# Solfec User Manual

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# Chapter 1

# Introduction

Solfec is a computational code aimed at simulation of multi-body systems with constraints. It implements an instance of the Contact Dynamics (CD) method by Moreau [11] and Jean [7], hence the constraints are handled implicitly. One of the main goals of the software is to provide a user friendly platform for testing formulations and solution methods for the (dynamic) frictional contact problem. It is also meant to serve as a development platform for other aspects of time-stepping methods (e.g. contact detection, time integration). The code implements several kinematic models (rigid, pseudo-rigid, finite element), few contact detection algorithms, several time integrators and a couple of constraint solvers (e.g. penalty, Gauss-Seidel). A distributed memory and a serial versions of the code are available. Solfec is an open-source software and can be downloaded from http://code.google.com/p/solfec.

# **Basics**

It will be useful to introduce some basic notions here. Let us have a look at a figure below



There are four bodies in the figure. Placement of each point of every body is determined by a configuration  $\mathbf{q}_i$ . Velocity of each point of every body is determined by a velocity  $\mathbf{u}_i$ . Let  $\mathbf{q}$  and  $\mathbf{u}$  collect configurations and velocities of all bodies. If the time history of velocity is known, the configuration time history can be computed as

$$\mathbf{q}(t) = \mathbf{q}(0) + \int_{0}^{t} \mathbf{u} dt \tag{1.1}$$

The velocity is determined by integrating Newton's law

$$\mathbf{u}(t) = \mathbf{u}(0) + \mathbf{M}^{-1} \int_{0}^{t} (\mathbf{f} + \mathbf{H}^{T} \mathbf{R}) dt$$
(1.2)

where  $\mathbf{M}$  is an inertia operator (assumed constant here),  $\mathbf{f}$  is an out of balance force,  $\mathbf{H}$  is a linear operator, and  $\mathbf{R}$  collects some point forces  $\mathbf{R}_{\alpha}$ . While integrating the motion of bodies, we keep track of a number of local coordinate systems (local frames). There are four of them in the above figure. Each local frame is related to a pair of points, usually belonging to two distinct bodies. An observer embedded at a local frame calculates the local relative velocity  $\mathbf{U}_{\alpha}$  of one of the points, viewed from the perspective of the other point. Let  $\mathbf{U}$  collect all local velocities. Then, we can find a linear transformation  $\mathbf{H}$ , such that

$$\mathbf{U} = \mathbf{H}\mathbf{u} \tag{1.3}$$

In our case local frames correspond to *constraints*. We influence the local relative velocities by applying local forces  $\mathbf{R}_{\alpha}$ . This can be collectively described by an implicit relation

$$\mathbf{C}\left(\mathbf{U},\mathbf{R}\right) = \mathbf{0}\tag{1.4}$$

Hence, in order to integrate equations (1.1) and (1.2), at every instant of time we need to solve the implicit relation (1.4). Here is an example of a numerical approximation of such procedure

$$\mathbf{q}^{t+\frac{h}{2}} = \mathbf{q}^t + \frac{h}{2}\mathbf{u}^t \tag{1.5}$$

$$\mathbf{u}^{t+h} = \mathbf{u}^t + \mathbf{M}^{-1}h\mathbf{f}^{t+\frac{h}{2}} + \mathbf{M}^{-1}\mathbf{H}^T\mathbf{R}$$
(1.6)

$$\mathbf{q}^{t+h} = \mathbf{q}^{t+\frac{h}{2}} + \frac{h}{2}\mathbf{u}^{t+h} \tag{1.7}$$

where h is a discrete time step. As the time step h does not appear by  $\mathbf{M}^{-1}\mathbf{H}^{T}\mathbf{R}$ ,  $\mathbf{R}$  should now be interpreted as an impulse (an *integral* of reactions over [t, t+h]). At a start we have

$$\mathbf{q}^0$$
 and  $\mathbf{u}^0$  as prescribed initial conditions. (1.8)

The out of balance force

$$\mathbf{f}^{t+\frac{h}{2}} = \mathbf{f}\left(\mathbf{q}^{t+\frac{h}{2}}, t + \frac{h}{2}\right) \tag{1.9}$$

incorporates both internal and external forces. The symmetric and positive-definite inertia operator

$$\mathbf{M} = \mathbf{M} \left( \mathbf{q}^0 \right) \tag{1.10}$$

is computed once. The linear operator

$$\mathbf{H} = \mathbf{H} \left( \mathbf{q}^{t + \frac{h}{2}} \right) \tag{1.11}$$

is computed at every time step. The number of rows of  $\mathbf{H}$  depends on the number of constraints, while its rank is related to their linear independence. We then compute

$$\mathbf{B} = \mathbf{H} \left( \mathbf{u}^t + \mathbf{M}^{-1} h \mathbf{f}^{t + \frac{h}{2}} \right) \tag{1.12}$$

and

$$\mathbf{W} = \mathbf{H}\mathbf{M}^{-1}\mathbf{H}^{T} \tag{1.13}$$

which is symmetric and semi-positive definite. The linear transformation

$$\mathbf{U} = \mathbf{B} + \mathbf{WR} \tag{1.14}$$

maps constraint reactions **R** into local relative velocities  $\mathbf{U} = \mathbf{H}\mathbf{u}^{t+h}$  at time t+h. Relation (1.14) will be here referred to as the *local dynamics*. Finally

$$\mathbf{R}$$
 is such that  $\mathbf{C}(\mathbf{U}, \mathbf{R}) = \mathbf{C}(\mathbf{B} + \mathbf{W}\mathbf{R}, \mathbf{R}) = \mathbf{C}(\mathbf{R}) = \mathbf{0}$  (1.15)

where  $\mathbf{C}$  is a nonlinear and usually nonsmooth operator. A basic Contact Dynamics algorithm can be summarised as follows:

- 1. Perform first half-step  $\mathbf{q}^{t+\frac{h}{2}} = \mathbf{q}^t + \frac{h}{2}\mathbf{u}^t$ .
- 2. Update existing constraints and detect new contact points.
- 3. Compute W, B.
- 4. Solve  $\mathbf{C}(\mathbf{R}) = \mathbf{0}$ .
- 5. Update velocity  $\mathbf{u}^{t+h} = \mathbf{u}^t + \mathbf{M}^{-1}h\mathbf{f}^{t+\frac{h}{2}} + \mathbf{M}^{-1}\mathbf{H}^T\mathbf{R}$ .
- 6. Perform second half-step  $\mathbf{q}^{t+h} = \mathbf{q}^{t+\frac{h}{2}} + \frac{h}{2}\mathbf{u}^{t+h}$ .

It should be stressed that the above presentation exemplifies only a particular instance of Contact Dynamics. Let us refer the reader to [10, 12, 3, 11, 7, 6, 1, 9, 13, ?] for more details.

# Chapter 2

# Installation

Solfec is hosted on GitHub and you will need the git command installed in order to download its source code. Have a look at https://git-scm.com for instructions. Once the git command is available in your command line, type

```
git clone https://github.com/tkoziara/solfec.git
```

This will create the directory solfec in your current directory. The next thing you need is a Make/C/C++/Fortran/Python development environment at your command line. Users of Unix type systems (e.g. Linux, FreeBSD, Mac OS X) may use a package manager to install those tools. Windows users can install Cygwin or Mingw instead. Solfec is written in C and it uses a simple makefile to get compiled. The file solfec/Config.mak needs to be modified to set up library paths and compilation flags. Here is an example:

```
# # Operating System (WIN32, SOLARIS, LINUX, AIX, IRIX, OSX)
#
OS = OSX
#
# Specify C compiler here
#
CC = cc
#
# Specify C++ compiler
#
CXX = g++
#
# Specify FORTRAN95 compiler and FORTRAN runtime library
#
FC = gfortran
FCLIB = -lgfortran
#
# Debug or optimized version switch (yes/no)
#
DEBUG = no
PROFILE = no
MEMDEBUG = no
GEOMDEBUG = no
PARDEBUG = no
PARDEBUG = no
```

```
NOTHROW = no
# TIMERS (enable/disable detailed solver timings)
TIMERS = yes
# POSIX
POSIX = yes
# HDF5
HDF5 = yes
HDF5INC = -I/usr/local/hdf5/include
HDF5LIB = -L/usr/local/hdf5/lib -lhdf5 -lhdf5_hl
# XDR (must be set when HDF5 = no)
XDR = no
XDRINC =
XDRLIB =
# BLAS
BLAS = -lblas
# LAPACK
LAPACK = -llapack
# Python
PYTHON = -I/usr/include/python2.7
PYTHONLIB = -L/usr/lib -lpython2.7
# OpenGL (yes/no)
OPENGL = yes
GLINC = -Wno-deprecated-declarations
GLLIB = -framework GLUT -framework OpenGL
# VBO (OPENGL == yes)
VBO = yes
# MPI (yes/no)
MPI = yes
MPICC = mpicc -Wno-unused-but-set-variable -fopenmp
# Zoltan (MPI == yes)
```

```
#
ZOLTANINC = -I/Users/tomek/Devel/lib/zoltan/include
ZOLTANLIB = -L/Users/tomek/Devel/lib/zoltan/lib -lzoltan
# Dynlb load balancer (MPI = yes) available at:
# https://github.com/tkoziara/dynlb
# This option is used when ZOLTAN = no above;
# Use path to dynlb directory below;
# Use -fopenmp flag with MPICC when compiling with dynlb;
DYNLB = ../dynlb
# PARMEC library available at:
# https://github.com/tkoziara/parmec
# This option is used to enable the HYBRID_SOLVER;
# If not required can be left as empty;
PARMEC = ../parmec
# Siconos (yes/no)
SICONOS = yes
SICONOSINC = -I/usr/local/include/Siconos/Numerics
SICONOSLIB = -L/usr/local/lib -l SiconosNumerics
```

The above configuration works on Mac OS X. To recap, what you need is:

- C, C++, FORTRAN 95 compilers
- HDF5 library
- (optional, deprecated) **XDR** (standard part of RPC on all Unix type systems)
- BLAS and LAPACK libraries (standard on most systems)
- Python together with development files and libraries (versions 2.x have been tested)
- OpenGL libraries and developments files (this enables Solfec's viewer)
- (optional) **VBO** (Vertex Buffer Object extension of OpenGL for faster rendering)
- MPI libraries and development files
- either **Zoltan** load balancing library or **dynlb** load balancing library
- (optional) Siconos contact solvers library

To compile Solfec, after editing the Config.mak file, the first compilation should look like this

```
cd solfec
```

This will create files solfec/solfec and solec/solfec-mpi, that is the serial and the parallel versions of the code. For every subsequent update and compilation you will like to do the following

• Back up your *Config.mak* file. For example

```
cd solfec
cp Config.mak ..
```

• Now update the sources

```
git pull
```

ullet Recover your Config.mak file

```
mv ../Congig.mak ./
```

• And finally compile again

```
make clean
make all
```

Use "DEBUG = no" most of the time: this will make Solfec about 40% faster. Nonetheless, when you experience trouble with running the code, recompile it with "DEBUG = yes" (this is slower but outputs more information in case you would encounter a bug) and run it again. The solfec/inp directory contains example input files. If you haven't used the "POSIX = yes" flag, you will need to create output directories yourself before running calculations (on systems where "POSIX = yes" works, this is done automatically). It may be convenient to modify the PATH variable to point to the solfec directory, making it easier to run Solfec form any location in your filesystem. You can ask for help, using the Solfec mailing list.

# Chapter 3

# Running Solfec

Solfec is a command line program. It can be run sequentially (command: solfec) or in parallel using the MPI runtime environment (command: solfec-mpi). Running it without parameters

```
./solfec
```

results in the hint

```
SYNOPSIS: solfec [-v] [-w] [-c] [-f] [-g WIDTHxHEIGHT] [-s sub-directory] [-i verbosity interval]
```

The -v switch opens the interactive graphical viewer (cf. Figure 3.1). In this mode the user can view the geometrical model, run or step through analysis, and view results. The right mouse click on the viewer window expands the menu.

The -w switch forces the computation (write) mode: if some results are present, they will be overwritten.

The -c switch forces the continued computation (write) mode: if some results are present, the analysis will be continued from where it was stopped. **NOTE1:** this option works correctly only if RUN is used once per input file; With -c Solfec terminates in case RUN is used multiple times; **NOTE2:** this option works only with the HDF5 output; in case of the XDR output it is the same as -w; **NOTE3:** in parallel continuation must be done using the same number of MPI ranks (e.g. N in "mpirun -np N ..." must not change);

The -f switch, together with -v, opens the viewer in the wire-frame mode, which requires substantially less memory and can be used to visualize large models.

The -g switch allows to specify the initial width and height of the viewer window (512 by default).

The -s switch allows to output or read the results from a sub-directory. This option is useful when one wishes to output results of similar analyses to different sub-directories of a common root directory specified when creating a SOLFEC object (cf. Section 4.2.5). For example, the bellow commands would run a parallel example and output the results into different sub-directories denoted by the number of processors involved in the analysis

```
mpirun -np 4 solfec-mpi -s 4 inp/cubes.py
mpirun -np 16 solfec-mpi -s 16 inp/cubes.py
```

Because the directory out/cubes is specified when creating the SOLFEC object in the inp/cubes.py input file, the above commands result in creation of two output directories: out/cubes/4 and out/cubes/16. One can then view a specific set of results by running

```
./solfec -v -s 16 inp/cubes.py
```

During a parallel run Solfec updates a file named STATE, placed in the output directory of a simulation. It contains statistics relevant to the run, including an estimated time until the end of the simulation. The output directory contains as well a copy of the input file, which makes reading results more self-contained (it is harder to mismatch input and output files this way). An analysis (both serial and parallel) can be stopped at any time by placing a file named STOP in the output directory of a simulation.

The -i switch allows to adjust the time interval of verbose output of runtime statistics (default is 1s).



Figure 3.1: Solfec viewer window.

# 3.1 Read / write mode

or

Let's say that you have just created an input file 'test.py' in the 'inp' directory. In this input file you have created a SOLFEC object as follows

```
argv = NON_SOLFEC_ARGV()
solfec = SOLFEC ('DYNAMIC', 0.001, 'out/test' + '/' + argv[0])
```

Hence, the results will be placed in the directory 'out/test/dir1/' + argv[0]. An analysis has not yet been run for this input file and there are no results. If you run

```
./solfec inp/test.py -s dir1 arg1 arg2

mpirun -np 4 ./solfec-mpi inp/test.py -s dir1 arg1 arg2
```

then results will be written into 'out/test/dir1/arg1'. You can see that command line input parameters can influence the location of the output directory. Since for this first run Solfec did not manage to find any results located at 'out/test/dir1/arg1' the analysis will be pursued and testing

```
if solfec.mode == 'WRITE': print 'WRITE MODE!'
elif solfec.mode == 'READ': print 'READ MODE!'
```

will output 'WRITE MODE!'. The first analysis is done in the write mode. After it has finished you will be able to access the results by again calling

```
./solfec inp/test.py -s dir1 arg1 arg2
./solfec out/test/dir1/arg1.py -s dir1 arg1 arg2
```

since 'out/test/dir1/arg1.py' is an exact copy of 'inp/test.py'. **But crucially note**, that the same parameters '-s dir1 arg1, arg2' need to be passed to Solfec so that the correct output path could be recognized! Of course, on this second run the above if test will result in the output 'READ MODE!'.

# 3.2 Output directory as an input path

Solfec creates a copy of an input file in the output directory. For example, if the output path is

```
out/analysis1
```

or

the corresponding copy of the input file will be

```
out/analysis1/analysis1.py
```

In order to view or post-process the results that have been saved in this directory, one can run

```
solfec -v out/analysis1
```

For this approach to be robust, care needs to be taken to ensure that the input file can be correctly run from any location (e.g. access to additional data or scripts required by an input file needs to be suitably resolved).

# Chapter 4

# Input language

Solfec input file is essentially a Python source code. Python interpreter is embedded in Solfec. At the same time Solfec extends Python by adding a number of objects and routines. There are few general principles to remember:

- Zero based indexing is observed in routine arguments.
- Parameters after the bar | are optional. For example FUNCTION (a, b/c, d) has two optional parameters c, d.
- Passing Solfec objects to some routines *empties* them. This means that a variable, that was passed as an argument, no longer stores data. For example: let x = CREATE1 () create an object x, and let y = CREATE2 (x) create an object y, using x. If CREATE2 (x) empties x, then after the call x becomes an empty placeholder. One can use it to assign value, x = CREATE1 (), but using it as an argument, z = CREATE2 (x), will cause an abnormal termination. One can create a copy of an object by calling z = COPY (x), hence using y = CREATE2 (x) leaves x intact.
- Routines marked as (Under development) are functional, although they may be unstable. Routines marked as (Experimental) are only moderately tested.

Sections below document Solfec objects and routines used for their manipulation.

