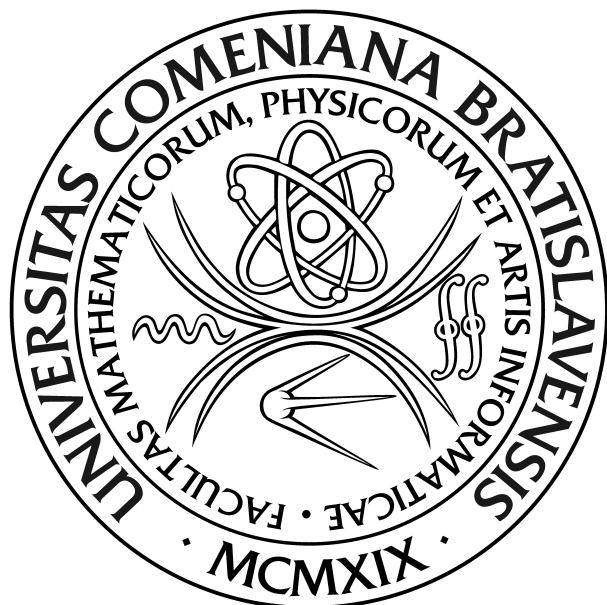


Comenius University
Faculty of Mathematics, Physics and Informatics

DIPLOMA THESIS



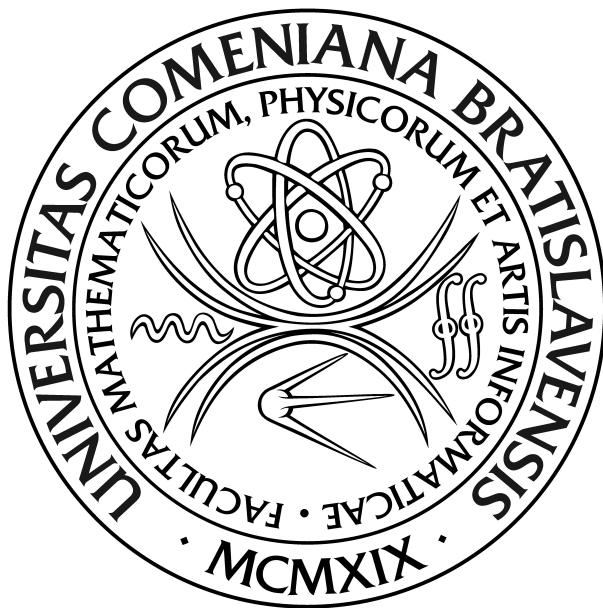
Jakub Bahyl

Drag Force Scaling and Quantum Turbulence in Superfluid Helium

Bratislava, 2018

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DIPLOMA THESIS



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Drag Force Scaling and Quantum Turbulence in Superfluid Helium

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Study programme: Condensed Matter Physics

Study programme number: 1160 Physics

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Názov: Drag Force Scaling and Quantum Turbulence in Superfluid Helium
Škálovanie odporových sôl a kvantová turbulencia v supratekutom héliu

Anotácia: Práca pozostáva z dvoch základných častí - experimentálnej a numerickej. Experimenty v supratekutom héliu predstavujú hlavnú náplň práce a budú vykonávané prevažne v oblasti dvojzložkového režimu supratekutého hélia (nad teplotou 1 K), pričom v spracovaní použijeme dodatočné dátá z oblasti balistického režimu (pod teplotou 0,6 K). V práci overíme nedávno navrhnutú univerzálnu škálovaciu funkciu popisujúcu odporové sily v oscilačnom prúdení v limite vysokého Stokesova čísla. Zatiaľ čo merania v dvojzložkovom režime môžu byť doplnené o dátá z tlmenia druhého zvuku, ktoré sú štandardným postupom pre meranie množstva kvantových vírov, merania v oblasti mK teplôt budú úplne závislé na skúmaní rezonančných vlastností použitých oscilátorov. V numerickej časti sa budeme zaoberať štúdiom dynamiky izolovaného kvantového víru v tvaru krúžku pomocou modelu vírových vláken - v jeho zjednodušenej forme lokálnej indukcie a zároveň aj v tej zložitejšej s pomocou výpočtu podľa analógie s Biot-Savartovým zákonom. Overíme taktiež aj platnosť numerických algoritmov preskúmaním správania sa voľne pohybujúcich kvantových vírových krúžkov.

Ciel: Náplňou tejto práce je použitie mechanických rezonátorov, napr. v tvaru vidličky, drôtokov alebo diskov na účel výskumu pôsobenia supratekutého hélia v jeho dvojzložkovom režime pri teplotách medzi 2,17 K a 1 K. Hlavným zámerom týchto experimentov je štúdium odporových sôl, ktoré pôsobia v supratekutom héliu a štúdium podmienok nukleácie a vývoja kvantovej turbulencie. Pri spracovaní výsledkov budú použité doplnkové dátá odmerané v balistickej režime pri teplotách pod 0,6 K. Študent získa skúsenosti s komplexnými aparáturami využívajúcimi v kryogennych experimentoch a rozšíri si vedomosti v oblasti kvantových kvapalín a supratekutých efektov. Celková práca bude doplnená o vývoj a validáciu numerických nástrojov pre simuláciu dynamiky kvantových vírov v supratekutom héliu.

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Lastly, I would like to express my disappointment about faculty recommendation to use *Mathworks* software company's products (Matlab), use of which extended all my data processing works into an abnormal time scale.

I declare that I carried out this master thesis independently, and only with the cited sources, literature and other professional sources.

In date

Signature of the author:

Názov práce

Škálovanie odporových sôl a kvantová turbulencia v supratekutom héliu

Autor

Jakub Bahyl

Školiteľ bakalárskej práce

RNDr. David Schmoranzer, Ph.D.

Abstrakt

V tejto diplomovej práci prezentujeme meranie kvantovej turbulencie generovanej viacerými oscilujúcimi rezonátormi (*kremenné oscilátory, vibrujúce drôty a torzné disky*) pri viacerých teplotách v škále $1.0 \text{ K} < T < 2.17 \text{ K}$. Hlavná pointa experimentálnej časti je analýza vzniku kvantovej turbulencie a odporových sôl normálnej a supratekutej zložky. Zozbierané dátá sú spolu s dátami z balistického režimu $T < 0.6 \text{ K}$ použité aj ako test tzv. *univerzálneho škálovania* popisujúceho odporové sily v režime vysokých Stokesových čísel oscilačného prúdenia.

Experimentálna časť je doložená numerickou implementáciou a validáciou programu, vyvinutého pre účel simulovania dynamiky kvantovaných vírov. V tejto časti skúmame použiteľnosť programu postaveného na princípe modelu *Vírových filamentov*.

Kľúčové slová

supratekutosť ${}^4\text{He}$ • kvantová turbulencia • vírový filament

Title

Drag Force Scaling and Quantum Turbulence in Superfluid Helium

Author

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Abstract

In this Thesis, mechanical resonators such as *tuning forks, wires are discs* are used to probe superfluid helium in the two-fluid regime at temperatures between temperatures $1.0 \text{ K} < T < 2.17 \text{ K}$. The principal aim of the experimental part is to study the drag forces arising from the superfluid and the nucleation and development of quantum turbulence. The obtained data, also with those from the ballistic regime $T < 0.6 \text{ K}$, are used to test a proposed *Universal scaling relation* describing the drag forces in high-Stokes-number oscillatory flow.

The experimental work is complemented by developing and validating the tools necessary for numerical simulations of quantized vortex dynamics in superfluid helium. In this part, dynamics of a single quantized vortex ring are studied using the *Vortex filament model*.

Keywords

superfluidity of ${}^4\text{He}$ • quantum turbulent • vortex filament

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Introduction

To this day, turbulent motion of fluids remains the last unresolved problem of classical physics. They present many practical challenges across different areas of industry (e.g. weather prediction). Quantum turbulence, in contrast, may occur only in superfluids and was first observed in superfluid state of ^4He . Compared to classical turbulence, it can be regarded as a simpler system from the theoretical and numerical point of view. Also, it shares many of the general properties of turbulence in classical viscous fluids.

In very low temperatures, the liquid state of ^4He exists in two phases:

- Helium-I: a high temperature liquid phase ($2.17\text{ K} < T < 4.2\text{ K}$)
- Helium-II: a low temperature superfluid phase ($T < 2.17\text{ K}$)

These two phases are connected with the *lambda transition*, as sketched in **Figure 1**, which occurs at the critical temperature $T_\lambda = 2.17\text{ K}$ at saturated vapor pressure . Helium-I is a classical fluid described by ordinary Navier-Stokes (N-S) equations, whereas Helium-II is a superfluid and behaves partly like a Bose-Einstein condensate.

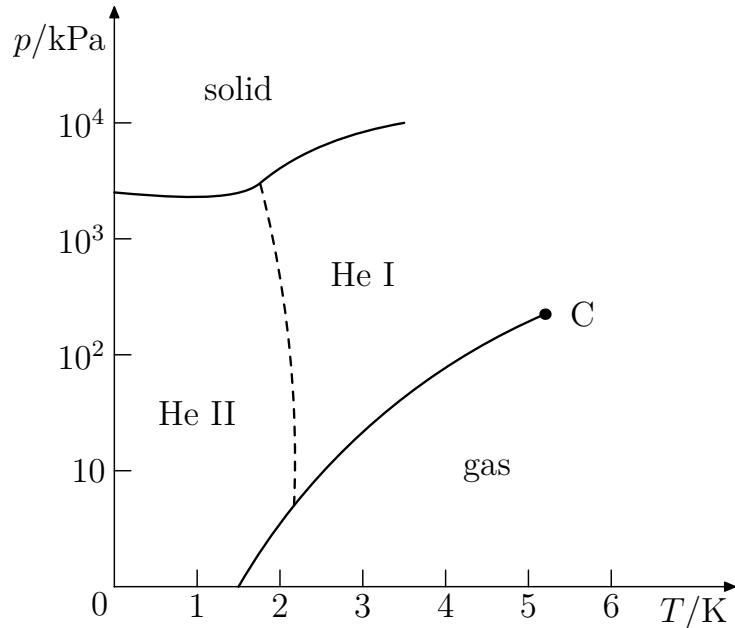


Figure 1: Pressure-Temperature diagram of ^4He . With a fixed pressure on the atmospheric value, a gas-liquid transition is present at temperature 4.2 K (He-I) and a superfluid transition near 2.17 K .

A simple, phenomenological model of the Helium-II composition was proposed by Tisza [1] and Landau [2], called as *two-fluid model*. According to this model, Helium-II behaves

as if composed of two inter-penetrating liquids - a *normal* and a *superfluid* component - with corresponding velocity fields and temperature-dependent, described as:

- normal component: density $\rho_n(T)$, velocity field $\mathbf{v}_n(\mathbf{r}, t)$, motion described by an ordinary viscous Navier-Stokes equation, carrying entropy and represented as a collection of thermal excitations.
- superfluid component: density $\rho_s(T)$, velocity field $\mathbf{v}_s(\mathbf{r}, t)$, motion described by a modified Euler equation (without viscosity) with quantum terms, carrying zero entropy and represented by a macroscopic wave function.

The total density of Helium-II sums up to $\rho = \rho_n(T) + \rho_s(T) \approx \text{const}$ and the relative proportion of normal/superfluid component is determined mainly by the temperature, as plotted in **Figure 2**.

Near $T \rightarrow 0$ Helium-II becomes entirely superfluid $\rho_s/\rho \rightarrow 1$, however, the temperature dependence of this ratio is highly nonlinear. For instance, the ratio ρ_n/ρ drops from 100% at 2.17 K to 50% at 1.95 K, to < 5% at 1.3 K, and is effectively negligible under 1 K.

