# CS1 Week 4 Empty

Time response, Stability





## Recap Last week



### Quiz 1

Which properties do linear systems need to fulfil?

- A. Linearity
- **B.** Superposition
- **C.** Homogeneity
- **D.** Additivity



### Quiz 2

#### Classify the following system

$$x_1(t) = \sin(t) - 5$$

$$x_2(t) = \cos(t)$$

$$y(t) = u(t) \left( x_1^2(t) + t \cdot x_2^2(t) \right)$$

A. Linear

**C.** Time invariant

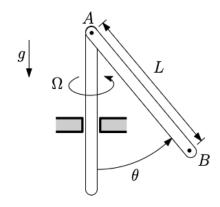
**B.** Static

**D.** Causal

Box 1: Questions 4, 5, 6, 7

You are given the mechanical system depicted below with the following equation of motion:

$$\frac{1}{3} \ddot{\theta}(t) - \frac{1}{3} \Omega^2 \sin(\theta(t)) \cos(\theta(t)) + \frac{g}{2L} \sin(\theta(t)) = 0. \label{eq:theta_def}$$



Question 4 Choose the correct answer. (1 Point)

Which of the following is the correct state representation of the above system?

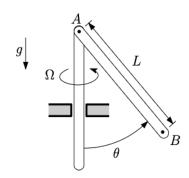
$$\begin{split} & \boxed{\mathbf{A}} \ \, \dot{x}(t) = \begin{bmatrix} x_2(t) \\ \frac{1}{3}\Omega^2 \sin x_1(t) \cos x_1(t) + \frac{3g}{2L} \sin x_1(t) \end{bmatrix} \ \, \boxed{\mathbf{C}} \ \, \dot{x}(t) = \begin{bmatrix} x_2(t) \\ \Omega^2 \sin x_1(t) \cos x_1(t) - \frac{3g}{2L} \sin x_1(t) \end{bmatrix} \\ & \boxed{\mathbf{B}} \ \, \dot{x}(t) = \begin{bmatrix} x_2(t) \\ \frac{1}{3}\Omega^2 \sin x_1(t) \cos x_1(t) - \frac{g}{2L} \sin x_1(t) \end{bmatrix} \ \, \boxed{\mathbf{D}} \ \, \dot{x}(t) = \begin{bmatrix} x_1(t) \\ \Omega^2 \sin x_1(t) \cos x_1(t) - \frac{3g}{2L} \sin x_1(t) \end{bmatrix} \end{split}$$



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$$\dot{x}(t) = \begin{bmatrix} x_2(t) \\ \Omega^2 \sin x_1(t) \cos x_1(t) - \frac{3g}{2L} \sin x_1(t) \end{bmatrix}$$

**Question 5** Mark all correct statements. (2 Points) Which of the following points  $x_e$  are equilibrium points of the system?

$$\underline{\mathbf{A}} \ x_e = \begin{bmatrix} \arccos\left(\frac{3g}{2\Omega^2 L}\right) + 3\pi \\ 0 \end{bmatrix}.$$

$$\boxed{\mathbf{B}} \ x_e = \begin{bmatrix} c \\ 0 \end{bmatrix}, \quad \forall c \in \mathbb{R}.$$

$$\boxed{\mathbf{C}} \ x_e = \begin{bmatrix} \arccos\left(\frac{3\Omega^2 g}{2L}\right) \\ 1 \end{bmatrix}.$$

$$\boxed{\mathbf{D}} \ x_e = \begin{bmatrix} \arccos\left(\frac{3g}{2\Omega^2L}\right) + 2\pi \\ 0 \end{bmatrix}.$$

$$\boxed{\mathbf{E}} \ x_e = \begin{bmatrix} 0 \\ 3\pi \end{bmatrix}.$$

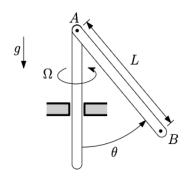
$$\boxed{\mathbf{F}} \ x_e = \begin{bmatrix} 3\pi \\ 0 \end{bmatrix}$$

$$\boxed{\mathbf{G}} \ x_e = \begin{bmatrix} 0 \\ \frac{\pi}{2} \end{bmatrix}.$$

Box 1: Questions 4, 5, 6, 7

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$$\dot{x}(t) = \begin{bmatrix} x_2(t) \\ \Omega^2 \sin x_1(t) \cos x_1(t) - \frac{3g}{2L} \sin x_1(t) \end{bmatrix}$$

