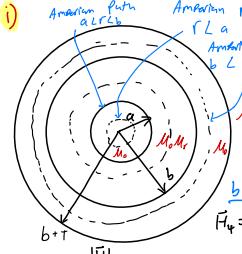


Infinity Long Cable

$$-a, b, +, M = M_0 \mu_r$$

thickness $a \ll L, b$: field intensity $\propto \frac{1}{r}$

$$\vec{H}_1 = \frac{I}{2\pi r} \hat{\phi}$$

$$H_0 2\pi r = \frac{I}{\pi a^2} \pi r^2$$

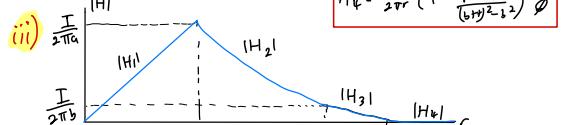
$$H_0 = \frac{I r}{2\pi a^2}$$

$$\vec{H}_2 = \frac{I}{2\pi r^2} \hat{\phi}$$

$$H_0 2\pi r = \frac{I}{2\pi r^2} \pi r^2$$

$$H_0 = \frac{I}{2\pi r^2}$$

$$\vec{H}_3 = \frac{I}{2\pi r^2} \hat{\phi}$$



(iii) $\frac{I}{2\pi b}$: $|H_1|, |H_2|, |H_3|$

$$W_{H_1} = \frac{M_0}{2} |H_1|^2 = \frac{M_0 I^2}{2} \frac{r^2}{4\pi^2 a^2} = \frac{M_0 I^2 r^2}{8\pi^2 a^2} \quad a \ll r \ll b$$

$$W_{H_2} = \frac{M_0}{2} |H_2|^2 = \frac{M_0 M_r I^2}{2} \frac{r^2}{4\pi^2 b^2} = \frac{M_0 M_r I^2}{8\pi^2 b^2} \quad a \ll r \ll b$$

(iv) $\int_V W_H dV$: $W_{H_1} = \int_V w_{H_1} dV = \frac{M_0 I^2}{8\pi^2 a^2} \int_V r^2 \cdot r dr d\theta dz = \frac{M_0 I^2}{8\pi^2 a^2} \int_0^{2\pi} d\theta \int_0^a r^3 dr \int_0^{2\pi} dz$

$$W_{H_1} = \frac{M_0 I^2}{16\pi} \quad W_{H_2} = \int_V w_{H_2} dV = \frac{M_0 M_r I^2}{8\pi^2} \int_a^b \frac{1}{r^2} \cdot r dr \int_0^{2\pi} d\theta dz$$

$$W_{H_2} = \frac{M_0 M_r I^2}{16\pi} \ln(\frac{b}{a})$$

(v) $W_H = W_{H_1} + W_{H_2} = \frac{M_0 I^2}{4\pi} \left[\frac{1}{4} + M_r \ln(\frac{b}{a}) \right]$

$$L = \frac{2W_H}{I^2} = \frac{M_0}{2\pi} \left[\frac{1}{4} + M_r \ln(\frac{b}{a}) \right]$$

Laplace - Dielectric

General stuff:
 $\nabla^2 V = 0$ Laplace equation
 $\frac{1}{r} \frac{\partial}{\partial r} (r \frac{\partial V}{\partial r}) = 0$

Integrate once
 $r \frac{\partial V}{\partial r} = A$

$V(r) = A \ln(r) + B$

at $r = a, V = 0$: $0 = A \ln(a) + B$

at $r = b, V = 100$: $100 = A \ln(b) + B$

$A = \frac{100}{\ln(\frac{b}{a})}$
 $B = -\frac{100}{\ln(\frac{b}{a})} \ln(a)$

$V(r) = \frac{100}{\ln(\frac{b}{a})} \ln(r) - \frac{100}{\ln(\frac{b}{a})} \ln(a) = \frac{100}{\ln(\frac{b}{a})} \ln(\frac{r}{a})$

