

## \* Servo Motors :

A servo motor is one in which output is some mechanical variable like position, velocity or acceleration.

Servo system are generally automatic control systems. They work on error signals. Error signals are amplified to drive the motors used in servo systems.

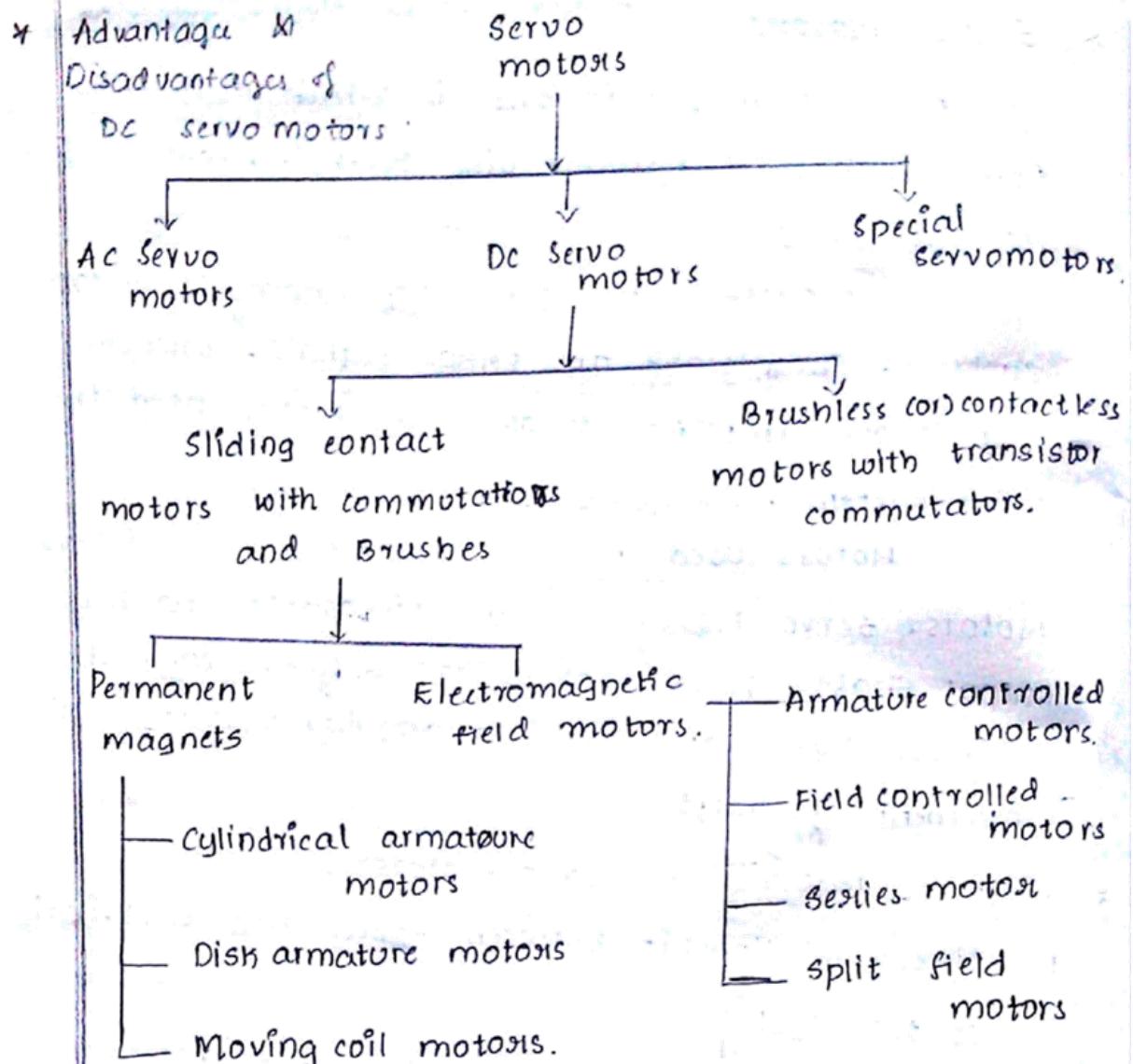
Motors used in servo systems are called servo motors. Servo motors are usually coupled to the output shaft. These motors are used to convert electrical signal applied, into angular velocity (or) movement of shaft.

