

# DH

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## First utilize DH representation:

1.  $Z^K$ : each Z always align with the axis of joint
2. origin<sup>K</sup>: intersection of Zs, or norm of Zs if parallel
3.  $X^K$ : to be orthogonal to Zs. away from prev Z
4.  $Y^K$ : right handed

as for the tool tip:

Z: r3 approach

Y:r2 sliding

X:r1 normal

## Second generate 4tuples for all joints(except joint0):

$\theta_k$ : Xs angle about prev Z

$d_k$ : Xs dist about prev Z

$a_k$ : Zs dist about now X

$\alpha_k$ : Zs angle about now X

## Third use forward kinematics to determine $T_{k-1}^k$

### Transferring Frame $k-1$ to Frame $k$

Operation	Description
1	<b>Rotate</b> $L_{k-1}$ about $z^{k-1}$ by $\theta_k$ .
2	<b>Translate</b> $L_{k-1}$ along $z^{k-1}$ by $d_k$ .
3	<b>Translate</b> $L_{k-1}$ along $x^{k-1}$ by $a_k$ .
4	<b>Rotate</b> $L_{k-1}$ about $x^{k-1}$ by $\alpha_k$ .

$$T_{k-1}^k(\theta_k, d_k, a_k, \alpha_k) = Rot(\theta_k, 3)Tran(d_k i^3)Tran(a_k i^1)Rot(\alpha_k, 1)$$

so we get Link-Coordinate Transformation

$$T_{k-1}^k = \begin{pmatrix} C\theta_k & -C\alpha_k S\theta_k & S\alpha_k S\theta_k & a_k C\theta_k \\ S\theta_k & C\alpha_k C\theta_k & -S\alpha_k C\theta_k & a_k S\theta_k \\ 0 & S\alpha_k & C\alpha_k & d_k \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

The inverse of  $T$  is:

$$T^{-1} = \begin{pmatrix} R^T & -R^T p \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

**Its inverse transformation** which maps link  $k-1$  coordinates to link  $k$  coordinates is given as:

$$T_k^{k-1} = \begin{pmatrix} C\theta_k & S\theta_k & 0 & -a_k \\ -C\alpha_k S\theta_k & C\alpha_k C\theta_k & S\alpha_k & -d_k S\alpha_k \\ S\alpha_k S\theta_k & -S\alpha_k C\theta_k & C\alpha_k & -d_k C\alpha_k \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

and we also **define**

$$q_k = \xi_k \theta_k + (1 - \xi_k) d_k.$$

because a joint can either be revolute or prismatic but not both

# Arm Equation

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$$T_{base}^{tool}(q) = \begin{pmatrix} R(q) & p(q) \\ 0 & 1 \end{pmatrix}$$

as for the  $p(q)$ , each dim denotes an axis

as for the  $R(q)$ , each column denotes an axis rotation

# Direct Kinematics

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$$R_1(\phi) = \begin{pmatrix} 1 & 0 & 0 \\ 0 & \cos \phi & -\sin \phi \\ 0 & \sin \phi & \cos \phi \end{pmatrix}$$

$$R_2(\phi) = \begin{pmatrix} \cos \phi & 0 & \sin \phi \\ 0 & 1 & 0 \\ -\sin \phi & 0 & \cos \phi \end{pmatrix}$$

$$R_3(\phi) = \begin{pmatrix} \cos \phi & -\sin \phi & 0 \\ \sin \phi & \cos \phi & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

The rotation matrix must be orthogonal matrix  
thus we have

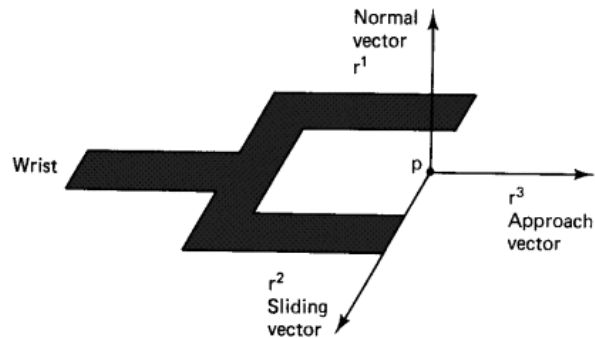
$$Rot^{-1}(\phi, k) = Rot(-\phi, k) = Rot^T(\phi, k) \text{ for } 1 \leq k \leq 3$$

## Inverse Homogeneous Transformation

The inverse of  $T$  is:

$$T^{-1} = \begin{pmatrix} R^T & -R^T p \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

## 2.5.2 Normal, Sliding, and Approach Vectors



The orientation of the tool can be expressed in rectangular coordinates by a rotation matrix  $R = [r^1, r^2, r^3]$ , where the three columns of  $R$  correspond to the

- normal vector,
- sliding vector, and
- approach vectors,

respectively. The origin of the  $\{r^1, r^2, r^3\}$  frame is usually placed at the tool tip.

# Tool-Configuration

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$$w = \begin{pmatrix} w_1 \\ w_2 \\ w_3 \\ w_4 \\ w_5 \\ w_6 \end{pmatrix} = \begin{pmatrix} p \\ \exp(q_n / \pi) r^3 \end{pmatrix}$$

$$q_n = \pi \ln(w_4^2 + w_5^2 + w_6^2)^{1/2}$$