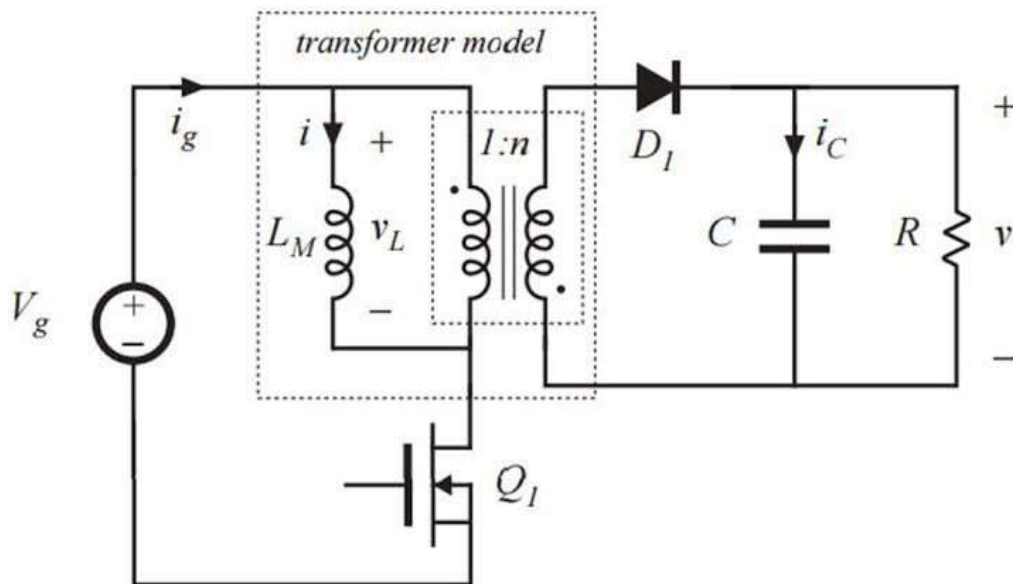


Design and simulate a 100W Flyback converter for EV battery Charging.

Input: 48V output 5V

Choose the appropriate transform/inductor turn ratio, magnetizing inductance, switching frequency, etc. Topology: Conventional flyback Design a single loop control with appropriate SSE, Settling time, and PM.

Show a step response in simulation and verify the setting time. From the digiky.in or mouser.in find the appropriate switching devices (Ex.MOSFET and Diode)



$$V_g = 48V, V = 5V, P = 100W, f = 50kHz$$

$$P = \frac{V^2}{R} \Rightarrow R = \frac{V^2}{P} = \frac{5^2}{100} = 0.25\Omega$$

$$\text{taking } \frac{N_1}{N_2} = 6$$

$$\Rightarrow V_o = V_g \frac{D}{1-D} \frac{N_1}{N_2}$$

$$\boxed{D = 0.384}$$

$$\Rightarrow P_o = P_{in}$$

$$\frac{V_o^2}{R} = V_g I_g \quad [I_g = D I_m]$$

$$I_m = \frac{P_i}{D V_g} = \frac{100}{0.384 \times 48} = 5.42A$$

$$\text{taking } \Delta I_L = 5.1.$$

$$\Rightarrow \Delta I_{Lm} = \frac{V_s D}{L_m f}$$

$$\Rightarrow 0.05 \times 5.42 = \frac{48 \times 0.384}{L_m \times 50 \times 10^3}$$

$$\boxed{L_m = 1.36mH}$$

$$\Rightarrow \frac{\Delta V}{V} = \frac{D}{RCf}$$

$$0.01 = \frac{0.384}{0.25 \times C \times 50 \times 10^3}$$

$$\boxed{C = 3.072\mu F}$$

$$G_c = n \left(v_g + \frac{V}{n} \right) \left[1 - \frac{S L I}{D' (v_g + \frac{V}{n})} \right]$$

$$\frac{\frac{n^2 L_c}{D'^2} s^2 + \frac{D^2 L S}{R D'^2} + 1}$$

$$= 21.108 \left[1 - \frac{S}{6518.35} \right]$$

$$\frac{3.058 \times 10^7 s^2 + 3.9823 \times 10^{-4} s + 1}{}$$

$$= G_0 \left[1 - \frac{S}{\omega_z} \right] \frac{1}{\left(\frac{\omega_z}{\omega_0} \right)^2 + \left(\frac{S}{Q \omega_0} \right) + 1}$$