## \* Features required in servo Motors :

1. Linear relationship between speed and electrical control system
2. Servo motor operation should be stable without any oscillations (or) overshoots.
3. Inertia of rotor should be as low as possible.
4. Its response should be as fast as possible.
5. It should have linear torque-speed characteristics.
6. Wide range of speed control is required.

## \* Types of Servo Motors:

Servo motors are basically classified depending upon the nature of electric supply to be used for its operation.



\* Armature controlled DC servo motor:

It is a DC shunt motor designed to satisfy the requirement of servomotor. The field is excited by constant DC supply.

If the field current is constant, then the speed is directly proportional to armature voltage and torque is directly proportional to armature current.

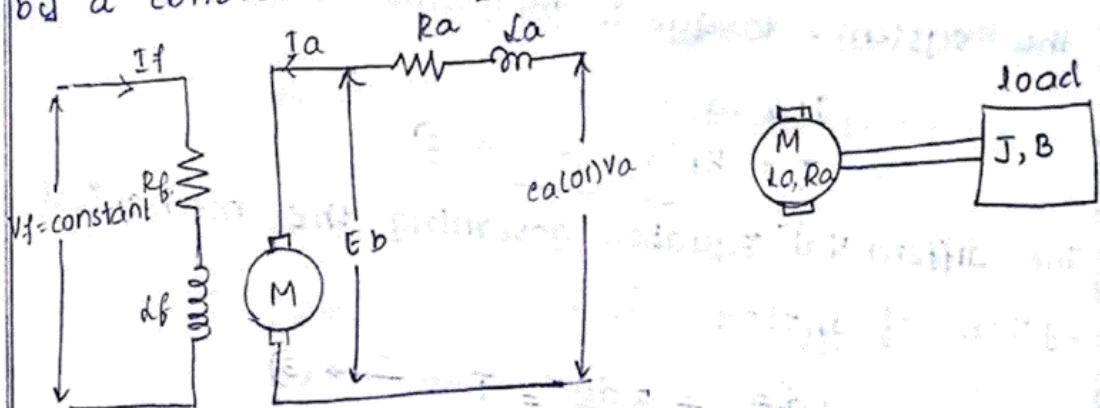
In small motors, armature voltage is controlled by variable resistance. In large motors, in order to reduce power loss, armature voltage

is controlled by Thyristors.

Transfer function of Armature controlled DC Motor:

In Armature controlled DC Motor, the desired speed is obtained by varying armature voltage.

The electrical system consists of armature and the field circuit. But for analysis purpose, only the armature circuit is considered because field is excited by a constant voltage.



Let  $R_a$  = Armature Resistance,  $\Omega$

$L_a$  = Armature Inductance,  $H$

$I_a$  = Armature current, Amps

$V_a$  = Armature voltage, V

$E_b$  = Back EMF, V

$K_t$  = Torque constant, Newton-meter/amp

$T$  = Torque developed by motor, N-m.

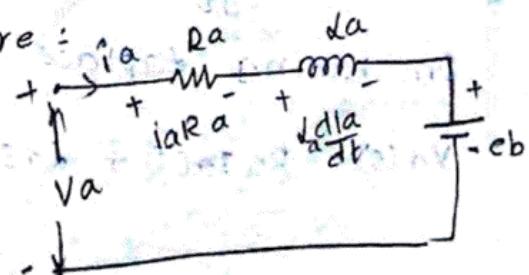
$\theta$  = Angular displacement of shaft, radians

$J$  = Moment of inertia of motor and load,  $\text{kg}\cdot\text{m}^2/\text{radian}$

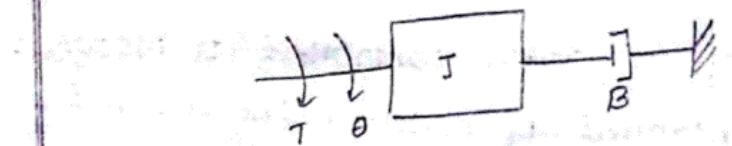
$B$  = Frictional coefficient of motor and load,  $\text{N}\cdot\text{m}/(\text{rad/sec})$

$K_b$  = Back EMF constant,  $V/\text{rad/sec}$

Equivalent circuit of Armature:



## Mechanical system of Motor:



By KVL, we can write

$$V_a = i_a R_a + \frac{d \phi}{dt} + e_b \rightarrow ①$$

Torque of DC Motor is proportional to product of flux and current. since flux is constant in this system, torque is proportional to  $i_a$  alone.