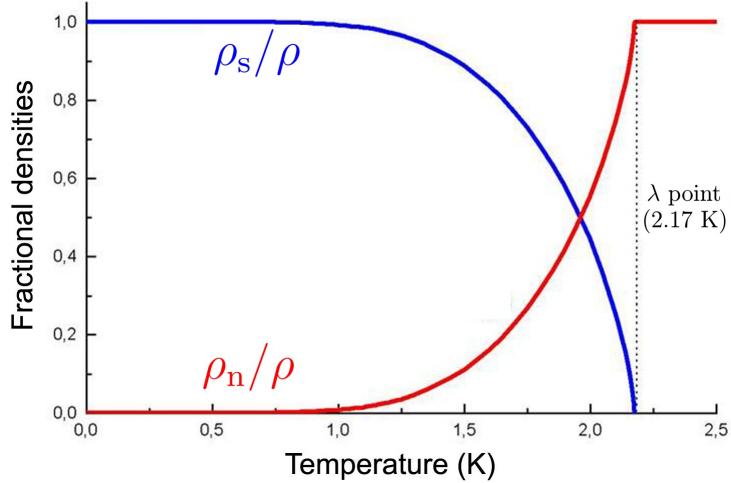


Figure 2: Temperature dependence of fractional densities of the normal (red) and superfluid (blue) components. Source:[25]

It arises from the quantum nature of Helium-II, that the superfluid component should not perform any rotation. However, when this component moves faster than a critical velocity, the circulation is *quantized* and so-called *quantized vortices* are created, which makes the hydrodynamics of Helium-II particularly interesting. However, the vortex nucleation process is still a subject of many current investigations.

Superfluid vortex lines were observed spatially organized [3], but also completely disorganized as showed also by a simulation in **Figure 3**. Quantum turbulence therefore usually

takes the form of a chaotic tangle of quantized vortices in the superfluid component which typically coexist with classical turbulent flow of the normal component.

In the presence of quantized vortices, the seemingly independent normal and superfluid velocity fields become coupled by the *mutual friction* force which arises due to quasiparticles scattering off the cores of vortices. More details about this interaction are provided in **Theoretical Background** chapter.

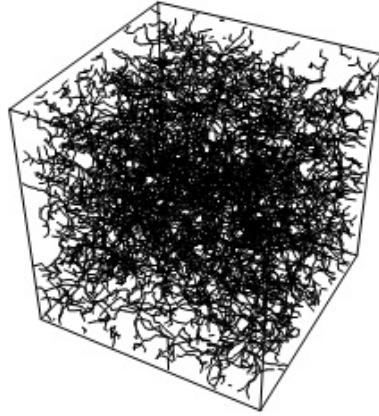


Figure 3: Cube of numerically simulated tangle of randomly distributed quantized vortices. Source:[25]

Quantum turbulence can be experimentally achieved in many traditional ways - driving a mass flow, spinning discs, oscillating grids and forks, ultrasound and jets. In order to characterize the turbulence, one may use a superfluid Reynolds number for steady flows, or a newly introduced (the last section of **Theoretical Background** chapter) *Donnelly number* for high-frequency oscillatory flows.

We find (see **Results** chapter) that for quantum turbulence originated in such high-frequency oscillation regime at temperatures $T > 1\text{ K}$, the measured drag forces are described in terms of a single dimensionless parameter and exhibit an *universal scaling* behavior. We identify and compare the critical conditions related to the production of both quantized vorticity and instabilities occurring in normal component.

Also we note that if we cool the experimental system below $\lesssim 0.6\text{ K}$, a transition to ballistic regime occurs in the normal component, as the mean free path of phonons exceeds the characteristic dimensions of the experimental setup. This situation is similar to the one of dilute classical gases, so the hydrodynamical description of the system is no longer valid. We discuss the applicability of *universal scaling* for such system in **Conclusions** chapter.

Besides experimental approaches on quantum fluids, one of the useful tools for understanding the geometry and flow of quantum turbulence, is the *vortex filament model*, pioneered by Schwarz [26] in late 80's. With the rapid development of available com-

putational power, large simulations have become the methods of choice for calculating the motion of fluids. In superfluids like Helium-II, due to the quantization of circulation, vorticity can only exist within vortex filaments with a certain core size, which makes the model highly applicable.

In this Thesis, we also propose an efficient numerical method to compute the time evolution of vortex filaments in superfluid Helium-II. We studied the performance and stability and well replicated the physical processes such as the annihilation of quantized vortex rings [4] phenomena while traveling across superfluid.

Hence, we present the `PyVort` codebase, a new platform in `Python 3` to simulate quantized rings motion. The implementation details are provided in **Simulation** chapter.

Motivations and Goals

Here we briefly present all motivations and goals plan that led us to our investigations with oscillators in superfluid Helium-II and vortex simulations we performed.

Experiments and Data analysis

- **construct** a low-temperature experiment using flow generators such as *vibrating wire, tuning fork and oscillating disc* in order to observe the drag phenomena
- **investigate** transition from laminar/potential flow of normal/superfluid components, respectively, to *classical, quantum and mixed turbulence* at various temperatures $T > 1 \text{ K}$ in a high-frequency regime.
- **apply** universal scaling method, **prove** the concept on collected experimental data and **test** the limitations using the ultra-low temperature data

Simulation

- **build** modular and reusable codebase in `Python 3` that simulates the dynamics of quantized vortices using the *Vortex Filament* model
- **implement** stable *stepping methods* and a reliable *re-segmentation process* that allows keeping a good resolution of quantized vortices in different situations
- **simulate** a real-time vortex ring motion and **compare** its properties evolving in time with the theoretical approaches, thus **validating** the new codebase

1. Theoretical Background

The theoretical part of this Thesis is composed of two chapters:

1. Micro/Meso-scopic view - provides a theoretical cover of Gross-Pitaevskii model of Helium-II, quantized vortex description, properties and motion, numerical modeling of such vortex and a brief view on quantized ring dynamics
3. Macroscopic view - provides a hydrodynamic description of two-fluid model, dynamical similarity principle, oscillatory flows in both classical viscous and superfluid He-II, creation of quantum turbulence, universal scaling principles and ultra-low temperature regime differences

The aim of this chapter is to introduce the basic properties of quantized vortex lines in Helium-II and summarize the state of art of current knowledge on superfluid turbulence. We also discuss the theoretical methods used to study quantized vorticity, quantum turbulence and some results obtained using such methods.

Micro/Meso-scopic view

One of the most useful ways of describing superfluid ^4He at $T = 0\text{ K}$ starts with non-linear Schrodinger equation (NLSE) for the one-particle wave function ψ . Since the superfluid ^4He is a strongly correlated system dominated by collective effects, this imperfect Bose-Einstein condensate (BEC) is approximately described by Gross-Pitaevskii equation (1.1). Although, it must be noted that the real Helium-II is a dense fluid, not a weakly interacting Bose gas described by NLSE.

1.1 Gross-Pitaevskii model

In terms of single-particle wavefunction $\psi(\mathbf{r}, t)$ we write the Gross-Pitaevskii model:

$$i\hbar \frac{\partial \psi}{\partial t} = -\frac{\hbar^2}{2m} \nabla^2 \psi + \psi \int |\psi(\mathbf{r}', t)|^2 V(|\mathbf{r} - \mathbf{r}'|) d\mathbf{r}', \quad (1.1)$$

where $V(|\mathbf{r} - \mathbf{r}'|)$ is the potential of two-body interaction between bosons. The normalization is set as $\int |\psi|^2 d\mathbf{r} = N$, where N is number of bosons. By replacing potential with repulsive δ -function of strength V_0 one obtains:

$$i\hbar \frac{\partial \Psi}{\partial t} = -\frac{\hbar^2}{2m} \nabla^2 \Psi - m\varepsilon \Psi + V_0 |\Psi|^2 \Psi, \quad (1.2)$$

where ε is the energy per unit mass and $\Psi = A e^{i\Phi}$ is a macroscopic wave function of condensate. In this way one can define the condensate's density $\rho_{BEC} = m\Psi\Psi^* = mA^2$ and velocity $\mathbf{v}_{BEC} = (\hbar/m)\nabla\Psi$. Note that equation (1.2) is equivalent to a continuity equation and a Euler equation (however, modified by the so called *quantum pressure term*).

Hereafter we identify ρ_{BEC} with ^4He superfluid component's ρ_s at absolute zero and \mathbf{v}_{BEC} with \mathbf{v}_s . It must be noted that this identification is convenient from the point of view of having a simple hydrodynamics model but is not entirely correct. The reason is that Helium-II is a dense fluid, not the weakly interacting Bose gas described by the NLSE (1.1), so the condensate is not the same as the superfluid component.

Even though the superfluid is irrotational: $\omega = \nabla \times \mathbf{v}_s = \mathbf{0}$, the NLSE has a vortex-like solution: $\mathbf{v}_s = \varkappa / 2\pi r \mathbf{e}_\theta$, where θ is the azimuthal angle and $\varkappa = 9.97 \times 10^{-8} \text{ m}^2/\text{s}$ is the *quantum of circulation*, obtained from:

$$\varkappa = \oint_{\mathcal{C}} \mathbf{v}_{BEC} \cdot d\ell = \frac{\hbar}{m}, \quad (1.3)$$

where \mathcal{C} is a closed loop surrounding the vortex core - a topological defect within macroscopic wavefunction Ψ , as sketched in **Figure 1.1**.

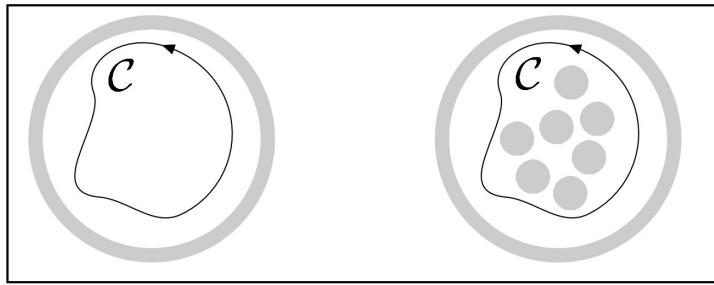


Figure 1.1: An illustration of topological singularities within a superfluid ${}^4\text{He}$. Left: A singly-connected irrotational region with circulation along \mathcal{C} loop equal to zero. Right: A multiply-connected region with depicted cores of quantized vortices with a finite circulation along \mathcal{C} loop.

1.2 Quantized vortex

As Feynman showed [5], superfluid vortex lines appear when Helium-II moves faster than a certain critical velocity. The simplest way to create quantized vortices is to rotate cylinder with superfluid Helium-II with high enough angular velocity Ω . Created vortex lines form an ordered array of density $L = 2\Omega/\varkappa$, all aligned along the axis of rotation, as sketched in **Figure 1.2**. *Vortex line density* L is usually interpreted as a total vortex length in a unit volume.

The key properties of Onsager-Feynman vortex [6] are the quantized circulation \varkappa , local superfluid rotational velocity field $v_s = \varkappa / 2\pi r$ and the *vortex core size* a_0 . The core size a_0 can be estimated by substituting v_s back into equation (1.2) and solving the resultant differential equation for $\rho_s(\mathbf{r})$. One finds that $\rho_s(\mathbf{r})$ tends to the bulk value $m^2\varepsilon/V_0$ for $r \rightarrow \infty$ from the vortex and to zero density for $r \rightarrow 0$. The characteristic distance over which Ψ collapses (superfluid density ρ_s drops $m^2\varepsilon/V_0 \rightarrow 0$) is $a_0 \approx 10^{-10} \text{ m} \equiv 1 \text{ \AA}$. From this, there is a conclusion that the vortex is hollow at its core and therefore, a topological defect occurs.

