

# **Fin Heat Transfer Equation**

## **Analyze and Simulation**

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# Outline



**01**

**Equation  
Analysis**

**02**

**Solidworks  
Simulation**

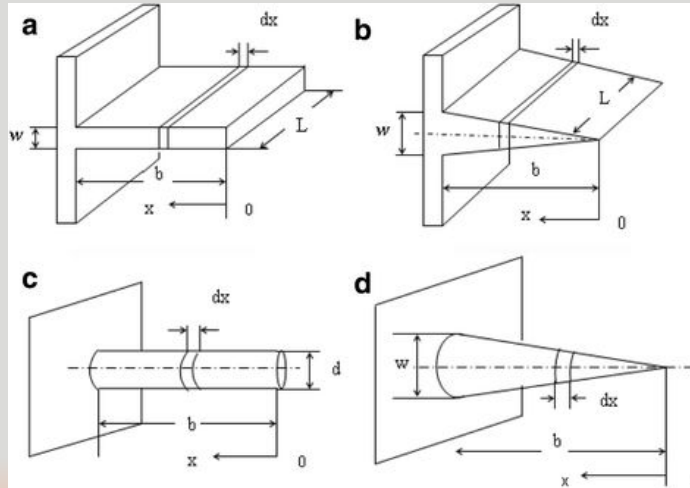
**03**

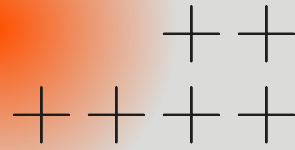
**Conclusions**



# Brief Intro

- Try to design fin in different cross areas ( $A_c$ ) and profiles ( $A_c(x)$ )
- Compare the temperature and heat flux between different shape of fins





# 01 Equation Analysis

# Equation derivation

I conservation of energy

$$q_x = q_{x+dx} + dq_{conv}$$

I convection

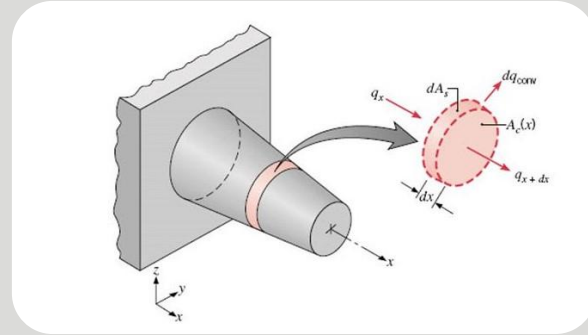
$$dq_{conv} = h dA_s (T - T_\infty) = h P dx (T - T_\infty)$$

I Fourier's Law

$$q_x = -k A_c \frac{dT}{dx}$$

$$q_{x+dx} = q_x + \frac{dq_x}{dx} dx$$

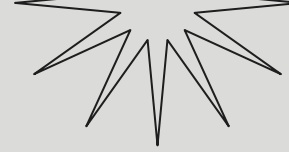
$$= -k A_c \frac{dT}{dx} - k \frac{d}{dx} \left( A_c \frac{dT}{dx} \right) dx$$



$$\frac{d}{dx} \left( A_c \frac{dT}{dx} \right) - \frac{hP}{k} (T - T_\infty) = 0$$

$$\Rightarrow \frac{d^2 T}{dx^2} + \left( \frac{1}{A_c} \frac{dA_c}{dx} \right) \frac{dT}{dx} - \frac{hP}{k A_c} (T - T_\infty) = 0$$

## Drive the general equation in state space form due to the scipy applied



The general fin equation is given by

$$\frac{d^2\theta}{dx^2} + \left(\frac{1}{A_c} \frac{dA_c}{dx}\right) \frac{d\theta}{dx} - \frac{hP}{kA_c} \theta = 0 \quad \text{where } \theta(x) \equiv T(x) - T_\infty$$

