

we know

$$\begin{aligned}y_3(t) &= t \cdot x_3(t) \\&= t [a x_1(t) + b x_2(t)] \\&= a t \cdot x_1(t) + b t \cdot x_2(t) \\|y_3(t) &= a \cdot y_1(t) + b \cdot y_2(t)|\end{aligned}$$

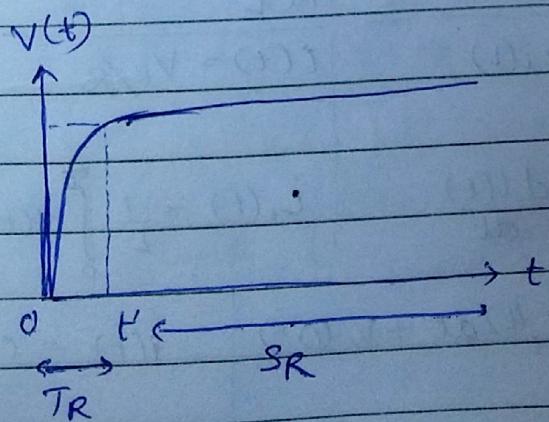
## UNIT - II

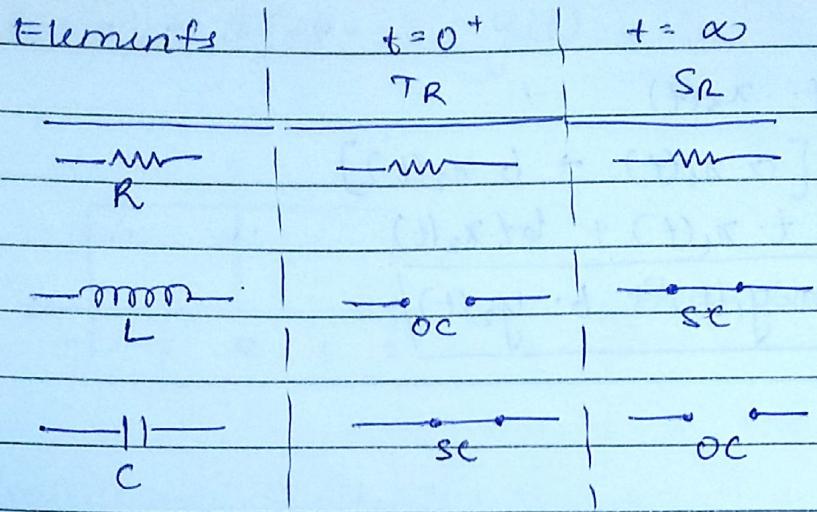
### Transient Response

The values of  $V$  and  $I$  during the transient period are known as transient response. It depends upon the network elements alone and independent of the source.

### \* Steady State Response

The values of  $V$  and  $I$  after the transient has died out, are known as steady state response. It is also defined as the part of the total time response which remains after the transient response has passed. It depends on both element and source.





$$\rightarrow X_C = \frac{1}{\omega C} = \frac{1}{2\pi f C} = \frac{T}{2\pi C}$$

$$\rightarrow X_L = \omega L = 2\pi f L = \frac{2\pi L}{T}$$

### \* Zero State Response

Find  $y(t)$  when initial states or conditions are zero.

### \* Zero Input Response (Natural Response)

Find  $y(t)$  when  $x(t) = 0$

(Find output when input is zero)

Element	KVL	KCL
$R$	$V_R = R \cdot i(t)$	$i(t) = V_R/R$
$L$	$V_L = L \cdot \frac{di(t)}{dt}$	$i_L(t) = \frac{1}{L} \int_0^t V(t) dt + i_L(0^+)$
$C$	$V_C = \frac{1}{C} \int_0^t i_C(t) dt + V_C(0^+)$	$i(t) = C \cdot \frac{dV_C(t)}{dt}$