Taking a_0 as core radius, the energy considerations showed that a single vortex containing

N circulation quanta owns more energy than N singly-quantized vortices. Hence it is generally assumed that only ground-state vortices are commonly observed.

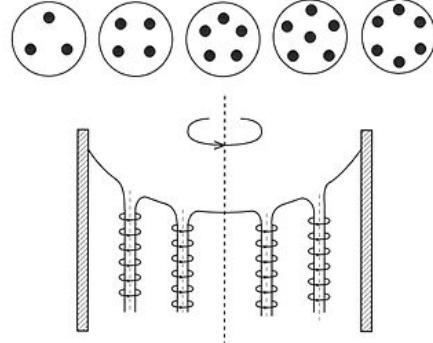


Figure 1.2: Array of quantized vortices in a rotating container. The 5 images at the top mark the position of various number of vortex lines from the upper point of view.

Clearly, vortex lines don't have to be aligned in general. In most cases , the superfluid flow is strongly chaotic, better known as *quantum turbulence*. This topic is covered in more detail later in this work.

1.3 Vortex filament model

The vortex line can be represented as a curve via position vector $\mathbf{s} = \mathbf{s}(\xi, t)$ in three-dimensional space. Here, ξ is arclength along the vortex line. Next we label \mathbf{s}' as $d\mathbf{s}/d\xi$ and \mathbf{s}'' as $d\mathbf{s}'/d\xi$. Within our context, \mathbf{s}' is a tangent vector and $|\mathbf{s}''|$ is a local curvature R^{-1} at a given point. The triad of vectors $\mathbf{s}', \mathbf{s}'', \mathbf{s}' \times \mathbf{s}''$ are perpendicular to each other, as sketched in **Figure 1.3**, and point along the tangent, normal and binormal respectively:

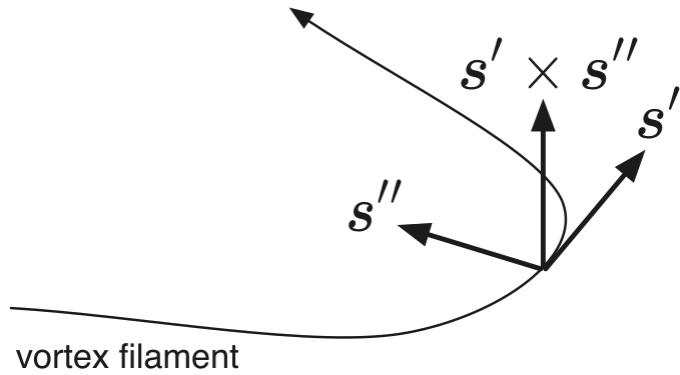


Figure 1.3: Schematic of the vortex filament and the triad vectors $\mathbf{s}', \mathbf{s}'', \mathbf{s}' \times \mathbf{s}''$. Source:[27]

We suppose that the superfluid component is incompressible $\nabla \cdot \mathbf{v}_s = 0$. Moreover, superfluid vorticity ω_s is localized only at positions of vortex filament $\omega_s(\mathbf{r}, t) = \nabla \times \mathbf{v}_s$.

Combining these two properties gives the Poisson equation $\Delta\phi = \omega_s$ for the potential ϕ . Using Fourier transform one obtains [13] the Biot-Savart law for the superfluid velocity:

$$\mathbf{v}_s(\mathbf{r}) = \frac{\kappa}{4\pi} \int_{\mathcal{L}} \frac{(\mathbf{r}' - \mathbf{r}) \times d\mathbf{r}'}{|\mathbf{r}' - \mathbf{r}|^3}, \quad (1.4)$$

where the integral path \mathcal{L} represents curves along all vortex filaments.

This law determines the superfluid velocity field $\mathbf{v}_s(\mathbf{r})$ via the arrangement of the vortex filaments. Now we define the *self-induced* velocity \mathbf{v}_{ind} , describing the motion which a vortex line induces onto itself ($\mathbf{r} \rightarrow \mathbf{s}$ in (1.4)) due to its own curvatures:

$$\mathbf{v}_{\text{ind}}(\mathbf{s}) = \frac{\kappa}{4\pi} \int_{\mathcal{L}} \frac{(\mathbf{r}' - \mathbf{s}) \times d\mathbf{r}'}{|\mathbf{r}' - \mathbf{s}|^3} \quad (1.5)$$

However, this integral (1.5) diverges as $\mathbf{r}' \rightarrow \mathbf{s}$ because the core structure of the quantized vortex was initially neglected. We avoid this divergence by splitting the integral into two parts - direct neighborhood of the point \mathbf{s} (local part) and the rest \mathcal{L}' (nonlocal part). The Taylor expansion of the local part leads [26] to a finite result:

$$\mathbf{v}_{\text{ind}}(\mathbf{s}) = \mathbf{v}_{\text{ind,local}} + \mathbf{v}_{\text{ind,nonlocal}} \approx \beta \mathbf{s}' \times \mathbf{s}'' + \frac{\kappa}{4\pi} \int_{\mathcal{L}'} \frac{(\mathbf{r}' - \mathbf{s}) \times d\mathbf{r}'}{|\mathbf{r}' - \mathbf{s}|^3}, \quad (1.6)$$

$$\text{where } \beta = \frac{\kappa}{4\pi} \ln(R/a_0), \quad (1.7)$$

where \mathcal{L}' is the original vortex line without a close area of the studied vortex point and R is a *local curvature* and often is calculated as $1/|\mathbf{s}''|$ [26].

Since the local part of induced velocity (1.6) is a dominant term (and also computationally faster), the nonlocal part can be neglected. Such approximation process is called as *Local Induction Approximation* (LIA). LIA represents the contribution of local curvature to the induced velocity, whereas nonlocal Biot-Savart part represents the global filament curvature.

Since in the system there could be present also external flow sources of superfluid component (e.g. heat resistors causing *counterflows*), we define the total superfluid velocity $\mathbf{v}_{s,tot}$, in a laboratory frame, as:

$$\mathbf{v}_{s,tot} = \mathbf{v}_{s,ext} + \mathbf{v}_{\text{ind}} \quad (1.8)$$

1.4 Vortex dynamics

To determine the equation of motion of $\mathbf{s}(t)$ we recognize the forces acting upon the line - the Magnus force \mathbf{f}_M and (at non-zero temperature $T > 0 \text{ K}$) the drag force \mathbf{f}_D (both are per unit length).

The Magnus force \mathbf{f}_M always arises when a rotating body moves in a flow. This causes a pressure difference, which in our case of moving vortex line with circulation quantum \varkappa , exerts a force:

$$\mathbf{f}_M = \rho_s \varkappa \mathbf{s}' \times (\dot{\mathbf{s}} - \mathbf{v}_{s,tot}), \quad (1.9)$$

where $\dot{\mathbf{s}} = d\mathbf{s}/dt$ is the velocity of a particular point on a vortex line.

The drag force \mathbf{f}_D arises from the *mutual friction*, the interaction between the normal component and vortex lines (quantized superfluid component). According to the findings of Vinen and Hall [7], the normal fluid flowing with velocity \mathbf{v}_n past a vortex core exerts a frictional force \mathbf{f}_D on the vortex line, given by:

$$\mathbf{f}_D = -\alpha(T) \rho_s \varkappa \mathbf{s}' \times [\mathbf{s}' \times (\mathbf{v}_{ns} - \mathbf{v}_{ind})] \quad (1.10)$$

$$-\alpha'(T) \rho_s \varkappa \mathbf{s}' \times (\mathbf{v}_{ns} - \mathbf{v}_{ind}), \quad (1.11)$$

where $\mathbf{v}_{ns} = \mathbf{v}_n - \mathbf{v}_{s,ext}$ is the difference between the average velocity of normal component and the applied superfluid velocity.

The temperature dependent dimensionless parameters $\alpha(T)$ and $\alpha'(T)$ are often written in terms of measured *mutual friction parameters* B and B' , which are known from experiments by Samuels and Donnelly [8]:

$$\alpha(T) = \frac{\rho_n B(T)}{2\rho} \quad \alpha'(T) = \frac{\rho_n B'(T)}{2\rho} \quad (1.12)$$

The precise calculation of the mutual friction parameters $B(T), B'(T)$ over the entire temperature range is still an open problem. Although, we already know that in the area of high temperatures, the friction arises mainly from the scattering processes of rotons.

Since the mass of vortex core is usually neglected, the two forces \mathbf{f}_M and \mathbf{f}_D add up to zero: $\mathbf{f}_M + \mathbf{f}_D = \mathbf{0}$. Hence, solving for $d\mathbf{s}/dt$, we obtain [26] the Schwarz's equation:

$$\dot{\mathbf{s}} = \mathbf{v}_{s, \text{ext}} + \mathbf{v}_{\text{ind}} + \mathbf{v}_{\text{drive}}, \text{ where} \quad (1.13)$$

$$\mathbf{v}_{\text{drive}} = \alpha \mathbf{s}' \times (\mathbf{v}_{ns} - \mathbf{v}_{\text{ind}}) - \alpha' \mathbf{s}' \times [\mathbf{s}' \times (\mathbf{v}_{ns} - \mathbf{v}_{\text{ind}})] \quad (1.14)$$

On the basis of Schwarz's equation (1.13), algorithms to numerically simulate vortex time evolution of an arbitrary configuration can be developed. Also, the vortex parametrization $\mathbf{s}(\xi, t)$ and dynamics description provide the baseline of what we call as Vortex Filament (VF) model. More on VF model is written later in **Simulation** chapter.

Quantized vortex rings

A special case of vortex line configuration are a freely moving vortex rings. Such rings are usually created as a result of multi-vortex interconnections [4] or by the self-reconnection of an oscillating loop pinned to the surface of a vibrating body. The exact expressions derived from the Gross-Pitaevskii equation (1.1) [9] for the energy E and induced center velocity v_{ind} of a vortex ring, moving in a Helium-II of density ρ and having a radius R much greater than its core radius $R \gg a_0$, are:

$$E = \frac{1}{2} \kappa^2 \rho R \left(\ln(8R/a_0) - 2 + c \right) \quad (1.15)$$

$$v_{\text{ind}} = \frac{\kappa}{4\pi R} \left(\ln(8R/a_0) - 1 + c \right), \quad (1.16)$$

where c is a constant based on inner structure of the vortex. Since we work with hollow core, we use [10] $c = 1/2$. Note that (1.15) and (1.16) depend on a_0 only logarithmically. The behavior of the vortex ring is thus quite insensitive to the exact value of a_0 (expected to be of the order of atomic dimension).

Relations (1.15) and (1.16) are derived directly from Gross-Pitaevskii description and no dissipative process (mutual friction) was included. Therefore, the relations hold only for temperature $T = 0$ K.

Using the explicit dynamical equation [10] for vortex ring motion, one can also derive the final ring center velocity \mathbf{v}_{ring} and energy E_{ring} using (1.15) and (1.16) like:

$$\mathbf{v}_{\text{ring}} = (1 - \alpha')(\mathbf{v}_{\text{ind}} - \mathbf{v}_{\text{s, ext}}) + \alpha' \mathbf{v}_{\text{n, ext}} \quad (1.17)$$

$$E_{\text{ring}} = \left(\frac{\alpha}{1 - \alpha'} \right) E \quad (1.18)$$

Several other interesting results come from the ring's dynamic motion equation and the mutual friction formula (1.10), (1.11). The second term (1.11) of friction force causes the decrease of vortex ring radius, whereas the first term (1.10) is the dissipative term. The superfluid vortex ring (**Figure (1.4)**) living in a mixture of a normal and superfluid component has therefore a limited lifetime expectancy and the traveled distance.