The state-space form,

$$\frac{dy}{dx} = \begin{bmatrix} y'_0 \\ y'_1 \\ y'_2 \\ y'_3 \\ y'_4 \end{bmatrix} = \begin{bmatrix} \theta' \\ \theta'' \\ A_c \\ A'_c \\ A''_c \end{bmatrix} = \begin{bmatrix} y_1 \\ -\frac{y_4}{y_3} y_1 + \frac{hP}{ky_3} y_0 \\ y_3 \\ y_4 \\ \dots \end{bmatrix}$$

$$y_0 = \theta(x)$$

$$y_1 = \theta'(x) = \frac{d\theta}{dx}$$

$$y_2 = V(x) = \int_0^x A_c dx$$

$$y_3 = A_c(x)$$

$$y_4 = A'_c(x) = \frac{dA_c}{dx}$$

where for a polygons,  $P = k\sqrt{A_c}$

# Parameter Setup

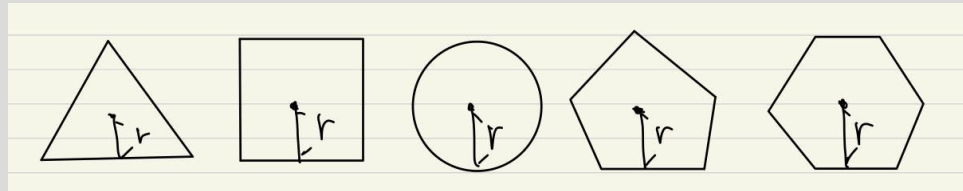
```
k: Final[float] = 3e-2      # W mm-1 K-1
h: Final[float] = 25e-6     # W mm-2 K-1 Aluminum Alloy
r: Final[float] = 5e-1      # mm
L: Final[float] = 5e0       # mm
T_b: Final[float] = 398.0   # K
T_inf: Final[float] = 298.0 # K
```

- r :  
The radius for circle area (We what to let heat sinks have **same volumes**, Ac different P)。
- k: alluminum Alloy ( 300 W/mk)
- h: natural convection air
- T(base) : 398 K
- T(surr): 298 K

# Parameter Setup

Pin Geometry condition of fin

- **Cross Section Area ( $A_c$ ):**
  - Circle
  - Equilateral Triangle
  - Square
  - Regular Pentagon
  - Regular Hexagon
- **Axial profile ( $A_c(x)$ )**
  1. Uniform :  $r = \text{constant}$
  2. Linear :  $r = r_0(1 - \frac{x}{L})$
  3. Parabolic :  $r = r_0(1 - \frac{x^2}{L^2})$
  4. Cosine :  $r = r_0 \cos(\frac{\pi x}{2L})$





# Code Implementation

## Model and solving state deriving

### State-space form

```
def deriv(self, x: np_arr_f64, y: np_arr_f64) -> np_arr_f64:
    y0, y1, _, y3, y4 = y
    return np.vstack(
        [
            y1,
            -y4 * y1 / y3
            + (self.h * self.cross_section.P(np.abs(y3))) / (self.k * y3) * y0,
            y3,
            y4,
            self.profile.d2Ac_dx2(x, y),
        ]
    )
```

### solving with scipy

```
@final
def solve(
    self,
    bc: Callable[[np_arr_f64, np_arr_f64], np_arr_f64],
) -> PPoly:
    x = np.linspace(0, self.L, 5)
    y = np.ones((5, x.size))

    self.res = scipy.integrate.solve_bvp(
        fun=self.deriv, bc=bc, x=x, y=y, max_nodes=100000
    )
    return self.res.sol
```

# Code Implementation

## Boundary Conditions

- thermal : uniform / linear
- geometry: fin volume constant / the cross section area on tip