By comparison

$$G_0 = 21.108, \omega_z = 6518.35 \text{ rad/s}$$

$$\omega_0 = 1808.22 \text{ rad/s}, Q = 1.388$$

System has Right hand zero that contributing -ve angle at ω_c

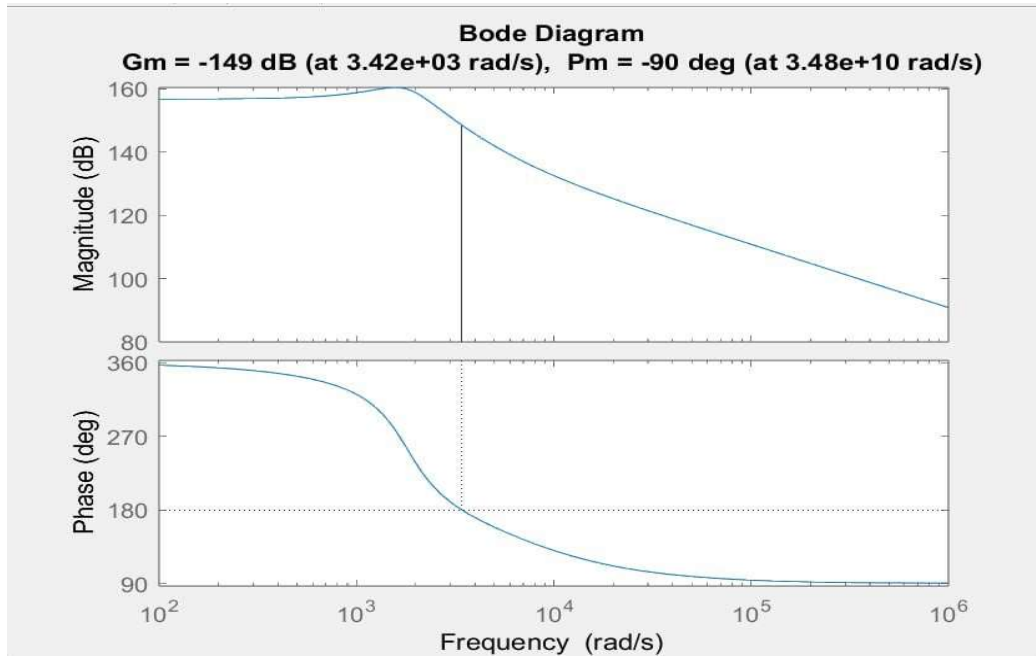
So our PM is -ve and system is unstable.
to make PM +ve we add a pole at ω_p
i.e. at 1 decade before RH zero.