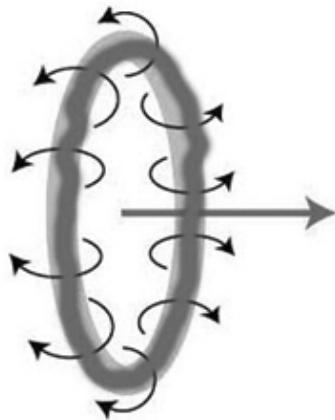


Figure 1.4: Depiction of quantized vortex ring motion and induced velocity field. Source: Huang, Kerson, *Quantum vorticity in nature*, arXiv.

More explicitly, it was shown [10] that in case of weak counterflow velocity \mathbf{v}_{ns} , the lifetime of vortex ring can be expressed as a simple relation:

$$\tau_{\text{ring}} = \frac{R_0}{2\alpha |\mathbf{v}_{\text{ring}}(R_0)|}, \quad (1.19)$$

where R_0 is the initial radius of created vortex ring.

By integrating the ring's motion equation from R_0 to $R(\tau) \approx a_0$ we obtain the distance traveled by the ring's center:

$$D_{\text{ring}} = \frac{\alpha}{1 - \alpha'} (R_0 - a_0) \quad (1.20)$$

Relations (1.19) and (1.20) are taken as a baseline in **Simulation** chapter.

Macroscopic view

Besides NLSE and Vortex filament model, there is also a third, *macroscopic* model in which the individual vortex lines are *invisible* and the superfluid component of Helium-II is considered as a continuous flow of vortices. Many phenomena are similar to those in classical hydrodynamics (some of them are illustrated in **Figure 1.5**), but there emerge also new and very special type of events that can happen within superfluid Helium-II, such as *second sound* or *counterflow effect*.

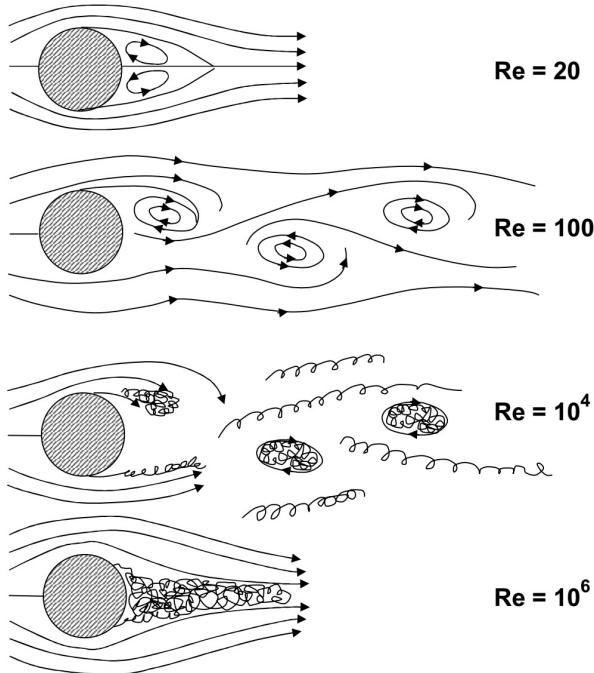


Figure 1.5: Depiction of a classical steady flow for various Reynolds number values. Many phenomena of laminar, semi-turbulent and turbulent flows are visible in depictions. Source:[12]

1.5 Hydrodynamics of superfluid

The macroscopic model is usually called the Hall-Vinen-Bekarevich-Khalatnikov (HVBK) model and provides a generalization of Landau's two-fluid model equations [2], including the presence of vortices. We treat the superfluid as a continuum and despite the fact that microscopically the superfluid velocity field is irrotational, we define a macroscopic superfluid vorticity $\Omega_s = \nabla \times \mathbf{v}_s$ accounting for quantized vortices.

The downside of this model is its assumption of spatially (not chaotically) organized vortices. The common example is a rotating cylinder [11].

The incompressible HVBK equations for normal component $\mathbf{v}_n(\mathbf{r}, t)$ and superfluid component $\mathbf{v}_s(\mathbf{r}, t)$, respectively, are [13]:

$$\frac{\partial \mathbf{v}_n}{\partial t} + (\mathbf{v}_n \cdot \nabla) \mathbf{v}_n = -\frac{1}{\rho} \nabla P - \frac{\rho_s}{\rho_n} S \nabla T + \frac{\eta}{\rho_n} \nabla^2 \mathbf{v}_n + \mathbf{F}_{ns}, \quad (1.21)$$

$$\frac{\partial \mathbf{v}_s}{\partial t} + (\mathbf{v}_s \cdot \nabla) \mathbf{v}_s = -\frac{1}{\rho} \nabla P + S \nabla T + \mathbf{T} - \frac{\rho_n}{\rho} \mathbf{F}_{ns}, \quad (1.22)$$

where we have defined several quantities:

$$\mathbf{F}_{ns} = \frac{1}{2} B(T) \hat{\boldsymbol{\Omega}} \times [\hat{\boldsymbol{\Omega}}_s \times (\mathbf{v}_n - \mathbf{v}_s - \nu_s \nabla \times \hat{\boldsymbol{\Omega}}_s)] \quad (1.23)$$

$$+ \frac{1}{2} B'(T) \boldsymbol{\Omega}_s \times (\mathbf{v}_n - \mathbf{v}_s - \nu_s \nabla \times \hat{\boldsymbol{\Omega}}_s), \quad (1.24)$$

$$\hat{\boldsymbol{\Omega}}_s = \boldsymbol{\Omega}_s / |\boldsymbol{\Omega}_s|, \quad (1.25)$$

$$\mathbf{T} = -\frac{\varkappa}{4\pi} \log(b_0/a_0) \boldsymbol{\Omega}_s \times (\nabla \times \hat{\boldsymbol{\Omega}}_s) \quad (1.26)$$

Here we can identify the quantities as \mathbf{F}_{ns} (mutual friction force), \mathbf{T} (vortex tension) and η (viscosity parameter). Usually, b_0 is the inter-vortex spacing and can be estimated as $b_0 = (2\Omega_s \varkappa)^{-1/2}$ [13].

The HVBK equations have well-defined limiting cases:

- $T \rightarrow T_\lambda$: In this case $\rho_s \rightarrow 0$ and the normal fluid motion equation (1.21) becomes the classical Navier-Stokes equation with viscosity term.
- $T \rightarrow 0$: In this case $\rho_n \rightarrow 0$ and the superfluid motion equation (1.22) describes a pure (potential) superflow. Additionally, taking the classical limit ($\hbar \rightarrow 0$) would give us the pure Euler equation of inviscid fluid.

The HVBK model has been widely used with success to study the transition from the laminar regime to the classical or quantum turbulence, for estimations of critical Reynolds numbers and their temperature dependence.

1.6 Dynamical similarity principle

An important role in the behavior of fluids is taken by the *fluid dimensional numbers*, which are used for scaling of motion equations in fluid mechanics.

The principle of *dynamical similarity* states that two flows of similar geometry have the same dynamical behavior, if they can be characterized by the same set of suitable dimensionless parameters representing transport phenomena. In order to describe Helium-II with correct equations and with the most precision, we have to choose which dimensionless parameters are useful.

- Knudsen number (Kn): This number helps determine whether statistical mechanics or the continuum mechanics formulation of fluid should be used to model the system. Kn is defined as the ratio of the molecular mean free path λ to a representative physical length scale D (container size): $\text{Kn} = \lambda/D$.

If the temperature of Helium-II is high enough $T > 1\text{ K}$, there is still sufficient amount of normal component, so the mean free path of thermal excitations is much smaller, comparing it with container scale $\lambda \ll D$. In that case, continuum mechanics could be used as a macroscopic theory for the normal component.

However, if temperature drops $T \lesssim 0.6\text{ K}$, mean free path λ increases, resulting in $\text{Kn} \sim 1$ and continuum model starts to break down. Here, the system is rather described as a gas of thermal excitations, thus calling it *ballistic regime*.

- Weissenberg number (Wi): This number relates the typical frequency ω of occurring fluid perturbations with the characteristic time τ that describes the relaxation of the fluid towards a thermodynamic equilibrium. The Weissenberg number is then given as a multiplication of this frequency and the relaxation time: $\text{Wi} = \omega\tau$.

Since the relaxation time of Helium-II is relatively small at temperatures $T > 1\text{ K}$, then $\text{Wi} \ll 1$ and Helium-II can be considered as a Newtonian fluid.

Once again, if temperature drops $T \lesssim 0.6\text{ K}$, the relaxation time τ of thermal excitations rises rapidly, resulting in $\text{Wi} \sim 1$, it will cause the fluid to become non-Newtonian.

- Reynolds number (Re): Let's consider the continuum and Newtonian assumptions ($\text{Kn} \ll 1$ and $\text{Wi} \ll 1$), so the fluid can be described by the raw form of Navier-Stokes (N-S) equation of motion. When we take into account also the incompressibility $\nabla \cdot \mathbf{v}_{n,s} = \mathbf{0}$, the N-S for classical fluid reduces itself to its most simplest form. In case of stationary flow ($\partial \mathbf{v}_{n,s} / \partial t = \mathbf{0}$), N-S can be rewritten into a dimensionless form [14]. Following these steps, there arises typical values of velocity U and length

scale L , at which there is the most significant change in velocity. Reynolds number Re thus can be expressed as a ratio of inertial and dissipative forces as $\text{Re} = UL\rho/\eta$, where η is the dynamic viscosity of the flow.

The case of oscillatory flow is described more in the next section.

The derivation of the *dynamical similarity* principle can be directly seen from the inspection of the underlying motion equation (1.21). In the classical fluid dynamics, we use dynamical similarity and dimensionless numbers for expressing various properties of data obtained from experiments.

Alternatively, the dissipative forces are usually described in terms of another dimensionless number, the *drag coefficient* C_D , representing the relation between applied *drag force* \mathbf{F} and a resulting velocity \mathbf{U} of a moving object submerged in a fluid:

$$C_D \propto U^\alpha, \quad \text{where } \begin{cases} \alpha = -1 & \text{for slow laminar flows with } \text{Re} \in (0 - 10) \\ \alpha = 0 & \text{for turbulent flows with } \text{Re} \in (10^3 - 10^5) \end{cases},$$

where the laminar case ($C_D \propto 1/U$) represents the viscous skin friction and the turbulent case ($C_D \approx \text{const.}$) represents the pressure drag. It is very common to plot the measured dependence of drag coefficient C_D against the Reynolds number (example in **Figure 1.6**):

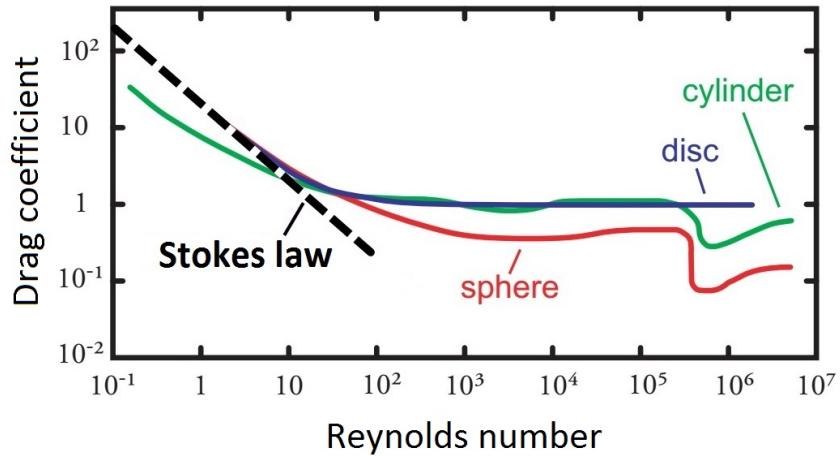


Figure 1.6: Drag coefficients C_D of different objects used in a steady flow with changing Reynolds number. Blue line - thin disc, Green line - cylinder with drag crisis near $\text{Re} \approx 10^6$, Red line - sphere with similar drag crisis as with cylinder, Black dashed line - laminar fit in the laminar area: $C_D \propto \text{Re}^{-1}$.