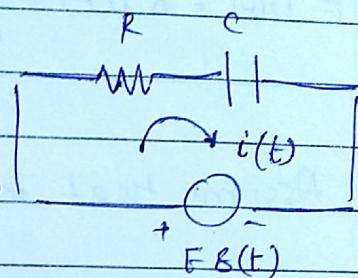
Methods

→ Classical Method (Time Domain Method)  
 → Laplace Method

\* Q Find impulse response of RC series network

$$V_E(t) = V_R(t) + V_C(t)$$

$$ES(t) = R i(t) + \frac{1}{C} \int_0^t i_c(t) dt + V_C(0^+)$$



Let us assume that initially the capacitor is fully discharged

$$\Rightarrow ES(t) = R i(t) + \frac{1}{C} \int_0^t i_c(t) dt$$

Using Laplace both sides

$$\Rightarrow F = R \cdot I(s) + \frac{1}{C} \cdot \frac{I(s)}{s}$$

$$= I(s) \left[ R + \frac{1}{sC} \right]$$

$$\Rightarrow I_s = \frac{E}{R + \frac{1}{sC}}$$

$$= \frac{E}{R} \left[ \frac{1}{1 + \frac{1}{sCR}} \right]$$

$$= \frac{E}{R} \left[ \frac{s}{s + \frac{1}{RC}} \right]$$

$$= \frac{E}{R} \left[ 1 - \frac{\frac{1}{RC}}{s + \frac{1}{RC}} \right]$$

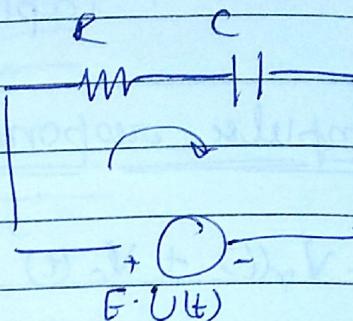
$\therefore ILT \Rightarrow$

$$i(t) = \frac{E}{R} \left[ S(t) - \frac{1}{RC} e^{-\frac{t}{RC}} \right] \text{Amp}$$

\* Q Find Step Response of RC series ckt

$$V_E = V_R + V_C$$

$$E \cdot U(t) = R i(t) + \frac{1}{C} \int_0^t i_c(t) dt + V_c(0)$$



Assume that initially capacitor is fully discharged

$$\Rightarrow E \cdot U(t) = R i(t) + \frac{1}{C} \int_0^t i_c(t) dt$$

Taking LT

$$\Rightarrow \frac{E}{s} = R I(s) + \frac{I(s)}{Cs}$$

$$\Rightarrow \frac{E}{s} = I(s) + \left( R + \frac{1}{sC} \right)$$

$$\Rightarrow I(s) = \frac{E}{s(R + \frac{1}{sC})}$$

$$\Rightarrow I(s) = \frac{E}{R} \left( \frac{1}{s + \frac{1}{RC}} \right)$$

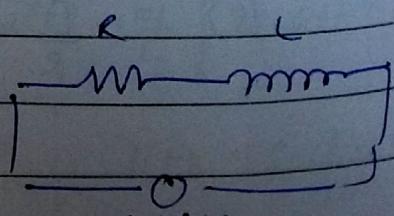
Taking ILT

$$\Rightarrow i(t) = \frac{E}{R} e^{-\frac{t}{RC}}$$

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\* Q Find the Impulse Response of RL series ckt.

$$V_E = V_R + V_L$$



$$E \cdot S(t) = R i(t) + L \cdot \frac{di(t)}{dt}$$

Taking L.T.

$$\begin{aligned} E \cdot I(s) &= R \cdot I(s) \cdot R + L \cdot I(s) \cdot s \\ &= I(s) (R + Ls) \end{aligned}$$

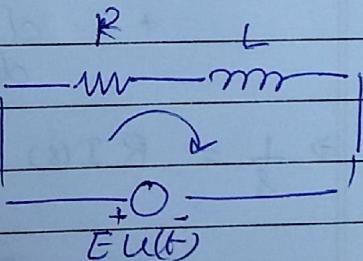
$$\Rightarrow I(s) = \frac{E}{L} \frac{1}{s + R/L}$$

Taking L.I.

$$i(t) = \frac{E}{L} e^{-Rt/L} \text{ Amp}$$

\* Q Find Step response of RL series ckt

$$\begin{aligned} V_E &= V_R + V_L \\ E \cdot U(t) &= R i(t) + L \cdot \frac{di(t)}{dt} \end{aligned}$$



Taking L.T.

$$\begin{aligned} \frac{E}{S} &= I(s) \cdot R + L \cdot I(s) \cdot s \\ &= (R + sL) I_s \end{aligned}$$

$$I(s) = \frac{E}{s(R + sL)}$$

$$= \frac{E}{L} \left[ \frac{1}{s(s + R/L)} \right]$$

$$= \frac{E}{L} \left[ \left( \frac{1}{s} - \frac{1}{s + R/L} \right) \cdot \frac{1}{R/L} \right]$$

$$\Rightarrow \frac{E}{R} \left( \frac{1}{s} - \frac{1}{s+R/C} \right)$$

Taking L.L.