$$H(s) = \frac{30}{1 + 0.833s}$$

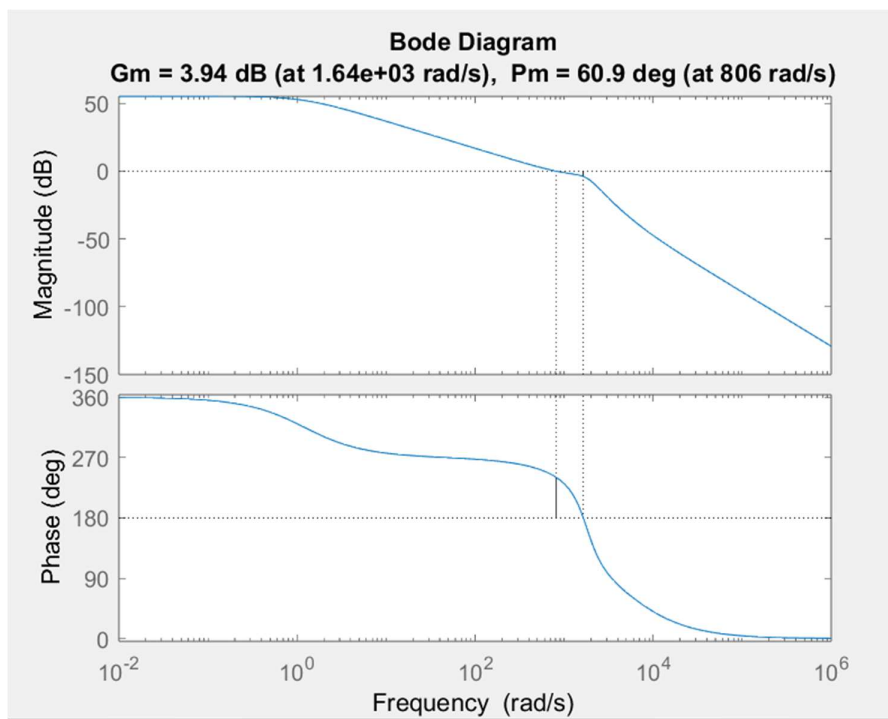
$$\text{So } G(s) H(s) = 633.24 \left[1 - \frac{S}{6518.35} \right]$$

