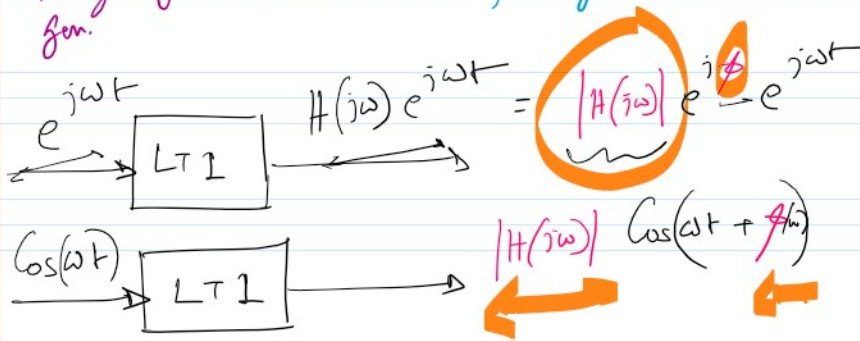


$$\cos(\omega t) = \frac{1}{2} [e^{j\omega t} + e^{-j\omega t}]$$

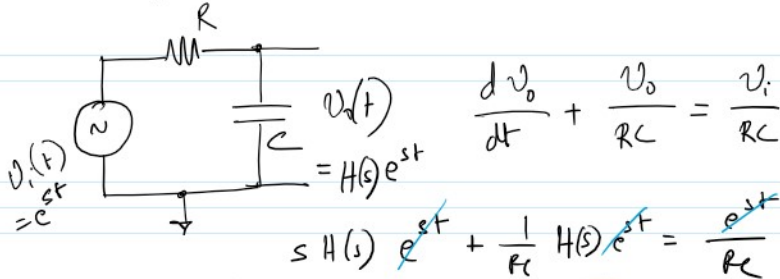
$$\sin(\omega t) = \frac{1}{2} [e^{j\omega t} - e^{-j\omega t}]$$

Can be applied through signal gen.

Cannot be applied through sig. gen BUT convenient for analysis.



Example:



$$s H(s) e^{st} + \frac{1}{RC} H(s) e^{st} = \frac{e^{st}}{RC}$$

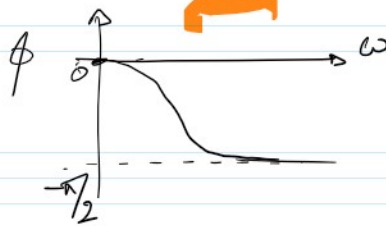
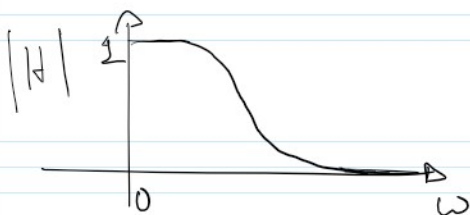
$$\Rightarrow H(s) = \frac{1}{1 + sRC}$$

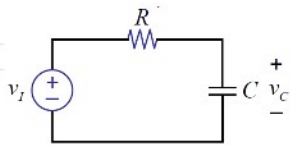
$$H(j\omega) = \frac{1}{1 + j\omega RC}$$