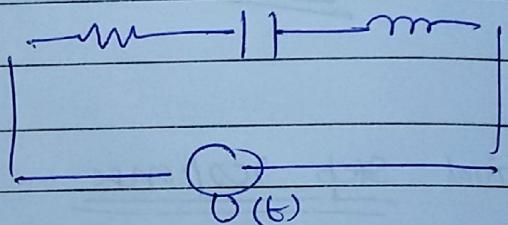
$$i(t) = \frac{E}{R} (U(t) - e^{-R/Ct}) \text{ Amp}$$

~~Ans~~

Ques Find the Step Response of RCL series ckt  
initially

Ans Let us assume that, inductor & capacitor are fully discharged.

$$U(t) = R i(t) + \frac{1}{C} \int_0^t i(t) dt + L \cdot \frac{di(t)}{dt}$$



$$\Rightarrow \frac{1}{s} = R I(s) + \frac{1}{C} \cdot \frac{I(s)}{s} + L I(s) \cdot s$$

$$= I(s) \left[ R + \frac{1}{Cs} + Ls \right]$$

$$\frac{1}{s} = I(s) \left( \frac{Rcs + 1 + Ls^2c}{Cs} \right)$$

$$I(s) = \frac{C}{s^2 LC + Rcs + 1}$$

$$= \frac{C}{Lc (s^2 + \frac{R}{L}s + \frac{1}{Lc})}$$

$$I(s) = \frac{\frac{1}{L}}{(s^2 + \frac{R}{L}s + \frac{1}{Lc})}$$

→ Roots.

$$\alpha, \beta = -\frac{R}{L} \pm \sqrt{\frac{R^2}{L^2} - \frac{4}{LC}}$$

$$= \left( -\frac{R}{2L} \pm \sqrt{\frac{R^2}{4L^2} - \frac{4}{LC}} \right) / 2$$

$$\therefore \omega = -\frac{R}{2L} \pm \sqrt{\left(\frac{R}{2L}\right)^2 - \frac{1}{LC}}$$

case I: Both  $\alpha$  &  $\beta$  are real and not equal

$$\Rightarrow \frac{R}{2L} > \frac{1}{\sqrt{LC}}$$

$$\therefore I(s) = \frac{Y_L}{(s+\alpha)(s+\beta)}$$

By partial fraction

$$= \frac{K_1}{s+\alpha} + \frac{K_2}{s+\beta}$$

$$\therefore K_1 = \frac{Y_L}{\beta - \alpha} \Big|_{s=-\alpha}$$

$$= \frac{Y_L}{\beta - \alpha}$$

$$\Rightarrow K_1 = \frac{1}{L(\beta - \alpha)}$$

$$K_2 = \frac{V_L}{s+\alpha} \quad |_{\alpha = -\beta}$$

$$\therefore = \frac{V_L}{\alpha - \beta}$$

$$\Rightarrow \boxed{K_2 = \frac{1}{L(\alpha - \beta)}}$$

$$\therefore I(s) = \frac{1}{(\beta - \alpha) \cdot L \cdot (\alpha - \beta)}$$

$\therefore$  Taking I.L.

$$i(t) = \frac{e^{-\alpha t}}{(\beta - \alpha)L} + \frac{e^{-\beta t}}{(\alpha - \beta)L}$$

$$\Rightarrow i(t) = \underline{\underline{\frac{1}{(\beta - \alpha)L}}} \cdot (e^{-\alpha t} - e^{-\beta t}) \text{ Amp}$$

$\rightarrow$  Case II:  $\alpha = \beta$

$$\text{Let } \alpha = \beta = \gamma$$

$$\therefore I(s) = \frac{1}{L(s+\gamma)^2}$$

$\therefore$  Taking I.L.

$$\cancel{i(t) = \frac{1}{L} + t \cdot e^{-\gamma t} \text{ Amp}}$$

→ Case IV : When the roots are Imaginary

$$\frac{R}{2L} \leftarrow \frac{1}{\sqrt{LC}}$$

$$\alpha = \beta^*$$

$$\alpha = A_0 - jB$$

$$\beta = A_0 + jB$$

$$\therefore I(s) = \frac{V_L}{(s + A_0 - jB)(s + A_0 + jB)}$$

$$= \frac{k_3}{(s + A_0 - jB)} + \frac{k_4}{(s + A_0 + jB)}$$

$$k_3 = \frac{1}{L(s + A_0 + jB)} \Big|_{s = -A_0 + jB}$$

$$\Rightarrow \underbrace{k_3 = \frac{1}{2iLB}}_{}$$

$$k_4 = \frac{1}{L(s + A_0 - jB)} \Big|_{s = -A_0 - jB}$$

$$\Rightarrow \underbrace{k_4 = \frac{-1}{2iLB}}_{}$$

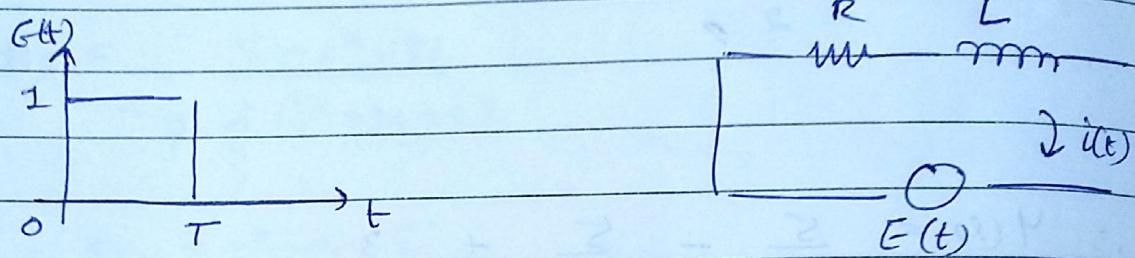
$$\therefore I(s) = \frac{1}{2iLB(s + A_0 + jB)} - \frac{1}{2iLB(s + A_0 - jB)}$$