Question 6 Choose the correct answer. (1 Point)

Consider the equilibrium point  $x_e = \begin{bmatrix} -5\pi \\ 0 \end{bmatrix}$ . Linearize the system. Which matrix A describes the linearized dynamics?

$$\boxed{\mathbf{A}} \ A = \begin{bmatrix} 0 & 1 \\ \Omega^2 + \frac{3g}{2L} & 0 \end{bmatrix}.$$

$$\boxed{\mathbf{B}} \ A = \begin{bmatrix} 0 & 1 \\ -\Omega^2 + \frac{3g}{2L} & 0 \end{bmatrix}.$$

C Since the given equilibrium is not stable,

a matrix A does not exist.

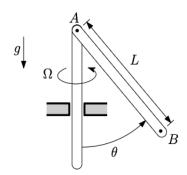
$$\boxed{\mathbb{D}} \ A = \begin{bmatrix} 1 & 0 \\ \Omega^2 - \frac{3g}{2L} & 0 \end{bmatrix}.$$

$$\boxed{\mathbf{E}} \ A = \begin{bmatrix} 0 & 1\\ \Omega^2 - \frac{3g}{2L} & 0 \end{bmatrix}.$$

Box 1: Questions 4, 5, 6, 7

You are given the mechanical system depicted below with the following equation of motion:

$$\frac{1}{3} \ddot{\theta}(t) - \frac{1}{3} \Omega^2 \sin(\theta(t)) \cos(\theta(t)) + \frac{g}{2L} \sin(\theta(t)) = 0. \label{eq:theta_def}$$



$$\dot{x}(t) = \begin{bmatrix} x_2(t) \\ \Omega^2 \sin x_1(t) \cos x_1(t) - \frac{3g}{2L} \sin x_1(t) \end{bmatrix}$$

Question 7 Mark all correct statements. (2 Points)

Which of the following statements about the system are true?

A The system is dynamic.

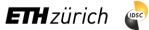
B The system is time-varying.

- C The dimension of the system is 2.
- D The dimension of the system can be 1.



### **Course Schedule**

	Subject	Week
Modeling -	Introduction, Control Architectures, Motivation	1
	Modeling, Model examples	2
	System properties, Linearization	3
Analysis -	Analysis: Time response, Stability	4
	Transfer functions 1: Definition and properties	5
	Transfer functions 2: Poles and Zeros	6
	Proportional feedback control, Root Locus	7
	Time-Domain specifications, PID control, Computer implementation	8
	Frequency response, Bode plots	9
L	The Nyquist condition, Time delays	10
Synthesis -	Frequency-domain Specifications, Dynamic Compensation, Loop Shaping	11
	Time delays, Successive loop closure, Nonlinearities	12
	Describing functions	13
	Intro to Uncertainty and Robustness	14



## Today

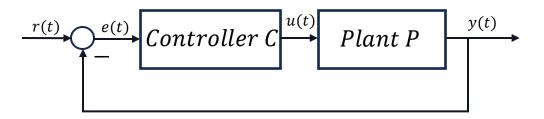
- 1. <u>Time response</u>
- 2. Stability



# 1. Time response



### **Motivation**





system modeling

Plant P

Linearization

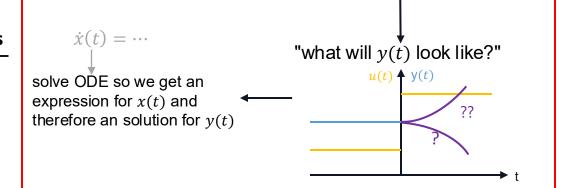
state-space representation  $\dot{x}(t) = Ax(t) + Bu(t)$ 

$$y(t) = Cx(t) + Du(t)$$

#### **Controller C**

Synthesis

- Recall modeling from week 2
- Recall linearization from week 3
- Today: Analysis
- End goal is a robust system