$y_a(x=0) / y_b(x=L)$

```
def bc_linear(ya, yb):  
    return np.array(  
        [  
            # Temperature BCs  
            ya[0] - (T_b - T_inf), #  $\theta(0) = T_b - T_{inf}$   
            yb[1], #  $\theta'(L) = 0$ ; adiabatic tip  
            # Geometry BCs  
            ya[2], #  $V(0) = 0$   
            yb[2] - np.pi * r**2 * L, #  $V(L) = \pi r^2 L$   
            yb[3] - 1e-12, #  $A_c(L) = 0$ ; reduces to a point  
        ]  
    )
```

```
def bc_uniform(ya, yb):  
    return np.array(  
        [  
            # Temperature BCs  
            ya[0] - (T_b - T_inf), #  $\theta(0) = T_b - T_{inf}$   
            h * yb[0] + k * yb[1], #  $\theta'(L) = 0$ ; adiabatic tip  
            # Geometry BCs  
            ya[2], #  $V(0) = 0$   
            ya[3] - np.pi * r**2, #  $A_c(0) = \pi r^2$   
            yb[3] - np.pi * r**2, #  $A_c(L) = \pi r^2$   
        ]  
    )
```

# Code Implementation

## Cross section and Profile models

- Define the Relation between Surface Area **Ac** and **P**
- For RegularPolygon:  $P = 2\sqrt{Ac * n \tan(\frac{\pi}{n})}$

```
class CircleCrossSection(CrossSection):
    def P(self, Ac: np_arr_f64) -> np_arr_f64:
        return 2 * np.sqrt(np.pi * np.abs(Ac))

class RectangleCrossSectionMeta(type):
    def __init__(self, name: str, w: float) -> None:
        super().__init__(self)

    def __new__(cls, name: str, w: float) -> type:
        kls = super().__new__(cls, name, (), {"w": w, "P": RectangleCrossSectionMeta.P})
        return kls

    @staticmethod
    def P(self, Ac: np_arr_f64) -> np_arr_f64:
        return np.full_like(Ac, 2 * self.w)
```

```
class RegularPolygonCrossSectionMeta(type):
    def __init__(self, name: str, n: int) -> None:
        super().__init__(self)

    def __new__(cls, name: str, n: int) -> type:
        kls = super().__new__(
            cls, name, (), {"n": n, "P": RegularPolygonCrossSectionMeta.P}
        )
        return kls

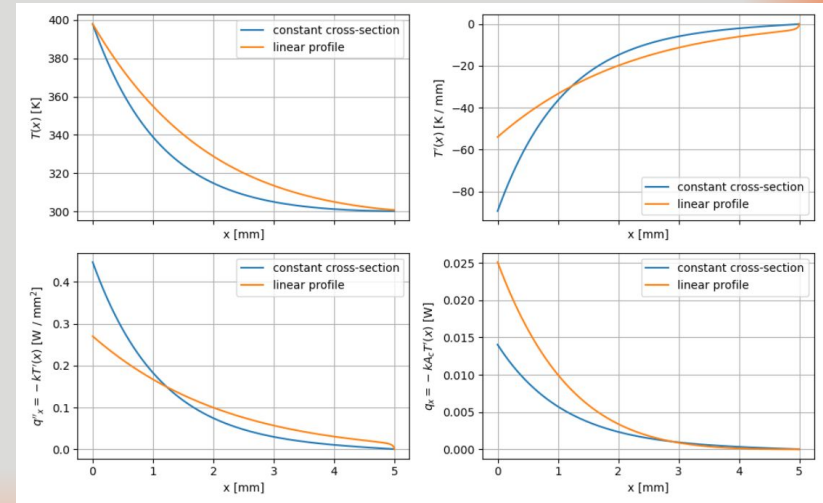
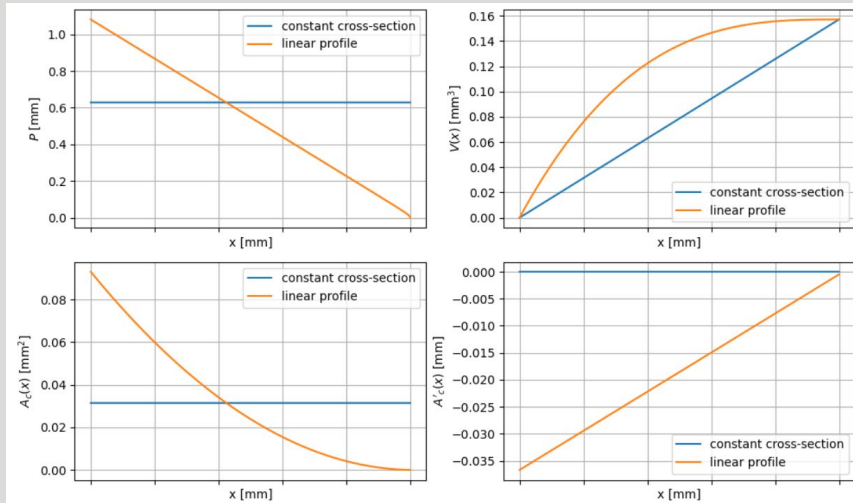
    @staticmethod
    def P(self, Ac: np_arr_f64) -> np_arr_f64:
        return 2 * np.sqrt(self.n * np.tan(np.pi / self.n) * Ac)

EquilateralTriangleCrossSection = RegularPolygonCrossSectionMeta(
    "EquilateralTriangleCrossSection", 3
)
SquareCrossSection = RegularPolygonCrossSectionMeta("SquareCrossSection", 4)
RegularPentagonCrossSection = RegularPolygonCrossSectionMeta(
    "RegularPentagonCrossSection", 5
)
RegularHexagonCrossSection = RegularPolygonCrossSectionMeta(
    "RegularHexagonCrossSection", 6
)
```