$$T \propto i_a$$

$$\Rightarrow T = k_t i_a \rightarrow ②$$

The differential equation governing the mechanical system of motor is,

$$J \frac{d^2\theta}{dt^2} + B \frac{d\theta}{dt} = T \rightarrow ③$$

Back EMF of DC machine is proportional to speed of shaft i.e., angular velocity of shaft.

$$e_b \propto \frac{d\theta}{dt}$$

$$e_b = k_b \frac{d\theta}{dt} \rightarrow ④$$

Differential Equations governing Armature control

Dc motor are

$$V_a = i_a R_a + \frac{d \phi}{dt} + e_b$$

$$T = k_t i_a$$

$$J \frac{d^2\theta}{dt^2} + B \frac{d\theta}{dt} = T$$

$$e_b = k_b \frac{d\theta}{dt}$$

On taking Laplace Transform, we will get

$$V_a(s) = R_a I_a(s) + L s I_a(s) + E_b(s) \rightarrow ⑤$$

$$T(s) = K_t I_a(s) \rightarrow ⑥$$

$$JS^2\theta(s) + BS\theta(s) = T(s) \rightarrow ⑦$$

$$E_b(s) = K_b s \theta(s) \rightarrow ⑧$$

Equating ⑥ and ⑦

$$\Rightarrow K_t I_a(s) = JS^2\theta(s) + BS\theta(s)$$

$$\Rightarrow I_a(s) = \left[ \frac{JS^2 + BS}{K_t} \right] \theta(s) \rightarrow ⑨$$

Substitute ⑧ and ⑨ in ⑤

$$\Rightarrow V_a(s) = (Ra + La s) \left[ \frac{JS^2 + BS}{K_t} \right] \theta(s) + K_b s \theta(s)$$

$$\Rightarrow V_a(s) = \theta(s) \left[ \frac{(Ra + La s)(JS^2 + BS) + K_t K_b s}{K_t} \right]$$

$$\Rightarrow \frac{\theta(s)}{V_a(s)} = \frac{K_t}{(Ra + La s)(JS^2 + BS) + K_t K_b s}$$

$$\frac{\theta(s)}{V_a(s)} = \frac{K_t}{Ra \left(1 + \frac{La s}{Ra}\right) BS \left(1 + \frac{JS^2}{BS}\right) + K_t K_b s}$$

$$\frac{\theta(s)}{V_a(s)} = \frac{K_t}{SRaB \left[\frac{La}{Ra} + 1\right] \left[1 + \frac{JS^2}{BS}\right] + K_t K_b s}$$

$$\frac{\theta(s)}{V_a(s)} = \frac{K_t}{SRaB (S\tau_a + 1) (T_M s + 1) + K_t K_b s}$$

where  $\tau_a = \frac{La}{Ra} \rightarrow$  Electrical Time constant

$T_M = JS^2/B \rightarrow$  Mechanical Time constant

1. Construct block diagram of Armature controlled DC Motor  
 Q: Differential eqns governing Armature controlled DC Motor are

Motors are

$$V_a = i_a R_a + \frac{d i_a}{dt} R_a + e_b \rightarrow ①$$

$$T = K t i_a \rightarrow ②$$

$$T = J \frac{d\omega}{dt} + B\omega \rightarrow ③$$

$$e_b = K_b \omega \rightarrow ④$$

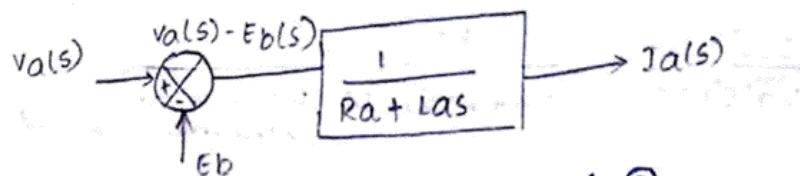
$$\omega = \frac{d\theta}{dt} \rightarrow ⑤$$