**Analysis** 





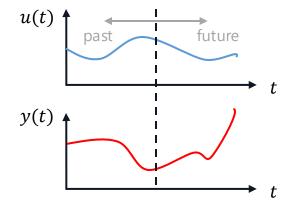
### Time response

$$u = ua + ub$$

$$\dot{x}(t) = Ax(t) + Bu(t)$$

$$y = ya + yb$$

$$y(t) = Cx(t) + Du(t)$$



- Since we deal with linearized systems, input & output can be split into two parts
- → To know the behavior of a system for all time t, we split input into
- $u = upast + ufut_{ure}$ , this is called the *time response* of a system
- Additionally, since we deal with real systems, causality holds (i.e. current output only depends on past and current inputs)
- $\rightarrow$  effects of  $u_{past}$  can be summarized by  $x(t^*)$  (state at any given time  $t^*$ )
- Usually time invariance holds  $\rightarrow$  reference time doesn't matter, we pick  $t^* = 0$
- → this leads to Initial Condition response



### **Initial and Forced Response**

 As said, since the system is linear, we take advantage of linearity and consider two separate cases:

#### **Initial-Conditions response:**

No external inputs

$$y_{IC} = u_{IC}(t) = 0, t \ge 0, x_{IC}(0) = x_0$$

#### Forced response:

due to external inputs or disturbances

$$y_F - u_F(t) = u(t), t \ge 0, x_F(0) = 0$$

After solving each case separately, we just add  $y_{\rm IC}$  and  $y_{\rm F}$  to get the complete output. This separation allows us to analyze the effects of non-zero initial conditions and non-zero inputs separately.



### Initial and Forced Response Solution

1. Initial Condition

$$x_{IC}(0) = x_0, u_{IC}(t) = 0, t \ge 0$$

2. Forced Response

$$u_F(t) = u(t), x_F(0) = 0$$

Solve

$$\dot{x}(t) = Ax$$

Solve

$$\dot{x}(t) = Ax + Bu$$

Solution:

$$x_{IC}(t) = e^{At}x_0$$

Solution:

$$x_F(t) = \int_0^t e^{A(t-\tau)} B u(\tau) d\tau$$

$$y_{IC}(t) = Ce^{At}x_0$$

initial response

feedthrough

$$y_F(t) = C \int_0^t e^{A(t-\tau)} B u(\tau) d\tau + Du(t)$$

today

$$y = y_{IC} + y_F = Ce^{At}x_0 + C\int_0^t e^{A(t-\tau)}B u(\tau)d\tau + Du$$

Time Response of an LTI system



### **Matrix Exponential**

If we take a closer look, we see that some terms contain the matrix exponential  $e^{At}$ .

But how do we compute it? Throwback to Linear Algebra II...

The matrix exponential can be defined through a Taylor-series:

$$e^{At} = \sum_{n=0}^{\infty} \frac{1}{n!} (At)^n = I + At + \frac{1}{2} (At)^2 + \dots + \frac{1}{n} (At)^n$$

For some matrices we can avoid infinitely many calculations and simplify calculations:

$$\rightarrow$$
 Diagonal:  $\exp\left(\begin{bmatrix} \lambda_1 & 0 \\ 0 & \lambda_2 \end{bmatrix} t\right) = \begin{bmatrix} \exp(\lambda_1 t) & 0 \\ 0 & \exp(\lambda_2 t) \end{bmatrix}$ 

$$\rightarrow$$
 Jordan Form:  $\exp\left(\begin{bmatrix}\lambda & 1\\ 0 & \lambda\end{bmatrix}t\right) = \begin{bmatrix}\exp(\lambda t) & t\exp(\lambda t)\\ 0 & \exp(\lambda t)\end{bmatrix}$ 

Where  $\lambda_i$  are the eigenvalues of the respective matrix





### Coordinate Transformation (LinAlg Recap)

To facilitate calculations, we can therefore do a coordinate transformation,  $x = T\tilde{x}$  such that is  $e^{At}$  easier to compute.