$$Y(s) = \frac{k_1}{s} + \frac{k_2}{s+4}$$

$$= \frac{12}{s} - \frac{9}{s+4}$$

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Ans

Response of RL-CR circuit with pulse input

$$E(t) = RI(t) + L \cdot \frac{di(t)}{dt}$$

$$\Rightarrow E = [U(t) - U(t-T)] = RI(t) + L \cdot \frac{di(t)}{dt}$$

Taking L.T.

$$\Rightarrow RI(s) + LS \frac{I(s)}{s} = \frac{1}{s} - \frac{e^{-st}}{s}$$

$$\Rightarrow I(s) = \frac{(1 - e^{-st})}{s(Rs + Ls)}$$

$$= \frac{1 - e^{-st}}{s(Rs + Ls)}$$

$$= \frac{1 - e^{-st}}{Ls(R/L + s)}$$

$$\text{Ans } I(s) = \frac{1 - e^{-st}}{Ls(R/L + s)}$$

$$\frac{I(s)}{1 - e^{-st}} = \frac{1}{2s(R_L + s)} \Rightarrow I'(s)$$

$$\therefore \frac{I'(s)}{L} = \frac{A}{s} + \frac{B}{R_L + s}$$

$$A = \left. \frac{1}{2(s+R_L)} \right|_{s=0} = \frac{1}{R}$$

$$B = \left. \frac{1}{2L} \right|_{s=-R_L} = -\frac{1}{R}$$

$$\therefore I'(s) = \frac{1}{Rs} - \frac{1}{R(s+R_L)}$$

$$\Rightarrow I(s) = \frac{1 - e^{-st}}{R} \left( \frac{1}{s} - \frac{1}{s+R_L} \right)$$

$$\Rightarrow \frac{1}{Rs} - \frac{1}{R(s+R_L)} - \frac{e^{-st}}{s} + \frac{e^{-st}}{R(s+R_L)}$$

Taking L.I.

$$i(t) = \frac{U(t)}{R} - \frac{e^{-R_L t}}{R} - \frac{U(t-T)}{R} + \frac{e^{-R_L t}}{R} \cdot S(t-T)$$

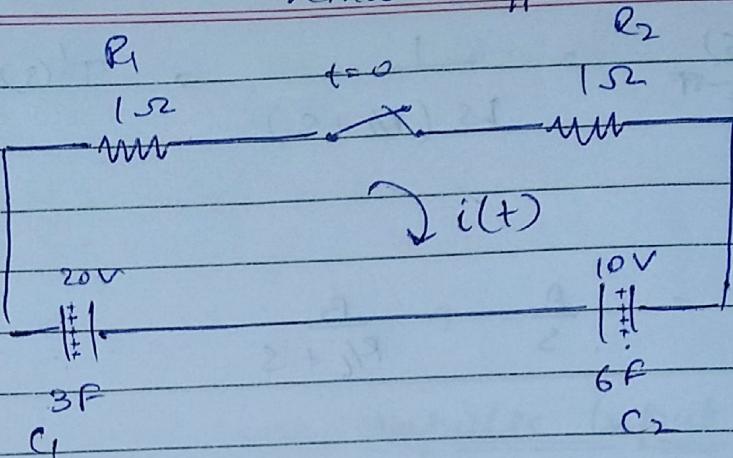
Solve for  $i(t)$  in given ckt. in which  $3F$  capacitor is initially charged to  $20V$  and  $6F$  capacitor to  $10V$  where switch is closed at  $t=0$

$$+V_c(0^+) \xrightarrow{\frac{1}{s+R_1+1}} -V_c(0^+) \quad \text{if the case is reversed then}$$

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only the direction will get changed, magnitude will remain unaffected



$$\frac{1}{4} \int_0^t i(t) dt = V_{C_1}(0^+) + R_1 i(t) + R_2 i(t) + V_{C_2}(0^+) + \frac{1}{C_2} \int_0^t i(t) dt = 0$$

∴ Taking L.T.