$$|H(j\omega)| = \frac{1}{\sqrt{1 + \omega^2 R^2 C^2}}$$

$$\phi = \tan^{-1} \frac{\text{Im}(H)}{\text{Re}(H)}$$

$$= -\tan^{-1}(\omega RC)$$





$$H(j\omega) = \frac{1}{1 + j\omega RC}$$

$$|H(j\omega)| = \frac{1}{\sqrt{1 + (\omega RC)^2}}$$

$$\omega \ll \omega_{3dB}$$

$$\omega \gg \omega_{3dB}$$

$$|H|_{dB} = -20 \log_{10} \sqrt{1 + (\omega RC)^2}$$

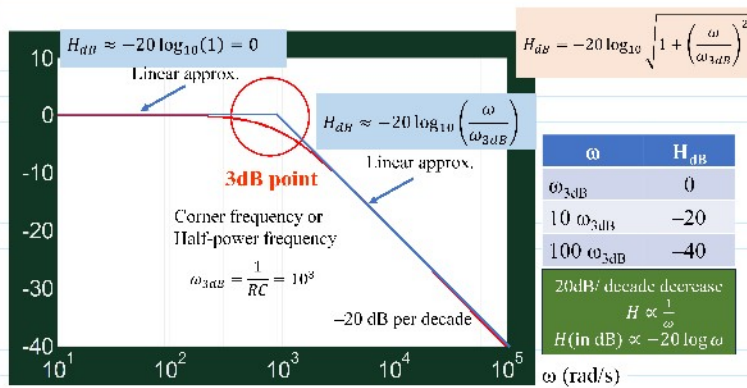
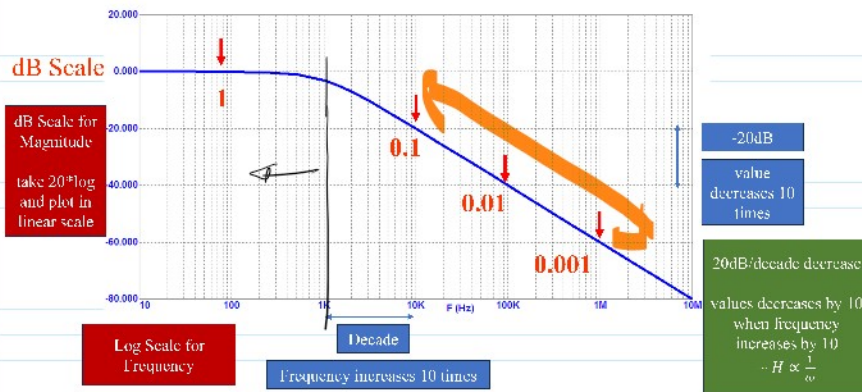
$$\omega = \frac{1}{RC} \Rightarrow |H(j\omega)| = \frac{1}{\sqrt{1 + (1)^2}} = \frac{1}{\sqrt{2}} = -3dB$$

$$\omega_{3dB}$$

$$|H|_{dB} = -20 \log_{10} \sqrt{1 + \left(\frac{\omega}{\omega_{3dB}}\right)^2}$$

$$|H|_{dB} \approx -20 \log_{10}(1) = 0$$

$$|H|_{dB} \approx -20 \log_{10} \left(\frac{\omega}{\omega_{3dB}} \right)$$



ALGO for BODE PLOT:

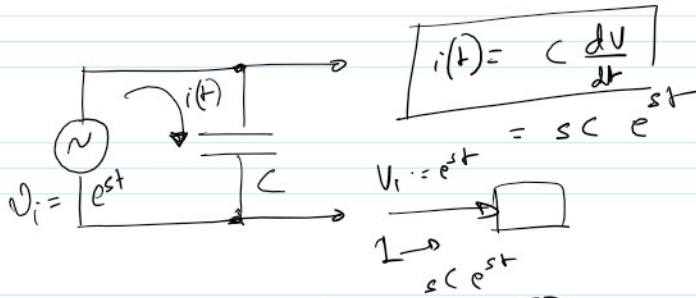
Find $H(j\omega) \Rightarrow$ Find the roots of $H(j\omega)$
 For plotting $|H(j\omega)|$ make the following approx.

$$1 + j\omega Z \approx 1 \quad (\text{if } \omega \ll 1/Z)$$

$$1 + j\omega Z \approx j\omega Z \quad (\text{if } \omega \gg 1/Z)$$

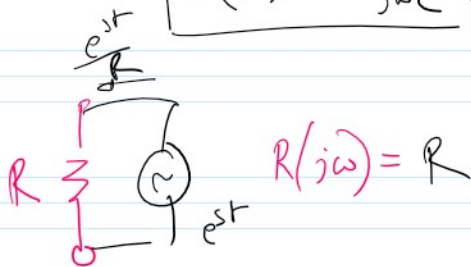
Plot in log-scale using straight line segments.

Impedance of a Capacitor



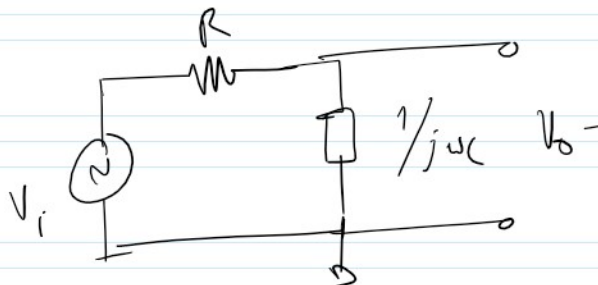
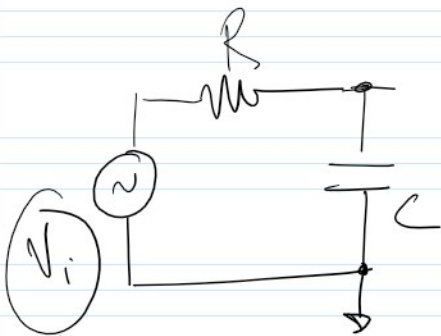
$$Z(s) = \frac{V_c(s)}{I_c(s)} = \left(\frac{1}{sC} \right)$$

$$Z(j\omega) = \frac{1}{j\omega C}$$



(For Sinusoidal Steady State analysis a Capacitor can be replaced with an impedance $= \left(\frac{1}{j\omega C} \right)$)