On taking Laplace Transform of ①

$$\Rightarrow V_a(s) = I_a(s)R_a + L_a s I_a(s) + E_b(s)$$

$$\Rightarrow V_a(s) = I_a(s)[R_a + L_a s] + E_b(s)$$

$$\Rightarrow I_a(s) = \frac{V_a(s) - E_b(s)}{R_a + L_a s}$$



On taking Laplace Transform of ②

$$T(s) = K_t I_a(s) \quad I_a(s) \xrightarrow{K_t} T(s)$$

On taking Laplace transform of ③

$$T(s) = J s \omega(s) + B \omega(s) \quad T(s) \xrightarrow{\frac{1}{J s + B}} \omega(s)$$

$$\Rightarrow \omega(s) = \frac{T(s)}{J s + B}$$

On taking Laplace transform of ④

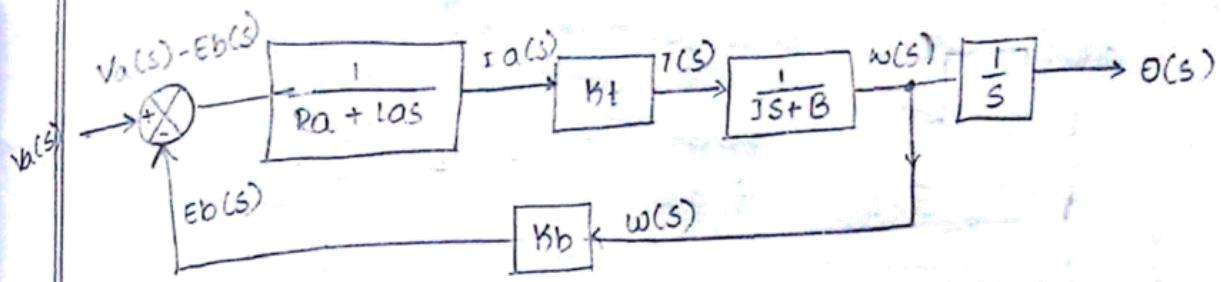
$$E_b(s) = K_b \omega(s) \quad \omega(s) \xrightarrow{K_b} E_b(s)$$

On taking Laplace transform of ⑤

$$\Rightarrow \omega(s) = s \theta(s)$$

$$\Rightarrow \theta(s) = \frac{\omega(s)}{s}$$

$$\omega(s) \xrightarrow{\frac{1}{s}} \theta(s)$$



\* Field control DC servo motor:

It is a DC shunt motor designed to satisfy the requirement of servo motor. In this the armature is supplied with a constant current or voltage.

When armature voltage is constant, the torque is directly proportional to field flux.

The torque of the motor is controlled by controlling field current.

\* Transfer function of Field control DC motor:

Let,

$R_f$  = Field Resistance,  $\Omega$

$L_f$  = Field Inductance,  $H$

$I_f$  = Field current, Amps

$V_{Bf}$  = Field voltage,  $V$

$T$  = Torque developed by the motor,  $N\cdot m$

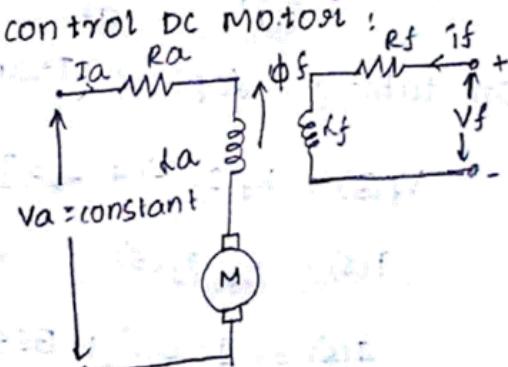
$K_{tf}$  = Torque constant,  $N\cdot m/Amp$

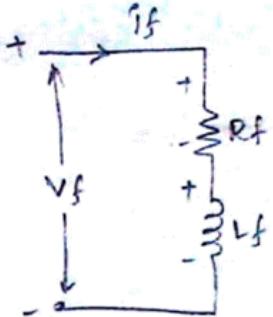
$K$  = Moment of Inertia of motor and load,  $kg\cdot m^2/rad$

$B$  = frictional coefficient of motor and load,  $\frac{N\cdot m}{rad/sec}$

The Electrical system consists of Armature and field circuit, but for analysis purpose only field circuit is considered because armature is excited by a constant voltage.

The mechanical system consists of the rotating part of motor and the load connected to shaft of the motor.