$$\frac{I(s)}{S C_1} + \frac{V_{C_1}(0^+)}{S} + R_1 I(s) + R_2 I(s) + \frac{V_{C_2}(0^+)}{S} + \frac{I(s)}{S C_2} = 0$$

$$\Rightarrow \frac{I(s)}{S \cdot 3} - \frac{20}{S} + 1 \cdot I(s) + 1 \cdot I(s) + \frac{10}{S} + \frac{I(s)}{S \cdot 6} = 0$$

$$\Rightarrow I(s) \left( \frac{1}{3S} + 2 + \frac{1}{6S} \right) - \frac{10}{S} = 0$$

$$\Rightarrow I(s) (2 + 12s + 1) = 10$$

$$\Rightarrow T(s) = \frac{6 \cdot 10}{(2 + 12s + 1)}$$

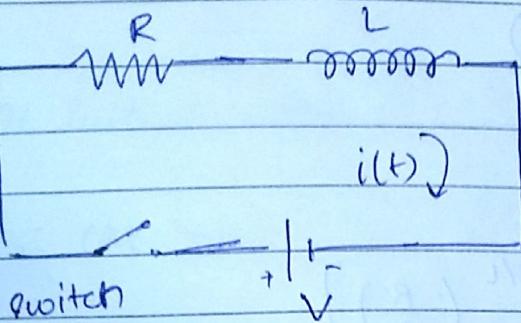
$$= \frac{6 \cdot 10}{(3 + 12s)}$$

$$= \frac{20}{4s + 1}$$

$$\Rightarrow I(s) = \frac{5}{s + 1/4}$$

$$= \frac{5}{s + 0.25}$$

$$\therefore i(t) = 5 \cdot e^{-0.25t} \text{ Amp}$$

Transient AnalysisTransient response of RL series ckt

$$R \cdot i(t) + L \cdot \frac{di(t)}{dt} = V \quad \text{--- (1)}$$

$$\frac{di(t)}{dt} + \frac{R}{L} \cdot i(t) = \frac{V}{L} \quad \text{--- (2)}$$

General 1<sup>st</sup> order linear Eq<sup>n</sup>

$$\frac{dy(t)}{dt} + P \cdot y(t) = Q \quad \left. \begin{array}{l} \\ \\ \end{array} \right\} \quad i(t) = \frac{V}{R} + K \cdot e^{-Rt/R}$$

$$y(t) = \frac{Q}{P} - K \cdot e^{-Pt} \quad \left. \begin{array}{l} \\ \\ \end{array} \right\} \quad .$$

$$K = \text{any const.} \quad \left. \begin{array}{l} \\ \\ \end{array} \right\}$$

Since inductor behave as open ckt. at  $t=0^+$   
Similarly at  $t=\infty$  inductor behave as short ckt.

$$t=0^+ \Rightarrow i(t)=0$$

$$\Rightarrow 0 = \frac{V}{R} + K$$

$$\Rightarrow \boxed{K = -\frac{V}{R}}$$

$$\therefore i(t) = \frac{V}{R} (1 - e^{-Rt/L}) \quad | \text{ Amp}$$

$$\Rightarrow V_R(t) = R i(t)$$

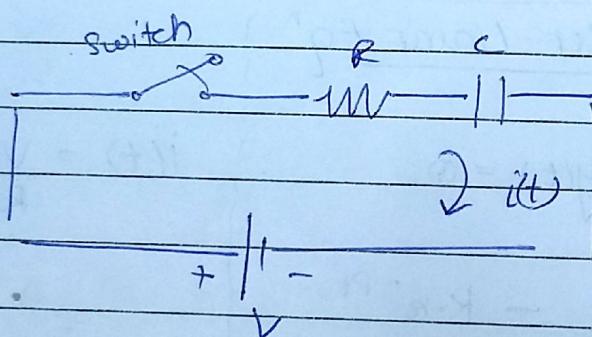
$$\Rightarrow V_R(t) = V (1 - e^{-Rt/L})$$

$$V_L(t) = L \cdot \frac{di(t)}{dt}$$

$$= L \cdot \frac{V}{R} \left[ 0 - e^{-Rt/L} \left( -\frac{R}{L} \right) \right]$$

$$\Rightarrow V_L(t) = V e^{-Rt/L}$$

### 6/9/17 Transient Response of RC-series Ckts



$$V = R i(t) + \frac{1}{C} \int_0^t i(t) dt$$

$$\Rightarrow 0 = R \cdot \frac{di(t)}{dt} + \frac{1}{C} \cdot i(t)$$

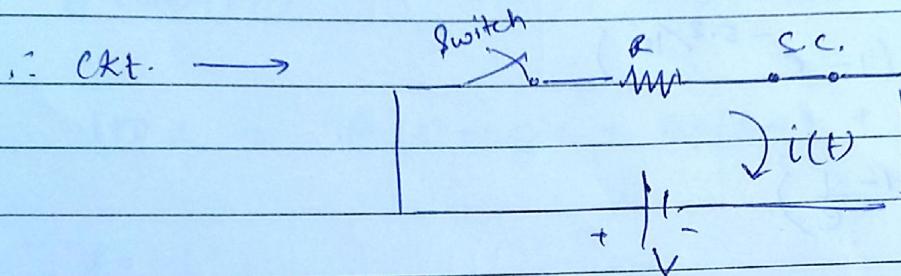
$$\Rightarrow R \left[ \frac{di(t)}{dt} + \frac{1}{RC} \cdot i(t) \right] = 0$$

$$\Rightarrow \frac{di(t)}{dt} + \frac{1}{RC} i(t) = 0$$

$$i(t) = 0 + k \cdot e^{-t/RC}$$

$$\Rightarrow i(t) = k \cdot e^{-t/RC}$$

At initial condition, capacitor behave as s.c.