Dynamical similarity argument also leads to the existence of critical Reynolds number estimations, at which the transition to turbulent regime occurs in case of classical viscous fluids. Note that since superfluid Helium-II is composed of two fluids, the mentioned applies only to the normal component. The transition of superfluid component to quantum turbulence is described in a more detail in **Quantum turbulence** section.

1.7 Oscillatory flows

If a given body is oscillating in a classical viscous fluid, described by ordinary Navier-Stokes equation, there appears another characteristic length scale, at which the oscillations attenuate, identified [2] [14] as the *viscous penetration depth*:

$$\delta(\omega) = \sqrt{\frac{2\eta}{\rho\omega}}, \quad (1.27)$$

where ω is the angular frequency of oscillations.

In order to calculate the Reynolds numbers correctly, we have to recognize the correct characteristic length scale (whether it should be the dimension D of the oscillating body or its penetration depth $\delta(\omega)$).

For this purpose, we define another dimensionless quantity, the Stokes number β , as the ratio of time-dependent term $\partial\mathbf{v}/\partial t$ from N-S equation (1.21) to the viscous term $\nabla^2\mathbf{v}$. We calculate the Stokes number [15] as $\beta = \omega\rho D^2/(\pi\eta)$, which can be reduced using (1.27) to $\beta = D^2/(\pi\delta^2)$.

According to this definition, we call the flow characteristics as the *high-frequency limit*, when the Stokes values are $\beta \gg 1$, so the penetration depth $\delta \ll D$. Consequently, the right choice for the characteristic length depends on this limitation.

Classical hydrodynamics

To describe fully an oscillatory flow for the classical viscous fluid, the governing Navier-Stokes equation may be expressed in terms of dimensionless velocity U , time T and positions L . The independent time scale is given by the angular frequency of oscillations ω . Candidates for characteristic length scale L may lead to the body size D , viscous penetration depth $\delta(\omega)$ or eventually to the surface roughness.

To reach the high-frequency limit, the condition directly from 1.27 for the oscillation frequency: $\omega \gg 2\eta/(\rho D^2)$ has to be fulfilled. Depending on body geometry, one can reach $\delta(\omega) \ll D$ and say that fluid oscillates in high-Stokes regime $\beta \gg 1$.

Also, when the surface roughness is sufficiently negligible, the laminar-turbulent transition may be finally expressed using a single dimensionless parameter: an *oscillatory Reynolds number* $Re_\delta = U\delta\rho/\eta$.

Superfluid Helium-II

Assuming two independent velocity fields $\mathbf{v}_n(\mathbf{r}, t)$, $\mathbf{v}_s(\mathbf{r}, t)$ as the normal and superfluid components in superfluid Helium-II, the above thoughts are applicable for the oscillatory viscous flow of the normal component. We therefore define the high frequency limit for normal component as:

$$\delta_n = \sqrt{\frac{2\eta}{\rho_n \omega}}, \quad Dn = \frac{U \delta_n \rho_n}{\eta}, \quad (1.28)$$

We will call the oscillatory Reynolds number for normal component in superfluid Helium-II as a *Donnelly number* with the abbreviation Dn , after Russell J. Donnelly, who as first came with this (1.28) idea.

At low velocities, below any critical thresholds for creating either classical or quantum turbulence, the flow of the superfluid component is expected to be purely potential and the normal component exhibiting laminar viscous flow.

Moreover, if the typical body curvature is of order $1/D$, the surface may be described as if consisting of many planar elements. In this case it is shown [16] that we can write for the average dissipated energy:

$$\langle \dot{E} \rangle = \frac{1}{2} \alpha \xi U_0^2 S_{eff} \sqrt{\frac{\eta \rho_n \omega}{2}}, \quad (1.29)$$

where U_0 is the velocity amplitude, S_{eff} the effective surface, α the *flow enhancement constant* (depending on object geometry) and ξ the integral of velocity profile along the resonator. The total energy of an oscillator is given as $E = \xi m U_0^2 / 2$ and moreover, we define a fluidic quality factor Q_f of an oscillator for a single oscillation as:

$$1/Q_f = \frac{\langle \dot{E} \rangle}{\omega E} = \frac{\alpha \rho_n S_{eff} \delta_n}{2m} \quad (1.30)$$

From (1.29), one can also derive the peak dissipative force (during a period of oscillation) and the dimensionless drag coefficient related to the normal component:

$$F_0 = \frac{2\omega \langle \dot{E} \rangle}{U_0} = \alpha \xi \omega S_{eff} U_0 \sqrt{\frac{\eta \rho_n \omega}{2}} \quad \rightarrow \quad C_D^n = \frac{2F}{A \rho_n U_0^2} = \frac{2S_{eff}}{AU_0} \sqrt{\frac{\eta \omega}{\rho_n}}, \quad (1.31)$$

where A is the cross-section of the body perpendicular to flow. According to dynamical

similarity principle, the drag coefficient (1.31) can be expressed as a function of the dimensionless Donnelly number (1.28):

$$C_D^n = \Phi/Dn , \quad (1.32)$$

where number Φ is determined by the oscillating body geometry. Clearly, the laminar behavior of the normal component is fully described by the classical hydrodynamic laws, whereas in turbulent case, we expect a constant value for C_D^n as long, as only normal component contributes to the drag force (no quantized vortices present).

1.8 Quantum turbulence

Turbulence of superfluid component can be viewed as a tangle of vortex lines, causing the drag due to their motion. Quantized vortices can be nucleated either *intrinsically*, by exceeding a critical velocity of order 10 m/s, or *extrinsically*, by stretching and reconnecting of vortex loops. The initial vortices in the extrinsic case are the *remnant vortices*, which always exist in macroscopic samples of Helium-II. This type of vortex nucleation is also driven by the excess of critical velocity, which is observed to be in order \sim cm/s and heavily depends on the motion characteristics of an object.

Let's say the superfluid component becomes turbulent at some critical velocity U_C . In such case we expect an increase in drag coefficient C_D much above the possible dependence caused by turbulence of normal component. The process of self-reconnecting remnant vortices due to body oscillatory motion was well studied [16] and the related critical velocity is expected to scale as $U_C \propto \sqrt{\varkappa\omega}$, where \varkappa is the circulation quantum and ω is the oscillation frequency. Hence, it is convenient to define a dimensionless velocity \hat{U} with related drag coefficient C_D^s as:

$$\hat{U} = U_0 / \sqrt{\varkappa\omega} \quad \rightarrow \quad C_D^s = \frac{2F_0}{A\rho_s U_0^2} = \frac{2F_0}{A\rho_s \varkappa\omega \hat{U}^2} \quad (1.33)$$

If we consider the superfluid component (a dense tangle of quantized vortices) to be already turbulent with velocities sufficiently above critical values, we expect both normal and superfluid components to be coupled due to the mutual friction. Normal component could be then easily triggered to become turbulent as well, so both components contribute to the pressure drag. In this case, the drag coefficient must be calculated classically as $C_D = 2F_0/(A\rho U_0^2)$, where ρ is the total density of Helium-II.

Ultra-low temperature regime

In classical fluids, when the mean free path λ of particles becomes comparable to a length scale D of the system ($\text{Kn} \sim 1$), the continuum model of the fluid starts to break down and the system can no longer be described by the Navier-Stokes equations. Similar arguments go when time period of oscillatory flow $1/\omega$ becomes comparable with the relaxation time τ of the fluid towards thermodynamic equilibrium ($\text{Wi} \sim 1$).

Considering this, the system is no longer be described as a continuum, but rather as a gas of thermal quasiparticles propagating ballistically through a physical vacuum. Therefore, we call this state as the *ballistic regime*.

In practice, the ballistic regime is usually reached by cooling fluid down to ultra-low temperatures $T < 0.6$ K where the normal component accounts for less than 1% of the total density. However, the Knudsen number increases unusually faster than the Weissenberg number, as plotted in **Figure 1.7**.

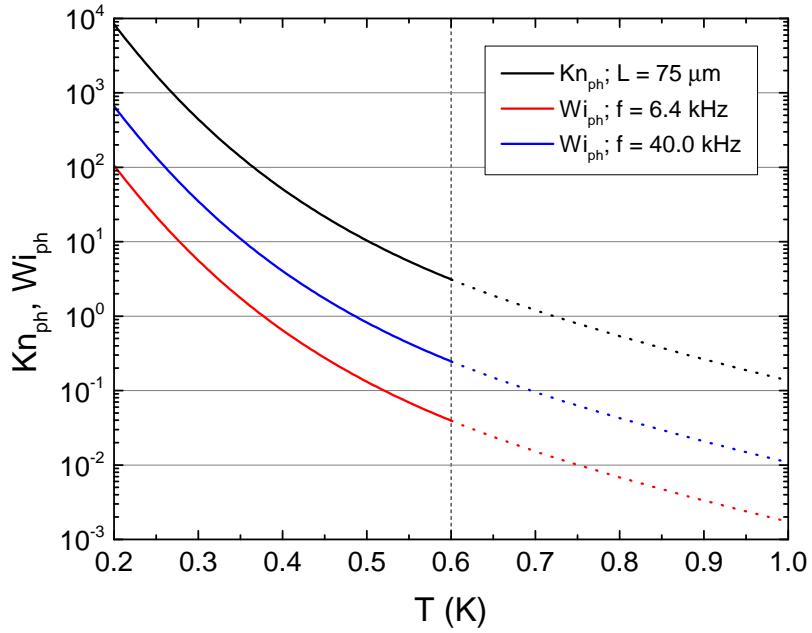


Figure 1.7: Plot of phonon Knudsen number and Weissenberg numbers against a range of temperatures for the fundamental and overtone modes of the tuning fork. The dashed line separates the interval $T < 0.6$ K, where the description of Helium-II as a gas of phonons is valid. Source:[16]

1.9 Universal scaling

A study was conducted in order to solve the Stokes' second problem with an oscillating plane in viscous fluid, using the Boltzmann kinetic equation. This solution was used to derive a universality relation valid in the high-frequency limit and at low velocities, thus with no turbulence present (neither classical nor quantum). This relation holds across both Newtonian and non-Newtonian regimes of the fluid.

A newly introduced scaling function $f(\text{Wi})$, derived by the authors in [16], relates the quality factor of an oscillator (1.30) with the geometric and hydrodynamic parameters:

$$1/Q_f = \frac{\alpha S_{eff}}{m} \sqrt{\frac{\eta \rho_n}{2\omega}} f(\text{Wi}), \quad (1.34)$$

where the scaling function $f(\text{Wi})$ is the added term and is defined as:

$$f(\text{Wi}) = \frac{(1 + \text{Wi}) \cos \phi - (1 - \text{Wi}) \cos \phi}{(1 + \text{Wi})^{3/4}} \quad (1.35)$$

$$\phi = \frac{\tan \text{Wi}^{-1}}{2} \quad (1.36)$$

In addition to the authors' original suggestion, we have explicitly included the flow enhancement factor α , which is necessary to recover the analytical solutions for drag on a sphere or a cylinder.