Equivalent circuit  
of field



Mechanical system of the  
motor

Apply KVL to the circuit

$$V_f = I_f R_f + L_f \frac{dI_f}{dt} \rightarrow ①$$

$$T = K_{tf} I_f \rightarrow ②$$

Equation of mechanical system

$$T = J \frac{d^2\theta}{dt^2} + B \frac{d\theta}{dt} \rightarrow ③$$

On taking, Laplace Transform we will get.

$$V_f(s) = R_f I_f(s) + L_f s I_f(s) \rightarrow ④$$

$$T(s) = K_{tf} I_f(s) \rightarrow ⑤$$

$$T(s) = JS^2\theta(s) + BS\theta(s) \rightarrow ⑥$$

Equating ⑤ and ⑥

$$K_{tf} I_f(s) = JS^2\theta(s) + BS\theta(s)$$

$$I_f(s) = \theta(s) \left[ \frac{BS + JS^2}{K_{tf}} \right]$$

sub in ④

$$\Rightarrow V_f(s) = I_f(s) [R_f + L_f s]$$

$$V_f(s) = \theta(s) \left[ \frac{BS + JS^2}{K_{tf}} \right] [R_f + L_f s]$$

$$\frac{\theta(s)}{V_f(s)} = \frac{K_{tf}}{(BS + JS^2)(R_f + L_f s)}$$

$$\frac{\theta(s)}{V_f(s)} = \frac{K_t f}{B s \left(1 + \frac{J s}{B}\right) R_f \left(1 + \frac{L_f s}{R_f}\right)}$$

$$\Rightarrow \frac{\theta(s)}{V_f(s)} = \frac{K_t f m}{s \left(1 + T_m s\right) \left(1 + T_f s\right)}$$

where

$$T_f = \frac{L_f}{R_f} = \text{Electrical Time constant}$$

$$T_m = \frac{J}{B} = \text{Mechanical Time constant}$$

$$K_m = \frac{K_t f}{R_f B} = \text{motor gain constant.}$$

1. Block Diagram of field control DC Motor :

$$V_f = I_f R_f + L_f \frac{dI_f}{dt} \rightarrow ①$$

$$T = K_t f I_f \rightarrow ②$$

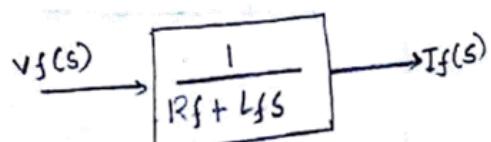
$$T = J \frac{d^2 \theta}{dt^2} + B \frac{d\theta}{dt} \rightarrow ③, \omega = \frac{d\theta}{dt} \rightarrow ④$$

Taking Laplace transform of ①

$$V_f(s) = R_f I_f(s) + L_f s I_f(s)$$

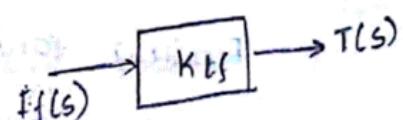
$$V_f(s) = I_f(s) [R_f + L_f s]$$

$$I_f(s) = \frac{V_f(s)}{R_f + L_f s}$$



Taking Laplace transform of ②

$$T(s) = K_t f I_f(s)$$



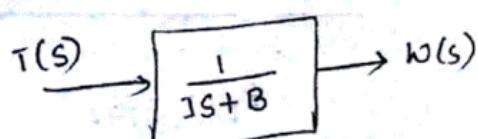
Taking Laplace transform of ③

$$T = J \frac{d\omega}{dt} + B \omega$$

$$\Rightarrow T(s) = J s \omega(s) + B \omega(s)$$

$$\Rightarrow T(s) = \omega(s) [J s + B]$$

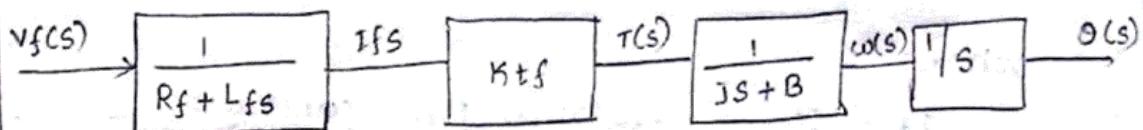
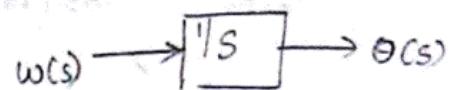
$$\Rightarrow \omega(s) = \frac{T(s)}{J s + B}$$