# Code Implementation

## Plotting the results

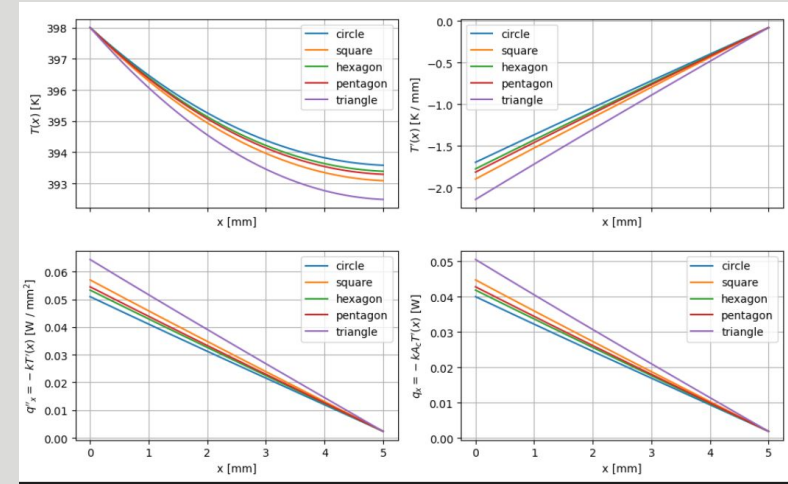
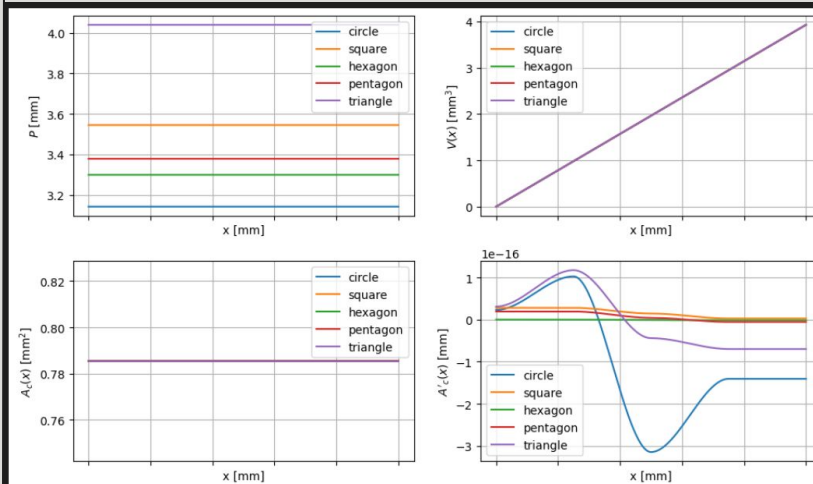
```
x_plot = np.linspace(0, L, 100001)
sol_uniform = CircularUniformPinFin(k, h, L, T_b, T_inf).solve(bc_uniform)(x_plot)
linear = CircularLinearPinFin(k, h, L, T_b, T_inf)
sol_linear = linear.solve(bc_linear)(x_plot)
```