$$\begin{cases} \dot{x}(t) = Ax(t) + Bu(t) \\ y(t) = Cx(t) + Du(t) \end{cases} \xrightarrow{x = T\tilde{x}} \begin{cases} T\dot{\tilde{x}}(t) = AT\tilde{x}(t) + Bu(t) \\ y(t) = CT\tilde{x}(t) + Du(t) \end{cases}$$
$$\begin{cases} \dot{\tilde{x}}(t) = (T^{-1}AT)\tilde{x}(t) + (T^{-1}B)u(t) \\ y(t) = CT\tilde{x}(t) + Du(t) \end{cases}$$
$$\begin{cases} \dot{\tilde{x}}(t) = \tilde{A}\tilde{x}(t) + \tilde{B}u(t) \\ y(t) = \tilde{C}\tilde{x}(t) + \tilde{D}u(t) \end{cases}$$

For a matrix  $A \in \mathbb{R}^{n \times n}$  with n eigenvalues  $\lambda_1, ..., \lambda_n$  and n <u>linearly independent</u> eigenvectors  $v_1, ..., v_n$  one can do a coordinate transformation such that  $\tilde{A} = T^{-1}AT = diag(\lambda_1, ..., \lambda_n)$  where  $\tilde{A}$  is a diagonal matrix with the eigenvalues  $\lambda_1, ..., \lambda_n$  on the diagonal and T a transformation matrix containing the eigenvectors as  $v_1, ..., v_n$  columns.

**Note:** the time response remains <u>unchanged</u>. Through the transformation, we simple use a different realization of the system, i.e. a different state vector.



### I.C Response: Real Eigenvalues

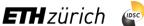
Let us know take a closer look at systems where A is diagonal. More specific we will look at the initial condition response, i.e. u(t) = 0

$$\rightarrow$$
 For a diagonal, real matrix:  $A = \begin{bmatrix} \lambda_1 & 0 \\ 0 & \lambda_2 \end{bmatrix}$ ,  $\lambda_i \in R$   $y(t) = Ce^{At}x_0$ 

where we can write out all terms and simplify for A being diagonal.

$$y(t) = \begin{bmatrix} c_1 c_2 \end{bmatrix} \begin{bmatrix} \exp(\lambda_1 t) & 0 \\ 0 & \exp(\lambda_2 t) \end{bmatrix} \begin{bmatrix} x_1(0) \\ x_2(0) \end{bmatrix}$$
$$y(t) = c_1 e^{\lambda_1 t} x_1(0) + c_2 e^{\lambda_2 t} x_2(0)$$

So for diagonal, real matrices the initial condition response is the linear combination of two t exponentials.





### I.C Response: Complex Eigenvalues

 $\rightarrow$  For a diagonal, complex matrix:  $A = \begin{bmatrix} \sigma + j\omega & 0 \\ 0 & \sigma - j\omega \end{bmatrix}$   $y(t) = CeAtx_0$ 

where we can write out all terms and simplify for A being diagonal.

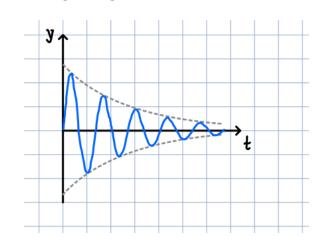
$$y = c_1 e^{\sigma t} e^{j\omega t} x_1(0) + c_2 e^{\sigma t} e^{-j\omega t} x_2(0)$$

$$= e^{\sigma t} \left( c_1 e^{j\omega t} x_1(0) + c_2 e^{-j\omega t} x_2(0) \right)$$

$$= e^{\sigma t} (\alpha_1 \sin(\omega t) + \alpha_2 \cos(\omega t))$$

$$= \alpha e^{\sigma t} \sin(\omega t + \phi)$$

- $\rightarrow$  if signal decays or not depends on  $Re(\lambda)!$
- → complex poles generate new frequencies
- → oscillations in output without any in input





### I.C Response: Repeated Eigenvalues

- If repeated eigenvalues appear (where algebraic and geometric multiplicity do not match), we cannot diagonalize the matrix
- We can still bring into Jordan form
- For a 2<sup>nd</sup> order system, the initial condition response would be:

$$y(t) = Ce^{At}x_0 = C\exp\left(\begin{bmatrix} \lambda & 1 \\ 0 & \lambda \end{bmatrix}t\right)x_0 = \begin{bmatrix} c_1 & c_2 \end{bmatrix}\begin{bmatrix} \exp(\lambda t) & t\exp(\lambda t) \\ 0 & \exp(\lambda t) \end{bmatrix}x_0 = c_1 e^{\lambda t}x_{0,1} + c_2 te^{\lambda t}x_{0,1}$$