# 4.1 Feature maturity matrix

The below table gives indicative assessment of the maturity of various Solfec commands.

	low	average	high
CONVEX		X	
HULL		X	
MESH2CONVEX		X	
MESH		X	
HEX			X
ROUGH_HEX	x		
PIPE			X
ELLIP_MESH	x		
TETRAHEDRALIZE	x		
SPHERE			X
ELLIP		X	

SOLFEC			x
SURFACE MATERIAL		X	Α
BULK_MATERIAL	x	Λ	
BODY	A	X	
TIME SERIES		X	
GAUSS SEIDEL SOLVER		А	37
PENALTY SOLVER			X
_		X	
NEWTON_SOLVER SICONOS SOLVER		X	
<u> </u>	X		
FIX_POINT			X
FIX_DIRECTION			X
SET_DISPLACEMENT	X		
SET_VELOCITY			X
SET_ACCELERATION	X		
PUT_RIGID_LINK			X
GRAVITY			X
FORCE		X	
TORQUE		X	
PRESSURE		X	
SIMPLIFIED_CRACK	X		
RUN			X
OUTPUT			X
EXTENTS			x
CALLBCK		X	
UNPHYSICAL PENETRARION		X	
GEOMETRIC EPSILON		X	
WARNINGS			x
INITIALIZE STATE	X		
IMBALANCE TOLERANCE		X	
RANK			x
BARRIER			x
NCPU			X
HERE		X	
VIEWER			x
BODY CHARS		X	1
INITIAL_VELOCITY			x
RIGID TO FEM		X	1
APPLY BULKMAT		X	
DELETE		X	
SCALE		Α	v
TRANSLATE			X
ROTATE			X
SPLIT	1.		X
COPY	X		+
	+ +	r-	X
BEND BYLABEL		X	
			X
MASS_CENTER			X
CONTACT_EXCLUDE_BODIES			X

CONTACT_EXCLUDE_SURFACES		X	
CONTACT_EXCLUDE_OBJECTS	x		
CONTACT_SPARSIFY		X	
LOCDYN_DUMP	x		
OVERLAPPING		X	
MBFC_EXPORT	x		
NON_SOLFEC_ARGV			X
MODAL_ANALYSIS	x		
COROTATED_DISPLACEMENTS	x		
RIGID_DISPLACEMENTS	x		
BODY_MM_EXPORT			X
DISPLAY_POINT		X	
RENDER	x		
XDMF_EXPORT	x		
REGISTER_BASE	x		
DURATION			X
FORWARD			X
BACKWARD			X
SEEK			X
DISPLACEMENT			X
VELOCITY			X
STRESS			X
ENERGY		X	
TIMING		X	
HISTORY		X	

# 4.2 Solfec objects

# **4.2.1** CONVEX

An object of type CONVEX is either an arbitrary convex polyhedron, or it is a collection of such polyhedrons.

# obj = CONVEX (vertices, faces, volid | convex)

This routine creates a CONVEX object from a detailed input data.

- ullet obj created CONVEX object
- vertices list of vertices: [x0, y0, z0, x1, y1, z1, ...]
- faces list of faces: [n1, v1, v2, ..., vn1, s1, n2, v1, v2, ..., vn2, s2, ...], where n1 is the number of vertices of the first face, v1, v2, ..., vn1 enumerate the vertices in the CCW order when looking from the outside, and s1 is the surface identifier of the face. Similarly for the second face and so on.
- volid volume identifier
- $\bullet$   $\mathbf{convex}$  (emptied) collection of CONVEX objects appending  $\mathbf{obj}$

Some parameters can also be accessed as members and methods of a CONVEX object. These are

Read-only members and methods		
obj.nver - number of convex vertices		
<b>obj.vertex</b> $(n)$ - returns a $(x, y, z)$ tuple storing coordinates of $n$ th $v$ ertex		

# obj = HULL (points, volid, surfid | convex)

This routine creates a CONVEX object as a convex hull of a point set.

- obj created CONVEX object
- **points** list of points: [x0, y0, z0, x1, y1, z1, ...]
- volid volume identifier
- surfid surface identifier common to all faces
- convex (emptied) collection of CONVEX objects appending obj

# obj = MESH2CONVEX (mesh)

This routine converts a MESH object into a list of CONVEX objects. It can be useful for containing one MESH defining a body shape inside of another background mesh defining deformability (see the background mesh parameters of the BODY object).

- obj created CONVEX object
- mesh input mesh

## 4.2.2 MESH

An object of type MESH describes an arbitrary volumetric mesh, comprising tetrahedrons, pyramids, wedges, and hexahedrons (Figure 4.1). First order elements are currently supported.



Figure 4.1: Element types in Solfec.

## obj = MESH (nodes, elements, surfids)

This routine creates a MESH object from a detailed input data.

- obj created MESH object
- **nodes** list of nodes: [x0, y0, z0, x1, y1, z1, ...]

- elements list of elements: [e1, n1, n2, ..., ne1, v1, e2, n1, n2, ..., ne2, v2, ...], where e1 is the number of nodes of the first element, n1, n2, ..., ne1 enumerate the element nodes, and v1 is the volume identifier of the element. Similarly for the second element and so on.
- surfids list of surface identifiers: [gid, f1, n1, n2, ..., nf1, s1, f2, n1, n2, ..., nf2, s2, ...], where gid is the global surface identifier for all not specified faces, f1 is the number of nodes in the first specified face, n1, n2, ..., nf1 enumerate the face nodes, and s1 is the surface identifier of the face. Similarly for other specified faces. If only the gid is given, this can be done either as [gid] or as gid alone.

Some parameters can also be accessed as members and methods of a MESH object. These are

#### Read-only members and methods

obj.nnod - number of mesh nodes

obj.get\_data() - return a tuple (nodes, elements, surfids), in the same format as for MESH(). Note these are read-only - changing the returned lists does not affect the mesh. obj.surface\_integration\_points( | surfid) - returns surface integration points as a list of tuples [(x0, y0, z0), (x1, y1, z1), ...]; if surfid is passed, integration points only fort that surface identifier are returned

 $obj.volume\_integration\_points( / volid)$  - returns volume integration points as a list of tuples [(x0, y0, z0), (x1, y1, z1), ...]; if volid is passed, integration points only fort that volume identifier are returned

obj.inter\_element\_faces() - returns a list of lists of node indices of inter-element faces, e.g. [[n0, n1, n2], [n0, n1, n2, n3], ...]

obj.inter\_element\_faces\_on\_plane(point, normal | ref, eps) - returns a list of lists of node indices of inter-element faces on a plane, e.g. [[n0, n1, n2], [n0, n1, n2, n3], ...], where point, normal define the plane, ref can be True or False and determines whether the plane is in the reference or current configuration (default: True), eps determines the tolerance for the "on plane" test (default: geometric epsilon, cf. Section 4.5)

#### Read-write members and methods

obj.node  $(n \mid x, y, z)$  - returns a (x, y, z) tuple storing coordinates of nth node; if x, y or z are given the current coordinates are overwritten

obj.nodes\_on\_surface (surfid) - returns a list of node numbers belonging to the given surface; None object is returned if the list is empty.

obj.set\_volid(volid) - set all elements to have the given volume ID. Returns the volid set. This is mostly useful for being able to distinguish bodies in the Viewer, using menu Kinds of -> Volumes. Note that materials are also assigned by volume ID.

# obj = HEX (nodes, i, j, k, volid, surfids | dx, dy, dz)

This routine creates a MESH object corresponding to a hexahedral shape (hexahedral elements are used).

- obj created MESH object
- nodes list of 8 nodes: [x0, y0, z0, x1, y1, z1, ..., x7, y7, z7]. The hexahedral shape will be stretched between those nodes using a linear interpolation.
- $\bullet\,$  i, j, k numbers of subdivisions along the local x, y, z directions.
- volid volume identifier
- surfids list of six surface identifiers: [s1, s2, ..., s6], corresponding to the faces of the hexahedral shape

• dx, dy, dz - lists of subdivision schemes along local x, y, z directions. By default a subdivision is uniform. When dx = [1, 1, 5, 5, 1, 1] is present, then this scheme will be normalised (actual numbers do not matter, but their ratios) and applied to the local x direction of the generated shape.

# $obj = ROUGH HEX (shape, i, j, k \mid dx, dy, dz)$

This routine creates a hexahedral MESH object corresponding to a given shape. The resultant mesh properly contains the input shape and with its orientation (which is based on the inertia properties of the shape).

- obj created MESH object
- **shape** an input shape defined by a collection of CONVEX objects; a list of CONVEX objects (or their collections) [cvx1, cvx2, cvx3, ....] is as well accepted.
- i, j, k numbers of subdivisions along the local x, y, z directions of the principal inertia axes
- dx, dy, dz lists of subdivision schemes along local x, y, z directions. By default a subdivision is uniform. When dx = [1, 1, 5, 5, 1, 1] is present, then this scheme will be normalised (actual numbers do not matter, but their ratios) and applied to the local x direction of the generated shape.

# obj = PIPE (pnt, dir, rin, thi, ndir, nrad, nthi, volid, surfids)

This routine creates a MESH object corresponding to a pipe (hexahedral elements are used).

- obj created MESH object
- pnt base point tuple (x, y, z)
- dir direction tuple (dx, dy, dz); length of the pipe equals to the length of the direction
- rin inner radius
- thi thickness
- ndir, nrad, nthi number of subdivisions along the direction, radius and thickness
- volid volume identifier
- surfids list of four surface identifiers [s1, s2, s3, s4] corresponding to the faces of the pipe

# obj = ELLIP\_MESH (center, radii, error, volid, surfid) (under development)

This routine creates a MESH object corresponding to an ellipsoid (tetrahedral elements are used).

- $\bullet~\mathbf{obj}$  created MESH object
- center tuple (x, y, z) defining the center
- radii tuple (rx, ry, rz) of ellipsoid radii
- error surface mesh error size (measured as distance from ellipsoid)
- volid volume identifier
- surfid surface identifier

# obj = TETRAHEDRALIZE (shape, path | volume, quality, volid, surfid)

This routine creates a tetrahedral mesh. Tetgen is invoked internally, http://tetgen.berlios.de/.

- obj created MESH object
- shape an input shape can be:
  - another MESH object
  - a path (e.g. 'path/to/file.stl') to an input file supported by Tetgen (e.g. http://tetgen.berlios.de/fformats.html)
- path path to the output file that will store the mesh; when called again and this file is found the mesh will be red from the file rather than generated
- volume maximum element volume (default: not enforced)
- quality value > 1.0 indicating element quality (default: not enforced); values close to 1.0 result in better mesh quality (mesh generation may fail for small values)
- volid volume identifier (default: 0); if only possible it is inherited from the input
- surfid surface identifier (default: 0); if only possible it is inherited from the input

## **4.2.3 SPHERE**

An object of type SPHERE represents a single sphere.

# obj = SPHERE (center, radius, volid, surfid)

This routine creates a SPHERE object.

- obj created SPHERE object
- center tuple (x, y, z) defining the center
- radius sphere radius
- volid volume identifier
- surfid surface identifier

Some parameters can also be accessed as members of a SPHERE object. These are

Read-only members and methods
obj.center, obj.radius

## 4.2.4 ELLIP

An object of type ELLIP represents a single ellipsoid.

# obj = ELLIP (center, radii, volid, surfid)

This routine creates an ELLIP object.

- obj created ELLIP object
- center tuple (x, y, z) defining the center
- radii tuple (rx, ry, rz) of ellipsoid radii
- volid volume identifier
- surfid surface identifier

Some parameters can also be accessed as members of a ELLIP object. These are

# Read-only members and methods obj.center, obj.radii obj.renter obj.radii obj.rot - tuple $(v_{1x}, v_{1y}, v_{1z}, v_{2x}, v_{2y}, v_{2z}, v_{3x}, v_{3y}, v_{3z})$ representing a rotation operator from the ellipsoid natural coordinaet (aligned with principal axes) system to the global cooridinate system

### 4.2.5 **SOLFEC**

An object of type SOLFEC represents the Solfec algorithm. One can use several SOLFEC objects to run several analyses from a single input file.

# obj = SOLFEC (analysis, step, output)

This routine creates a SOLFEC object.

- obj created SOLFEC object
- analysis 'DYNAMIC' or 'QUASI STATIC' analysis kind
- step initially assumed time step, regarded as an upper bound
- output defines the output directory path (Important note: if this directory exists and contains valid output data SOLFEC is created in 'READ' mode, otherwise SOLFEC is created in 'WRITE' mode)

Some parameters can also be accessed as members of a SOLFEC object. These are

Read-only members		
obj.analysis		
obj.time - current time		
obj.mode - either 'READ' or 'WRITE' as described above		
obj.constraints - list of constraints (cf. Section 4.2.16)		
obj.ncon - number of constraints		
obj.bodies - list of bodies (cf. Section 4.2.9)		
obj.nbod - number of bodies		
obj.outpath - output path, including the sub-directory if the "-s" command line		
argument has been passed		

#### Read/write members

obj.step

obj.verbose - 'ON' or 'OFF' enabling or disabling writing to standard output (default: 'ON'); '%' can also be used to enable plain percentage printout per individual RUN obj.cleanup - either 'ON' or 'OFF' enabling or disabling removal of the output directory in 'WRITE' mode if none results were saved (default: 'OFF' in which case the initial geometry is saved as a result); Note: POSIX=yes must be set in Config.mak for the 'ON' functionality to work;

## 4.2.6 FIELD

An object of type FIELD represents a three-dimensional, scalar, time dependent field.

# obj = FIELD (solfec, field callback | label, data)

This routine creates a FIELD object.

- **obj** created FIELD object
- solfec obj is created for this SOLFEC object
- field callback the Python function defining the scalar field:

$$value = field \ callback \ (data, x, y, z, t)$$

where **data** is the optional user data passed to **FIELD** routine (if **data** is a tuple it will expand the list of parameters to the callback), **x**, **y**, **z** are the point coordinates, and **t** is time. The function should return a numeric value of the scalar field at given point and instant of time.

- label label string (default: 'FIELD i', where i is incremented for each call)
- data callback routine user data

Some parameters can also be accessed as members of a FIELD object. These are

Read-only members	
obj.label	

# 4.2.7 SURFACE MATERIAL

An object of type SURFACE\_MATERIAL represents material properties on the interface between two surfaces. Surfaces identifiers are included in definitions of all geometric objects.

# obj = SURFACE\_MATERIAL (solfec | surf1, surf2, model, label, friction, cohesion, restitution, spring, dashpot, hpow)

This routine creates a SURFACE MATERIAL object.

- obj created SURFACE MATERIAL object
- solfec obj is created for this SOLFEC object
- surf1 first surface identifier

Model name	Employs variables
'SIGNORINI_COULOMB'	friction, cohesion, restitution (cf. Section
	8.1.1)
'SPRING_DASHPOT'	spring, dashpot, friction, cohesion, hpow
	(cf. Section 8.1.2)

Table 4.2: Surface material models.

- surf2 second surface identifier; If only surf1 is specified, the surface material is used for all contacts with the specified surface; If neither surf1 or surf2 are specified, the surface material is used for any contacts where a more-specific pairing cannot be found.
- model material model name (default: 'SIGNORINI\_COULOMB'), see Table 4.2 and Chapter 8
- label label string (default: 'SURFACE MATERIAL i', where i is incremented for each call)
- friction friction coefficient (default: 0.0)
- cohesion cohesion per unit area (default: 0.0)
- restitution velocity restitution (default: 0.0)
- spring spring stiffness (default: 0.0)
- dashpot dashpot stiffness (default: 0.0); any negative value indicates critical damping
- hpow Hertz's law power (default: 1.0)

Some parameters can also be accessed as members of a SURFACE MATERIAL object. These are

Read-only members		
obj.surf1, obj.surf2, obj.label		
Read/write members		
obj.model,obj.friction, obj.cohesion, obj.restitution, obj.spring, obj.dashpot		

# 4.2.8 BULK MATERIAL

An object of type BULK MATERIAL represents material properties of a volume.

# obj = BULK\_MATERIAL (solfec| model, label, young, poisson, density, tensile, fields, fracene)

This routine creates a BULK MATERIAL object.

- $\bullet$   $\mathbf{obj}$  created BULK\_MATERIAL object
- $\bullet$   $\mathbf{solfec}$   $\mathbf{obj}$  is created for this SOLFEC object
- model material model name (default: 'KIRCHHOFF'), see Table 4.3 and Chapter 8
- label label string (default: 'BULK MATERIAL i', where i is incremented for each call)
- young Young's modulus (default: 1E9)
- poisson Poisson's coefficient (default: 0.25)

Model name	Employs variables
'KIRCHHOFF'	young, poisson, density (cf. Section 8.2.1)

Table 4.3: Bulk material models.

- density material density (default: 1E3)
- tensile tensile strength for fracture check (default:  $\infty$ )
- fields list [field1, field1, ..., fieldN] of FIELD objects (or FIELD object labels) needed by the material model.
- fracene fracture energy threshold (default:  $\infty$ )

Some parameters can also be accessed as members of a BULK MATERIAL object. These are

Read-only members	
obj.model, obj.label	
Read/write members	
obj.young, obj.poisson, obj.density	

#### 4.2.9 BODY

An object of type BODY represents a solid body.

## obj = BODY (solfec, kind, shape, material | label, form, mesh, base)

This routine creates a body.

- obj created BODY object
- solfec obj is created for this SOLFEC object
- kind a string: 'RIGID', 'PSEUDO\_RIGID', 'FINITE\_ELEMENT' or 'OBSTACLE' describing the kinematic model. See Table 4.4.
- **shape** (emptied) this is can be a CONVEX/MESH/SPHERE/ELLIP object, or a list [obj1, obj2, ...], where each object is of type CONVEX/MESH/SPHERE/ELLIP. If the **kind** is 'FINITE\_ELEMENT', then two cases are possible:
  - **shape** is a single MESH object: the mesh describes both the shape and the discretisation of the motion of a body
  - shape is solely composed of CONVEX objects: here a separate mesh must be given to discretise motion of a body (see the mesh argument below)
- material a BULK\_MATERIAL object or a label of a bulk material (specifies an initial body-wise material, see also the MATERIAL (...) routine in Section 4.6)
- label a label string (no label is assigned by default)
- form valid when kind equals 'FINITE\_ELEMENT', ignored otherwise (default: 'TL'). This argument specifies a formulation of the finite element method. See Table 4.5.