In hydrodynamical regime, when there is enough normal component present $T > 1 \text{ K}$, the limit $\text{Wi} \ll 1$ clearly shows the constant behavior of scaling function $f(\text{Wi}) \rightarrow 1$. However, when Wi reaches the critical value $\text{Wi} \sim 1$, the scaling function increases and in an extreme non-Newtonian case when $\text{Wi} \ll 1$, the scaling function converges to the relation $f(\text{Wi}) \propto \text{Wi}^{-1/2}$.

In the hydrodynamical regime, the relaxation time of the normal component is closely related with the viscosity, which leads to the estimation of Weissenberg number: $\text{Wi} \approx \eta \omega / (\rho_n c_2^2)$, where c_2 is the velocity of second sound wave.

Finally, this allows us to use the scaling relation both for the hydrodynamical regime ($T > 1 \text{ K}$) and the phonon gas ($T \lesssim 0.6 \text{ K}$), so the fluidic quality factor can be rewritten:

$$1/Q_f = \frac{\alpha S_{eff} \rho_x c_2}{m \omega} \sqrt{\text{Wi}/2} f(\text{Wi}), \quad (1.37)$$

where ρ_x means either normal component ρ_n or phonon density ρ_{ph} .

In **Results** chapter we use this form of universality scaling for comparison against experimental data collected in both temperature ranges $T > 1\text{ K}$ and $T < 0.6\text{ K}$.

Multiple critical velocities

Here is briefly commented the transition to quantum turbulence regime observed at very low temperatures ($T \ll 1\text{ K}$). A couple of experimental studies in milliKelvin temperatures reported [17] the existence of more critical velocities related with superfluid component flow within single experiment:

- First critical velocity is related to the formation of pinned vortex loops at the surface of oscillating body - possibly forming a thin layer with different hydrodynamic behavior which increases the effective mass of the oscillating object. Such critical velocity is hard to observe at higher than ultra-low temperatures.
- Second critical velocity is a consequence of vortex rings escaping from the oscillator body into the superfluid bulk and eventually forming a vortex tangle. Here the sudden raise of drag is observed, usually with hysteresis effect.
- Third critical velocity is the highest critical velocity of order $\sim \text{m/s}$ which can be observed. The origin of this velocity is linked to the development of larger quantized vortex structures, which in larger scale start to mimic the classical turbulence. Due to the high value of this critical velocity, it is not likely reachable within experiments reported in this Thesis.

Additional dissipation mechanisms

In addition to expected viscous drag and a drag caused by the created vortex tangle, the losses in energy may be caused also due to the sound emissions through the surrounding fluid.

In this Thesis, such sound emissions can be completely neglected, based on previous studies [18] [22] of acoustic emissions by oscillating object in Helium-II. Perhaps a very small contribution could occur in the first overtone mode of oscillated tuning fork (explained in more detail in **Experimental approach**)

2. Experimental Approach

Experiments presented and analyzed in this Thesis were conducted in Prague, with members of department of low-temperature physics, under Charles University.

Many experimental methods are known and were conducted in order to launch the quantum turbulence: by an oscillating objects (wires, tuning forks, oscillating discs, etc.) or by *coflow* and *counterflow* techniques (in other words, using indirect flow sources).

In our investigation, we used entirely 3 types of oscillating objects: vibrating NbTi wire, oscillating disc and tuning fork oscillator, driven by alternating source Agilent A33220 and measured by SR830 amplifying lock-in, using an I/V converter with an conversion ratio 1000 V/A [19]. We measured both the in-phase and anti-phase components and also the quadratures of signals.

Experimental data of vibrating wire and oscillating disc are included and analyzed in this Thesis, but a pure experimental work by the author of this Thesis, was performed only with the tuning forks.

In this chapter, we introduce the technical details of all used oscillators, their integration within the whole experimental setup and in the end, the measurement techniques performed on these oscillators.

2.1 Apparatus

All measurements were performed in a helium cryostat, cooled down to the desired temperatures using a rotary and Roots pump, and stabilized (with errors of a few mK) either manually or using a Lake Shore temperature controller Model 340. The most of used technologies are captured in a photograph in **Figure 2.1**.

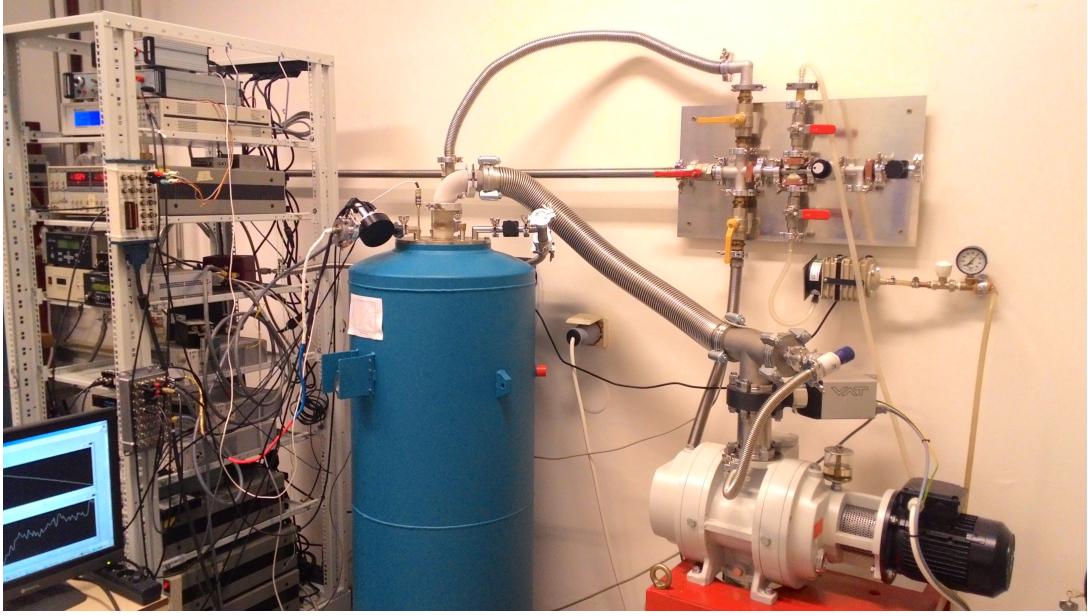


Figure 2.1: A photograph of the experimental setup. From left: source generators Agilent A33220, amplifying lock-ins SR830 with an I/V converters, cryostat, gas handling system (pipes) for emerging gas, rotary and Roots pump. Source: [14]

Our chosen studied temperatures are from a wide range from a little below the transition temperature $\sim 2.17\text{ K} \gtrsim T_\lambda$ to the lowest (experimentally) possible one $\sim 1.35\text{ K}$. We also performed series of measurements in the area far above the transition temperature $\sim 3\text{ K} > T_\lambda$ in order to test all used components.

The studied range ($1.35\text{ K} - 2.17\text{ K}$) allows access to the wide range of normal/superfluid components ratios of the two-fluid model ($\rho_s/\rho_n \ll 1$ at $T \lesssim 2.17\text{ K}$ and $\rho_s/\rho_n \approx 16$ at $T \sim 1.35\text{ K}$).

Measurements at ultra-low temperatures $T < 0.6\text{ K}$ in the ballistic regime of Helium-II were performed on a Leiden Cryogenics MNK126-400 dilution refrigerator with a base temperature below 10 mK . The description of sub-Kelvin measurements is not included in this chapter, but is discussed in sufficient detail in [16]. However, refrigerator results are analyzed in the last section of **Results** chapter in order to test the validity of the *uniform scaling* concept, introduced in the last section of the **Theoretical Background**.

The tuning fork oscillators were tightly attached in the inner space of the cylindrical *second-sound resonator* cavity, also capable to produce the second sound on the one side and receive it on the other side. We drilled a small hole to the resonator body in order to fill it with Helium-II.

This resonator (**Figure 2.2**) was attached at the bottom of the *insert* - a large metallic construction holding all measuring micro-devices, thermometers and coaxial cables.

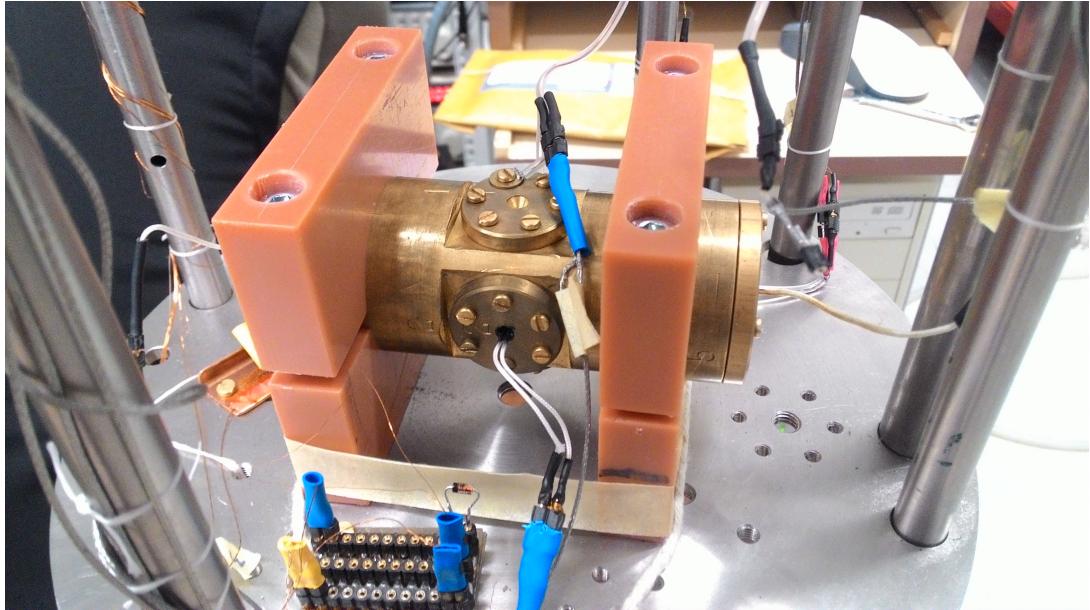


Figure 2.2: A photograph of the second-sound resonator attached at the bottom of metallic insert with cables and thermometers. Source: [14]

To obtain the best results at low temperatures, the cryostat containing oscillators was repeatedly flushed with pure liquid ^4He from Dewar transport container. After this pre-cooling step, the liquid ^4He was transferred using a siphon.

The inner space of resonator was additionally separated from the outer part (cryostat body) by a sintered copper, forming a solid mass of material by pressure. This ensures that no parasitic helium ices micro-particles or other impurities will interfere with the oscillators inside of resonator.

2.2 Resonators

In this section we briefly describe the principles of micro-scale oscillators used in experiments with Helium-II.

2.2.1 Vibrating Wire

Vibrating NbTi wire resonator consists of a semi-circular loop of wire inserted to a vertical magnetic field \mathbf{B} , as shown in **Figure 2.3**. As we turn on the alternating current flux $\mathbf{j} \propto e^{i\omega t}$ inside the wire, these currents force the wire to oscillate due to Lorentz force $\mathbf{F}_L \propto \mathbf{j} \times \mathbf{B}$. As the wire moves through the field, the Faraday voltage is induced of magnitude [20]:

$$V = -\frac{d(\mathbf{B} \cdot \mathbf{S})}{dt} \sim \frac{\pi}{4} B D U, \quad (2.1)$$

where \mathbf{S} is the area vector, enclosed by the wire loop and D is the distance between wire's legs. Experimentally used magnetic field was about ≈ 170 mT with an uncertainty of ± 10 mT.