$E = -\nabla V = -\frac{\partial V}{\partial r} \hat{r} = -\frac{A}{r} \hat{r} = -\frac{100}{r \ln(\frac{b}{a})} \hat{r}$

$\rho_s = |\vec{E}| = \epsilon |\vec{E}| = \frac{-400 \epsilon_0}{r \ln(\frac{b}{a})}$

negative sign indicates lower potential than $r = b$

$C = \frac{1}{\epsilon} = \frac{8\pi}{\ln(\frac{b}{a})}$

$|Q| = \int \rho_s dV = \frac{-400 \epsilon_0}{a \ln(\frac{b}{a})} 2\pi a$

$R = \frac{E}{\sigma} = \frac{4 \epsilon_0}{\sigma \ln(\frac{b}{a})}$

$R = \frac{4 \epsilon_0}{\sigma \ln(\frac{b}{a})}$

$R = \frac{4 \epsilon_0}{\sigma \ln(\frac{b}{a})}$

Generic Formulas

$$\int_V dV \Rightarrow R^2 \sin \theta dr d\theta d\phi$$

$$\int_S dA \Rightarrow R^2 \sin \theta d\theta d\phi$$

$$\int_L dl = R d\phi$$

$$\vec{r} = \text{point of observation}$$

$$\vec{r}' = \text{generic point on a source}$$

$$\sin^2 \theta + \cos^2 \theta = 1$$

$$\sin 2\theta = 2 \sin \theta \cos \theta$$

$$\cos 2\theta = \cos^2 \theta - \sin^2 \theta$$

$$\sin(\theta \pm \phi) = \sin \theta \cos \phi \pm \cos \theta \sin \phi$$

$$\cos(\theta \pm \phi) = \cos \theta \cos \phi \mp \sin \theta \sin \phi$$

Biot - Savart

$$\vec{H} = \int_S \frac{Idl' \times (\vec{r} - \vec{r}')}{4\pi r^3}$$

$$\vec{r} = 0$$

$$\vec{r}' = K\hat{r} + b\hat{z}$$

$$dl = K d\phi \hat{\phi}$$

$$\vec{H}_1 = \frac{IK d\phi \hat{\phi} \times (-K\hat{r} - b\hat{z})}{4\pi (K^2 + b^2)^{3/2}}$$

$$= \frac{IK}{4\pi (K^2 + b^2)^{3/2}} \int_0^K K d\phi \hat{\phi} \times -b \int_0^\pi \hat{\phi} d\theta \hat{x}$$

$$= \frac{IK}{4\pi (K^2 + b^2)^{3/2}} \left[K \tau \hat{z} - b [\sin \theta]^\pi \hat{x} + b [\cos \theta]^\pi \hat{y} \right]$$

$$\vec{H}_2 = \frac{IK}{2\pi b^2 \sqrt{K^2 + b^2}} \hat{y}$$

$$\vec{H} = \vec{H}_1 + \vec{H}_2$$

$$\vec{H} = \frac{IK}{2\pi \sqrt{K^2 + b^2}} \left[\frac{1}{b} \hat{y} + \frac{K\tau}{2(K^2 + b^2)} \hat{z} - \frac{b}{(K^2 + b^2)} \hat{x} \right]$$

Infinity Long Filament

$$I_1 \text{ in } \hat{z}, I_2 \text{ in clockwise}$$

$$b) \vec{B} = \vec{B}_1 = \frac{\mu_0 I_1}{2\pi r} \hat{\phi}$$

$$c) \vec{F}_1 = \int S_1 d\vec{l}_1 \times \vec{B}_1$$

$$= \int_1^0 I_2 dz \hat{z} \times \frac{\mu_0 I_1}{2\pi r} \hat{\phi}$$

$$= -\frac{\mu_0 I_1 I_2}{2\pi} (0) \hat{y}$$

$$\vec{F} = \vec{F}_1 + \vec{F}_2 + \vec{F}_3 + \vec{F}_4$$

$$\therefore \vec{F} = \vec{F}_1 + \vec{F}_3$$

$$= -\frac{9\mu_0 I_1 I_2}{2\pi} \hat{y} + \frac{9\mu_0 I_1 I_2}{10\pi} \hat{y}$$