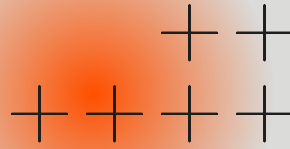


# Case Analysis

## Case1: Different cross section in uniform profile (volume constant)

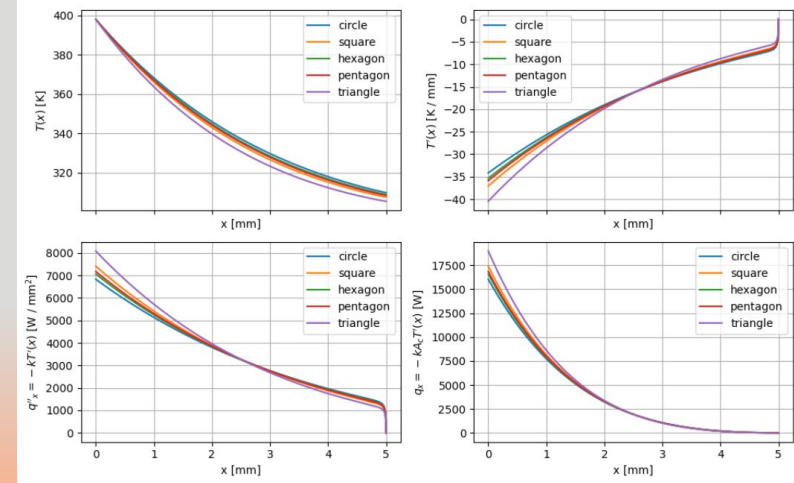
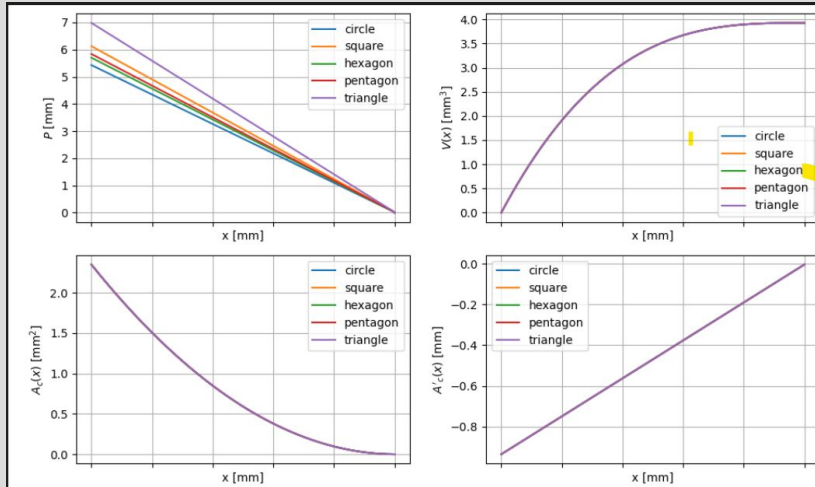
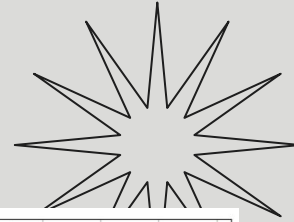
- Testing on circle, square, triangle, pentagon and hexagon cross section



