left(rac{\partial U}{\partial V}
ight)_T
ight]\left(rac{\partial V}{\partial T}
ight)_P$ 

For a constant volume process (w=0), the 1st Law gives:

$$dU = \delta q_v$$

From the definition of enthalpy:

@ constant pressure:

$$dH = dU + PdV + VdP$$
  $dH = dU + PdV$   $dH = \delta q_p$ 

From the definition of  $c_v$  and  $c_p$  ,

$$egin{aligned} c_v &= \left(rac{\delta q}{dT}
ight)_v = \left(rac{\partial U}{dT}
ight)_v ext{, as } dU = c_v dT \ c_p &= \left(rac{\delta q}{dT}
ight)_p = \left(rac{\partial H}{dT}
ight)_p ext{, as } dH = c_p dT \end{aligned}$$

If the process is carried out at constant volume, all the thermal energy is used to raise the temperature of the system.

If the process is carried out at constant pressure, some thermal energy is used to raise the temperature of the system and some is used to provide the work required to expand the system.

$$\frac{PdV}{dT} = P\left(\frac{\partial V}{\partial T}\right)_p$$
 is the work of expansion

So, it's expected  $c_p$  to be greater than  $c_v$ . Therefore:

$$c_p - c_v = Pigg(rac{\partial V}{\partial T}igg)_p$$

From the definition of enthalpy:

$$H = U + PV$$
  $dH = dU + PdV + VdP$   $dH = dU + PdV$  @ constant pressure  $\left( \frac{\partial H}{dT} \right)_p = \left( \frac{\partial U}{dT} \right)_p + P \left( \frac{\partial V}{dT} \right)_p$ 

So:

And:

$$c_p = \left(rac{\partial H}{dT}
ight)_p = \left(rac{\partial U}{dT}
ight)_p + Pigg(rac{\partial V}{dT}igg)_p$$
 $c_v = igg(rac{\partial U}{dT}igg)_v$ 

For any gas

$$c_p - c_v = \left(rac{\partial U}{dT}
ight)_n + Pigg(rac{\partial V}{dT}igg)_n - \left(rac{\partial U}{dT}
ight)_v$$

$$U = U(V,T)$$
 $dU = \left(\frac{\partial U}{\partial V}\right)_T dV + \left(\frac{\partial U}{\partial T}\right)_V dT$ 
 $\left(\frac{\partial U}{\partial T}\right)_P = \left(\frac{\partial U}{\partial V}\right)_T \left(\frac{\partial V}{\partial T}\right)_P + \left(\frac{\partial U}{\partial T}\right)_V (1)$ 

So,

$$c_p - c_v = \left(rac{\partial U}{\partial V}
ight)_T \left(rac{\partial V}{\partial T}
ight)_P + \left(rac{\partial U}{\partial T}
ight)_V + Pigg(rac{\partial V}{dT}igg)_P - \left(rac{\partial U}{dT}
ight)_V \ c_p - c_v = \left(rac{\partial U}{\partial V}
ight)_T \left(rac{\partial V}{\partial T}
ight)_P + Pigg(rac{\partial V}{dT}
ight)_P$$

$$c_p - c_v = \left(rac{\partial V}{dT}
ight)_P \left[\left(rac{\partial U}{\partial V}
ight)_T + P
ight]$$

Let's demonstrate:  $P + \left(rac{\partial U}{\partial V}
ight)_T = T \left(rac{\partial P}{\partial T}
ight)_V$ 

For one mole in a closed system:

$$dU = TdS - PdV$$
  $\left(rac{\partial U}{\partial V}
ight)_T = T\left(rac{\partial S}{\partial V}
ight)_T - P(1)$  using the Maxwell relation:  $\left(rac{\partial S}{\partial V}
ight)_T = \left(rac{\partial P}{\partial T}
ight)_V$   $\left(rac{\partial U}{\partial V}
ight)_T = T\left(rac{\partial P}{\partial T}
ight)_V - P$ 

$$\left(\frac{\partial U}{\partial V}\right)_T + P = T \left(\frac{\partial P}{\partial T}\right)_V$$

Let's calculate  $ar{C_P} - ar{C_V}$  for a van der Waals gas.

$$dS = \left(rac{\partial S}{\partial T}
ight)_V dT + \left(rac{\partial S}{\partial V}
ight)_T dV$$

Differentiate with respect to T (P constant)

$$\left(\frac{\partial S}{\partial T}\right)_P = \left(\frac{\partial S}{\partial T}\right)_V + \left(\frac{\partial S}{\partial V}\right)_T \left(\frac{\partial V}{\partial T}\right)_P$$

From the definitios of the heat capacities:

$$c_v = T \left( rac{\partial S}{\partial T} 
ight)_V ext{ and } c_p = T \left( rac{\partial S}{\partial T} 
ight)_P \ rac{c_p - c_v}{T} = \left( rac{\partial S}{\partial T} 
ight)_P - \left( rac{\partial S}{\partial T} 
ight)_V \ rac{c_p - c_v}{T} = \left( rac{\partial S}{\partial T} 
ight)_V + \left( rac{\partial S}{\partial V} 
ight)_T \left( rac{\partial V}{\partial T} 
ight)_P - \left( rac{\partial S}{\partial T} 
ight)_V \ rac{c_p - c_v}{T} = \left( rac{\partial S}{\partial V} 
ight)_T \left( rac{\partial V}{\partial T} 
ight)_P \end{aligned}$$