$$\vec{F} = -\frac{3.6 \mu_0 I_1 I_2}{\pi} \hat{y} [N]$$

$$D) \text{ Force on filament due to } L_{loop}: F_N = -F$$

$$F_N = \frac{3.6}{\pi} \mu_0 I_1 I_2 \hat{y} [N]$$

Generic Questions

Maxwell Equations

Gauss' Law	$\nabla \cdot \vec{E} = \frac{\rho}{\epsilon_0}$	$\nabla \cdot \vec{D} = \rho_v$	$\oint_c \vec{D} \cdot d\vec{s} = Q$
Maxwell-Faraday	$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$	$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$	$\oint_c \vec{E} \cdot d\vec{l} = \int_S \frac{\partial \vec{B}}{\partial t} \cdot d\vec{s}$
Gauss' Law for Magnetism	$\nabla \cdot \vec{B} = 0$	$\nabla \cdot \vec{B} = 0$	$\oint_c \vec{B} \cdot d\vec{s} = 0$
Ampere's Circuit	$\nabla \times \vec{B} = \mu_0 (\vec{J} + \epsilon_0 \frac{\partial \vec{E}}{\partial t})$	$\nabla \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t}$	$\oint_c \vec{H} \cdot d\vec{l} = \int_S (\vec{J} + \frac{\partial \vec{D}}{\partial t}) \cdot d\vec{s}$

Continuity of Current

Point form: $\nabla \cdot \vec{J} = -\frac{\partial \vec{A}}{\partial t}$ Integral form: $I_n = \int_S \frac{\partial \vec{A}}{\partial t} \cdot d\vec{s}$

Displacement Current density

$$\nabla \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t} \Rightarrow \int_S (\nabla \times \vec{H}) \cdot d\vec{s} = \int_S \vec{J} \cdot d\vec{s} + \int_S \frac{\partial \vec{D}}{\partial t} \cdot d\vec{s}$$

Stokes: $\oint_c \vec{H} \cdot d\vec{l} = I_c + \int_S \frac{\partial \vec{D}}{\partial t} \cdot d\vec{s}$

$$\therefore I_n = \int_S \vec{J}_n \cdot d\vec{s} = \int_S \frac{\partial \vec{D}}{\partial t} \cdot d\vec{s} \quad \therefore I_n = \frac{\partial \vec{D}}{\partial t}$$

Mechanisms that cause EMF with 3 fixes

Mechanism:

- Ground
- Antenna effect
- Cross talk
- Switching operations
- Differential Mode

Fixes:

- Shielding
- Filtering and grounding
- Layout and component placement

Magnetic Boundary

$$\mu_1 = \mu_0, \mu_2 = 500\mu_0$$

Normal direction $\hat{n} = \hat{r}$
 \rightarrow Normal component of magnetic flux

a) $B_{2n} = B_2 \cdot \hat{n} = 15$

$$B_{2t} = 100\hat{\theta} + 250 \cos \phi \hat{z}$$

b) \rightarrow find B_2 with $\phi = 0^\circ$

$$\begin{aligned} B_2 &= 15\hat{r} + 100\hat{\theta} + 250\hat{z} \\ \hat{n} \times (\vec{B}_1 - \vec{B}_2) &= \vec{J}_s \quad \vec{H}_1 \times \hat{r} = \vec{J}_s + \vec{H}_2 \times \hat{r} \\ &= -T_o \hat{z} + \frac{B_2}{\mu_2} \end{aligned}$$

$$(H_{1r}\hat{r} + H_{1\theta}\hat{\theta} + H_{1z}\hat{z})\hat{r} = -T_o \hat{z} - \frac{100\hat{z}}{\mu_2} + \frac{250\hat{\theta}}{\mu_2}$$