$$\therefore i(0^+) = \frac{V}{R}$$

$$\Rightarrow \frac{V}{R} = k \cdot e^{-0/RC}$$

$$\Rightarrow \frac{V}{R} = k$$

$$\therefore i(t) = \frac{V}{R} \cdot e^{-t/RC}$$

Amp

$$V_R(t) = R \cdot i(t)$$

$$\Rightarrow V_R(t) = R \cdot \frac{V}{R} \cdot e^{-t/RC}$$

$$V_R(t) = V e^{-t/RC}$$

$$V_C(t) = \frac{1}{C} \int_0^t i(t) dt$$

$$= \frac{1}{C} \int_0^t \frac{V}{R} e^{-t/RC} dt$$

$$= \frac{-V}{R C} \left[ e^{-t/RC} \right]_0^t$$

$$V_C(t) = \frac{(1 - e^{-t/RC}) \cdot V}{R C^2}$$

$$\text{Time const. } T = \frac{L}{R} \quad RC$$

$$LT \text{ of } \sin \omega t = \frac{\omega}{\omega^2 + s^2} \quad \cos \omega t = \frac{s}{\omega^2 + s^2}$$

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Q: Find the current in a series RL-ckt. having  $R = 2\Omega$  and  $L = 10H$ , with a DC voltage of 100V is applied. What is the value of the current after 5 sec.

Ans:  $i(t) = \frac{V}{R} (1 - e^{-\frac{tR}{L}})$

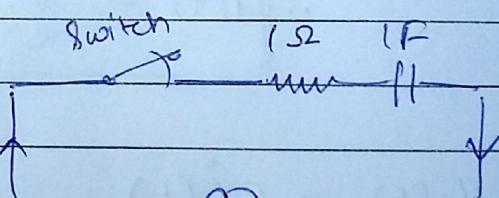
$$i(5\text{sec}) = \frac{100}{2} (1 - e^{-5 \cdot 2 / 10})$$

$$= 50 \left(1 - \frac{1}{e}\right)$$

$$= \underline{31.6 \text{ Amp}}$$

Q: Find the complete solution for current, using Laplace Transform, assume capacitor is fully discharged initially

$$V = R i(t) + \frac{1}{C} \int_0^t i(t) dt$$



$$\Rightarrow 10 \sin(10t) = i(t) + \int_0^t i(t) dt$$

LT on both sides

$$\frac{100}{s^2 + 100} = I(s) + \frac{I(s)}{s}$$

$$I(s) = \frac{100s}{(s^2 + 100)(s + 1)}$$

By Partial fraction.

$$I(s) = \frac{A}{s+1} + \frac{Bs+D}{s^2+100}$$

$$\frac{100}{(s^2+100)(s+1)} = \frac{A}{s+1} + \frac{Bs+D}{s^2+100}$$

$$100_s = A(s^2+100) + Bs(s+1) + D(s+1)$$

$$s = -1$$

$$\Rightarrow A = \frac{-100}{101} = -0.99$$

$$s = 0$$

$$\Rightarrow D = \frac{100 \cdot 100}{101} = 99$$

$$\Rightarrow B = 0.99$$

$$\therefore I(s) = \frac{-0.99}{s+1} + \frac{0.99s+99}{s^2+100}$$

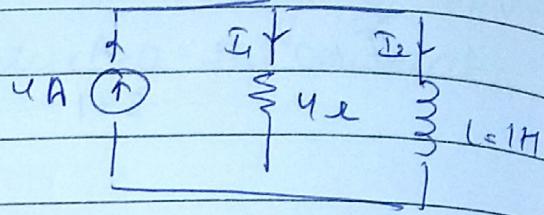
$$= -\frac{0.99}{s+1} + \frac{0.99s}{s^2+100} + \frac{99}{s^2+100} \times \frac{10}{10}$$