Maxwell relationship:

$$\left(\frac{\partial S}{\partial V}\right)_T = \left(\frac{\partial P}{\partial T}\right)_V$$

The Cycle Rule:

$$\begin{split} &\left(\frac{\partial P}{\partial T}\right)_{V} \left(\frac{\partial T}{\partial V}\right)_{P} \left(\frac{\partial V}{\partial P}\right)_{T} = -1 \\ &\left(\frac{\partial V}{\partial T}\right)_{P} = -\left(\frac{\partial P}{\partial T}\right)_{V} \left(\frac{\partial V}{\partial P}\right)_{T} \end{split}$$

So:

$$egin{aligned} rac{c_p - c_v}{T} &= \left(rac{\partial P}{\partial T}
ight)_V \left[-\left(rac{\partial P}{\partial T}
ight)_V \left(rac{\partial V}{\partial P}
ight)_T
ight] \ c_p - c_v &= -Trac{\left(rac{\partial P}{\partial T}
ight)_V}{\left(rac{\partial P}{\partial V}
ight)_T} \end{aligned}$$

For a van der Waals gas,

$$P = \frac{RT}{V - b} - \frac{a^2}{V^2}$$

$$\left(\frac{\partial P}{\partial T}\right)_V = \frac{R}{V - b} \text{ and } \left(\frac{\partial P}{\partial V}\right)_T = \frac{2a^2}{V^3} - \frac{RT}{(V - b)^2}$$

Thus,

$$c_p-c_v=-Trac{\left(rac{R}{V-b}
ight)^2}{rac{2a^2}{V^3}-rac{RT}{\left(V-b
ight)^2}}$$

$$c_p - c_v = rac{R^2 T V^3}{-2 a^2 (V-b)^2 + R T V^3}$$

Let's compare  $c_p-c_v$  for He and  $CO_2$ 

```
In [1]: def Cp_min_Cv(T, V, R, a, b):
            numer = (R^{**2})^*T^*(V^{**3});
            denom = -2*(a**2)*(V - b)**2 + R*T*(V**3);
            return numer / denom;
        # constants
        T = 200; \#K
        V = 0.2; \#L/mol
        R = 0.082057; #L atm/K mol
        # for He
        a = 0.0346; #atm L^2/mol^2
        b = 0.0238; \#L/mol
        He_Cp_min_Cv = Cp_min_Cv(T, V, R, a, b)
        # for CO2
        a = 3.64; #atm L^2/mol^2
        b = 0.0427; #L/mol
        CO2\_Cp\_min\_Cv = Cp\_min\_Cv(T, V, R, a, b)
        print("gas Cp_min_Cv")
        print("----")
        print("{} {:>5.3f} {}".format("He ", He_Cp_min_Cv, "L atm/K mol"))
        print("{} {:>5.3f} {}".format("CO2", CO2_Cp_min_Cv, "L atm/K mol"))
            Cp_min_Cv
        gas
        He
              0.082 L atm/K mol
```

```
The values differ by 0.082-(-0.021)=0.103rac{Latm}{Kmol}
```

[1] R. Gaskell, D., & E. Laughlin, D. (2018). Introcuction to the Thermodynamics of Materials. (C. Press, Ed.). Taylor & Francis Group.
[2] Berberan-santos, M. N. (2008). The van der Waals equation: analytical and approximate solutions, 43(4), 1437–1457. https://doi.org/10.1007/s10910-

Q 10

007-9272-4

$$\frac{T_H-T_C}{L} \mbox{ is the bar temperature gradient}$$
 
$$T_x=T_C+\frac{(T_H-T_C)x}{L} \mbox{ is the temperature at the cross section at distance x}$$

Since the process is isobaric ans adiabatic,

C02

-0.021 L atm/K mol

$$egin{split} \int_{0}^{L}
ho c_{p}\left[T_{C}+rac{(T_{H}-T_{C})x}{L}-T_{f}
ight]\,dx &=0 \ rac{1}{2}L
ho c_{p}T_{C}-L
ho c_{p}T_{f}+rac{1}{2}L
ho c_{p}T_{H} &=0 \ rac{1}{2}T_{C}-T_{f}+rac{1}{2}T_{H} &=0 \end{split}$$

$$T_f = rac{T_H + T_C}{2}$$

Let's calculate the change in entropy

$$\Delta S = c_p 
ho A \int_0^L \, dx \int_{T_x}^{T_f} rac{dT}{T} \ \Delta S = c_p 
ho A L \left[ ln \left( rac{T_H + T_C}{2} 
ight) - ln \left( T_C + rac{(T_H - T_C)x}{L} 
ight) 
ight]$$

$$\Delta S = c_p 
ho AL \left[ 1 + ln \left( rac{T_H + T_C}{2} 
ight) + rac{T_C}{T_H - T_C} ln(T_C) - rac{T_H}{T_H - T_C} ln(T_H) 
ight]$$

[1] Lim, Y.-K. (2019). Problems and Solutions on Thermodynamics and Statistical Mechanics. Journal of Chemical Information and Modeling, 53(9), 1689–1699. https://doi.org/10.1017/CBO9781107415324.004

```
In [ ]:
```