$$-H_{1\theta}\hat{z} + H_{1z}\hat{\theta} = -T_o \hat{z} - \frac{100\hat{z}}{\mu_2} + \frac{250\hat{\theta}}{\mu_2}$$

$$H_{1\theta} = J_o + \frac{100}{\mu_2} \quad H_{1z} = \frac{250}{\mu_2}$$

$$\vec{H}_{1t} = (J_o + \frac{100}{\mu_2})\hat{\theta} + \frac{250}{\mu_2}\hat{z}$$

$$\vec{B}_{1t} = M_1 H_{1t} = (M_1 J_o + \frac{100}{500})\hat{\theta} + \frac{250}{500}\hat{z} = (M_1 J_o + 0.2)\hat{\theta} + 0.5\hat{z}$$

$$\vec{B}_1 = 15\hat{r} + (M_1 J_o + 0.2)\hat{\theta} + 0.5\hat{z}$$

c) \rightarrow find B_2 with $\phi = 90^\circ$

$$\begin{aligned} B_{2n} &= 15\hat{r} = \vec{B}_{1n} \\ B_{2t} &= 100\hat{\theta} \quad H_{2t} = H_{1t} \Rightarrow \frac{B_{2t}}{\mu_2} = \frac{B_{1t}}{\mu_1} \\ B_{1t} &= \frac{\mu_1}{\mu_2} \vec{B}_{2t} = \frac{\mu_0}{500\mu_0} 100\hat{\theta} = 0.2\hat{\theta} \end{aligned}$$

$$\vec{B}_1 = 15\hat{r} + 0.2\hat{\theta} \text{ at } \phi = 0^\circ$$

Stationary Loop

x-y plane, $a = 0.5m$
 $R = 400\Omega$, $L = 10^6 \text{ mH}$
 $B(t) = 6(3t^2 - 5r^2) \cos(\omega t)$

a) $\oint \vec{B}(t) \cdot d\vec{l}$

$$\begin{aligned} &= \int_{r=0}^a \int_{\theta=0}^{2\pi} (18r^2 - 30r^2) \cos(\omega t) \cdot r dr d\theta \\ &= +30 \cos(\omega t) \int_0^a r^2 dr \int_0^{2\pi} d\theta \\ &= +10\pi (0.5)^3 \cos(10^6 t) \end{aligned}$$

$$\Phi = \frac{5\pi}{2} \cos(10^6 t)$$

b) $V_{emf}^{tr} = - \int \frac{\partial \vec{B}}{\partial t} \cdot d\vec{s}$

$$= - \int_S \frac{\partial}{\partial t} (18r^2 - 30r^2) \cos(\omega t) \cdot r dr d\theta \quad (\hat{z})$$

$$= + \int_S w \sin(\omega t) (18r^2 - 30r^2) \cdot r dr d\theta \quad (\hat{z})$$

$$= w \sin(\omega t) \cdot 30 \int_0^{2.5} r^2 dr \int_0^{2\pi} d\theta$$

$$= 30 \times (0.5)^3 \times 2\pi \times w \sin(\omega t) = 2.5 \sin(\omega t)$$

c) Set $w = 10^6$ and $\omega t = \frac{\pi}{4}$

$$w \sin(\omega t) = \frac{5\pi}{4}$$

$$I = \frac{V_{emf}^{tr}}{R} = \frac{V_1 - V_2}{400} = \frac{-1.76 \times 10^6}{400}$$