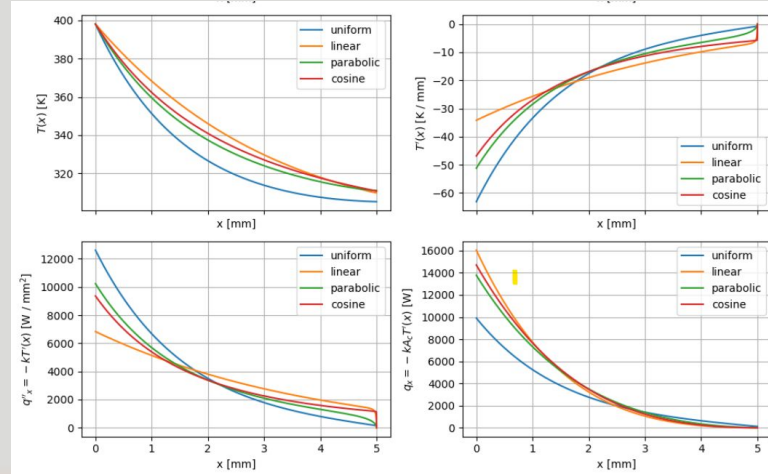


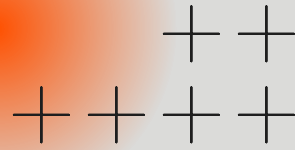
## Case2: Different cross section in linear profile (volume constant)

- Testing on circle, square, triangle, pentagon and hexagon cross section



- Testing on uniform, linear, parabolic and cosine profile





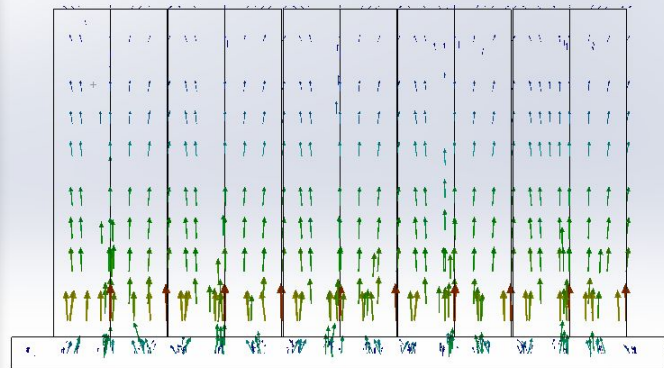
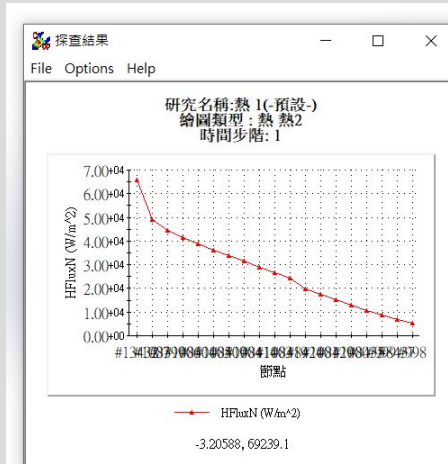
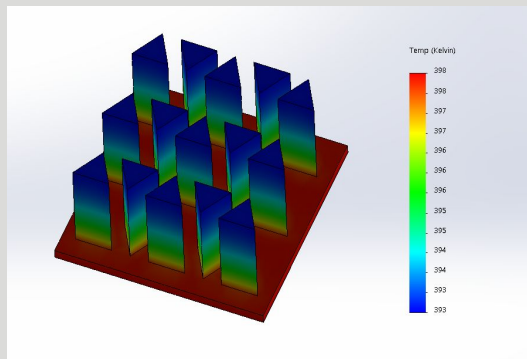
# 02 Solidworks Simulation