- mesh optional when kind equals 'FINITE\_ELEMENT', ignored otherwise. This variable must be a MESH object describing a finite element mesh properly containing the shape composed solely of CONVEX objects. This way the 'FINITE\_ELEMENT' model allows to handle complicated shapes with less finite elements, e.g. an arbitrary shape could be contained in just one hexahedron.
- base optional reduced order or modal base definition, or a string label of a registered base (see **REG-ISTER\_BASE** on page 47); when **form** = 'BC-MODAL', results of the **MODAL\_ANALYSIS** command (page 44), or equivalent user data, can be used; the same format is used for the 'BC-RO' formulation; This argument must be passed if **form** = 'BC-MODAL' or 'BC-RO', see Table 4.5.

Some parameters can also be accessed as members of a BODY object. These are

# Read-only members

obj.kind, obj.label, obj.material

obj.mass - referential mass of the body

obj.volume - referential volume of the body

obj.center - referential mass center of the body

obj.tensor - referential Euler (pseudo-rigid, finite element kinematics) or inertia tensor (rigid kinematics) of the body

obj.constraints - list of constraints attached to the body (cf. Section 4.2.16)

obj.ncon - number of constraints attached to the body

obj.id - unique identifier

obj.display\_points - list of tuples of display point labels and coordinates: [('label', (x, y, z)), ('label', (x, y, z)), ...]

**obj.mesh** - returns computational MESH associated with a 'FINITE\_ELEMENT' body; for other body kinds a MESH or a list of MESH objects is returned if such are present as components of the body shape

#### Read/write members

obj.conf - tuple (q1, q2, ..., qN) storing configuration of the body. See Table 4.6.

**obj.velo** - tuple (u1, u2, ..., uN) storing velocity of the body. See Table 4.7.

**obj.selfcontact** - self-contact detection flag (default: 'OFF") taking values 'ON' or 'OFF'.

**obj.scheme** - time integration scheme (default: 'DEFAULT') used to integrate motion. See Table 4.8.

*obj.damping* - stiffness proportional damping coefficient (default: 0.0) for the dynamic case (ignored for rigid bodies).

obj.fracturecheck - check fracture criterion for FEM bodies ('ON', or default: 'OFF').(Under development)

obj.disable\_rotation - for rigid bodies disable integration of rotation ('ON', or
default: 'OFF')

## **4.2.10 TIME SERIES**

An object of type TIME\_SERIES is a linear spline based on a series of 2-points.

## obj = TIME SERIES (points | label, cache)

This routine creates a TIME SERIES object.

• obj - created TIME SERIES object

Body kind	Remarks
'OBSTACLE'	A rigid body ignoring external loads and not
	contributing to contact constraints. Motion of an
	obstacle can be controlled through single-body
	constraints. An obstacle-to-obstacle contact is ignored.
	Moving obstacles will not correctly work in the
	quasi-static case (use rigid bodies instead).
	Obstacle bodies do generate contact constraints with
	other non-obstacle bodies.
'RIGID'	A classical rigid body.
'PSEUDO_RIGID'	A simple body with global linear deformation state.
'FINITE_ELEMENT'	A body discretised with finite elements. Only first
	order elements are supported at present.

Table 4.4: Body kinds.

Formulation	Remarks
'TL'	Total Lagrangian (default)
'BC'	Body co-rotational (one co-rotated frame per body,
	suitable for stiff bodies)
'BC-MODAL'	Body co-rotational, modal approach; 'DEF_LIM'
	integration scheme is always used for this formulation
	(there is no computational advantage in using
	'DEF_EXP' since all system matrices are diagonal);
	Note: the base argument must be passed; (Under
	${f development})$
'BC-RO'	Body co-rotational, reduced order approach;
	'DEF_LIM' integration scheme is always used for this
	formulation (there is no computational advantage in
	using 'DEF_EXP' since all system matrices are
	dense); Note: the base argument must be passed;
	$( { m Under \ development} )$

Table 4.5: Finite element formulations

Body kind	Configuration description
'RIGID'	Column-wise rotation matrix followed by the current
	mass center.
'PSEUDO_RIGID'	Column-wise deformation gradient followed by the
	current mass center.
'FINITE_ELEMENT'	Current coordinates x, y, z of mesh nodes.
'OBSTACLE'	Column-wise rotation matrix followed by the current
	mass center.

Table 4.6: Types of configurations.

Body kind	Velocity description
'RIGID'	Referential angular velocity followed by the spatial
	velocity of mass center.
'PSEUDO_RIGID'	Deformation gradient velocity followed by the spatial
	velocity of mass center.
'FINITE_ELEMENT'	Components x, y, z of spatial velocities of mesh nodes.
'OBSTACLE'	Referential angular velocity followed by the spatial
	velocity of mass center.

Table 4.7: Types of velocities.

• **points** - either a list [t0, v0, t1, v1, ...] or a list of lists [[t0, v0], [t1, v1], ...] of points (where ti < tj, when i < j), or a path to a file storing times and values pairs in format:

```
# comment 1 ...
# comment 2 ...
t0 v0
t1 v1
# comment 3 ...
t2 v2
...
```

- label optional label string; if a label is provided than the TIME\_SERIES object is stored in memory just once; this facilitates more optimal memory usage in cases where many identical TIME\_SERIES objects are used in multiple constraints (for example); the label should be unique
- **cache** optional partial cache size; if **points** = file path and **cache** > 0 then only the cache size of points is stored in memory at any given time; this helps to save memory in case of a need for many large time series objects; default: 0 (entire time series is stored in memory) (**Under development**)

Some parameters can also be accessed as members of a TIME\_SERIES object. These are

Read-only members	
obj.times - list [t0, t1,] storing times.	
obj.values - list [v0, v1,] storing values.	
obj.derivative - returns a TIME_SERIES object representing a derivative of the	
current object	
obj.integral - returns a TIME_SERIES object representing an integral of the current	
object	

Scheme	Kinematics	Remarks
'DEFAULT'	all	Use a default time integrator regardless of underlying
		kinematics.
'RIG_POS'	rigid	NEW1 in [8]: explicit, positive energy drift, no
		momentum conservation
'RIG_NEG'	rigid	NEW2 in [8]: explicit, negative energy drift, exact
		momentum conservation; default for rigid kinematics
'RIG_IMP'	rigid	NEW3 in [8]: semi-explicit, no energy drift and exact
		momentum conservation
'DEF_EXP'	pseudo-rigid, finite	Explicit scheme described in Chapter 5 of [?]; default
	element	for deformable kinematics, energy and momentum
		conserving, conditionally stable
'DEF_LIM'	pseudo-rigid, finite	Linearly implicit scheme similar to [14]; energy and
	element	momentum conserving, stable for moderate to large
		steps; <b>NOTE:</b> if the time step is too large, artificial
		negative internal energy increments may be produced
		in the event of impacts

Table 4.8: Time integration schema.

# 4.2.11 GAUSS SEIDEL SOLVER

An object of type GAUSS\_SEIDEL\_SOLVER represents a nonlinear block Gauss-Seidel solver, employed for the calculation of constraint reactions (cf. Section 10.1).

# obj = GAUSS\_SEIDEL\_SOLVER (epsilon, maxiter | meritval, failure, diagepsilon, diagmaxiter, diagsolver, data, callback)

This routine creates a GAUSS\_SEIDEL\_SOLVER object.

- obj created GAUSS SEIDEL SOLVER object
- epsilon relative accuracy of constraint reactions sufficient for termination
- maxiter maximal number of iterations before termination
- meritval constraints satisfaction merit function value sufficient for termination (default: 1, unused), cf. Chapter 9 for more details.
- failure failure (lack of convergence) action (default: 'CONTINUE'). Available failure actions are: 'CONTINUE' (simulation is continued), 'EXIT' (simulation is stopped and Solfec exits), 'CALLBACK' (a callback function is called if it was set or otherwise the 'EXIT' scenario is executed). In all cases *obj.error* variable is set up, cf. Table 4.9.
- diagepsilon diagonal block solver relative accuracy of constraint reactions (default: min (epsilon, meritval, 1E-4) / 100)
- diagmaxiter diagonal block solver maximal number of iterations (default: max (100, maxiter / 100))
- diagsolver diagonal block solver kind (default: 'SEMISMOOTH\_NEWTON'). Available diagonal solvers are 'SEMISMOOTH\_NEWTON', 'PROJECTED\_GRADIENT', 'DE\_SAXCE\_FENG', 'PROJECTED\_NEWTON', cf. Chapter 10.
- data data passed to the failure callback function (if this is a tuple it will accordingly expand the parameter list of the callback routine)

 $\bullet$  callback - failure callback function of form:  $value = callback \ (obj, \ data)$ , where for the returned value equal zero Solfec run is stopped

Some parameters can also be accessed as members of a GAUSS\_SEIDEL\_SOLVER object. These are

Read-only members	
obj.failure	
obj.error - current error code, cf. Table 4.9	
obj.iters - number of iterations during a last run of solver	
obj.rerhist - a list of relative error values for each iteration of the last run	
obj.merhist - a list of merit function values for each iteration of the last run	

## Read/write members

obj.epsilon, obj.maxiter, obj.meritval, obj.diagepsilon, obj.diagmaxiter, obj.diagsolver

obj.reverse - 'ON' or 'OFF' flag switching iteration reversion modes (whether to alternate backward and forward or not, default is 'OFF')

obj.variant - variant of parallel Gauss-Seidel update (default: 'FULL'), cf. Table 4.10. Ignored in sequential mode.

obj.innerloops - number of inner Gauss-Seidel loops per one global step during a parallel run (default: 1). Ignored in sequential mode.

*obj.itershist* - set to 'ON' before reading; when red returns a Python list storing iterations counts from all solver runs.

'OK'	No error has occurred
'DIVERGED'	Global iteration loop divergence
'DIAGONAL_DIVERGED'	Diagonal solver iteration loop divergence
'DIAGONAL FAILED'	Failure of a diagonal solver (e.g. singularity)

Table 4.9: Error codes of GAUSS\_SEIDEL\_SOLVER object.

'FULL'	Full Gauss-Seidel update as in sequential case. Although the
	slowest, it works in all cases. It should be noted, that all of the
	below variants will usually fail for all-rigid-body models.
'MIDDLE_JACOBI'	Jacobi update for off-processor data of W matrix blocks
	communicating with processors of higher and lower colors. Of use
	for deformable kinematics, where off-diagonal interactions are
	weaker. The Gauss-Seidel run-time should be halved for large
	numbers of processors.
'BOUNDARY_JACOBI'	Use Jacobi update for all off-processor data. This approach will
	fail in most cases. It servers as illustration.

Table 4.10: Variants of parallel Gauss-Seidel update.

# 4.2.12 PENALTY SOLVER

An object of type PENALTY\_SOLVER represents a penalty based constraint solver (cf. Section 10.2). When in use, all 'SIGNORONI\_COULOMB' type contact interfaces are regarded as 'SPRING\_DASHPOT' ones. One should then remember about specifying the *spring* value for those.

# obj = PENALTY SOLVER ( | variant)

- obj created PENALTY SOLVER object
- variant 'IMPLICIT' or 'EXPLICIT' normal force computation variant (default: 'IMPLICIT')

# 4.2.13 NEWTON SOLVER

Object of type NEWTON\_SOLVER represents a projected quasi-Newton constraints solver (cd. Section 10.3). If local dynamics is enabled (locdyn = 'ON') and iterations fail to converge, the Gauss-Seidel solver will be invoked, starting from the previous time step solution. **WARNING:** for the moment NEWTON\_SOLVER may not work well for friction > 1.0.

# obj = NEWTON\_SOLVER (| meritval, maxiter, locdyn, linver, linmaxiter, maxmatvec, epsilon, delta, theta, omega, gsflag, reldelta)

- $\bullet~{\bf obj}$  created NEWTON\_SOLVER object
- meritval value of merit function sufficient for termination (default: 1E-8), cf. Chapter 9 for more details
- maxiter iterations bound (default: 1000)
- locdyn 'ON' or 'OFF' deciding whether to fully assemble local dynamics (default: 'ON'); using the 'OFF' value may be more efficient for implicitly integrated FEM bodies with large meshes
- linver 'GMRES' or 'DIAG' being the linear solver kind (default: 'GMRES')
- limaxiter GMRES iterations bound (ignored for linver = 'DIAG', default: 10)
- maxmatvec GMRES matrix-vector products bound (default: linmaxiter \* maxiter)
- ullet epsilon relative GMRES accuracy (default: 0.25)
- delta non-negative amount of diagonal regularization (used only for linver = 'GMRES', default: 0.0); this parameter has a decisive influence on global convergence; for well-conditioned problems it can be very small or zero; for ill-conditioned problems one should pick a value that delivers an overall best convergence behavior; large values will slow down convergence, but stabilize it; small values may destabilize convergence for ill-conditioned problems; delta (typically \le 1) should be tuned together with epsilon and linmaxiter, so that the linear sub-problems are solved only roughly; since rigorous analysis is still missing for these parameters, please experiment before settling on specific values for a specific problem;
- theta relaxation parameter greater than 0 and not greater than 1 (used only for linver = 'DIAG', default: 0.25); smaller initial theta may improve overall convergence behavior
- omega positive equation smoothing omega (default: meritval · 0.01)
- gsflag 'ON' or 'OFF' deciding whether to us Gauss-Seidel iterations in case of failure (default: 'ON')
- reldelta make delta relative to the generalized inverse inertia **W** operator; possible choices are: 'OFF' delta is regarded as an absolute value, 'avgWii' delta is relative to the average of the diagonal entries of **W**, 'minWii' delta is relative to the minimum of the diagonal entries of **W**, 'maxWii' delta is relative to the maximum of the diagonal entries of **W**; (default: 'OFF')

Some parameters can also be accessed as members of a NEWTON SOLVER object. These are

# $\overline{\textbf{Read-only}}$ members

obj.iters - number of iterations during a last run of solver

obj.merhist - a list of merit function values for each iteration of the last run

obj.mvhist - a list of matrix-vector products for each iteration of the last run

#### Read/write members

 $obj.meritval,\ obj.maxiter,\ obj.locdyn,\ obj.linver,\ obj.linmaxiter,\ obj.maxmatvec,\ obj.epsilon,\ obj.delta,\ obj.theta,\ obj.omega,\ obj.gsflag$ 

**obj.itershist** - set to 'ON' before reading; when red returns a Python list storing iterations counts from all solver runs.

# 4.2.14 SICONOS SOLVER

Object of type SICONOS\_SOLVER represents the frictional contact solvers available from Siconos<sup>1</sup>. Currently only the the nonlinear Gauss-Seidel solver is enabled, making the SICONOS\_SOLVER equivalent to the GAUSS\_SEIDEL\_SOLVER. WARNING1: only contact constraints are supported at this stage. WARNING2: velocity restitution is ignored at the moment. WARNING3: only the serial version is available. WARNING4: Solfec needs to be compiled with Sicons support for this solver to work.

# obj = SICONOS SOLVER (| epsilon, maxiter, verbose)

- ullet obj created SICONOS\_SOLVER object
- epsilon relative accuracy of constraint reactions sufficient for termination (default: 1E-4)
- maxiter iterations bound (default: 1000)
- verbose verbosity flag: 'ON' or 'OFF' (default: 'OFF')

Some parameters can also be accessed as members of a SICONOS\_SOLVER object. These are

#### Read/write members

obj.epsilon, obj.maxiter

# 4.2.15 HYBRID SOLVER (under development)

Hybrid solver allows to combine smooth rigid body nonlinear spring based PARMEC models with non-smooth SOLFEC models. The solver is supported both in the serial and MPI version of Solfec. The Parmec library is shared memory parallel and in the MPI mode this part of modeling is executed on MPI rank 0 process, employing maximum available shared memory parallelism.

# $obj = HYBRID\_SOLVER$ (parmec\_file, parmec\_step, parmec2solfec, solfec\_solver | parmec\_argv, boundary\_contact\_detection)

- $\bullet~{\bf obj}$  created HYBRID\_SOLVER object
- parmec\_file PARMEC input file path
- $\bullet$   $\mathbf{parmec\_step}$  an upper bound of the PARMEC time step
- parmec2solfec Python dictionary based mapping of PARMEC particle numbers to SOLFEC body identifiers; these are the "boundary" bodies

 $<sup>^{1} \</sup>rm http://siconos.gforge.inria.fr/HomePage/index.html$ 

- solfec solver SOLFEC constraint solver (e.g. NEWTON SOLVER)
- parmec argv optional list of PARMEC arguments, retrieved by PARMEC command ARGV
- boundary contact detection optional boundary contact detection flag ('ON', or default: 'OFF')

#### Notes:

- motion of the boundary bodies listed in the parmec2solfec mapping is driven by the SOLFEC model
- boundary bodies listed in the parmec2solfec mapping must be rigid

Some parameters can also be accessed as members of a HYBRID\_SOLVER object. These are

#### Read/write members

obj.parmec\_interval - PARMEC output interval specification (as in parmec's DEM command); when not specified PARMEC will not write output files; the read value is [(d,d), (O,O), (i, i)], where the first tuple contains floating point intervals, the second tuple contains Python callbacks, the third tuple contains TSERIES numbers

obj.parmec prefix - PARMEC output file name prefix (as in parmec's DEM command)

# 4.2.16 CONSTRAINT

An object of type CONSTRAINT represents a constraint and some of its associated data (e.g. constraint reaction). Both user prescribed constraints and contact constraints are represented by an object of the same type.

# obj = FIX POINT (body, point | strength)

This routine creates a fixed point constraint.