$$\frac{0.833 s^3 + 1087 s^2 + 2.701 \times 10^6 s + 3.27 \times 10^6}{}$$

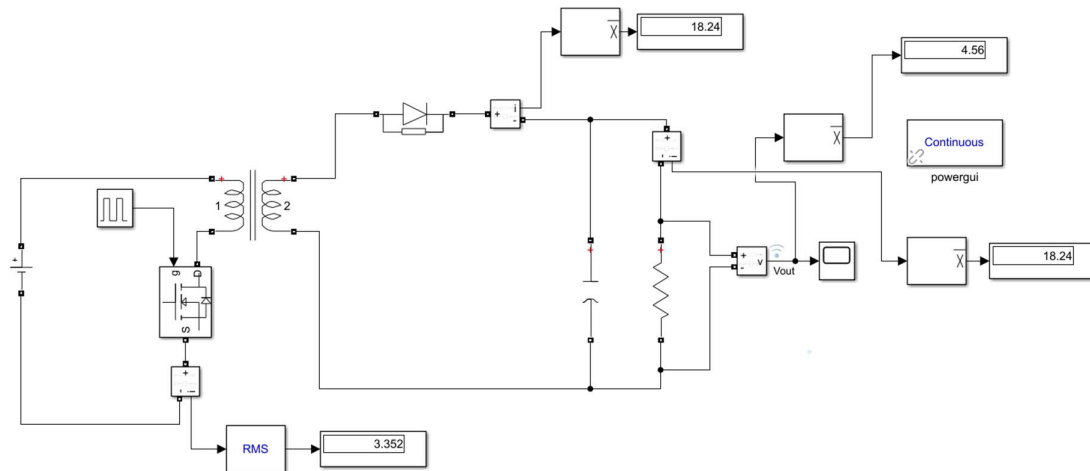
- **Bode plot of uncompensated system**



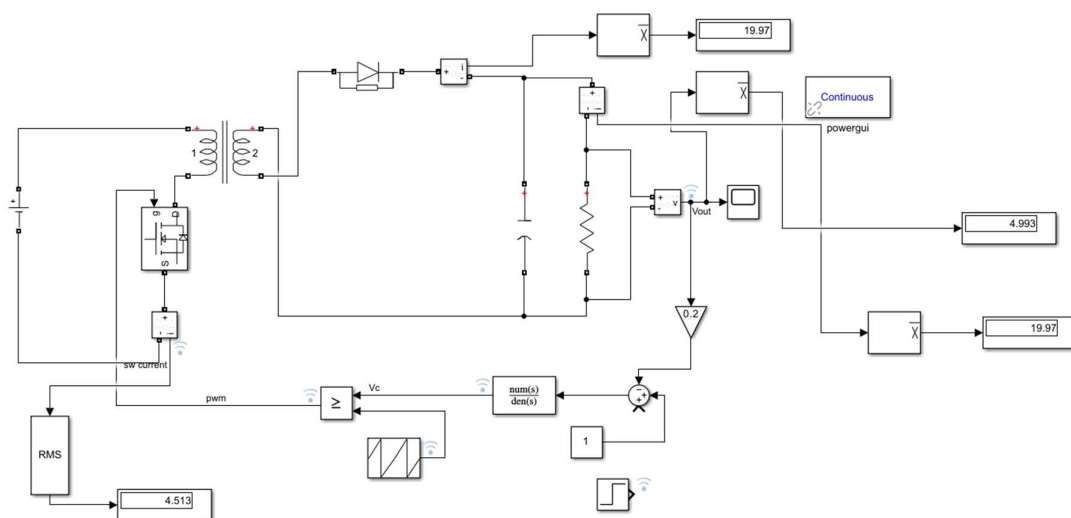
- **Bode plot of compensated system**



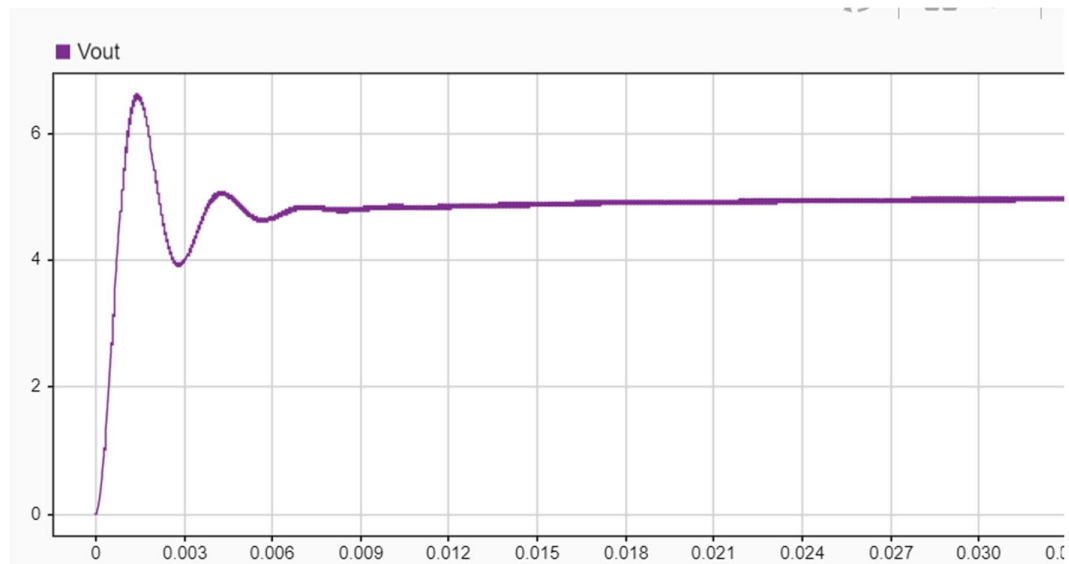
- **Uncompensated circuit**



- **Compensated circuit**



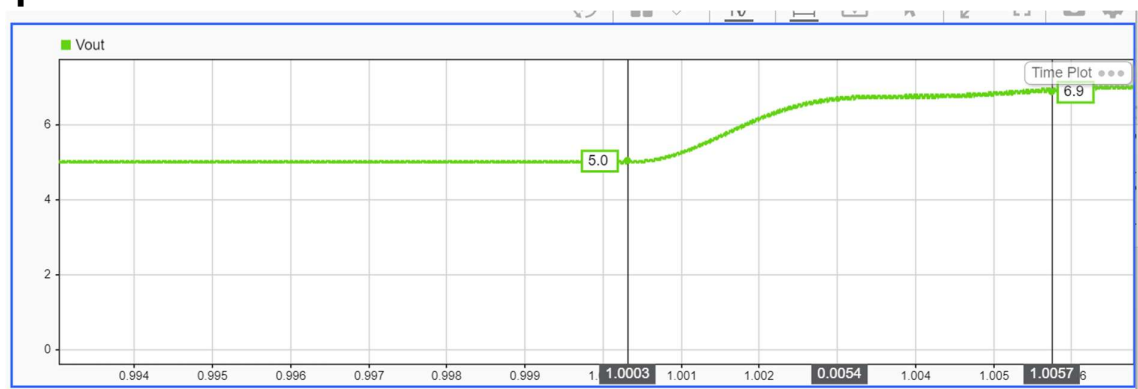
- **Output voltage waveform**



$V_o=4.993$

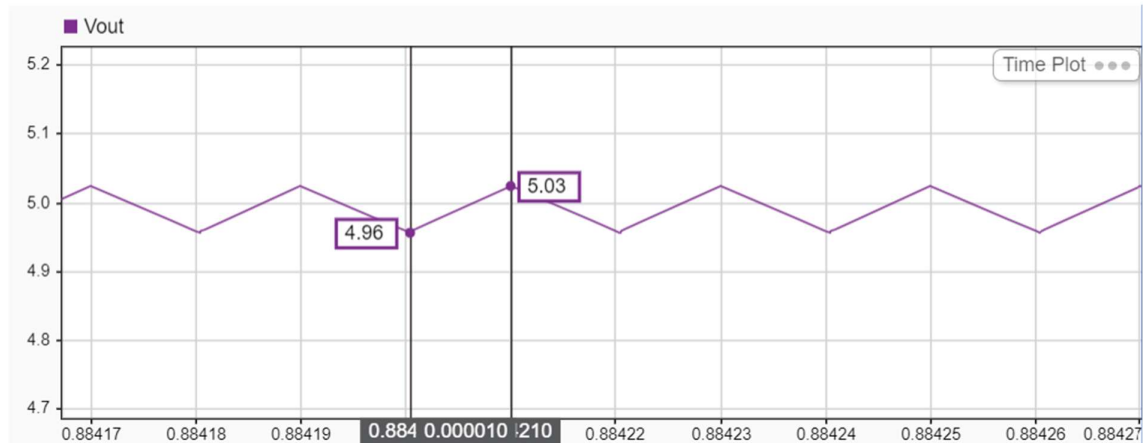
- **Settling time**

4



$T_s= 5.4$ msec (approx.)

- **Steady state error**



Ess=0.07 V i.e 1.4 %

- **SWITCH SELECTION**

1.MOSFET SELECTION

$$V_{ds}=[v_g+(V_o+v_d)*(N_p/N_s)]*2$$

Safety factor =2

$$V_{ds}= 165 \text{ V}$$

$$I_{rms}= 5*2=10 \text{ A}$$

For the flyback converter presented, the required minimum voltage rating of the MOSFET calculates to be 160V. An IXFH150N17T2 N-channel power MOSFET is chosen.

2. Diode selection

$$V_d= (V_o+V_g*(N_p/N_s))*2=26 \text{ V}$$

$$I_d= 20*2=40 \text{ A}$$

Schottky for a specific application depends mainly on the working peak reverse voltage rating, the average forward current rating of the device. An VS-42CTQ030-M3 Schottky diode is chosen

- **Results**

- 1. Uncompensated system**

$V_o=4.56$ V

$W_{gc}=3.48e10$ rad/sec

PM= -90 deg

GM= -149 db

unstable system

- 2. Compensated system**

$V_o=4.996$ V

$W_{gc}=806$ rad/sec

$T_s= 5$ msec (theoretical)

$T_s= 5.4$ sec (simulation)

PM= 60.9 deg

Gm 3.94 db

Stable system