Taking L.I

$$i(t) = \underbrace{-0.99 e^{-t}}_{\text{Am}} + 0.99 \cos(10t) + 9.9 \sin(10t)$$

$$I = I_1 + I_2$$

$$V = \frac{V(t)}{R} + \frac{1}{L} \int_0^t V(t) dt$$



Diff

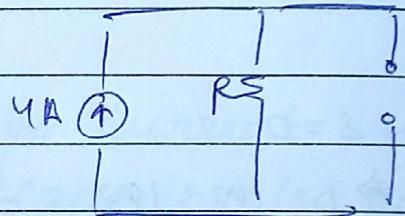
$$0 = \frac{1}{R} \frac{dV(t)}{dt} + \frac{V(t)}{L}$$

$$\Rightarrow \frac{dV(t)}{dt} + \frac{R}{L} V(t) = 0$$

$$V(t) = Ke^{-R/L \cdot t} \quad V$$

At  $t = 0^+$ , our inductor device behaves as 0.c'

$$\therefore V(0^+) = 4 \times 4 \\ = 16 \text{ V}$$



$$\text{At } t = 0^+ \\ 16 = Ke^{-R/L \times 0}$$

$$\Rightarrow \boxed{K = 16}$$

$$\therefore \underline{V(t) = 16 \cdot e^{-4t} \text{ V}}$$

$$i_R(t) = \frac{V(t)}{R} = \frac{16 \cdot e^{-4t}}{4} \quad \left. \begin{array}{l} i_L(t) = \frac{1}{L} \int_0^t V(t) dt \\ = \frac{1}{1} \int_0^t 16 e^{-4t} dt \end{array} \right\}$$

$$\underline{i_R(t) = 4e^{-4t} \text{ Amp}}$$

$$= -\frac{16}{4} \int e^{-4t} dt$$

$$= 4(1 - e^{-4t}) \text{ Amp}$$

$$\frac{V}{R} = -V$$

Taking L.T.

$$\frac{Y}{S} = \frac{V(S)}{R} + \frac{V(S)}{S \cdot L}$$

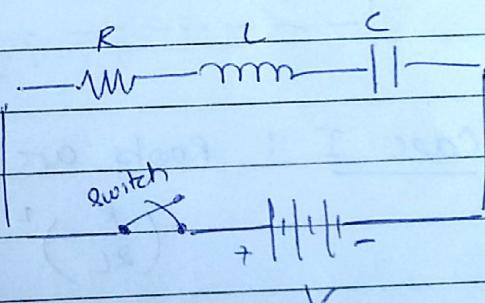
$$\Rightarrow \frac{Y}{S} = \frac{V(S)}{R} + \frac{V(S)}{S}$$

$$\Rightarrow V(S) = \frac{Y \cdot Y}{S+Y}$$

∴

### Transient response of RLC circuit in DC source

$$Ri(t) + L \cdot \frac{di(t)}{dt} + \frac{1}{C} \int_0^t i(t) dt = V$$



On diff.

$$\Rightarrow R \frac{di(t)}{dt} + L \cdot \frac{d^2i(t)}{dt^2} + \frac{i(t)}{C} = 0$$

$$\Rightarrow \frac{d^2i(t)}{dt^2} + \frac{R}{L} \frac{di(t)}{dt} + \frac{i(t)}{LC} = 0$$

$$\frac{d}{dt} \rightarrow P$$

$$\Rightarrow \left( P^2 + \frac{R \cdot P}{L} + \frac{1}{LC} \right) i(t) = 0$$

$$\therefore P^2 + \frac{R}{L}P + \frac{1}{LC} = 0$$

$$\Rightarrow P = -\frac{R}{2L} \pm \sqrt{\left(\frac{R}{2L}\right)^2 - \frac{1}{LC}}$$

$$\Rightarrow P = -\frac{R}{2L} \pm \sqrt{\left(\frac{R}{2L}\right)^2 - \frac{1}{LC}}$$

$$\therefore P_1 = \alpha + \beta \quad \text{and} \quad P_2 = \alpha - \beta$$

NOTE: Solution for 2nd order linear differential equation

$$i(t) = C_1 e^{\alpha t} + C_2 e^{\beta t}$$

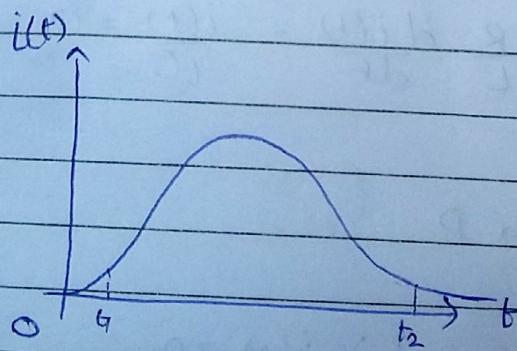
where  $C_1$  &  $C_2$  are constants

Case I: Roots are real & unequal

$$\left(\frac{R}{2L}\right)^2 > \frac{1}{LC}$$

over damping situation

$$\begin{aligned} \therefore i(t) &= C_1 e^{(\alpha+\beta)t} + C_2 e^{(\alpha-\beta)t} \\ &= e^{\alpha t} [C_1 e^{\beta t} + C_2 e^{-\beta t}] \end{aligned}$$