- **obj** created CONSTRAINT object
- body BODY object whose motion is constrained
- **point** (x, y, z) tuple with referential point coordinates
- **strength** optionally an ultimate magnitude of the reaction force, beyond which the constraint will be deleted (default: infinity)

# obj = FIX DIRECTION (body, point, direction | body2, point2)

This routine fixes the motion of a referential point along a specified spatial direction. If **body2** is given the motion of **point2** along the **direction** convected with the first **body** is fixed.

- $\bullet~{\bf obj}$  created CONSTRAINT object
- body BODY object whose motion is constrained
- point (x, y, z) tuple with referential point coordinates
- direction (vx, vy, vz) tuple with spatial direction components
- **body2** BODY object whose motion is constrained with respect to the motion of the first **body** (in this case **body** and **body2** can only be either *rigid* or *pseudo-rigid*)
- $\mathbf{point2}$  (x, y, z) tuple with referential point on  $\mathbf{body2}$

# obj = SET DISPLACEMENT (body, point, direction, tms)

This routine prescribes a displacement history of a referential point along a specified spacial direction.

- obj created CONSTRAINT object
- body BODY object whose motion is constrained
- point (x, y, z) tuple with referential point coordinates
- direction (vx, vy, vz) tuple with spatial direction components
- tms TIME SERIES object with the displacement history

# $obj = SET_VELOCITY (body, point, direction, value)$

This routine prescribes a velocity history of a referential point along a specified spacial direction.

- obj created CONSTRAINT object
- body BODY object whose motion is constrained
- **point** (x, y, z) tuple with referential point coordinates
- direction (vx, vy, vz) tuple with spatial direction components
- value a constant value or a TIME SERIES object with the velocity history

# obj = SET ACCELERATION (body, point, direction, tms)

This routine prescribes an acceleration history of a referential point along a specified spacial direction.

- obj created CONSTRAINT object
- body BODY object whose motion is constrained
- point (x, y, z) tuple with referential point coordinates
- direction (vx, vy, vz) tuple with spatial direction components
- tms TIME SERIES object with the acceleration history

# obj = PUT RIGID LINK (body1, body2, point1, point2 | strength)

This routine creates a rigid link constraints between two referential points of two distinct bodies.

- obj created CONSTRAINT object
- **body1** BODY object one whose motion is constrained (could be *None* when **body2** is not *None* then one of the points is fixed "in the air")
- body2 BODY object two whose motion is constrained (could be *None* when body1 is not *None*)
- point1 (x1, y1, z1) tuple with the first referential point coordinates
- point2 (x2, y2, z2) tuple with the second referential point coordinates
- **strength** optionally an ultimate tensile strength if **point1** != **point2**, beyond which the link will be deleted (default: infinity); or ultimate reaction magnitude (**point1** == **point2**)

# obj = PUT\_SPRING (body1, point1, body2, point2, function, limits | direction, update) (Under development)

This routine creates an arbitrary spring between two referential points of two distinct bodies.

- **obj** created CONSTRAINT object
- body1 BODY object one whose motion is constrained
- **point1** (x1, y1, z1) tuple with the first referential point coordinates
- body2 BODY object two whose motion is constrained
- point2 (x2, y2, z2) tuple with the second referential point coordinates
- function Python function callback returning the value of force as the function of stroke: force = function (stroke, velocity), where stroke= $\mathbf{n} \cdot \text{current}$  (point2 point1) initial (|point2 point1|) and velocity is the current relative velocity along the spring direction  $\mathbf{n}$  (positive if stroke increases).
- limits (smin, smax) tuple defining stroke limits  $(smin \leq 0 \text{ and } smax \geq 0)$
- **direction** (nx, ny, nz) tuple storing spring direction **n**. Default: **n** = normalized(current (point2 point1)) resulting in a follower type spring. When specified, **n** will be updated according to the value of **update**.
- **update** direction update kind (default: 'FIXED'); one of: 'FIXED' where **n** is kept fixed, or 'CONV1' where **n** is convected with body1, or 'CONV2' where **n** is convected with body2.

Some parameters can also be accessed as members of a CONSTRAINT object. These are

# Read-only members

obj.kind - kind of constraint: 'CONTACT', 'FIXPNT' (fixed point), 'FIXDIR' (fixed direction), 'VELODIR' (prescribed velocity; note that prescribed displacement and acceleration are converted into this case), 'RIGLNK' (rigid link)

obj.R - current average (over time step [t,t+h]) constraint reaction in a form of a tuple: (RT1,RT2,RN) given with respect to a local base stored at obj.base

 ${\it obj.U}$  - constraint output relative velocity tuple: (UT1, UT2, UN) given with respect to a local base stored at  ${\it obj.base}$ 

 ${\it obj.V}$  - contact input relative velocity tuple: (VT1, VT2, VN) given with respect to a local base stored at  ${\it obj.base}$ 

**obj.base** - current spatial coordinate system in a form of a tuple: (eT1x, eT2x, eNx, eT1y, eT2y, eNy, eT1z, eT2z, eNz) where x, y, z components are global

**obj.point** - current spatial point where the constraint force acts. This is a (x, y, z) tuple for all constraint types, but 'RIGLNK' for which this is a (x1, y1, z1, x2, y2, z2) tuple.

obj.area - current area for contact constraints or zero otherwise

obj.gap - current gap for contact constraints or zero otherwise

 $\boldsymbol{obj.merit}$  - current value of the per-constraint merit function

obj.adjbod - adjacent bodies. This is a tuple (body1, body2) of BODY objects for 'CONTACT' and 'RIGLNK' or a single BODY object otherwise.

 ${\it obj.matlab}$  - surface material label for constraints of kind 'CONTACT', or a  ${\it None}$  object otherwise.

obj.spair - pairing of surfaces (surf1, surf2) for contact constraints or None object otherwise. The tuple (surf1, surf2) corresponds to the surface identifiers for the (body1, body2) body pairing returned by obj.adjbod

# 4.3 Applying loads

Routines listed in this section apply loads.

# GRAVITY (solfec, vector)

This routine sets up the gravitational acceleration.

- solfec SOLFEC object for which the acceleration is set up
- **vector** (vx, vy, vz) tuple defining the gravity acceleration. Each entry is a number or a TIME\_SERIES object defining the value of the acceleration component.

# FORCE (body, kind, point, direction, value | data)

This routine applies a point force to a body.

- body BODY object to which the force is applied
- kind either 'SPATIAL' or 'CONVECTED'; the *spatial* direction remains fixed, while the *convected* one follows deformation
- **point** (x, y, z) tuple with the referential point where the force is applied
- direction (vx, vy, vz) tuple defining the direction of force
- value a number, a TIME\_SERIES object or a callback routine defining the value of the applied force. In case of a callback routine, the following format is assumed:

$$force = value\_callback\ (data,\ q,\ u,\ time,\ step)$$

where: **data** is the optional user data passed to **FORCE** routine (if **data** is a tuple it will expand the list of parameters to the callback), **q** is the configuration of the body passed to the callback, **u** is the velocity of the body passed to the callback, **time** is the current time passed to the callback and **step** is the current time step passed to the callback. The callback returns a **force** tuple. For rigid body the force reads (*spatial force*, *spatial torque*, *referential torque*), while for other kinds of bodies this is a generalized force of the same dimension as the velocity **u** (power conjugate to it).

• data - callback routine user data

# TORQUE (body, kind, direction, value)

This routine applies a torque to a rigid body.

- body BODY object of kind 'RIGID' to which the torque is applied
- kind either 'SPATIAL' or 'CONVECTED'; the *spatial* direction remains fixed, while the *convected* one follows deformation
- direction (vx, vy, vz) tuple defining the direction of torque
- value a number or a TIME SERIES object defining the value of the applied torque

Criterion	Parameters	Description
'TENSILE'	ft	Tensile stress at any point of the the crack plane is
		larger than the tensile strength.

Table 4.11: Cracking criteria.

# PRESSURE (body, surfid, value)

This routine applies a constant surface pressure to MESH based bodies.

- body BODY object to which the pressure is applied (the shape has to be composed of a single MESH)
- surfid the integer surface identifier
- value a number or a TIME SERIES object defining the value of the applied load

# 4.4 Fragmentation (Under development)

Routines listed in this section control fragmentation of bodies.

# SIMPLIFIED\_CRACK (body, point, normal, surfid, criterion | topoadj, ft, Gf) (Under development)

This routine prescribes a potential body-wise planar crack together with a cracking criterion. Depending on the topological properties of the body shape, creation of a body-wise crack may or may not result in splitting of the body in two parts.

- body a pseudo-rigid or FEM based BODY object
- **point** crack plane referential point (x, y, z); if **topoadj** = 'ON' then the **point** is meant to belong to the crack tip
- normal crack plane referential normal  $(n_x, n_y, n_z)$
- surfid tuple (surf1, surf2) of the two new crack surfaces identifiers; Surface surf1 has normal  $(n_x, n_y, n_z)$ .
- criterion cracking criterion, cf. Table 4.11
- topoadj 'ON' or 'OFF' (default: 'OFF'); when 'OFF' the crack will always propagate across the whole body and result in two body fragments; when 'ON' the crack will propagate from the crack tip through the topologically adjacent elements, which may not produce fragmentation;
- ft tensile strength (default: 0.0)
- Gf fracture energy (default: 0.0); currently unused

# $(body2, lst1, lst2) = RT\_SPLIT (body1, surf | sid1, sid2, label1, label2) (Experimental)$

This routine splits a meshed BODY object along a surface aligned with internal element boundaries. It can be invoked from within a callback function - see the CALLBACK command in Section 4.5 - and hence "RT" stands for "runtime".

• body2 - created BODY object or *None* if the split does not create another body

- lst1, lst2 lists mapping original mesh node numbers to new mesh node numbers in body1 and body2. Only lst1 is valid in case of a split which does not create two separate bodies in this case lst2 = None
- $\bullet$   $\mathbf{body1}$  a MESH based BODY which is split
- surf surface definition of the split plane on **body1**: a list of lists of face nodes [[n0, n1, n2], [n3, n4, n5, n6], ...] defining the splitting surface (zero based indexing)
- sid1 optional identifier for the newly created surface on body1; default: 0
- sid2 optional identifier for the newly created surface on body2; default: 0
- label1 optional label of body1; default: *None* (split in two bodies) or no change (a partial split of body1)
- label2 optional label of body2; default: None

#### Properties:

- 1. **surf** normals are calculated so that the face nodes are counter clockwise oriented when looking from the positive normal direction.
- 2. **body2** is on the *positive* side of **surf**, i.e. the normals of **surf** points towards the newly created body.
- 3. ID of **body1** changes every time a split happens (even if **body2** is *None*).
- 4. All constraints attached to **body1** are deleted during splitting.
- 5. All forces applied to **body1** are deleted during splitting.
- 6. RT SPLIT terminates with an error message in case none or more then two mesh fragments were created.

## 4.5 Running simulations

Routines listed in this section control the solution process.

#### RUN (solfec, solver, duration)

This routine runs a simulation.

- solfec SOLFEC object
- solver constraint solver object (e.g. GAUSS SEIDEL SOLVER, PENALTY SOLVER)
- duration duration of analysis. Note: this parameter is ignored when an analysis is run in the viewer mode (with -v switch).

#### OUTPUT (solfec, interval | compression)

This routine specifies the frequency of writing to the output file.

- solfec SOLFEC object
- interval length of the time interval elapsing before consecutive output file writes
- **compression** output compression mode: 'OFF' (default) or 'ON'. Compressed output files are smaller, although they might not be portable between hardware platforms.

### EXTENTS (solfec, extents)

This routine bounds the simulation space. Bodies falling outside of the extents are deleted from the simulation.

- solfec SOLFEC object
- extents (xmin, ymin, zmin, xmax, ymax, zmax) tuple

### CALLBACK (solfec, interval, data, callback)

This routine defines a callback function, invoked during a run of Solfec every interval of time. A callback routine can interrupt the course of **RUN** command by returning 0.

- solfec SOLFEC object
- interval length of the time interval elapsing before consecutive callback calls
- data data passed to the callback function
- $\bullet$  callback callback function of form:  $value = callback \ (data)$ , where for the returned value equal zero Solfec run is stopped

## UNPHYSICAL\_PENETRATION (solfec, depth)

This routine sets a depth of an allowed unphysical interpenetration. Once it is exceeded, the simulation is stopped and a suitable error message printed out.

- solfec SOLFEC object
- depth interpenetration depth bound (default:  $\infty$ )

#### GEOMETRIC EPSILON (epsilon)

This routine sets a numerical tolerance for geometric tests performed within Solfec. The tolerance is a characteristic distance between two distinct points below which they can be regarded as one.

• epsilon - geometrical tolerance (default: 1E-6)

#### WARNINGS (state)

This routine disables or enables Solfec warnings. It is a good practice to have the warnings enabled and only switch them off after making sure, that they can be ignored.

• state - 'ON' or 'OFF' (default: 'ON')

## INITIALIZE\_STATE (solfec, path, time | subset)

This routine initializes the state of a Solfec object with the state red from an output directory at a given time. It is ignored in the 'READ' mode.

- solfec Solfec object in the 'WRITE' mode
- path path to the output directory containing matching analysis results (**note:** this cannot be the same output directory as for the **solfec** object)
- time time at which the state should be red from the output files

• subset - defines a subset of initialized bodies; a string can be used to define a POSIX regular expression<sup>2</sup> that will be matched against body labels; a list of such strings can also be passed; e.g. ['^BOD.\*A\$', '^BODY1\$', '^BODY2\$', '^BOD.\*B\$'] defines two direct labels 'BODY1' and 'BODY2' and two possible subsets made of labels such as 'BODY123A', 'BODY anything B', etc.

## RIGID TO FEM (path, time, solfec | subset)

This routine initializes the state of FEM bodies within the Solfec object with the state of rigid bodies red from an output directory at a given time. It is ignored in the 'READ' mode. **NOTE:** rigid displacements are applied to the finite element bodies; this implies that when you add boundary conditions to finite element bodies, after their state was updated with RIGID\_TO\_FEM, you still use the original referential point coordinates as the locations of the constraints (e.g. when using SET\_DISPLACEMENT or SET\_VELOCITY).

- path path to the output directory containing matching rigid body analysis results; the number of rigid bodies in this analysis must match the number of FEM bodies in the Solfec object; the identifiers of rigid bodies must match the identifiers of FEM bodies; this is guaranteed if the input files for both analyses differ only by the prescribed body kinds;
- time time at which the state should be red from the output files
- solfec Solfec object in the 'WRITE' mode
- subset defines a subset of initialized bodies; a string can be used to define a POSIX regular expression<sup>3</sup> that will be matched against body labels; a list of such strings can also be passed; e.g. ['^BOD.\*A\$', '^BODY1\$', '^BODY2\$', '^BOD.\*B\$'] defines two direct labels 'BODY1' and 'BODY2' and two possible subsets made of labels such as 'BODY123A', 'BODY anything B', etc.

#### 4.6 Utilities

Various utility routines are listed below.

#### IMBALANCE TOLERANCE (solfec, tolerance | weightfactor, updatefreq)

This routine sets the imbalance tolerance for parallel balancing of Solfec data. A ratio of maximal to minimal per processor count of objects used. Hence, 1.0 indicates perfect balance, while any ratio > 1.0 indicates an imbalance. Initially imbalance tolerance is set to 1.1. This routine is ignored during sequential runs.

- solfec SOLFEC object
- tolerance data imbalance tolerance (default: 1.1)
- weightfactor a local dynamics weight factor between 0.0 and 1.0 (default: 1.0). Computational load of local dynamics assembling is best balanced when weightfactor equals 1.0. This however can sometimes result in a poor load balance for contact detection or time integration. Making it smaller than 1.0 can improve the overall balance in such cases. *Note:* This parameter is ignored if DYNLB load balancer is used; in this case, on a per-rank basis, body centroids are used to guide load balancing if there is more bodies than constrains on a given rank at given time; otherwise contact/constraint points are used to guide load balancing.
- updatefreq geometrical domain partitioning is updated every updatefreq time steps (default: 10)

 $<sup>^2\</sup>mathrm{Follow}$  this link for the syntax of POSIX regular expressions.

<sup>&</sup>lt;sup>3</sup>Follow this link for the syntax of POSIX regular expressions.

#### num = RANK ()

This routine returns the rank of the CPU that runs the current copy of Solfec.

• num - the CPU rank

### BARRIER ()

This routine sets up a parallel barrier in the MPI mode (all processes need to meet at it before they can continue). It is ignored in the serial mode.

### num = NCPU (| solfec)

This routine returns the number CPUs used in the analysis.

- num the number of CPUs
- solfec optional SOLFEC object (useful in 'READ' mode)

#### ret = HERE (solfec, object)

This routine tests whether an object is located on the current processor. During parallel runs objects migrate between processors. When calling a function (or a member) for an object not present on the current processor, the call will usually return None or be ignored. Hence, it is convenient to check whether an object resides on the current processor.

- ret True or False
- solfec SOLFEC object
- object BODY or CONSTRAINT object

#### obj = VIEWER ()

This routine tests whether the viewer is enabled.

• obj - True or False depending on whether the viewer (-v command line option) was enabled

#### obj = SUBDIR ()

This routine returns the optional output subdirectory.

• obj - None object or subdirectory string depending on whether the -s command line option was used

#### BODY CHARS (body, mass, volume, center, tensor)

This routine overwrites referential characteristics of a body.

- body BODY object
- mass body mass
- volume body volume
- center (x, y, z) mass center
- tensor  $(t_{11}, t_{21}, \dots, t_{33})$  column-wise inertia tensor for a rigid body or Euler tensor otherwise

#### INITIAL VELOCITY (body, linear, angular)

This routine applies initial (at time zero) linear and angular (in the sense of rigid motion) velocity to a body.