$$I = -4.42 \text{ in counter clockwise}$$

Moving Loop in Static field

$$B(y) = 5 \cos(\alpha_1 y) \hat{z} \leq Wb/m^2$$

a) B at $y_1 \Rightarrow B(y_1) = 5 \cos(\alpha_1 x_1) \hat{z}$

$$B(y_1) = 4.605 \text{ Wb/m}^2$$

b) $V_{12} = V_{emf}^{tr} = \int \vec{u} \times \vec{B} \cdot d\vec{l}$

$$= \int_1^2 (-10^6 \times 4.605 \hat{z}) \cdot dL \hat{x}$$

$$V_{12} = 92.1 \text{ V}$$

c) B at $y_2 \Rightarrow B(y_2) = 5 \cos(\alpha_1 x_2) \hat{z}$

$$B(y_2) = 4.502 \hat{z} \leq Wb/m^2$$

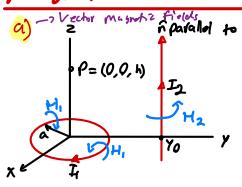
d) $V_{43} = \int (-10^6 \times 4.502 \hat{z}) dL \hat{x}$

$$V_{43} = 90.04 \text{ V}$$

e) $V_{41} = V_{32} = 0$

f) $I = \frac{V_{12} - V_{43}}{R} = \frac{92.1 - 90.04}{R} = \frac{1.7}{25} \text{ counter clockwise}$

Magnetic field of a wire



b) → Find magnetic field H for I_2 :

$$\vec{H}_2 = \frac{I_2}{2\pi r_2} \hat{z}$$

$$= \frac{I_2}{2\pi r_2} [-\sin\theta \hat{x} + \cos\theta \hat{y}] \quad \theta = \frac{\alpha}{2}$$

$$\boxed{\vec{H}_2 = \frac{I_2}{2\pi r_2} \hat{z}}$$

c) → find H given ρ, a, I, l, z

$$H = -\frac{20 \times \mu^2}{2(l^2 + a^2)^{3/2}} \left[\frac{39}{2\pi(2a)} \right] [A/cm]$$

d) $\vec{F} = I \vec{l} \times \vec{B}$
 $\vec{F} = I \oint_C dl \times \vec{B}$

$$\vec{r} = a\hat{z} \quad \text{for } I_1:$$

$$\vec{r}' = a\hat{r} \quad \text{for } I_2:$$

$$\vec{r} - \vec{r}' = a\hat{z} - a\hat{r}$$

$$|\vec{r} - \vec{r}'| = \sqrt{a^2 + a^2} = a\sqrt{2}$$

$$I_2 dL = I_2 a d\phi$$

$$\vec{H}_1 = \int \frac{Idl_1}{4\pi} \frac{x(\vec{r} - \vec{r}')}{|\vec{r} - \vec{r}'|^3}$$

$$= -\frac{I_1 a}{4\pi(a^2 + h^2)^{3/2}} \left[\int_0^{2\pi} h d\phi \hat{x} + \int_0^{2\pi} a d\phi \hat{z} \right]$$

$$= -\frac{I_1 a}{4\pi(a^2 + h^2)^{3/2}} (a L_2 \hat{z})$$

$$\boxed{\vec{H}_1 = \frac{-I_1 a^2}{2(a^2 + h^2)^{3/2}} \hat{z}}$$

$$\boxed{\vec{H} = \vec{H}_1 + \vec{H}_2}$$

Amperes Law for Cylinder

c) $\oint \vec{H} \cdot d\vec{l} = \int \vec{j} \cdot d\vec{s}$

$$\Rightarrow H_\phi 2\pi r = \int \frac{J_0}{r} e^{-r} \hat{z} \cdot r dr d\phi \hat{z}$$

$$H_\phi 2\pi r = J_0 \int_0^r e^{-r} dr \int_0^{2\pi} d\phi$$

$$H_\phi = -J_0 (e^{-r} - 1)$$

$$\boxed{\vec{H}_1 = -\frac{J_0}{r} (1 - e^{-r}) \hat{z}}$$

b) $H_2 = \frac{J_0}{r} (1 - e^{-a}) \hat{z}$

c) $|H_1| = \frac{3}{5} (1 - e^{-5}) \hat{z}$ ← Same
 $|H_2| \frac{3}{5} (1 - e^{-5}) \hat{z}$