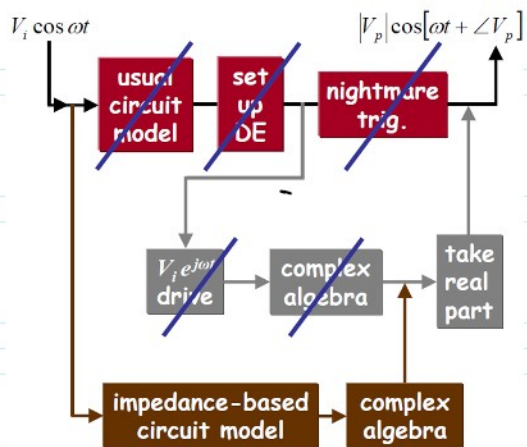
Transformed Network in phasor domain,



\Rightarrow Represents amplitude and phase of i/p. Not a time dependent source any more

$$V_o = \frac{1/j\omega C}{R + 1/j\omega C} = \frac{1}{1 + j\omega RC}$$

$$V_o = \frac{L}{R + 1/j\omega C} = \frac{1}{1 + j\omega RC}$$

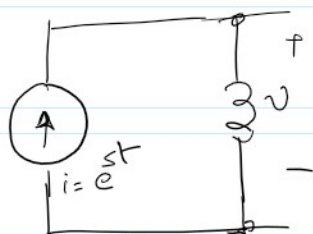


Inductor



$$\phi = L i$$

$$v = L \frac{di}{dt}$$



$$v = sL e^{st}$$

$$\Rightarrow \frac{v}{i} = sL = j\omega \quad | \quad s = j\omega$$

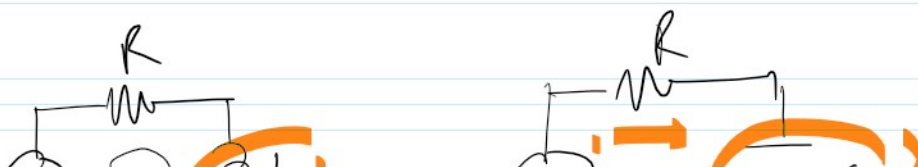
C	L
$i = C \frac{dv}{dt}$	$v = L \frac{di}{dt}$
$I(j\omega) = j\omega C V(j\omega)$	$V(j\omega) = j\omega L I(j\omega)$

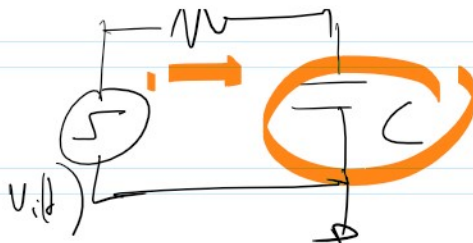
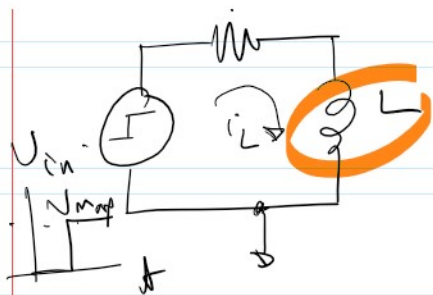
Mathematically there is no difference between an L and a C if the variables are hidden from us,
as long as I and V are interchanged.

\Rightarrow Behavior of voltage in L will be IDENTICAL to the " " current through C iff all the L's and C's are interchanged.