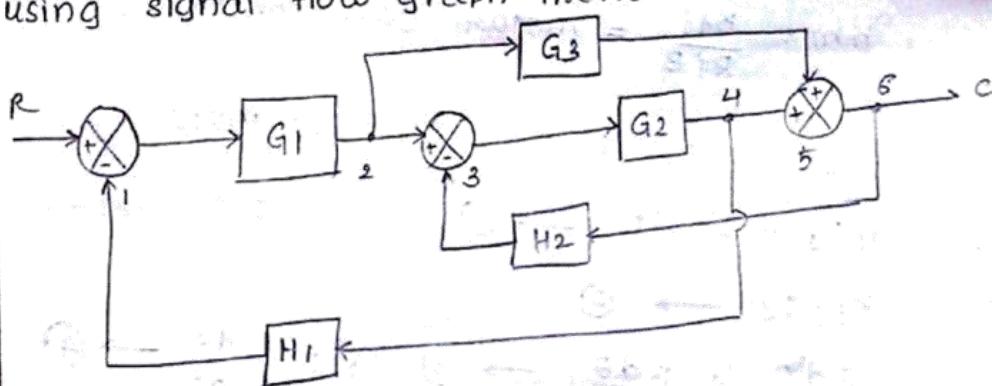
Taking Laplace transform of 4

$$w(s) = s\theta(s)$$

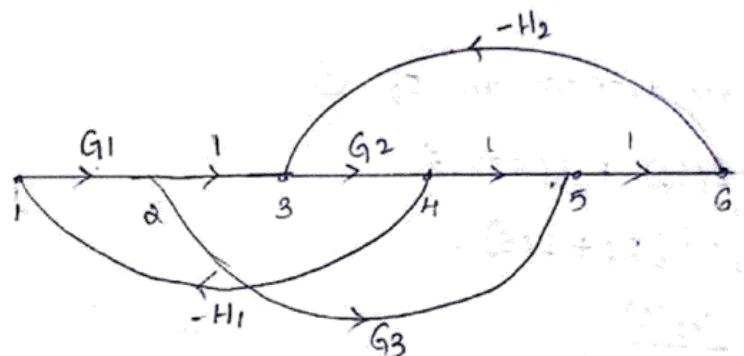
$$\Rightarrow \theta(s) = w(s)/s$$



- \* Find transfer function for the following block diagram using signal flow graph method.



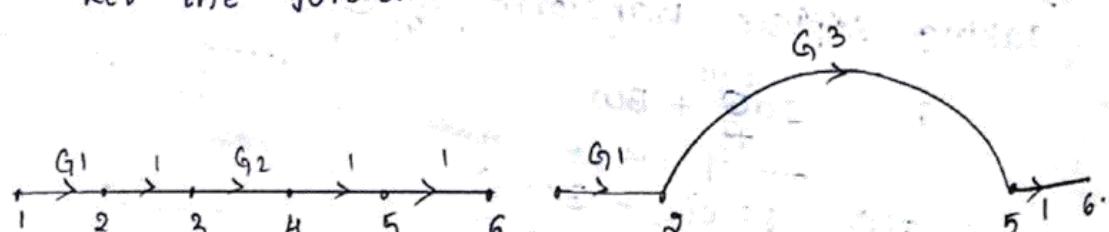
SOL:



- Finding forward path gains.

No. of forward paths = 3

Let the forward paths be  $P_1$  &  $P_2$

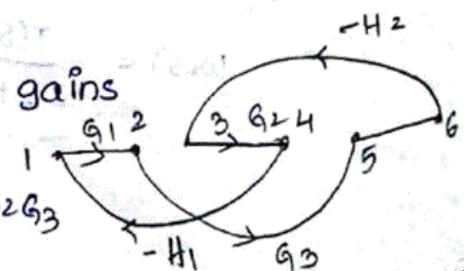


$$P_1 = G_1 G_2$$

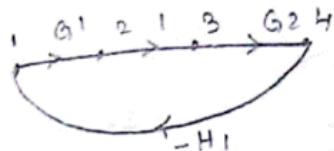
$$P_2 = G_1 G_3$$

- Finding individual loop gains

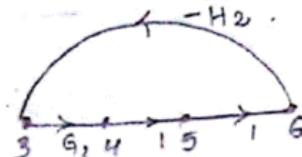
$$P_{13} = H_1 H_2 G_1 G_2 G_3$$



There are 2 loops and let them be  $P_{11} \rightarrow P_{12}$



$$P_{11} = -H_1 G_1 G_2$$



$$P_{12} = -H_2 G_1 G_2$$

3. Finding gain product of a non-touching loops.

There are no non-touching loops.