- body BODY object
- linear linear velocity  $(v_x, v_y, v_z)$
- angular angular velocity  $(\omega_x, \omega_y, \omega_z)$

## APPLY\_BULKMAT (solfec, body, volid, material)

This routine applies bulk material to a subset of geometric objects with the given volume identifier.

- solfec SOLFEC object
- body BODY object
- volid volume identifier
- material MATERIAL object or material label

#### DELETE (solfec, object)

This routine deletes a BODY object or a CONSTRAINT object from a SOLFEC object.

- solfec SOLFEC object
- object (emptied) BODY or CONSTRAINT object

#### obj = SCALE (shape, coefs)

This routine scales a geometrical object or a collection of such objects.

- **obj** when **shape** is not (x, y, z) tuple: same as **shape**, returned for convenience. Otherwise the  $(x \cdot coefs[0], y \cdot coefs[1], z \cdot coefs[2])$  tuple.
- **shape** object, collection of objects, or a list [a, b, c, ...] of objects of type CONVEX, MESH, SPHERE, ELLIP. Alternately this can be a single (x, y, z) tuple, but then one must use **point** = **SCALE** (**point**, **coefs**) in order to modify the **point** (Python tuples are immutable they cannot be modified "in place" after creation).
- coefs (cx, cy, cz) tuple of scaling factors along each axis

### obj = TRANSLATE (shape, vector)

This routine translates a geometrical object or a collection of such objects.

- **obj** when **shape** is not (x, y, z) tuple: same as **shape**, returned for convenience. Otherwise the (x + vector[0], y + vector[1], z + vector[2]) tuple.
- **shape** object, collection of objects, or a list [a, b, c, ...] of objects of type CONVEX, MESH, SPHERE, ELLIP. Alternately this can be a single (x, y, z) tuple, but then one must use **point** = **TRANSLATE** (**point**, **vector**) in order to modify the **point** (Python tuples are immutable they cannot be modified "in place" after creation).
- vector (vx, vy, vz) tuple defining the translation

#### obj = ROTATE (shape, point, vector, angle)

This routine rotates a geometrical object or a collection of such objects.

- **obj** when **shape** is not (x, y, z) tuple: same as **shape**, returned for convenience. Otherwise the rotated (x1, y1, z1) image of (x, y, z).
- shape object, collection of objects, or a list [a, b, c, ...] of objects of type CONVEX, MESH, SPHERE, ELLIP. Alternately this can be a single (x, y, z) tuple, but then one must use **point1** = **ROTATE** (**point1**, **point2**, **vector**, **angle**) in order to modify **point1** (Python tuples are immutable they cannot be modified "in place" after creation).
- point (px, py, pz) tuple defining a point passed by the rotation axis
- vector (vx, vy, vz) tuple defining a direction of the rotation axis
- angle rotation angle in degrees

# (one, two) = SPLIT (shape, point, normal | surfid, topoadj, remesh) (Under development)

This routine splits a geometrical object (or a collection of objects) by a plane passing by a point. Depending on the topological properties of the body shape and plane position this may or may not result in splitting of the body in two parts.

- one objects placed below the splitting plane (*None* if no objects were placed below the plane)
- two objects placed above the splitting plane (*None* if no objects were placed above the plane, or if the initial shape has not been fragmented in two parts)
- shape (emptied) object, collection of objects, or a list [a, b, c, ...] of objects of type CONVEX, SPHERE, ELLIP or MESH
- point (px, py, pz) tuple defining a point passed by the splitting plane
- normal (nx, ny, nz) tuple defining the splitting plane normal
- **surfid** (*surf1*, *surf2*) tuple defining a pair of surface identifier for the two newly created surfaces (default: 0,0). Surface *surf1* has the outward normal (*nx*, *ny*, *nz*).
- topoadj 'ON' or 'OFF' (default: 'OFF'); when 'OFF' the splitting will always propagate across the whole body and result in two body fragments; when 'ON' the splitting will propagate from the input point through the topologically adjacent elements, which may not produce fragmentation;
- remesh 'ON' or 'OFF' (default: 'ON') flag used only for MESH based shapes; when 'ON' mesh splitting away from inter-element boundaries will lead to tetrahedral re-meshing; when 'OFF' it will raise an error.

**WARNING:** Mesh splitting generates tetrahedral mesh in place of the input one if the splitting plane is not aligned with element boundaries. The meshing is randomized and it may generate different results for the same input. Use TETRAHEDRALIZE in order to refine and save the generated mesh parts. Otherwise you may encounter input/output errors.

# $[out1, out2, ...] = MESH\_SPLIT (mesh | nodeset, faceset, surfid1, surfid2) (Under development)$

This routine splits a mesh object along internal element boundaries whose nodes belong to the given node or face set. Depending on the topological properties of the mesh this may or may not result in splitting of the mesh in multiple parts.

- [out1, out2, ...] a list of output meshes (*None* if no internal element boundaries in the input mesh were split)
- mesh input MESH object (the input mesh is not modified by this routine)
- **nodeset** a list of nodes [n0, n1, n2, ...] defining the splitting surface (zero based indexing); ignored when **faceset** is passed
- faceset a list of lists face nodes [[n0, n1, n2], [n3, n4, n5, n6], ...] defining the splitting surface (zero based indexing)
- surfid1 surface identifier for the newly created surfaces (default: 0); used with nodeset or outward-counter-clockwise-normal aligned with faceset
- surfid2 surface identifier for the newly created surfaces (default: 0); inward-counter-clockwise-normal aligned with faceset

#### obj = COPY (shape)

This routine makes a copy of input objects.

- obj created collection of copied objects
- **shape** object, collection of objects, or a list [a, b, c, ...] of objects of type CONVEX, MESH, SPHERE, ELLIP

#### obj = BEND (shape, point, direction, angle)

This routine bends a shape around an axis. The bending is performed from the section of the shape closest to the axis onward. The orientation of the axis direction determines the orientation of the bending according to the right hand rule. Let  $\mathbf{q}$  be the closest to the axis mesh node. Then  $\mathbf{v} = \mathbf{d} \times (\mathbf{q} - \operatorname{proj}(\mathbf{q}))$ , where  $\mathbf{d}$  is the axis direction and  $\operatorname{proj}[\cdot]$  projects a point onto the axis. Bending starts from the section containing  $\mathbf{q}$  and proceeds in the direction of  $\mathbf{v}$ .

- obj same as shape
- shape object of type MESH
- point axis point
- direction axis direction
- angle positive bending angle in degrees

#### obj = BYLABEL (solfec, kind, label)

This routine finds a labelled object inside of a SOLFEC object.

- **obj** returned object (*None* if a labelled object was not found)
- solfec SOLFEC object
- kind labelled object: 'SURFACE MATERIAL', 'BULK MATERIAL', 'BODY', 'FIELD'
- label the label string

### obj = MASS CENTER (shape)

This routine calculates the mass center of a geometrical object or a collection of such objects.

- $\bullet$  **obj** (x, y, z) tuple storing the mass center
- **shape** object, collection of objects, or a list [a, b, c, ...] of objects of type CONVEX, MESH, SPHERE, ELLIP. Alternately this can be a single BODY object.

#### CONTACT EXCLUDE BODIES (body1, body2)

This routine disables contact detection for a specific pair of bodies. By default contact detection is enabled for all possible body pairs. **NOTE:** must be invoked on all processors during a parallel run (do not use from within a callback).

- body1 first BODY object
- body2 second BODY object

## CONTACT\_EXCLUDE\_SURFACES (solfec, surf1, surf2)

This routine disables contact detection for a specific pair of surfaces. By default contact detection is enabled for all possible surface pairs. **NOTE:** must be invoked on all processors during a parallel run (do not use from within a callback).

- solfec SOLFEC object
- $\bullet$  surf1 first BODY object
- surf2 second BODY object

#### CONTACT SPARSIFY (solfec | threshold, minarea, mindist)

This routine modifies contact filtering (sparsification) behaviour. Generally speaking, some contact points are filtered out in order to avoid unnecessary dense contact point clusters. If a pair of bodies is connected by two or more contact points, one of the points generated by topologically adjacent entities (elements, convices) will be removed (sparsified) if the ratio of contact areas of the contact points is smaller than the prescribed threshold (cf. Section 7.2).

- solfec SOLFEC object
- threshold sparsification threshold (default: 0.01) from within the interval [0, 1]. Zero corresponds to the lack of sparsification.
- minarea minimal contact area (default: 0.0). Contact points with area smaller then minarea are dropped.
- mindist minimal distance between distinct contact points (default: GEOMETRIC EPSILON).

### LOCDYN DUMP (solfec, path)

This routine dumps into a file the most recent state of local dynamics. It is meant for debugging and test purposes, e.g. comparing local dynamics between runs on various processor counts.

- solfec SOLFEC object
- path file path

## obj = OVERLAPPING (obstacles, shapes | not, gap)

This routine looks for shapes (not) overlapping the obstacles.

- obj list of shapes (not) ovrelapping the obstacles.
- obstacles object, collection of objects, or a list [a, b, c, ...] of objects of type CONVEX, MESH, SPHERE, ELLIP.
- **shapes** (emptied) object, collection of objects, or a list [a, b, c, ...] of objects of type CONVEX, MESH, SPHERE, ELLIP.
- not 'NOT' string.
- gap maximal negative gap.

### MBFCP EXPORT (solfec, path)

This routine exports Solfec model into the MBFCP problem definition format. See http://code.google.com/p/mbfcp/for details.

- solfec SOLFEC object
- path output path

## argv = NON SOLFEC ARGV ()

This routine returns all command line arguments (in the form of a list of strings) that have been passed to 'solfec' or 'solfec-mpi' application and has not been identified as valid Solfec arguments. This way the user can pass some arguments to the input scripts.

• argv - list of non-solfec specific arguments passed to 'solfec' or 'solfec-mpi' command

## obj = MODAL ANALYSIS (| body, num, path, abstol, maxiter, verbose)

This routine performs modal analysis of FEM bodies. The modal analysis results are stored with bodies and can be viewed.

- obj = (val, vec) the returned tuple of: val = obj[0] list of eigenvalues and vec = obj[1] list of eigenvectors (stored contiguously one after another)
- body input FEM body; the model analysis results are stored with this body
- num number of lowest modes to extract

- path path to file where the results will be stored (to avoid recomputing if possible). Note, that if previous modal analysis results are found they are used rather then recomputed if the number of modes and num are the same. If num is different from the previous modes count, then new num modes is computed from scratch. Also note, that path can be a sole parameter and in this case the routine will attempt to read and return existing results. Note: ".h5" extension is automatically added to the stored path;
- abstol residual tolerance for the eigenvalue solver (default: 1E-11)
- maxiter iterations bound for the eigenvalue solver (default: 100)
- verbose 'ON' or 'OFF' verbosity flag for the eigenvalue solver (default: 'OFF')

# $obj = COROTATED\_DISPLACEMENTS$ (solfec, subset | sampling) (Experimental)

This routine extracts snapshots of co-rotated displacements of FEM bodies. Co-rotated displacements factor out the rigid body rotation, only including deformational motion about the initial configuration of the body. Multiple calls to this command need to be used to extract multiple snapshot sets for distinct subsets of bodies. Note 1: identical sequence of calls to this routine must be executed on all MPI ranks; Note 2: this routine is relevant in the context of the 'BC-RO' FEM formulation, see BODY (page 23) and Table 25, and Python's modred package which can be used to calculate a reduced base; before being passed to the modred package, the outputted displacements snapshots need to be complemented by the six rigid displacements generated by the RIGID\_DISPLACEMENTS command (defined below);

- **obj** upon termination of all RUN commands (page 36), a list of lists of displacement snapshots; this works both in 'WRITE' and 'READ' modes; MPI-parallel extraction of co-rotated displacement snapshots is enabled in the 'WRITE' mode: in this case only MPI rank 0 process will store a valid output list (*None* is returned for ranks > 0); in 'READ' mode enable the **corotated\_displacements** flag of the FORWARD command (page 47) in order to sample displacements while skipping forward through results;
- solfec SOLFEC object
- subset specification of a subset of bodies for which co-rotated displacements are to be extracted; a string can be used to define a POSIX regular expression<sup>4</sup> that will be matched against body labels; a list of body objects or integer body identifiers can be used [body1, body2, id3, id4, body5, ...] mixed up in an arbitrary manner; or a tuple specifying extents of a bounding box can be used (xlow, ylow, zlow, xhigh, yhigh, zhigh), which the bounding boxes of exported bodies will overlapped at time t = 0; also a list of an arbitrary combination of those can be used, e.g. ['BOD\*A', 123, body1, body2, 256, (0, 0, 0, 1, 1, 1), 'KEY??7', (3, 3, 3, 4, 4, 4)] defines two labels, two integer body ids, two body objects, and two bounding boxes, that together define a subset of bodies that will be used during snapshot extraction; Note: meshes of all bodies in the subset must have the same number of nodes;
- sampling optional collection of time instants, e.g. [t0, t1, t2, ..., tN], or a time interval, e.g. dt0, at which the displacement snapshots are to be sampled; default: same as the output interval, see OUTPUT (page 36)

## obj = RIGID\_DISPLACEMENTS (body) (Experimental)

This routine outputs six unit vectors of rigid displacements of a FEM body (three translations and three rotations). *Note:* this routine is relevant in the context of the 'BC-RO' FEM formulation, see BODY (page 23) and Table 25, and Python's modred package which can be used to calculate a reduced base; see also the COROTATED DISPLACEMENTS command (defined above);

<sup>&</sup>lt;sup>4</sup>Follow this link for the syntax of POSIX regular expressions.

- obj a list comprising six lists representing the unit displacement vectors
- body a finite element BODY object

## BODY MM EXPORT (body, pathM, pathK | spdM, spdK)

Export body matrices in the MatrixMarket sparse format.

- body BODY object of 'FINITE ELEMENT' kind
- ullet path M output path for mass matrix M
- ullet path K output path for stiffness matrix K
- spdM symmetric positive definite flag M; 'ON' or 'OFF' (default: 'ON'); only lower triangle is exported
  when 'ON'
- spdK symmetric positive definite flag K; 'ON' or 'OFF' (default: 'ON'); only lower triangle is exported when 'ON'

#### DISPLAY POINT (body, point | label)

Attach a display point to a body. Display points are defined in reference configuration and convected with bodies. Display points can be visualised by selecting 'display points on/off' in the 'tools' viewer menu. They serve purely auxiliary purpose, for example allowing to make sure that the results are read from correct locations.

- body BODY object
- **point** referential (x, y, z) point
- label optional label

#### RENDER(solfec, object) (Experimental)

Render selected bodies in the Viewer.

- solfec SOLFEC object
- object BODY object or a list of BODY objects

NB: This CANNOT be used from within a normal analysis script, but only from a Viewer script, cf. 5.

#### XDMF EXPORT (solfec, time, path | subset, attributes) (Experimental)

Export results in XDMF format. In 'WRITE' mode only the geometry at time t = 0 is saved, while arguments time and attributes are ignored.

- solfec SOLFEC object
- **time** A time instant, e.g. t0, a collection of time instants, e.g. [t0, t1, t2, ..., tN], or a time interval, e.g. (t0, t1);
- path output path to the directory that will contain the XDMF markup file(s) and a HDF5 data file, e.g. '/tmp/sim0' will possibly result in a /tmp/sim0/sim0\_grids.xmf, /tmp/sim0/sim0\_constraints.xmf, /tmp/sim0/sim0 spheres.xmf markup files and a /tmp/sim0/sim0.h5 data file output;

- subset specification of a subset of exported bodies; a string can be used to define a POSIX regular expression<sup>5</sup> that will be matched against body labels; a list of body objects or integer body identifiers can be used [body1, body2, id3, id4, body5, ...] mixed up in an arbitrary manner; or a tuple specifying extents of a bounding box can be used (xlow, ylow, zlow, xhigh, yhigh, zhigh), which the bounding boxes of exported bodies will overlapped at time t = 0; also a list of an arbitrary combination of those can be used, e.g. ['BOD\*A', 123, body1, body2, 256, (0, 0, 0, 1, 1, 1), 'KEY??7', (3, 3, 3, 4, 4, 4)] defines two labels, two integer body ids, two body objects, and two bounding boxes, that together define a subset of bodies that will be used during export;
- attributes specify a list of export attributes; default ['DISP', 'VELO', 'REAC', 'GAP']; available attributes are 'DISP' (body displacement), 'VELO' (body velocity), 'STRESS' (body stress), 'REAC' (constraint reactions), 'RELV' (relative constraint velocities), 'GAP' (contact gaps); a non-optional scalar attribute 'BID' (body identifier) is always included with exported geometry

## REGISTER BASE (solfec, base, label) (Experimental)

Register 'BC-RO' or 'BC-MODAL' base for the finite element BODY formulation (page 23). Registering a reduced order or modal base saves memory when multiple instances of bodies employing the same base are used.

- solfec SOLFEC object
- base base definition: (val, vec) where val is a list of eigenvalues and vec is a list of eigenvectors (stored contiguously one after another)
- label unique string label

#### 4.7 Results access

Results can be accessed either in the 'READ' mode of a SOLFEC object, or in the 'WRITE' mode once some analysis has been run.

#### value = DURATION (solfec)

This routine returns the duration of a simulation in SOLFEC's 'READ' mode, or **solfec.time** in the 'WRITE' mode.

- value (t0, t1) duration limits of the simulation in 'READ' mode or current time in 'WRITE' mode
- solfec SOLFEC object

#### FORWARD (solfec, steps | corotated displacements)

This routine steps forward within the simulation output file. Ignored in SOLFEC's 'WRITE' mode.