- In general: the initial condition response is a linear combination of terms of the form  $\exp(\lambda t)$  and  $t^m \exp(\lambda t)$
- Often, repeated eigenvalues occur at  $\lambda = 0$ :

$$y(t) = c_1 x_{1,0} + c_1 t x_{1,0}$$



### Time Response Overview

• Any matrix A can be transformed into a diagonal or Jordan matrix

The response of a system will always be a linear combination of terms in the following form:

• Real eigenvalues:  $e^{\lambda_{\rm i} t}$ 

• Complex conjugate eigenvalues:  $e^{\sigma t} \sin(\omega t + \phi)$ 

• Repeated real eigenvalues:  $te^{\lambda_{\rm i}t}$ 

• The input and its derivatives: u(t),  $\dot{u}(t)$ , ...

Important takeaway:

The stability of a system can be determined by the real part of the eigenvalues of A



### Quiz

$$\delta(x-a) := \begin{cases} \infty & x = a \\ 0 & x \neq a \end{cases} \quad a \in [0, \infty) \quad \delta \notin \mathcal{H}$$
$$\int_0^\infty \delta(x-a) \, dx = 1 \qquad \int_0^\infty g(x) \delta(x-a) \, dx = g(a)$$

What is the time response of a **first order system** with  $u(t) = \delta(t)$ , d = 0,  $x_0 \neq 0$ ?

$$y = y_{IC} + y_F = Ce^{At}x_0 + C\int_0^t e^{A(t-\tau)}B u(\tau)d\tau + Du$$

**A.** 
$$y(t) = Ce^{at}x_0 - \frac{cb}{a}(1 - e^{-at})$$

C. You can't apply impulse as input

**B.** 
$$y(t) = Ce^{at}(x_0 + b)$$

D. quantum state detected

## 2. Stability



### **Stability**

We observed that the time response is linked to *exponential terms*.

$$y(t) = c_1 e^{\lambda_1 t} x_1(0) + c_2 e^{\lambda_2 t} x_2(0)$$
$$y(t) = \alpha e^{\sigma t} \sin(\omega t + \phi)$$

The growth of these terms is dictated by the real part of the eigenvalues of A. We can see that if the eigenvalues  $\lambda$  have a positive real part, the output will grow exponentially over time, i.e. become unstable.  $(y \rightarrow \infty)$ 

But what does stability really mean? There are a few ways to classify stability...



### **Stability Conditions**

A linearized, diagonalized system with A, B, C, D matrices is called

- Lyapunov stable if  $Re(\lambda_i) \leq 0 \ \forall i$
- **Asymptotically** stable if  $Re(\lambda_i) < 0 \ \forall i$
- Unstable if  $\exists Re(\lambda_i) > 0 \ \forall i$

A linearized system with non-diagonizable A matrix is called

• **Lyapunov stable** if  $Re(\lambda_i) \le 0 \ \forall i$  and there are no repeated eigenvalues with  $Re(\lambda_i) = 0$ 

For minimal LTI systems:

Asymptotic stability = BIBO stability

Bounded Input Bounded Output (BIBO) Stability: for every bounded input, the output will remain bounded



### Old Exam Question (Summer 2018)

Question 7 Choose the correct answer. (1 Point)

Consider the two systems with output signal y(t) and input signal u(t), described below

- 1.  $y(t) = \sin(t)u(t)$
- 2.  $y(t) = \int_0^t \sin(\tau) u(\tau) d\tau$

Which system is BIBO stable?

A. None

A. System 2

B. Both

**D.** System 1

## **Questions?**



## Feedback?

Too fast? Too slow? Less theory, more exercises?

I would appreciate your feedback. Please let me know.

https://docs.google.com/forms/d/e/1FAIpQLSdHl0kjWo63aNzDkAV0cnmQadCAj5L0 D7v7aSh0BK7BBdEgpA/viewform?usp=header