4. Finding  $\Delta$  and  $\Delta_K$ .

$$\Delta = 1 - (P_{11} + P_{12}) - P_{13}$$

$$= 1 + H_1 G_1 G_2 + H_2 G_2 - G_1 G_2 G_3 H_1 H_2$$

$$\Delta_K = 1 - [0]$$

since there is no part of graph non-touching

two forward paths

$$\Rightarrow \Delta_1 = 1, \Delta_2 = 1$$

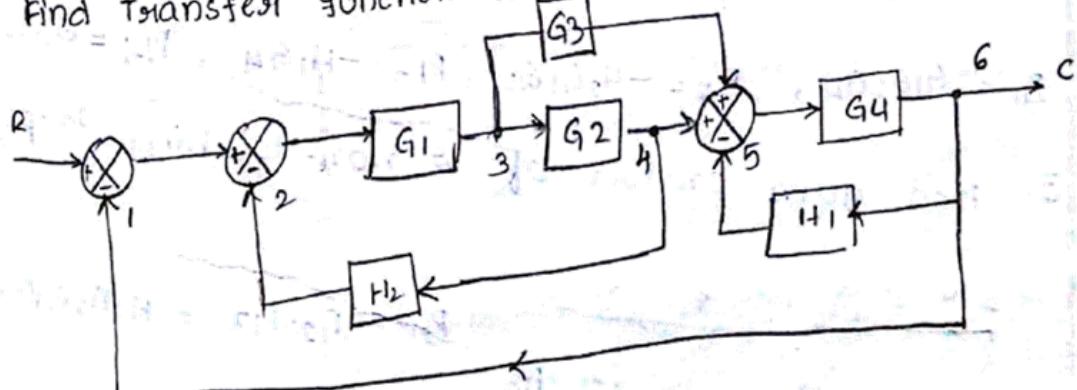
5. Find transfer function.

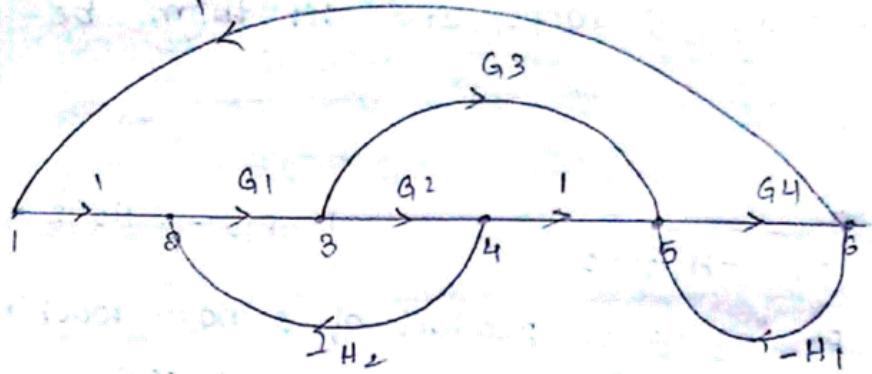
$$T = \frac{1}{\Delta} \sum P_K \Delta_K$$

$$= \frac{1}{\Delta} [P_1 \Delta_1 + P_2 \Delta_2]$$

$$T = \frac{G_1 G_2 + G_1 G_3}{1 + H_1 G_1 G_2 + H_2 G_2 - G_1 G_2 G_3 H_1 H_2}$$

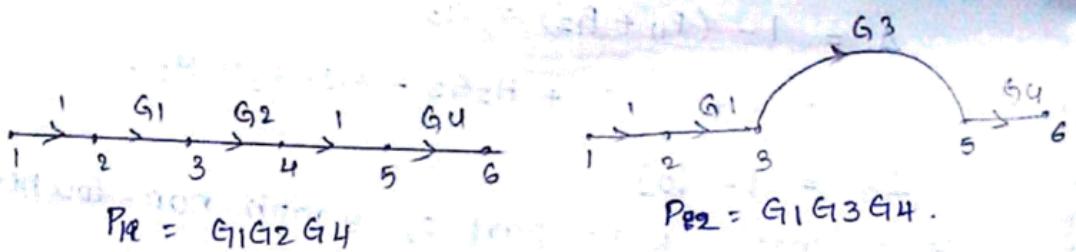
2. Find Transfer function using signal flow graph method