To transform a network with C and R with L and resistances.

$$\begin{array}{ccc} \text{C or } \omega C & \xrightarrow{\text{transformation}} & L \text{ or } \omega L \\ V & \xrightarrow{\quad} & I \\ R & \xrightarrow{\quad} & 1/R \end{array}$$





$$i_L(t) = I_{\max} \left(1 - e^{-t/(L/R)} \right) \quad v_C(t) = V_{\max} \left(1 - e^{-t/RC} \right)$$

$$I_{\max} \left(1 - e^{-\left(\frac{tR}{L} \right)} \right) \quad \left(\tau = L/R \right)$$

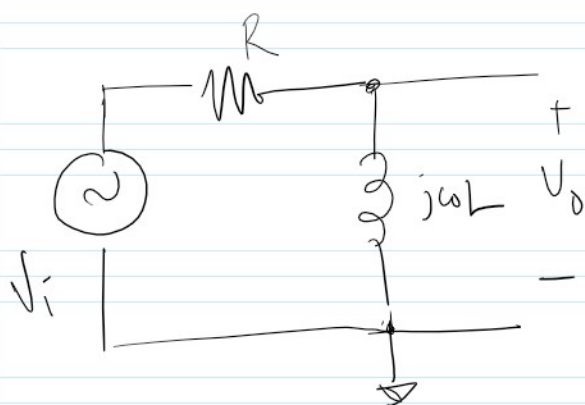
$$\tau = \frac{L}{R} = \text{const}$$

What happens to L if there is a sudden change in current?



$$I_{\max} = \frac{V_{\max}}{R}$$

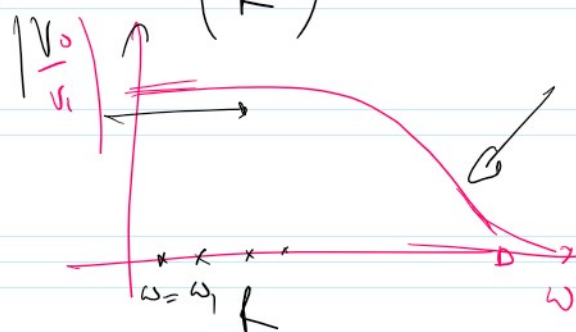
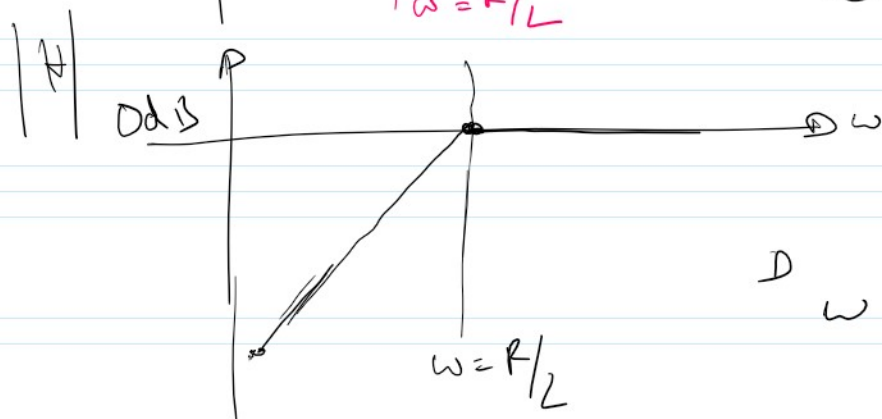
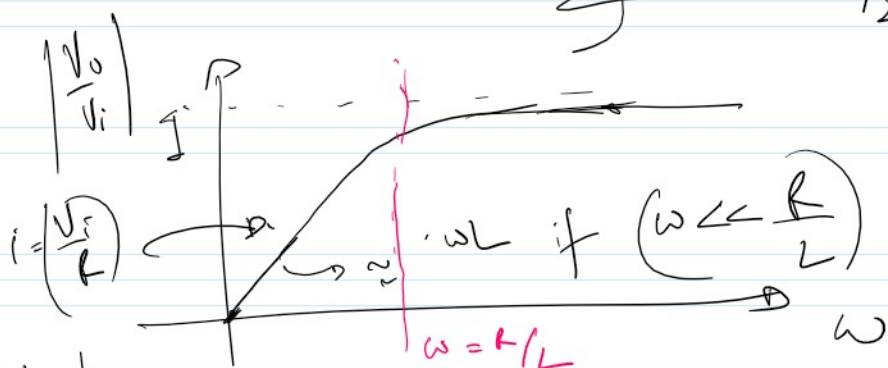
Phasor Representation.



$$\frac{V_o(j\omega)}{V_i(j\omega)} = \frac{j\omega L}{R + j\omega L}$$

$$\left| \frac{V_o}{V_i} \right| = \frac{\omega L}{\sqrt{R^2 + \omega^2 L^2}}$$

$$\angle = +\pi/2 - \tan^{-1}\left(\frac{\omega L}{R}\right)$$



@ very high freq
($\gg \omega_{3dB}$)

$$i \approx \frac{V_i}{R} \quad V_o(j\omega) = \frac{V_i}{j\omega R}$$