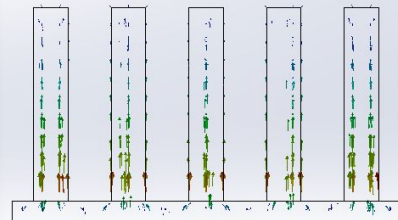




# Case: Uniform Profile simulation

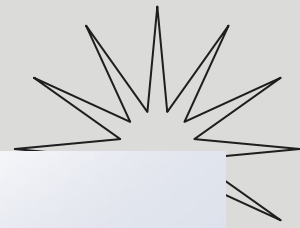
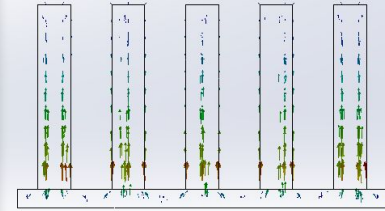
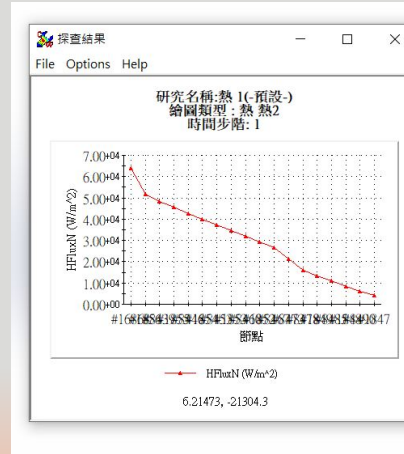
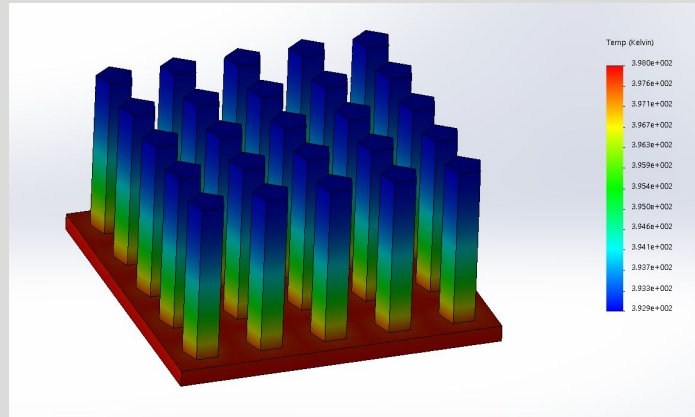
Triangular Cross section



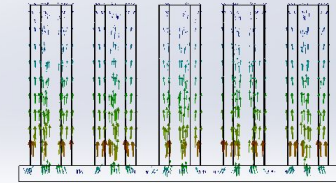
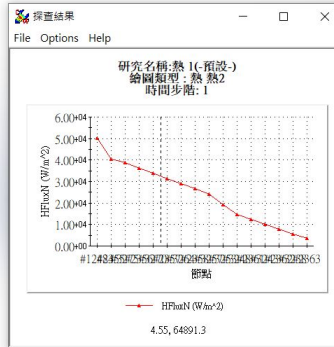
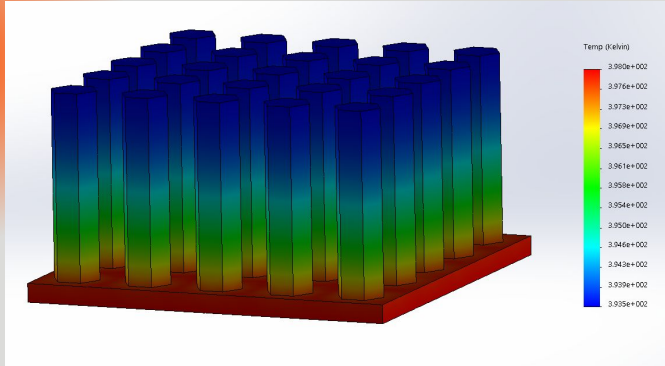




## Pengaton Cross section

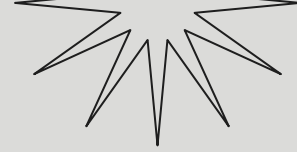


## Hexagon Cross section





# 03 Conclusion

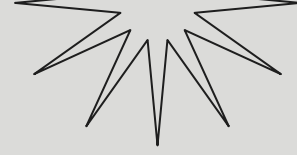


	triangle	square	circle	hexagon	pengaton
qx(w)	17620	17551	16524	16642	16742

- As the table shown above, we find that the **triangular** cross section fin perform best in linear profile and constant volume
- As x become longer, the efficiency of heat fin becomes worse

github link:

<https://github.com/dvnatanael/fin-equation-analysis/tree/david-scipy>



# Thanks