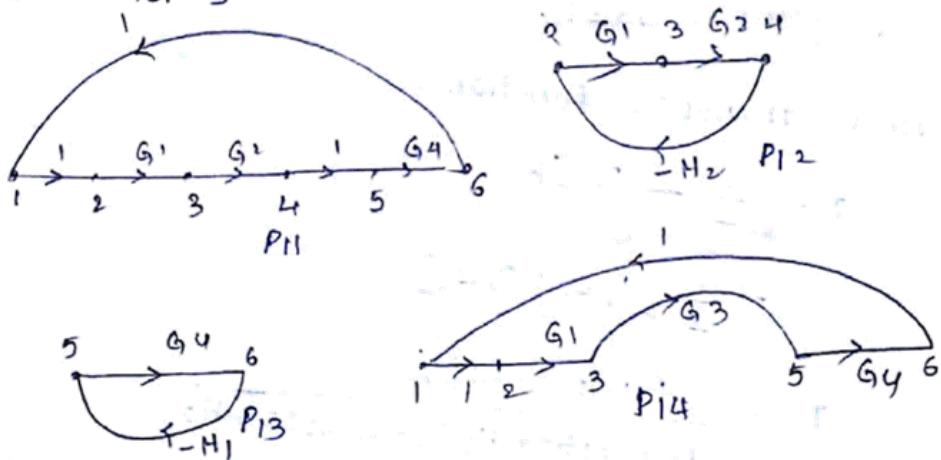


1. Find forward path gains.

No. of forward paths  $B = 2$  so let them be  $P_{11}, P_{12}$



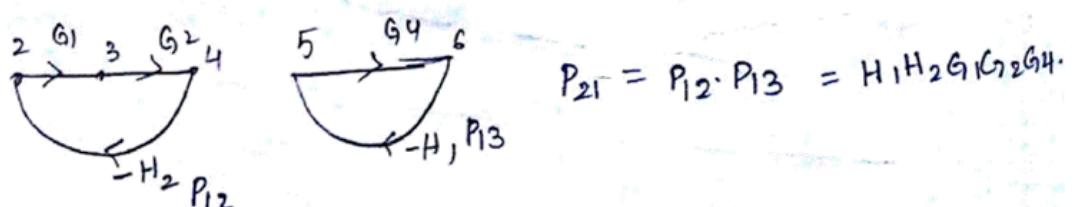
2. Finding individual loop gains.



Let the loops be  $P_{11}, P_{12}, P_{13}, P_{14}$ .

$$P_{11} = G_1 G_2 G_4, \quad P_{12} = -H_2 G_1 G_2, \quad P_{13} = -H_1 G_4, \quad P_{14} = G_1 G_3 G_4$$

3. Find gain product of 2 non-touching loops.



4. Finding  $\Delta$  &  $\Delta_K$ .

$$\Delta = 1 - (P_{11} + P_{12} + P_{13} + P_{14}) + (P_{21})$$

$$= 1 - (G_1 G_2 G_4 - H_2 G_1 G_2 + H_1 G_4 + G_1 G_3 G_4) + H_1 H_2 G_1 G_2 G_4$$

$$= 1 - G_1 G_2 G_4 + H_2 G_1 G_2 + H_1 G_4 - G_1 G_3 G_4 + H_1 H_2 G_1 G_2 G_4.$$

$$\Delta_1 = 1 - [0] = 1$$

$$\Delta_2 = 1 - [0] = 1$$

5 A. find Transfer function

$$T = \frac{1}{\Delta} [\sum P_k \Delta_k]$$

$$T = \frac{1}{\Delta} [P_1 \Delta_1 + P_2 \Delta_2]$$

$$T = \frac{G_1 G_2 G_4 + G_1 G_3 G_4}{1 - G_1 G_2 G_4 + H_2 G_1 G_2 + H_1 G_4 - G_1 G_3 G_4 + H_1 H_2 G_1 G_2 G_4}$$

\* Equivalent all pole will be dominant

\* Dominant pole will be dominant and the rest of the

\* Non dominant poles will have smaller effect on response

\* Non dominant poles will have smaller effect on response

\* Non dominant poles will have smaller effect on response

\* Non dominant poles will have smaller effect on response

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