- solfec SOLFEC object
- steps numbers of steps forward
- corotated\_displacements optional co-rotated displacements sampling flag; if 'TRUE' and a call or multiple calls to COROTATED\_DISPLACEMENTS (page 45) was/were made prior to FORWARD, co-rotated displacements will be sampled for every time instant visited by FORWARD (the original sampling interval will be ignored); default: 'FALSE'

<sup>&</sup>lt;sup>5</sup>Follow **this link** for the syntax of POSIX regular expressions.

### BACKWARD (solfec, steps)

This routine steps backward within the simulation output file. Ignored in SOLFEC's 'WRITE' mode.

- solfec SOLFEC object
- steps number of steps backward

#### SEEK (solfec, time)

This routine to a specific time within the simulation output file. Ignored in SOLFEC's 'WRITE' mode.

- solfec SOLFEC object
- time time to start reading at

### disp = DISPLACEMENT (body, point)

This routine outputs the displacement of a referential point.

- disp (dx, dy, dz) tuple storing the displacement
- body BODY object
- point (x, y, z) tuple storing the referential point

#### velo = VELOCITY (body, point)

This routine outputs the velocity of a referential point.

- velo (vx, vy, vz) tuple storing the velocity
- body BODY object
- point (x, y, z) tuple storing the referential point

#### stre = STRESS (body, point)

This routine outputs the Cauchy stress of a referential point.

- stre (sx, sy, sz, sxy, sxz, syz, mises) tuple storing the Cauchy stress and the von Mises norm of it
- body BODY object
- point (x, y, z) tuple storing the referential point

#### $ene = ENERGY (solfec \mid object)$

The routine outputs the value of energy of a specific object.

- ene (kinetic, internal, external, contact, friction) tuple of energy values; internal energy corresponds to the work of internal forces, external energy corresponds to the work of external forces (including constraint reactions), contact energy corresponds to the work of normal contact reactions, friction energy corresponds to the work of tangential contact reactions
- solfec SOLFEC object
- object SOLFEC object, BODY object or a list of BODY objects

#### tim = TIMING (solfec, kind)

The routine outputs the value of a specific action timing per time step.

- tim value of timing (or Python None object if solfec was in the 'WRITE' mode)
- solfec SOLFEC object in 'READ' mode
- kind this is one of: 'TIMINT' (time integration), 'CONUPD' (constraints update), 'CONDET' (contact detection), 'LOCDYN' (local dynamics setup), 'CONSOL' (constraints solution), 'PARBAL' (parallel load balancing). The load balancing timing is non-zero only for parallel runs.

#### hist = HISTORY (solfec, list, t0, t1 | skip, progress)

This routine outputs time histories of entities.

- hist a tuple of list objects storing the histories: (times, values1, values2, ..., valuesN)
- solfec SOLFEC object
- list list of objects [object1, object2, ..., objectN] indicating requested values. The valid objects are:
  - a tuple (body, point, entity) where body is a BODY object or a body label string, point is a (x, y, z) tuple storing the referential point, and entity is one of: 'CX', 'CY', 'CZ' (current coordinate), 'DX', 'DY', 'DZ' (displacement), 'VX', 'VY', 'VZ' (velocity), 'SX', 'SY', 'SZ', 'SXY', 'SXZ', 'SYZ' (stress), 'MISES' (von Mises norm of stress); Note: if body label is used and the body initially did not exist (e.g. it was inserted during simulation or produced as a result of fragmentation) corresponding values for times when it did not exit are NaN;
  - a tuple (object, kind) where object is a SOLFEC object, a BODY object or a list of BODY objects, and kind is a string 'KINETIC', 'INTERNAL', 'EXTERNAL', 'CONTACT' (included in external), 'FRICTION' (included in external) and it corresponds to the energy kind; if the list of BODY objects is used, their energies are summed up
  - a string 'TIMINT', 'CONUPD', 'CONDET', 'LOCDYN', 'CONSOL', 'PARBAL' for timing histories
  - a string 'STEP' for time step history
  - a string 'CONS', 'BODS' for constraint and body number histories
  - a string 'DELBODS', 'NEWBODS' for deleted and inserted (after time 0) body number histories (nonzero only for uncompressed outputs)
  - a string 'GSITERS' (Gauss-Seidel iterations count), 'GSCOLORS' (Gauss-Seidel processor colors count), 'GSBOT', 'GSMID', 'GSTOP', 'GSINN' (Gauss-Seidel bottom, middle, top and inner set sizes), 'GSINIT' (Gauss-Seidel setup time), 'GSRUN' (Gauss-Seidel computations time), 'GSCOM' (Gauss-Seidel communication time, except the middle set), 'GSMCOM' (Gauss-Seidel middle set communication time); values other than 'GSITERS' are non-zero only for parallel runs
  - a string 'MERIT' for the time history of the constraints satisfaction merit function
  - a string 'NTITERS' for the NEWTON\_SOLVER iterations count
  - a tuple (object, entity) or (object, direction, pair, entity) where object is a SOLFEC object, a BODY object or a list of BODY objects, direction is a tuple  $(d_x, d_y, d_z)$  storing a direction (use **None** if the normal direction is preferred), pair is a tuple (surf1, surf2) defining a surface pair (use **None** if no surface pair is preferred), and entity is:
    - $\ast$  'GAP' for the time history of the minimal contact gap among constraints attached to given bodies (negative gap corresponds to the penetration depth)

- \* 'R' for the time history of the resultant (and average over time step [t, t+h]) constraint reactions along the directions: normal or given by the direction
- $\ast\,$  'U' for the time history of the average constraint velocities along the directions: normal or given by the direction
- \* 'CR' for time histories like in the 'R' case, but for contact constraints only
- \* 'CU' for time histories like in the 'U' case, but for contact constraints only
- $\bullet~t0$  time interval start
- $\bullet$  **t1** time interval end
- skip number of steps to skip between two time instants
- progress 'ON' or 'OFF'; print out a percentage based progress bar (default: 'OFF'); useful for large output files and slow hard disks

## Chapter 5

# Viewer Scripts

Arbitrary scripts can be run from within the Viewer, using Tools -> Run Python Script or the "P" key. This brings up a dialog where a string should be entered to specify the script to run and any arguments. The string is split into sub-strings on white-space and the parts interpreted as follows:

- All parts are loaded into sys.argv
- The first part is assumed to be the path to the script, from the present working directory. A trailing ".py" is added if necessary.
- Python's execfile() is called to execute the script at this path. Note that code in this Viewer script runs as it if was actually defined in the analysis script, i.e. all names defined by the analysis script are available. It is *not* imported as a module see the Python documentation for further details. If no script is found at the specified path an error occurs.

At present the only commands which make much sense from within a Viewer script are either printing information about the analysis (e.g. len(solfec.bodies)) or using the RENDER() command to control what is displayed.

## Chapter 6

## **Tutorials**

## 6.1 Three basic geometric objects

This example illustrates the three basic geometric objects: CONVEX, MESH and SPHERE. We are going to construct a simple structure and hit it with a ball. Let us first create a horizontal floor.

We simply created a convex hull about eight points. This is only a geometric object for the moment. It exists only in Python interpreter, but not yet inside of a Solfec model. In order to insert it into a model, we need first to create a SOLFEC object, a BULK\_MATERIAL object, and finally a BODY object having the shape described by the *floor*. Here we go.

Note, that the floor is simply an obstacle - it does not move. Before creating the floor body we had to create a SOLFEC object. This object gather all necessary data for an individual simulation. In our case this will be a dynamic simulation, pursued with the time step at least as small as the specified one. The time step can be automatically decreased during a simulation due to stability requirements. The result files of this tutorial will

be written to the specified path - relative to from there the 'solfec' command was involved. Once a body has been inserted into a model, we can view the effect as follows

```
> ./solfec -v inp/tutorial/three-basic-geometric-objects.py
```

This will create a Solfec viewer, which should result in the following picture

t=0



Le us now construct a stack made of two bodies. The first one comprises four juxtaposed convex objects.

```
a = 2
b = 2
c = 2
brick\_vid = 2
brick\_sid = 2
brick = CONVEX ([0, 0, 0,
                 a/2, 0, 0,
                 a/2, b/2, 0,
                 0, b/2, 0,
                 0, 0, c/2,
                 a/2, 0, c/2,
                 a/2, b/2, c/2,
                 0, b/2, c/2],
                 [4, 0, 3, 2, 1, brick_sid,
                 4, 1, 2, 6, 5, brick_sid,
                 4, 2, 3, 7, 6, brick_sid,
                 4, 3, 0, 4, 7, brick_sid,
                 4, 0, 1, 5, 4, brick_sid,
                 4, 4, 5, 6, 7, brick_sid], brick_vid)
b1 = COPY (brick)
b2 = TRANSLATE (COPY (brick), (a, 0, 0))
b3 = TRANSLATE (COPY (brick), (0, b, 0))
```

```
b4 = TRANSLATE (COPY (brick), (a, b, 0))
shape = [b1, b2, b3, b4]
TRANSLATE (shape, (-a, -b, 0))
BODY (solfec, 'RIGID', shape, bulk)
```

Note, that a base brick was created first. Then this brick was copied and manipulated into four different objects: b1,b2, ..., b4. The list of those objects was passed as a shape when creating the first rigid body. The second body will be pseudo-rigid and will have its shape defined by a mesh.

The hexahedral mesh is spanned on eight nodes and has an inclined shape due to z level slope. Note, that we have specified the "dy" argument of the HEX command, so to illustrate non-uniform meshing along one of the directions. The mesh is translated to rest on top of the previous body. Then a pseudo-rigid body is created. Now, let us create the sphere.

```
sphere = SPHERE ((0, 0, 5), 1, 1, 1)
body = BODY (solfec, 'RIGID', sphere, bulk)
INITIAL_VELOCITY (body, (0, 0, -10), (0, 0, 0))
```

When creating the rigid body corresponding to the sphere, we have now retrieved the *body* object. It is needed in order to prescribe the initial velocity. The sphere has the initial linear velocity  $v_z = -10$  m/s. Let us have a look at the model so far.





Now, in order to be able to control contact behaviour, we need to define a surface material. This will be a default material, hence we shall not specify a surface pairing (int this example surface identifiers are not used). Whenever a contact is detected, the following Signorini-Coulomb model is employed

```
SURFACE_MATERIAL (solfec, model = 'SIGNORINI_COULOMB', friction = 0.5, restitution = 0.0)
```

It will be also of use to apply some gravity loading.

```
GRAVITY (solfec, (0, 0, -10))
```

Before running the actual simulation, it remains to create a solver object. We use the Gauss-Seidel solver here.

```
gs = GAUSS_SEIDEL_SOLVER (1E-3, 1000)
```

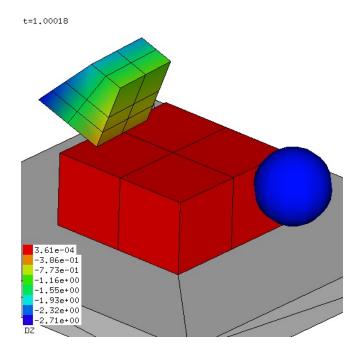
The relative constraint reaction accuracy was set to 1E-3, while the maximal the maximal number of iterations is 1000. It remains to run the simulation.

```
RUN (solfec, gs, 1.0)
```

And then actually run solfec from the command line

```
./solfec inp/tutorial/three-basic-geometric-objects.py
```

One second of the simulation was computed. Let us have a look at the displacement along z at the end of this time



## 6.2 Ball impact

This example illustrates using multiple SOLFEC objects, application of the PENALTY\_SOLVER, and using HISTORY to retrieve and then plot time histories. First we define a Python function that will create a model of ball impacting a plate for a specific set of parameters.

```
def ball_impact (step, stop, spring_value, dashpot_value, output):
  w = 2
 1 = 2
 h = 1
  floor_vid = 1
  floor_sid = 1
  floor = HULL ([-w/2, -1/2, -h],
                  w/2, -1/2, -h,
                  w/2, 1/2, -h,
                 -w/2, 1/2, -h,
                 -w/2, -1/2, 0,
                  w/2, -1/2, 0,
                  w/2, 1/2, 0,
                 -w/2, 1/2, 0], floor_vid, floor_sid)
  solfec = SOLFEC ('DYNAMIC', step, output)
  bulk = BULK_MATERIAL (solfec, model = 'KIRCHHOFF',
                        young = 15E9, poisson = 0.3, density = 2E3)
  BODY (solfec, 'OBSTACLE', floor, bulk)
  sphere = SPHERE ((0, 0, 1.0), 1, 1, 1)
  body = BODY (solfec, 'RIGID', sphere, bulk)
  INITIAL_VELOCITY (body, (0, 0, -5), (0, 0, 0))
  SURFACE_MATERIAL (solfec, model = 'SPRING_DASHPOT', friction = 0.0,
                    spring = spring_value, dashpot = dashpot_value)
  GRAVITY (solfec, (0, 0, -10))
  xs = PENALTY_SOLVER ()
  RUN (solfec, xs, stop)
  return solfec
```

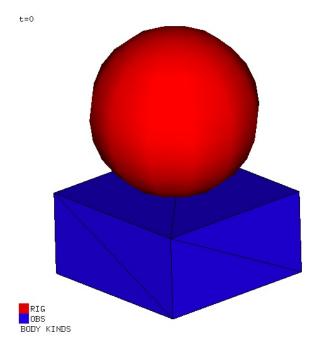
The above code is similar to the previous example. Here though the complete model is created inside of a Python function called <code>ball\_impact</code>. By itself this will not run any simulation - this function needs to be called from the main module of the input file (we remind that Python uses indentation to decide upon code blocking - in our case no indentation indicates the main module). Above the 'SPRING\_DASHPOT' material model is used for the contact interface. The parameters of the spring and damper are passed as arguments of the <code>ball\_impact</code> function. It should be noted, that the SOLFEC object is returned from the routine. Now, here is the main module

```
step = 1E-3
stop = 2.0
spring = 1E+9
sol1 = ball_impact (step, stop, spring, 0E0, 'out/tutorial/ball-impact-1')
sol2 = ball_impact (step, stop, spring, 1E6, 'out/tutorial/ball-impact-2')
sol3 = ball_impact (step, stop, spring, 1E7, 'out/tutorial/ball-impact-3')
```

We simply run three different simulations for three values of the dashpot parameter. We can now view the three models by typing

#### ./solfec -v ./inp/tutorial/ball-impact.py

The viewer allows change the current model by using '<' and '>' keyboard shortcuts, or using the right-mouse click for the drop-down menu and then selecting *menu: domain: previous* or *menu: domain: next*. In this example the three models do not visibly differ.



We could now run each model in the viewer mode (menu: analysis: run), but it will be more useful to plot kinetic energy and compare it for all the three values of the dashpot parameter. The code below does the job

```
if not VIEWER() and sol1.mode == 'READ':
   import matplotlib.pyplot as plt
   th = HISTORY (sol1, (sol1, 'KINETIC'), 0, stop)
   plt.plot (th [0], th [1], lw = 2, label='kin (0)')
   th = HISTORY (sol2, (sol2, 'KINETIC'), 0, stop)
   plt.plot (th [0], th [1], lw = 2, label='kin (1E6)')
   th = HISTORY (sol3, (sol3, 'KINETIC'), 0, stop)
   plt.plot (th [0], th [1], lw = 2, label='kin (1E7)')
   plt.axis (xmin = 0, xmax = 2, ymin=-10000, ymax=110000)
   plt.legend(loc = 'upper right')
   plt.savefig ('doc/figures/ball-impact.eps')
```

First, we check whether Solfec is not run with the -v option and whether it is in 'READ' mode. This is the case, when after running the complete analysis

```
./solfec ./inp/tutorial/ball-impact.py we again run
```

```
./solfec ./inp/tutorial/ball-impact.py
```

Now, Solfec will find out that the output files in out/tutorial/ball-impact-(1,2,3) are present. It will open in 'READ' mode. In order to create the plot we are going to use the matplotlib Python package - please refer to

http://matplotlib.sourceforge.net/index.html in order to learn how to install it. We next use the HISTORY command in order to retrieve the time histories of the kinetic energy for all three created SOLFEC objects. The result in plotted into an EPS file, visible below.



We can see that the dashpot=0 results in a fully elastic impact (energy conserving behaviour), dahspot=1E6 introduces some fractional energy restitution after impacts, while dashpot=1E7 results in a nearly plastic impact.

## Chapter 7

# Contact points

## 7.1 Contacts from overlaps

Body shapes are juxtapositions of convex objects (Sections 4.2.1, 4.2.2, 4.2.3). A contact point and normal direction result from an overlap of two convex objects (Figure 7.1). This is motivated by two factors. Firstly, the point and the normal direction derived from an overlap are well defined for nonsmooth geometry. Secondly, we wish to use as few contact points as possible, but still be able to control the accuracy of contact resolution by mesh refinement. A non-positive gap function is suitably derived from such overlap. We refer the reader to Chapter 9 of [?] for more details.

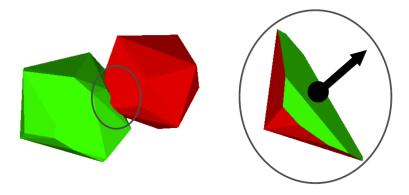


Figure 7.1: A contact point and normal direction extracted from an intersection of two convex objects.

