Table 18 Output from BIGBOSOR4 corresponding to the axisymmetric nonlinear prebuckling analysis of the final optimized configuration with 15 modules and truss-like (slanted) webs subjected to Load Steps 1 and 2

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**Output contained in the greatly abridged file, try4.OUT, after execution of BIGBOSOR4 independently of the GENOPT system**

Axisymmetric equilibrium from a nonlinear static analysis (INDIC=0)

OUTPUT FROM BIGBOSOR4 FOR **LOAD STEP NO. 1** (Load Set B only, that is,

PINNER = 0 psi, PMIDDL = 60 psi, POUTER = 0 psi, DELTAT = -99.623 deg.):

PRESSURE MULTIPLIER, P= 0.000000E+00, TEMPERATURE MULTIPLIER,TEMP = 1.000000E+00

ANGULAR VELOCITY, OMEGA= 0.000000E+00

PRESTRESS STIFFNESS MATRIX CALCULATED FOR ITERATION NO. 0. START FACTORING AND SOLVING

Factoring done for iteration 0; Load step, ISTEP= 1

FACTORING AND SOLVING COMPLETED FOR PRESTRESS ITERATION NO. 0

ITERATION NO. 0 MAXIMUM DISPLACEMENT= 4.8040E+00

PRESTRESS STIFFNESS MATRIX CALCULATED FOR ITERATION NO. 1. START FACTORING AND SOLVING

Factoring done for iteration 1; Load step, ISTEP= 1

FACTORING AND SOLVING COMPLETED FOR PRESTRESS ITERATION NO. 1

ITERATION NO. 1 MAXIMUM DISPLACEMENT= 4.4950E+00

PRESTRESS STIFFNESS MATRIX CALCULATED FOR ITERATION NO. 2. START FACTORING AND SOLVING

Factoring done for iteration 2; Load step, ISTEP= 1

FACTORING AND SOLVING COMPLETED FOR PRESTRESS ITERATION NO. 2

ITERATION NO. 2 MAXIMUM DISPLACEMENT= 4.3692E+00

PRESTRESS STIFFNESS MATRIX CALCULATED FOR ITERATION NO. 3. START FACTORING AND SOLVING

Factoring done for iteration 3; Load step, ISTEP= 1

FACTORING AND SOLVING COMPLETED FOR PRESTRESS ITERATION NO. 3

ITERATION NO. 3 MAXIMUM DISPLACEMENT= 4.3409E+00

PRESTRESS STIFFNESS MATRIX CALCULATED FOR ITERATION NO. 4. START FACTORING AND SOLVING

Factoring done for iteration 4; Load step, ISTEP= 1

FACTORING AND SOLVING COMPLETED FOR PRESTRESS ITERATION NO. 4

ITERATION NO. 4 MAXIMUM DISPLACEMENT= 4.3338E+00

PRESTRESS STIFFNESS MATRIX CALCULATED FOR ITERATION NO. 5. START FACTORING AND SOLVING

Factoring done for iteration 5; Load step, ISTEP= 1

FACTORING AND SOLVING COMPLETED FOR PRESTRESS ITERATION NO. 5

ITERATION NO. 5 MAXIMUM DISPLACEMENT= 4.3338E+00

NUMBER OF NEWTON-RAPHSON ITERATIONS REQUIRED FOR CONVERGENCE = ITER = 5

OUTPUT FROM BIGBOSOR4 FOR **LOAD STEP NO. 2** (Load Sets B + A, that is,

PINNER = 0 psi, PMIDDL = 60 psi, POUTER = 15 psi, DELTAT = -99.623 deg.):

PRESSURE MULTIPLIER, P= 1.000000E+00, TEMPERATURE MULTIPLIER,TEMP = 1.000000E+00

ANGULAR VELOCITY, OMEGA= 0.000000E+00

PRESTRESS STIFFNESS MATRIX CALCULATED FOR ITERATION NO. 0. START FACTORING AND SOLVING

Factoring done for iteration 0; Load step, ISTEP= 2

FACTORING AND SOLVING COMPLETED FOR PRESTRESS ITERATION NO. 0

ITERATION NO. 0 MAXIMUM DISPLACEMENT= 5.7900E-01

PRESTRESS STIFFNESS MATRIX CALCULATED FOR ITERATION NO. 1. START FACTORING AND SOLVING

Factoring done for iteration 1; Load step, ISTEP= 2

FACTORING AND SOLVING COMPLETED FOR PRESTRESS ITERATION NO. 1

ITERATION NO. 1 MAXIMUM DISPLACEMENT= 5.6731E-01

PRESTRESS STIFFNESS MATRIX CALCULATED FOR ITERATION NO. 2. START FACTORING AND SOLVING

Factoring done for iteration 2; Load step, ISTEP= 2

FACTORING AND SOLVING COMPLETED FOR PRESTRESS ITERATION NO. 2

ITERATION NO. 2 MAXIMUM DISPLACEMENT= 5.7204E-01

PRESTRESS STIFFNESS MATRIX CALCULATED FOR ITERATION NO. 3. START FACTORING AND SOLVING

Factoring done for iteration 3; Load step, ISTEP= 2

FACTORING AND SOLVING COMPLETED FOR PRESTRESS ITERATION NO. 3

ITERATION NO. 3 MAXIMUM DISPLACEMENT= 5.7211E-01

PRESTRESS STIFFNESS MATRIX CALCULATED FOR ITERATION NO. 4. START FACTORING AND SOLVING

Factoring done for iteration 4; Load step, ISTEP= 2

FACTORING AND SOLVING COMPLETED FOR PRESTRESS ITERATION NO. 4

ITERATION NO. 4 MAXIMUM DISPLACEMENT= 5.7211E-01

NUMBER OF NEWTON-RAPHSON ITERATIONS REQUIRED FOR CONVERGENCE = ITER = 4

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