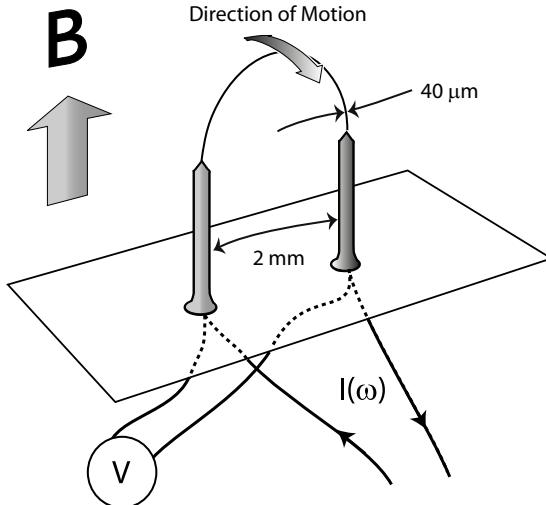


Figure 2.3: Schematic diagram of the vibrating wire resonator. Source: [16]

2.2.2 Oscillating Disc

The torsional oscillator consists of a $50\mu\text{m}$ wire with a glass disc fixed to the wire at its midpoint. The disc is 1 mm thick with a diameter of 40 mm. A schematics is sketched in **Figure 2.4**.

Sixteen black marks around the circumference of the disc are used to determine the deflection and angular velocity of the disc from recorded video sequences.

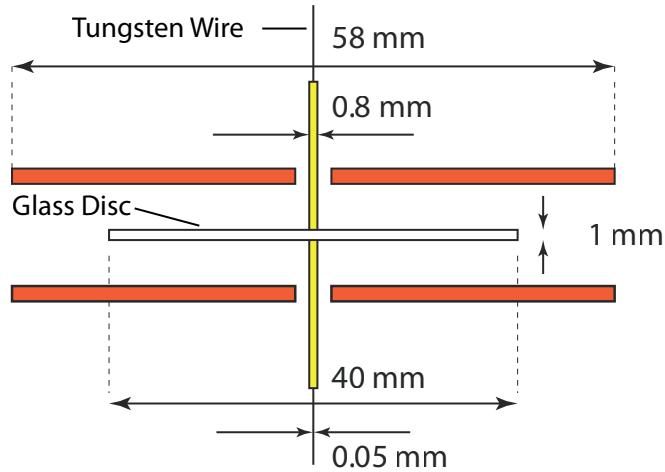


Figure 2.4: Schematic diagram of the torsionally oscillating disc. Source: [16]

The raw data is in the form of video recordings of the disc motion and fairly complex post-processing method was required to extract quantities. The optical distortion from the lenses and the curved walls of the cryostat are negligible. More details about data processing can be found in [16].

2.2.3 Tuning Fork

Quartz tuning forks (TF) are commercial piezoelectric oscillators with a well-calibrated resonant frequency. They are usually used as frequency standards in watches or as force sensors in microscopes. Also, TFs have started to be widely used in cryogenic Helium II experiments [21].

In our experimental setup, we used the fork of following dimensions: prongs length $\mathcal{L} = 3.50\text{ mm}$, prongs width (perpendicular to the fork plane) $\mathcal{W} = 75\mu\text{ m}$, thickness $\mathcal{T} = 90\mu\text{m}$ prongs inter-distance $\mathcal{D} = 90\mu\text{m}$. The same type of fork was also used and discussed in [22] [24] A sketch of the fork architecture is depicted in **Figure 2.5**:

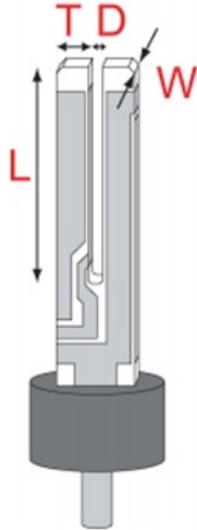


Figure 2.5: Schematic diagram of the quartz tuning fork. Source: [14]

There are several achievable resonant modes at which the fork can oscillate. We chose to work with the *fundamental* one at $f_0 \sim 6400$ Hz and with the first *overtone* one at $f_1 \sim 40\,200$ Hz.

The fork is driven by applying an alternating voltage $V(t) \propto e^{i\omega t}$ from a generator to the metallic plates (deposited on fork surface). The piezoelectric effect causes a tension resulting in a force, which is proportional to the applied voltage. In fundamental mode, the fork exhibits an anti-phase oscillating motion of its prongs with a single node. In case of overtone, there would be just two nodes. The fork's bend induces a piezoelectric current $I(t)$ which is proportional to the velocity $U(t)$.

The conversion relations between applied $V(t)$, measured $I(t)$ and mechanical properties $F(t)$, $U(t)$ are given [21] as:

$$F(t) = \frac{1}{2}a_f V(t), \quad U(t) = \frac{I(t)}{a_f}, \quad (2.2)$$

where a_f is the so-called *fork constant*. This constant can be derived from a fork's geometry, material properties and its oscillation mode. The formula the fork constant calculation is given usually by a deflection measurement:

$$a_f = \sqrt{4\pi m_{eff} \Delta f \frac{I}{V}}, \quad (2.3)$$

where $m_{eff} = TWL\rho_q/4$ (ρ_q as the quartz density) is the fork's effective mass and Δf is the measured peak width from the frequency-sweep deflection measurement. In our case

we used fork with the effective mass and fork constants for fundamental and overtone mode of following values:

$$m_{eff} = 1.52 \times 10^{-8} \text{ kg}, \quad a_{f0} = 3.665 \times 10^{-7} \text{ Cm}^{-1}, \quad a_{f1} = 14.094 \times 10^{-7} \text{ Cm}^{-1} \quad (2.4)$$

The measurement scheme of the experiment with tuning fork is shown in **Figure 2.6**. The arrangement of experiments using dilution refrigerator were slightly more complex and are described in [19] .

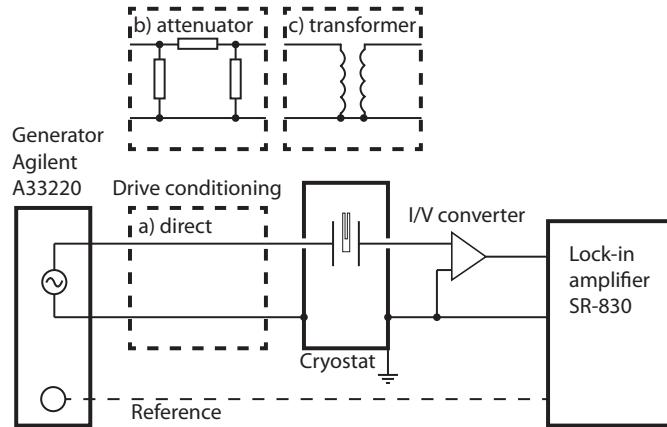


Figure 2.6: Diagram of the measurement scheme used in Prague. To achieve the full range of velocities, the applied voltage was either (a) directly fed to the tuning fork, (b) attenuated by one or more in-line attenuators, or (c) amplified by a transformer. The transformer's output was constantly monitored by a Keithley digital multimeter Model 2100. The I/V converter is detailed in [23] Source:[24]

2.3 Measurement technique

It was shown in previous works [25] [22] with tuning forks submerged in Helium-II that it is important to perform full *frequency sweeps* across the resonant response of an oscillator in order to reveal relevant details about any nonlinear effects.

However, these frequency sweeps, at fixed source drive, are heavily time-consuming and sometimes it is useful (especially when we are confident about present laminar mode) to use an *amplitude sweep* with changing drives, a fixed resonant frequency.

Since many hydrodynamic features could be overlooked by using pure amplitude sweeps, we therefore focus in our analysis mainly on the frequency sweeps.

3. Experimental Results

In this chapter we present our obtained data and their analysis of the measurements from oscillatory experiments as introduced in **Experimental Approach** chapter.

In the first part, we present our drag force measurements by using all three oscillators submerged in superfluid Helium-II in hydrodynamical regime at temperatures $T > 1 \text{ K}$.

Next, we add measurements from the ballistic regime at temperatures $T < 0.6 \text{ K}$ and connect them in order to prove the concept of universal scaling.

As the last analysis we introduce a *flow phase diagram*, summarizing all our findings basically in a single graph, representing the areas of different non-linear regimes.

3.1 Drag force measurements

As we introduced in the last section of **Experimental approach** chapter, we used the full frequency sweep method for vibrating wire and tuning fork. Each point on following graphs was obtained by a pair of full frequency sweeps across the resonance of given oscillator. One sweep was performed with increasing frequency and the second one with decreasing frequency, which made us confident that no hysteresis effect was present.

We present all the measurements in the form of typical hydrodynamic visualizations (velocity-force response, drag coefficients and appropriate dimensionless numbers) of oscillating wire, torsional disc and tuning fork, respectively.

3.1.1 Vibrating NbTi wire

We were measuring both the voltage in-phase with the driving current and the quadrature signal, in order to obtain the resonant response. When a high enough applied drives were reached ($\gtrsim 0.8$ mA at temperature 1.67 K, responding in ~ 0.1 m/s peak velocity), there was present a resonant frequency shift and a *peak softening* effect.

As the calibration of the magnetic field produced by permanent magnets was performed only at room temperature, the peak velocity on the wire top is known with the accuracy about $\pm 20\%$. This error doesn't affect the scaling process obtained from the data.

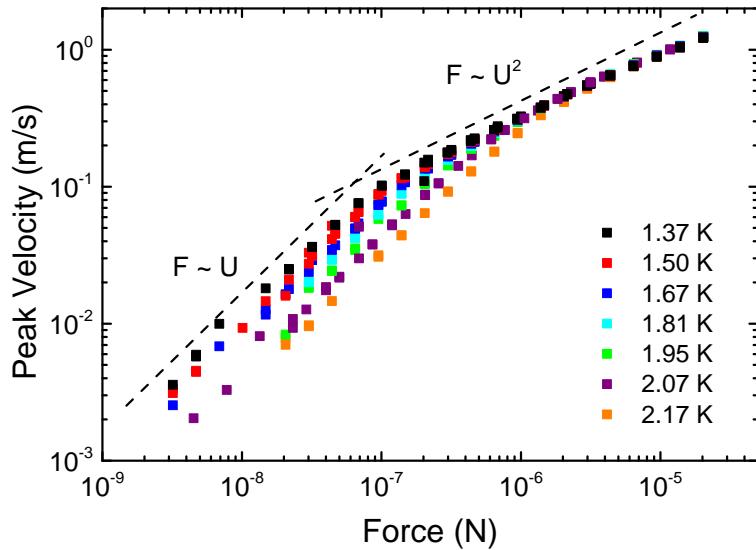


Figure 3.1: Plot of peak velocity U_0 against the applied peak force F_0 for the vibrating wire submerged in superfluid ${}^4\text{He}$ at several temperatures. The black dashed lines serve as sketch of theoretical laminar and turbulent regimes.

We plot in **Figure 3.1** the peak velocity of the wire top U_0 against the applied peak force F_0 at various temperatures from two-fluid regime ($T > 1.0\text{ K}$).

Clearly, the wire exhibits linear drag at low velocities and non-linear additional drag in the area of higher velocities. The energy losses of the wire in the low-velocity part are dominated by the viscous drag of the present normal component. Other loss mechanisms like acoustic emission are in principle present as well, but neglected in further discussion. The additional dissipation process in the higher-velocity part indicates either classical or quantum turbulence (or both) and the measured drag F_0 is roughly proportional to U_0^2 .