## 7.2 Contact sparsification

Let us have a look at an arch in Figure 7.2. The detail of two bricks shows narrow meshing near the inner and outer boundaries. This will allow to better reproduce the hinging mechanism of arch collapse. A single brick is composed of six elements: the two large middle elements and the four narrow inner and outer elements. If we now apply contact detection algorithm, all possible volumetric overlaps will be detected. Because identically meshed bodies are perfectly adjacent to each other we shall end up with a clutter of contact points, generated by all of the adjacent element volumes. This is visible on the left in Figure 7.3. If one would have to generate contact points by hand, they would probably look like those on the right in Figure 7.3. A heuristic sparsification algorithm filters out redundant contact points (cf. Algorithm 7.1).

#### Algorithm 7.1 Contact sparsification algorithm.

```
SPARSIFY ()
  for each contact1 do
    for each body adjacent to contact1 do
    for each contact2 adjacent to body do
       if contact1 = contact2 skip
       if area (contact1) < threshold · area (contact2) and
            topologically_adjacent (contact1, contact2) then remove contact1
       else if point (contact1) = point (contact2) then remove contact1</pre>
```

We walk over all contact points and compare each of them with other contacts adjacent through common bodies. If the area of a contact is a smaller than an area of a topologically adjacent neighbouring contact, then we remove it. The same happens if the two contact points coincide. Topological adjacency of contact points indicates that they have been created between the mesh elements that are topologically adjacent. We know then, that next to a contact point with a small supporting area there is another one with a suitably larger contact area. The Solfec command CONTACT\_SPARSIFY sets the *threshold* value (cf. Section 4.6).



Figure 7.2: An arch and a detail of two bricks. Note the narrow meshing near the edge of inner and outer boundaries.



Figure 7.3: A detail of the arch from Figure 7.2. Contact points on the left are not sparsified. Contact points on the right are sparsified.

## Chapter 8

## Materials

#### 8.1 Surface materials

A surface material is assigned to a pairing of surfaces. See Section 4.2.7 for the input syntax.

#### 8.1.1 Signorini-Coulomb

The velocity Signorini condition reads

$$\bar{U}_N \ge 0 \ R_N \ge 0 \ \bar{U}_N R_N = 0$$
 (8.1)

where  $\bar{U}_N = U_N^{t+h} + \eta \min{(0, U_N^t)}$ ,  $\eta$  is the velocity restitution coefficient,  $U_N$  is the normal relative velocity, and  $R_N$  is the normal reaction. The normal direction is consistent with the positive gap velocity so that (8.1) states, that any violation of the non-penetration results in a reactive force or velocity driving at the penetration-free configuration. Using  $\bar{U}_N$  allows to account for the Newton impact law. Only restitution = 0 or 1 is energy consistent TODO (cf. Section 10.5 of [?]). The Coulomb's friction law reads

$$\begin{cases}
\|\mathbf{R}_T\| \le \mu R_N \\
\|\mathbf{R}_T\| < \mu R_N \Rightarrow \mathbf{U}_T = \mathbf{0} \\
\|\mathbf{R}_T\| = \mu R_N \Rightarrow \exists_{\lambda \ge 0} \mathbf{U}_T = -\lambda \mathbf{R}_T
\end{cases}$$
(8.2)

A friction force smaller than  $\mu R_N$  implies sticking, while sliding occurs with the force of value  $\mu R_N$  and direction opposite to the slip velocity. The two laws can expressed in a compact from  $\mathbf{C}(\mathbf{U}, \mathbf{R}) = \mathbf{0}$ . An examples is

$$\mathbf{C}(\mathbf{U}, \mathbf{R}) = \begin{bmatrix} \max(\mu d_N, \|\mathbf{d}_T\|) \mathbf{R}_T - \mu \max(0, d_N) \mathbf{d}_T \\ R_N - \max(0, d_N) \end{bmatrix}$$
(8.3)

where

$$d_N = R_N - \rho \bar{U}_N \tag{8.4}$$

$$\mathbf{d}_T = \mathbf{R}_T - \rho \mathbf{U}_T \tag{8.5}$$

and  $\rho > 0$ . We refer the reader to Chapter 10 of [?] for more details.

#### 8.1.2 Spring-dashpot

Let

$$s = spring \text{ and } d = dashpot \text{ and } g = gap \text{ and } m = hpow$$
 (8.6)

The normal reaction is computed as follows

$$R_N = -s \cdot \frac{g^{t+h} + g^t}{2} - d \cdot \frac{U_N^{t+h} + U_N^t}{2}$$
(8.7)

where  $U_N$  is the normal relative velocity. Recall, that the gap function is computed for the configuration  $\mathbf{q}^t + \frac{h}{2}\mathbf{u}^t$ , so that the gap function value computed during geometrical contact detection reads

$$g = g^t + \frac{h}{2}U_N^t \tag{8.8}$$

We then have

$$g^{t+h} = g^t + \frac{h}{2} \left( U_N^{t+h} + U_N^t \right) = g + \frac{h}{2} U_N^{t+h}$$
(8.9)

and since  $g^t = g - \frac{h}{2}U_N^t$  we can estimate

$$R_N = -s \cdot \left( g + \frac{h}{4} \left( U_N^{t+h} - U_N^t \right) \right) - \frac{d}{2} \cdot \left( U_N^{t+h} + U_N^t \right)$$
 (8.10)

We then use the diagonal block of local dynamics

$$\mathbf{U}^{t+h} = \mathbf{B} + \mathbf{WR} \tag{8.11}$$

in order to estimate  $U_N^{t+h}$  as follows

$$U_N^{t+h} = B_N + \mathbf{W}_{NT} \mathbf{R}_T + W_{NN} R_N \tag{8.12}$$

where a previous tangential reaction  $\mathbf{R}_T$  is employed. Inserting this it into (8.10) results in

$$\bar{B}_N = B_N + \mathbf{W}_{NT} \mathbf{R}_T \tag{8.13}$$

$$R_N = \left[ -s \cdot \left( g + \frac{h}{4} \left( \bar{B}_N - U_N^t \right) \right) - \frac{d}{2} \cdot \left( \bar{B}_N + U_N^t \right) \right] / \left[ 1 + \left( s \cdot \frac{h}{4} + \frac{d}{2} \right) \cdot W_{NN} \right]$$
(8.14)

The reason for using the above, rather than the classical  $R_N = -s \cdot g - d \cdot U_N^t$  is in an increased stability of the current approach. Since we aim at simplicity and want to avoid any nonlinear solve only at this stage we include the Hertz law power

$$g_1 = \min\left(g + \frac{h}{4}\left(\bar{B}_N - U_N^t\right), 0\right)$$

$$s_1 = sm \left( -g_1 \right)^{m-1}$$

$$R_{N} = \left[ s \cdot (-g_{1})^{m} - \frac{d}{2} \cdot (\bar{B}_{N} + U_{N}^{t}) \right] / \left[ 1 + \left( s_{1} \cdot \frac{h}{4} + \frac{d}{2} \right) \cdot W_{NN} \right]$$

Again aiming at maximum simplicity and assuming  $\mathbf{U}_{T}^{t+h} = 0$  we then estimate the tangential stick reaction

$$\mathbf{R}_T = -\mathbf{W}_{TT}^{-1} \left( \mathbf{B}_T + \mathbf{W}_{TN} R_N \right) \tag{8.15}$$

The complete interface law is expressed in Algorithm 8.1 ( $\mu$  refers there to the coefficient of friction). We refer the reader to Chapter 7 of [?] for more details on local dynamics.

#### 8.2 Bulk materials

A bulk material is assigned to a volume. See Section 4.2.8 for the input syntax.

#### 8.2.1 Kirchhoff - Saint Venant

This is a simple extension of the linearly elastic material to the large deformation regime. Suitable for large rotation, small strain problems. The strain energy function  $\Psi$  of the Kirchhoff - Saint Venant materials reads

$$\Psi = \frac{1}{4} \left[ \mathbf{F}^T \mathbf{F} - \mathbf{I} \right] : \mathbf{C} : \left[ \mathbf{F}^T \mathbf{F} - \mathbf{I} \right]$$
 (8.16)

where

$$C_{ijkl} = \lambda \delta_{ij} \delta_{kl} + \mu \left[ \delta_{ik} \delta_{jl} + \delta_{il} \delta_{jk} \right] \tag{8.17}$$

In the above  $\lambda$  and  $\mu$  are Lamé constants, while  $\delta_{ij}$  is the Kronecker delta. The Lamé constants can be expressed in terms of the Young modulus E and the Poisson ratio  $\nu$  as

$$\lambda = \frac{E\nu}{(1+\nu)(1-2\nu)} \tag{8.18}$$

$$\mu = \frac{E}{2 + 2\nu} \tag{8.19}$$

The first Piola stress tensor is computed as a gradient of the hyperelastic potential  $\Psi$ 

$$\mathbf{P} = \partial_{\mathbf{F}} \Psi \left( \mathbf{F} \right) \tag{8.20}$$

where  $\mathbf{F}$  is the deformation gradient.

#### Algorithm 8.1 Spring-dashpot reaction calculation.

```
\begin{split} & \text{SPRING\_DASHPOT} \ (h,g,s,d,\mu,cohesion,cohesive) \\ & \bar{B}_N = B_N + \mathbf{W}_{NT} \mathbf{R}_T \\ & \text{if implicit then} \\ & g_1 = \min \left(g + \frac{h}{4} \left(\bar{B}_N - U_N^t\right), 0\right) \\ & s_1 = sm \left(-g_1\right)^{m-1} \\ & R_N = \left[s \cdot \left(-g_1\right)^m - \frac{d}{2} \cdot \left(\bar{B}_N + U_N^t\right)\right] / \left[1 + \left(s_1 \cdot \frac{h}{4} + \frac{d}{2}\right) \cdot W_{NN}\right] \\ & \text{else } R_N = s \cdot \left(-\min \left(g,0\right)\right)^m - d \cdot U_N^t \\ & \text{if not } cohesive \text{ and } R_N < 0 \text{ then } \mathbf{R} = 0 \text{ return} \\ & \mathbf{R}_T = -\mathbf{W}_{TT}^{-1} (\mathbf{B}_T + \mathbf{W}_{TN} R_N) \\ & \text{if } cohesive \text{ and } R_N < -cohesion \text{ then } cohesive = false \text{ and } R_N = -cohesion \\ & \text{if } \|\mathbf{R}_T\| > \mu \, |R_N| \text{ then} \\ & \mathbf{R}_T = \mu R_N \mathbf{R}_T / \|\mathbf{R}_T\| \\ & \text{if } cohesive \text{ then } cohesive = false \end{split}
```

## Chapter 9

## Constraints accuracy

As explained in Chapter 1, at every time step an implicit equation  $\mathbf{C}(\mathbf{R}) = \mathbf{0}$  is solved. Ideally, when for some  $\mathbf{R}$  there holds  $\mathbf{C}(\mathbf{R}) = \mathbf{0}$  we have an exact solution. Of course, in numerical terms this is not possible. For very large problems, and especially for problems where the amount of constraints exceeds the amount of kinematic freedom, obtaining very accurate solutions is hard and often impractical. In any case, it is useful to have an accuracy measure that has some physical interpretation. In order to compute constraints accuracy, we formulate  $\mathbf{C}(\mathbf{R})$  in terms of velocity (cf. Section 9.1 for the Signorini-Coulomb law) and use

$$g(\mathbf{R}) = \sum_{\alpha} \langle \mathbf{W}_{\alpha\alpha}^{-1} \mathbf{C}_{\alpha} (\mathbf{R}), \mathbf{C}_{\alpha} (\mathbf{R}) \rangle / \sum_{\alpha} \langle \mathbf{W}_{\alpha\alpha}^{-1} \mathbf{B}_{\alpha}, \mathbf{B}_{\alpha} \rangle$$
(9.1)

in order to approximately measure the relative amount of spurious energy, due to an inexact satisfaction of constraints. The denominator corresponds to the kinetic energy of the relative free motion, hence  $g(\mathbf{R})$  is the ratio of the spurious energy over the nominal amount of the energy available at the constraints. Since inverting  $\mathbf{W}$  would be unpractical or impossible due to singularity, we only use the diagonal blocks, which are always positive definite. To recapitulate, in short

$$g(\mathbf{R}) \simeq \frac{\text{spurious energy due to inaccurate solution}}{\text{free energy available at the constraints}}$$
 (9.2)

## 9.1 Signorini-Coulomb revisited

We express the Signorini-Coulomb law defined in Section 8.1.1 in the form suitable for (9.1). The friction cone  $K_{\alpha}$  is defined as

$$K_{\alpha} = \{ \mathbf{R}_{\alpha} : \| \mathbf{R}_{\alpha T} \| \le \mu_{\alpha} R_{\alpha N}, R_{\alpha N} \ge 0 \}$$

$$(9.3)$$

where  $\mu_{\alpha}$  is the coefficient of friction. It has been shown by De Saxcé and Feng [4], that the Signorini-Coulomb law can be expressed in a compact form

$$-\left[\begin{array}{c}\mathbf{U}_{\alpha T}\\\bar{U}_{\alpha N}+\mu_{\alpha}\|\mathbf{U}_{\alpha T}\|\end{array}\right]\in N_{K_{\alpha}}\left(\mathbf{R}_{\alpha}\right)$$
(9.4)

where  $N_{K_{\alpha}}$  stands for the normal cone of the set  $K_{\alpha}$ . For a convex set A the normal cone  $N_A(\mathbf{R})$  at point  $\mathbf{R} \in A$  is defined as the set of all vectors  $\mathbf{V}$  such that  $\langle \mathbf{V}, \mathbf{S} - \mathbf{R} \rangle \leq 0$  for all  $\mathbf{S} \in A$ . Let

$$\mathbf{F}(\mathbf{R}) = \begin{bmatrix} \dots \\ \mathbf{U}_{\alpha T}(\mathbf{R}) \\ \bar{U}_{\alpha N}(\mathbf{R}) + \mu_{\alpha} \|\mathbf{U}_{\alpha T}(\mathbf{R})\| \\ \dots \end{bmatrix}$$
(9.5)

and

$$K = \bigcup_{\alpha} K_{\alpha} \tag{9.6}$$

where the dependence  $\mathbf{U}_{\alpha}(\mathbf{R})$  is defined in (1.14). Formula (9.4) states, that the frictional contact constraints are satisfied if  $-\mathbf{F}(\mathbf{R})$  belongs to the normal cone of the friction cone at  $\mathbf{R}$ . Hence

$$-\mathbf{F}(\mathbf{R}) = \mathbf{R} - \mathbf{F}(\mathbf{R}) - \operatorname{proj}_{K}(\mathbf{R} - \mathbf{F}(\mathbf{R}))$$
(9.7)

which can be reduced to the usual projection formula  $\mathbf{R} = \operatorname{proj}_K(\mathbf{R} - \mathbf{F}(\mathbf{R}))$ . Let us not do it though, but rather define a vector field

$$\mathbf{m}(\mathbf{S}) = \mathbf{S} - \operatorname{proj}_{K}(\mathbf{S}) = \mathbf{n}(\mathbf{S}) \langle \mathbf{n}(\mathbf{S}), \mathbf{S} \rangle$$
 (9.8)

where

$$\mathbf{n}_{\alpha}\left(\mathbf{S}_{\alpha}\right) = \begin{cases} \mathbf{0} & \text{if } \|\mathbf{S}_{\alpha T}\| - \mu_{\alpha} S_{\alpha N} \leq 0\\ \mathbf{S}_{\alpha} / \|\mathbf{S}_{\alpha}\| & \text{if } \mu_{\alpha} \|\mathbf{S}_{\alpha T}\| + S_{\alpha N} < 0\\ \frac{1}{\sqrt{1 + \mu_{\alpha}^{2}}} \begin{bmatrix} \mathbf{S}_{\alpha T} / \|\mathbf{S}_{\alpha T}\| \\ -\mu_{\alpha} \end{bmatrix} & \text{otherwise} \end{cases}$$
(9.9)

We can rewrite (9.4) as

$$C(R) = F(R) + m(R - F(R)) = 0 \text{ and } R \in K$$
 (9.10)

Note, that  $F(\mathbf{R})$  is expressed in terms of velocity, and so is  $C(\mathbf{R})$ .

## Chapter 10

## Solvers

Development of solvers for unilateral dynamics is one of the main driving forces behind Solfec. The two solvers described in Sections 10.1 and 10.2 are the classical Gauss-Seidel approach of Contact Dynamics and a somewhat modified penalty solver of the Discrete Element Method. The projected quasi-Newton solver from Section 10.3 has been designed specifically for Solfec.

### 10.1 Gauss-Seidel solver

The equations of local dynamics (1.14) read

$$\mathbf{U}_{\alpha} = \mathbf{B}_{\alpha} + \sum_{\beta} \mathbf{W}_{\alpha\beta} \mathbf{R}_{\beta} \tag{10.1}$$

where  $\mathbf{U}_{\alpha}$  are relative velocities and  $\mathbf{R}_{\alpha}$  are reactions at constraint points.  $\mathbf{U}_{\alpha}, \mathbf{R}_{\alpha}, \mathbf{B}_{\alpha}$  are 3-vectors, while  $\mathbf{W}_{\alpha\beta}$  are  $3 \times 3$  matrix blocks. Each constraint equation can be formulated as

$$\mathbf{C}_{\alpha}\left(\mathbf{U}_{\alpha}, \mathbf{R}_{\alpha}\right) = \mathbf{0} \tag{10.2}$$

or in other words

$$\mathbf{C}_{\alpha} \left( \mathbf{B}_{\alpha} + \sum_{\beta} \mathbf{W}_{\alpha\beta} \mathbf{R}_{\beta}, \mathbf{R}_{\alpha} \right) = \mathbf{0}$$
 (10.3)

Algorithm 10.1 is quite simple: diagonal block problems are solved until reaction change is small enough. The Gauss-Seidel paradigm corresponds to the fact, that the most recent off-diagonal reactions are used when solving the diagonal problem. Of course, because of that, a perfectly parallel implementation is not possible. After all, reactions are updated in a sequence. We can nevertheless relax the need for sequential processing.