Over damping  
of current

Case II : Roots are imaginary and complex conjugate of each other

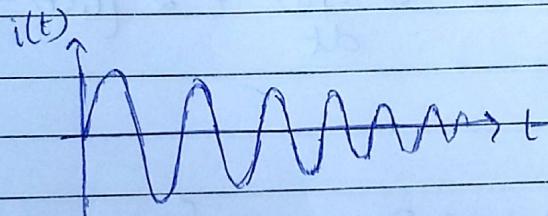
$$\left(\frac{R}{2L}\right)^2 < \frac{1}{LC}$$

oscillation

$$\therefore \alpha = * \beta$$

$$P_1 = \alpha + j\beta \quad \text{and} \quad P_2 = \alpha - j\beta$$

$$\begin{aligned} i(t) &= c_1 e^{(\alpha+j\beta)t} + c_2 e^{(\alpha-j\beta)t} \\ &= e^{\alpha t} [c_1 e^{j\beta t} + c_2 e^{-j\beta t}] \\ &= e^{\alpha t} [c_1 (\cos \beta t + j \sin \beta t) + c_2 (\cos \beta t - j \sin \beta t)] \\ &= e^{\alpha t} [(c_1 + c_2) \cos \beta t + j (c_1 - c_2) \sin \beta t] \end{aligned}$$



Oscillations

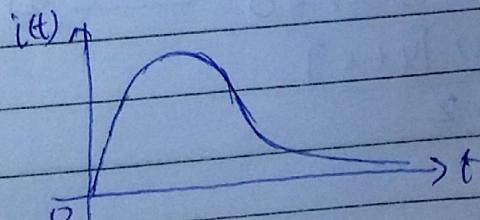
Case III : Roots are equal & real

$$\left(\frac{R}{2L}\right)^2 = \frac{1}{LC}$$

critical  
damped

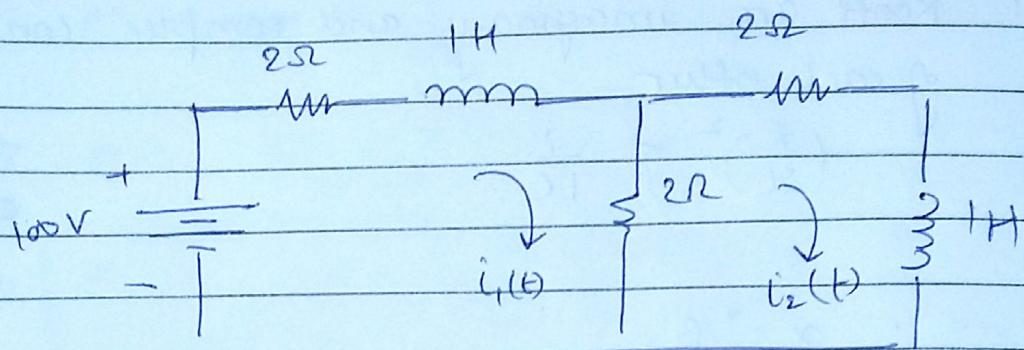
$$\therefore P_1 = P_2 = \gamma$$

$$\begin{aligned} i(t) &= c_1 e^{\gamma t} + c_2 t e^{\gamma t} \\ &= (c_1 + c_2 t) e^{\gamma t} \end{aligned}$$



critical damped

I =



Assume that the inductor is initially fully discharged.

$$\cancel{2i_1(t)} = 2i_2(t) + L \frac{di_2(t)}{dt}$$

Mesh ①

$$100 = 2i_1(t) + \frac{d}{dt} i_1(t) + 2[i_1(t) - i_2(t)]$$

Taking L.T.

$$\frac{100}{s} = 2I_1(s) + 8I_2(s) + 2[I_1(s) - I_2(s)]$$

$$\Rightarrow \frac{100}{s} = I_1(s)[4+8] - 2I_2(s) \quad \text{--- ①}$$

Mesh ②

$$2i_2(t) + \frac{di_2(t)}{dt} + 2[i_2(t) - i_1(t)] = 0$$

Taking L.T.

$$2I_2(s) + 8I_2(s) + 2[I_2(s) - I_1(s)] = 0 \quad \text{---}$$

$$\Rightarrow I_2(s)(4+8) - 2I_1(s) = 0 \quad \text{--- ②}$$

$$\Rightarrow I_1(s) = \frac{I_2(s)[4+8]}{2}$$

: ① will be

$$\frac{100}{8} = I_2(s) \frac{(4+s)^2}{2} - 2 I_2(s)$$

$$\Rightarrow \frac{100}{8} = I_2(s) \left[ \frac{(4+s)^2}{2} - 2 \right]$$

$$\Rightarrow \frac{100}{8} = I_2(s) \left( \frac{16 + s^2 + 8s - 4}{2} \right)$$

∴