#### Algorithm 10.1 Serial Gauss-Seidel algorithm

```
SERIAL_GAUSS_SEIDEL (Constraints, \epsilon, \gamma)
1 do
2 for each \alpha in Constraints do
3 \mathbf{S}_{\alpha} = \mathbf{R}_{\alpha}
4 find \mathbf{R}_{\alpha} such that \mathbf{C}_{\alpha} \left( \mathbf{B}_{\alpha} + \sum_{\beta} \mathbf{W}_{\alpha\beta} \mathbf{R}_{\beta}, \mathbf{R}_{\alpha} \right) = \mathbf{0}
5 assuming \mathbf{R}_{\beta} = \mathrm{constant} for \beta \neq \alpha
6 while \|\mathbf{S} - \mathbf{R}\| / \|\mathbf{R}\| > \epsilon and g(\mathbf{R}) > \gamma
```

#### Algorithm 10.2 Simple processor coloring.

```
COLOR ()  \begin{array}{llll} & \text{1 for } i=1,...,n \text{ do } color\left[i\right]=0 \\ & \text{2 for } i=1,...,n \text{ do} \\ & \text{3 do} \\ & & & color\left[i\right]=color\left[i\right]+1 \\ & \text{5 while for any } j\in adj\left(i\right) \text{ there holds } color\left[i\right]=color\left[j\right] \\ \end{array}
```

Perhaps the most scalable Gauss-Seidel approach to date was devised by Adams [2]. Although originally it was used as a multi-grid smoother, the core idea can be as well applied in our context. Each processor owes a subset of (internal) constraints  $Q_i$ , where i = 1, 2, ..., n are the processors indices. Therefore the local velocity update can be rewritten as

$$\mathbf{U}_{\alpha} = \mathbf{B}_{\alpha} + \sum_{\beta \in Q_i} \mathbf{W}_{\alpha\beta} \mathbf{R}_{\beta} + \sum_{\beta \notin Q_i} \mathbf{W}_{\alpha\beta} \mathbf{R}_{\beta}$$
 (10.4)

Some of the  $\mathbf{W}_{\alpha\beta}$  blocks and reactions  $\mathbf{R}_{\beta}$  correspond to the (external) constraints stored on other processors  $(\beta \notin Q_i)$ . Let us denote the set of corresponding reaction indices by  $P_i$ . That is

$$P_i = \{\beta : \exists \mathbf{W}_{\alpha\beta} \neq \mathbf{0} \text{ and } \alpha \in Q_i \text{ and } \beta \notin Q_i\}$$
 (10.5)

For each  $\beta \in P_i$  we know an index of processor  $cpu(\beta)$  storing the constraint with index  $\beta$ . For processor i we can then define a set of adjacent processors as follows

$$adj(i) = \{cpu(\beta) : \beta \in P_i\}$$
(10.6)

When updating reactions, a processor needs to communicate only with other adjacent processors. We are going to optimise a pattern of this communication by *coloring* the processors. We shall then assign to each processor a color, such that no two adjacent processors have the same color. A simple coloring method is summarised in Algorithm 10.2. We try to assign as few colors as possible. We then split the index sets  $Q_i$  as follows

$$Top_{i} = \{\alpha : \forall \mathbf{W}_{\alpha\beta} : \beta \in P_{i} \land color [cpu (\beta)] < color [i]\}$$

$$(10.7)$$

$$Bottom_{i} = \{\alpha : \forall \mathbf{W}_{\alpha\beta} : \beta \in P_{i} \land color [cpu(\beta)] > color [i] \}$$

$$(10.8)$$

$$Middle_i = \{\alpha : \forall \mathbf{W}_{\alpha\beta} : \beta \in P_i \land \alpha \notin Top_i \cup Bottom_i\}$$
 (10.9)

$$Inner_i = Q_i \setminus \{Top_i \cup Bottom_i \cup Middle_i\}$$
 (10.10)

The top constraints require communication only with processors of lower colors. The bottom constraints require communication only with processors of higher colors. The middle constraints require communication with either. The inner constraints require no communication. The inner reactions are further split in two sets

$$Inner_i = Inner1_i \cup Inner2_i \tag{10.11}$$

so that

$$|Bottom_i| + |Inner2_i| = |Top_i| + |Inner1_i|$$
(10.12)

The parallel Gauss-Seidel scheme is summarised in Algorithm 10.3. The presented version is simplified in the respect, that alternate forward and backward runs are not accounted for (in terms of constraints ordering).

#### Algorithm 10.3 Parallel Gauss-Seidel algorithm.

```
SWEEP (Set)
    for each \alpha \in Set do
         find \mathbf{R}_{lpha} such that \mathbf{C}_{lpha}\left(\mathbf{B}_{lpha}+\sum_{eta}\mathbf{W}_{lphaeta}\mathbf{R}_{eta},\mathbf{R}_{lpha}\right)=\mathbf{0} assuming \mathbf{R}_{eta}= constant for eta
eq lpha
3
LOOP (Set)
    descending sort of \alpha \in Set based on \max(color[cpu(\beta)]) where \exists \mathbf{W}_{\alpha\beta}
     for each ordered \alpha in Set do
          for each \beta such that \exists \mathbf{W}_{\alpha\beta} and color\left[cpu\left(\alpha\right)\right] < color\left[cpu\left(\beta\right)\right] do
3
              if not received (\mathbf{R}_{eta}) then receive (\mathbf{R}_{eta})
4
         find \mathbf{R}_{\alpha} such that \mathbf{C}_{\alpha}\left(\mathbf{B}_{\alpha}+\sum_{\beta}\mathbf{W}_{\alpha\beta}\mathbf{R}_{\beta},\mathbf{R}_{\alpha}\right)=\mathbf{0} assuming \mathbf{R}_{\beta}= constant for \beta\neq\alpha
5
6
7
         send (\mathbf{R}_{lpha})
     receive all remaining \mathbf{R}_{eta}
PARALLEL_GAUSS_SEIDEL (\epsilon,\gamma)
       COLOR ()
1
2
       do
3
            S = R
           SWEEP (Top_i)
4
           send (Top_i)
5
           SWEEP (Inner2_i)
6
7
           receive (Top_i)
           LOOP (Middle_i)
8
           SWEEP (Bottom_i)
9
10
           send (Bottom_i)
11
           SWEEP (Inner1_i)
12
           receive (Bottom_i)
13 while \|\mathbf{S} - \mathbf{R}\| / \|\mathbf{R}\| > \epsilon and g(\mathbf{R}) > \gamma
```

We first process the  $Top_i$  set: a single sweep over the corresponding diagonal block problems is performed in line 3. Then we send the computed top reactions to the processors with lower colors. We try to overlap communication and computation, hence we sweep over the  $Inner2_i$  set (line 5) while sending. We then receive the top reactions. It should be noted that all communication is asynchronous - we only wait to receive reactions immediately necessary for computations. In line 7 we enter the loop processing the  $Middle_i$  set. This is the location of the computational bottleneck. Middle nodes communicate with processors of higher and lower colors and hence, they need to be processed in a sequence. The sequential processing is still relaxed by using processor coloring. In the LOOP algorithm we first sort the constraints according to the descending order of maximal colors of their adjacent processors (line 1). We then maintain this ordering while processing constraints. As the top reactions were already sent, some of the constraints from the middle set will have their external reactions from higher colors fully updated. These will be processed first in line 5 of LOOP and then sent to lower and higher (by color) processors in line 7. This way some processors with lower colors will have their higher color off-diagonal reactions of middle set constraints fully updated and they will proceed next. And so on. At the end (line 8), we need to receive all remaining reactions that have been sent in line 7 of LOOP. Coming back to PARALLEL GAUSS SEIDEL, after the bottleneck of the LOOP, in lines 8-11 we process the  $Bottom_i$  and  $Inner1_i$  sets in the same way as we did with the  $Top_i$  and  $Inner2_i$  sets. The condition (10.12) attempts to balance the amount of computations needed to hide the communication (e.g. the larger the  $Top_i$  set is, the larger the  $Inner2_i$  set becomes). It should be noted that the convergence criterion in line 12 is global across all processors.

In Section 4.2.11 several variants of the parallel algorithm are listed. Algorithm 10.3 corresponds to the FULL variant. We might like to relax the bottleneck of LOOP in line 7 of Algorithm 10.3 by replacing it with

```
7.1 SWEEP (Middle_i)
```

- 7.2 send  $(Middle_i)$
- 7.3 receive  $(Middle_i)$

so that the middle nodes are processed in an inconsistent manner: the off-processor information corresponds to the previous iteration (just like in the Jacobi method). Usually the  $Middle_i$  sets are small and hence this inconsistency does not have to lead to divergence (especially for deformable kinematics, where constraint interactions are weak, while  $\mathbf{W}$  is diagonally dominant). This is the MIDDLE\_JACOBI variant of the algorithm. The last variant corresponds to a rather gross inconsistency: something usually called "a processor Gauss-Seidel method". Let us define the set

$$All_i = Top_i \cup Bottom_i \cup Middle_i \cup Inner_i$$
 (10.13)

In this case, lines 3-11 of PARALLEL GAUSS SEIDEL from Algorithm 10.3 need to be replaced with

```
3 SWEEP (All_i)
```

- 4 send  $(All_i)$
- 5 receive  $(All_i)$

Although this kind of approach does work as a multi-grid smoother, it has little use in our context. Nevertheless, we use it for illustration sake and name the BOUNDARY JACOBI.

## 10.2 Penalty solver

The penalty solver is quite straightforward. On each processor we split the constraints into  $Contacts_i$  and  $Others_i$ , hence we separate contact constraints from bilateral ones. We then update the contacts using the spring-dashpot model and calculate reactions of bilateral constraints using the Gauss-Seidel solver (fixed accuracy epsilon=1E-4, maxiter = 1000 is used). We use the Gauss-Seidel approach for non-contacts because in this case it is quite fast, while it avoids issues related to penalisation of bilateral constraints. Algorithm 10.4 summarises the method.

#### Algorithm 10.4 Parallel penalty solver.

PARALLEL\_PENALTY\_SOLVER ()

- 1 for all  $\alpha$  in  $Contacts_i$  do
- 2 SPRING\_DASHPOT  $(h, gap_{\alpha}, spring_{\alpha}, dashpot_{\alpha}, friction_{\alpha}, cohesion_{\alpha}, cohesive_{\alpha})$
- 3 send  $(Contacts_i)$
- 4 receive  $(Contacts_i)$
- 5 GAUSS\_SEIDEL  $(Others_i)$

## 10.3 Projected quasi-Newton solver

Let us rewrite the frictional contact problem (9.10) once again

$$C(R) = F(R) + m(R - F(R)) = 0 \text{ and } R \in K$$
 (10.14)

where K is the direct sum of friction cones at all contact points. Since  $\mathbf{C}(\mathbf{R})$  is not smooth, to compute  $\nabla \mathbf{C}$  we generalize the approach from [5], where only the self-dual case (friction coefficient equal to 1) was considered. Our idea is to employ the following projected quasi-Newton step

$$\mathbf{R}^{k+1} = \operatorname{proj}_{K} \left[ \mathbf{R}^{k} - \mathbf{A}^{-1} \mathbf{C} \left( \mathbf{R} \right) \right]$$
(10.15)

so that, as required, the iterates remain within the friction cone and where

$$\mathbf{A} \simeq \nabla \mathbf{C} \tag{10.16}$$

is an easy to invert approximation of  $\nabla \mathbf{C}$ . Since in many practical situations  $\nabla \mathbf{C}$  is singular, we cannot hope to employ  $\nabla \mathbf{C}$ . We then employ two variants of  $\mathbf{A} \simeq \nabla \mathbf{C}$ . The first one reads

$$\mathbf{A}_1 = \nabla \mathbf{C} + \delta \mathbf{I}$$
, combined with GMRES. (10.17)

where  $\delta \geq 0$ . This is related to numerical integration of an artificial ODE

$$\frac{d\mathbf{R}}{dt} = \mathbf{C}(\mathbf{R}) \tag{10.18}$$

to a steady state (take one step of implicit Euler, in the literature this is called *pseudo-transient continuation*). The second variant reads

$$\mathbf{A}_2 = \operatorname{diag}_{3\times 3} [\nabla \mathbf{C}], \text{ combined with direct inversion.}$$
 (10.19)

and it is combined with a heuristic stabilization technique

$$\Delta \mathbf{R}^{k+1} = (1-\theta) \Delta \mathbf{R}^k - \theta \left(\mathbf{A}^k\right)^{-1} \mathbf{C}^k$$
(10.20)

where

$$\theta \in [0,1]. \tag{10.21}$$

We then have two variants of the projected quasi-Newton step:

1. PQN1 (cf. Algorithm 10.5):

$$\mathbf{R}^{k+1} = \operatorname{proj}_{K} \left[ \mathbf{R}^{k} - \left( \nabla \mathbf{C}^{k} + \delta \mathbf{I} \right)_{\mathrm{GMRES}(\epsilon \parallel \mathbf{C}^{k} \parallel, m)}^{-1} \mathbf{C}^{k} \right]$$

where GMRES is preconditioned with  $\left[\operatorname{diag}_{3\times3}\left(\nabla\mathbf{C}_{\alpha\alpha}^{k}+\delta\mathbf{I}\right)\right]^{-1}$  and  $\delta$ ,  $\epsilon$  and m need to be suitably selected. The linear problem should be solved only roughly, usually  $\epsilon=0.25$  and m=10 (iterations bound)

Algorithm 10.5 The projected quasi-Newton method with GMRES. Use linver = 'GMRES' in NEW-TON\_SOLVER to enable this variant (this is the default).

**PQN1**( $\mathbf{R}, \gamma, n, \omega, \delta, m, \epsilon$ ):

- 1.  $\triangle \mathbf{R}^0 = \mathbf{0}, k = 0.$
- 2. Do
  - (a)  $\mathbf{U}^k = \mathbf{W}\mathbf{R}^k + \mathbf{B}$ .
  - (b) Compute  $\mathbf{C}^k$  and  $\mathbf{A}^k = \nabla \mathbf{C}_{\alpha\alpha}^k + \delta \mathbf{I}$  using smoothing  $\omega$ .
  - (c)  $\triangle \mathbf{R}^{k+1} = -\left(\mathbf{A}^{k}\right)_{\text{GMRES}(\epsilon \parallel \mathbf{C}^{k} \parallel, m)}^{-1} \mathbf{C}^{k}$ .
  - (d)  $\mathbf{R}^{k+1} = \operatorname{proj}_K \left[ \mathbf{R}^k + \triangle \mathbf{R}^{k+1} \right].$
  - (e) k = k + 1.

while  $g(\mathbf{R}^k) \ge \gamma$  and k < n.

work well. For ill-conditioned problems a too accurate solution of the linear sub-problem results in a poor convergence rate. The diagonal regularization  $\delta$  needs to be adjusted "by hand". The automatic update formulas that can be found in literature work only for well-conditioned cases and hence they are not very useful for us. For ill-conditioned problems one should pick  $\delta$  that delivers an overall best convergence behavior. Large values will slow down convergence, but stabilize it; small values may destabilize convergence for ill-conditioned problems;  $\delta$  (typically  $\ll 1$ ) should be tuned together with  $\epsilon$  and m (e.g. find a suitably small  $\delta$  first, then tweak  $\epsilon$ ). Since rigorous analysis is still missing for these parameters, please experiment before settling on specific values for a specific problem. Use linver = 'GMRES' in NEWTON\_SOLVER to enable this variant (this is the default).

2. PQN2 (cf. Algorithm 10.6):

$$\mathbf{R}^{k+1} = \operatorname{proj}_{K} \left[ \mathbf{R}^{k} + (1 - \theta) \triangle \mathbf{R}^{k} - \theta \left( \operatorname{diag}_{3 \times 3} \left[ \nabla \mathbf{C}^{k} \right] \right)^{-1} \mathbf{C}^{k} \right]$$

where  $\theta \in [0,1]$  and the diagonal  $3 \times 3$  blocks of  $\nabla \mathbf{C}^k$  are directly inverted. This simple scheme is interesting because it converges for a sufficiently small  $\theta$ , while it is essentially a nonlinear Jacobi-type method. Use linver = 'DIAG' in NEWTON SOLVER to enable this variant.

Algorithm 10.6 The projected quasi-Newton method with diagonal direct solve and averaging. Use linver = 'DIAG' in NEWTON SOLVER to enable this variant.

 $\overline{\mathbf{PQN2}(\mathbf{R}, \theta, \gamma, n, \omega)}$ :

1. 
$$\triangle \mathbf{R}^0 = \mathbf{0}, k = 0.$$

2. Do

(a) 
$$\mathbf{U}^k = \mathbf{W}\mathbf{R}^k + \mathbf{B}$$
.

(b) Compute 
$$\mathbf{C}^k$$
 and  $\mathbf{A}^k = \operatorname{diag}_{3\times 3} \left[ \nabla \mathbf{C}_{\alpha\alpha}^k \right]$  using smoothing  $\omega$ .

(c) 
$$\triangle \mathbf{R}^{k+1} = (1-\theta) \triangle \mathbf{R}^k - \theta (\mathbf{A}^k)^{-1} \mathbf{C}^k$$
.

(d) 
$$\mathbf{R}^{k+1} = \operatorname{proj}_K \left[ \mathbf{R}^k + \triangle \mathbf{R}^{k+1} \right]$$
.

(e) 
$$k = k + 1$$
.

while  $g(\mathbf{R}^k) \ge \gamma$  and k < n.

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