Next we plot in **Figure 3.2** the classical drag coefficient as a function of peak force and velocity $C_D \sim F_0/U_0^2$ using the same data as presented in **Figure 3.1**.

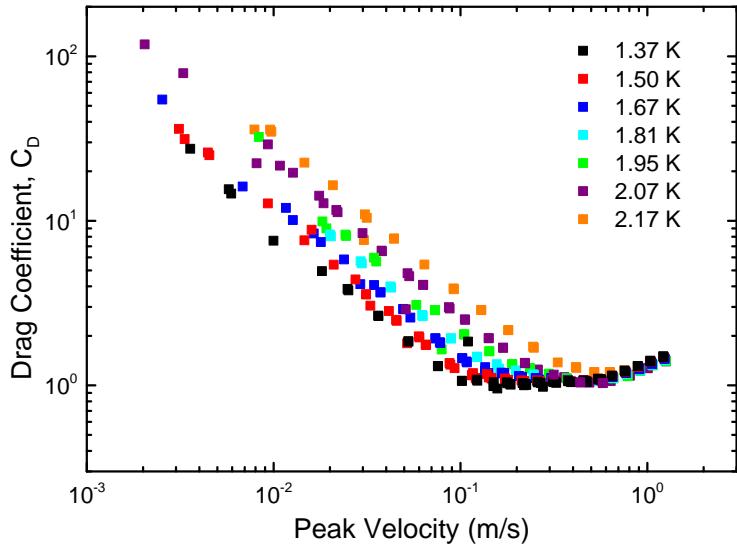


Figure 3.2: Plot of drag coefficient C_D against the velocity peak response U_0 for the vibrating wire at several temperatures.

In order to perform the universal scaling, we collapse the contribution of the normal component in the following way:

$$C_D^n \leftarrow C_D \frac{\rho}{\rho_n}, \quad Dn \leftarrow U_0 \sqrt{\frac{2\rho_n}{\eta\omega}}, \quad (3.1)$$

where η is the dynamical viscosity of Helium-II for a given temperature. Relations in (3.1) are applied in the same way as described (1.31), (1.28) in the last section of **Theoretical background** chapter.

The resulting plot **Figure 3.3** clearly shows the collapse of all linear parts of the measured drag into a single line. However, the theoretical pre-factor ($\Phi_{\text{cyl}} = 4\pi$) is smaller than the fitted one ($\Phi \sim 26$). This cannot be explained by experimental errors such as the

magnet calibration, so the most likely reason behind it is the effect of irregularities on the surface of the wire. Indeed, excrescences of order $5\mu\text{m}$ were observed on the $40\mu\text{m}$ wire under an optical microscope.

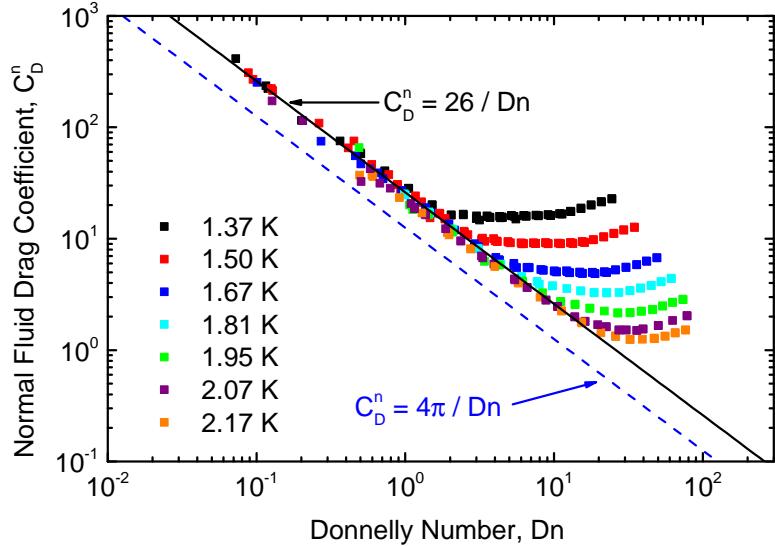


Figure 3.3: Plot of normal fluid drag coefficient C_D^n against the dimensionless Donnelly number (Dn) for the vibrating wire at several temperatures. The blue dashed line shows the expected theoretical dependence [16] for a smooth cylinder. The solid black line is a numerical fit of the linear part of data.

One may see from the **Figure 3.3** that all temperature curves are visually sorted in an ascending order as the non-linear behavior occurs at certain starting points. These points of non-linearity emergence cannot be governed by a single value of Donnelly number, but rather with a critical velocity U_C .

We show in **Figure 3.4** that all deviations can be connected by the exceeding of critical dimensionless velocity $\hat{U}_C = U_C/\sqrt{\kappa\omega}$. The approximate value of the critical \hat{U}_C was found using *error plot*, where the *error* is defined via the absolutized errors of linear superfluid drag coefficient function $C_D^s = C_D\rho/\rho_s = \gamma/\hat{U}$:

$$\text{Error} = \frac{\text{abs}(C_D^s \hat{U} - \gamma)}{C_D^s \hat{U}} \in (0, 1), \quad (3.2)$$

where γ is the pre-factor coefficient, different for each temperature curve.

The single critical value $\hat{U}_C \sim 1.0 \pm 0.2$ (see **Figure 3.4**) is thus a clear sign of the onset of quantum turbulence by the superfluid component.

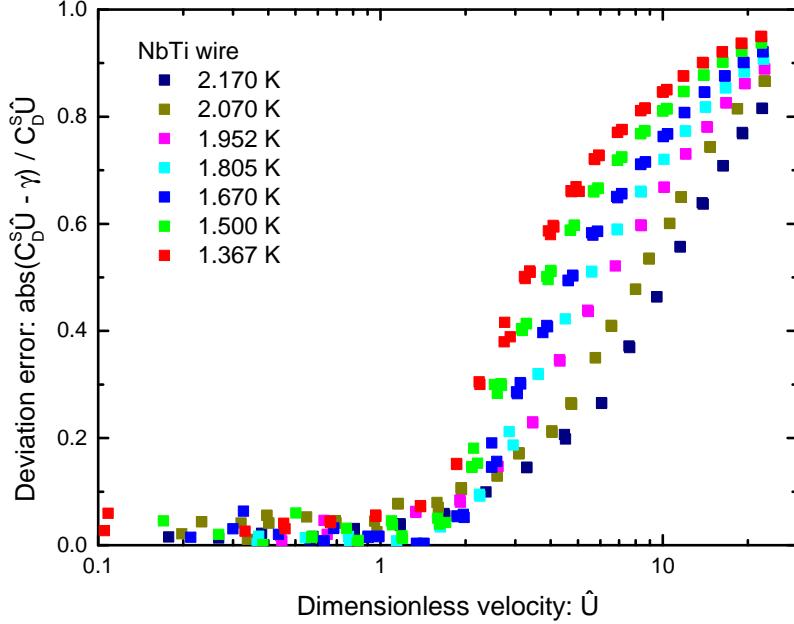


Figure 3.4: Plot of normalized deviations from the linear fits $C_D^s = \gamma/\hat{U}$ with γ differing for each curve, as a function of the dimensionless velocity \hat{U} for various temperatures from the studied range. The critical dimensionless velocity $\hat{U}_C 1.0 \sim \pm 0.2$ is taken as an average of deviation origin from all temperature curves.

3.1.2 Oscillating disc

The (torsionally) oscillating disc differs from the vibrating wire in several technicalities:

- Oscillating disc does not displace any fluid and thus The superfluid is at rest unless quantized vorticity is produced
- It is not possible to perform measurements in a steady state of flow, but decayed flow was measured instead
- Drag force has to be inferred from the decaying amplitude of oscillator deflection.

As a consequence of mentioned differences (examples showed in **Figure 3.5**), we have to substitute $U_0 = \omega R \phi_0$ within the Donnelly number and define a new drag coefficient, specific for our mechanical system of torsionally oscillating disc in a viscous fluid of density ρ_n as:

$$C_D^n \leftarrow \frac{2M_f}{A\rho_n\Omega_0^2 R^3}, \quad Dn \leftarrow R\omega\phi_0 \sqrt{\frac{2\rho_n}{\eta\omega}}, \quad (3.3)$$

where M_f is the moment of friction forces, R the radius of the disc, $A = \pi R^2$ the area of the disc and Ω_0 is the amplitude of angular frequency $\omega(t)$. It was already showed [16]

the relation between such drag coefficient (3.3) can be expressed in laminar flow in terms of the Donnelly number as $C_D^n = \Phi/Dn$ with the pre-factor $\Phi_{\text{disc}} = 2$.

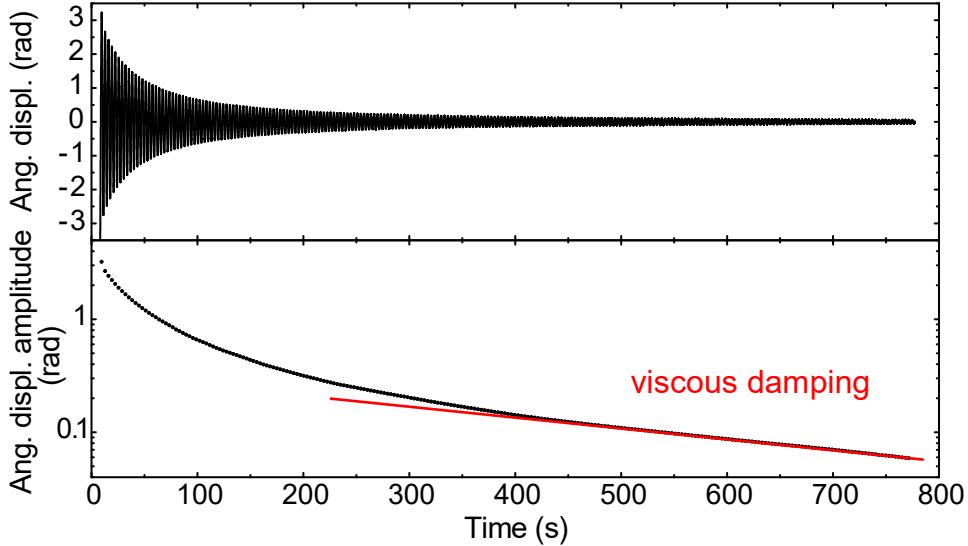


Figure 3.5: Example of angular displacement measurement in time of the torsionally oscillating disc. Top picture: The decreasing angular displacement amplitudes $\phi_0(t)$. Bottom picture: The logarithmic plot $\phi_0(t)$ shows two distinct regions – nonlinear decay in the area of earlier times $t < 400$ due to turbulent drag forces and an exponential (viscous) decay due to laminar flow of the normal component at the later times $t > 500$.

We plot the re-defined drag coefficient C_D^n from Eq.(3.3) against the Donnelly number in **Figure 3.6**. Again, as in case of vibrating wire, the data collapse to a single inverse dependence $C_D^n = 2/Dn$ in the area of small values of Donnelly number, which illustrates and proves the universal scaling concept.

One would naturally expect the normal component to transit to turbulent regime earlier than the superfluid one since the oscillating disc directly moves only with the normal component. However, **Figure 3.6** clearly shows that non-linearities are not characterized by a single value of Dn , but rather continuously with ascending temperature. This implies that instabilities cannot be explained by pure viscous fluid dynamics and must relate to the quantum turbulence produced by a Donnelly-Glaberson instability.

We don't provide the error plot for this oscillator since it looks practically identical to the one presented with vibrating wire and brings no additional information. The critical dimensionless velocity of the torsionally oscillating disc is estimated (from the error plot) as $\hat{U}_C \sim 12.0 \pm 0.5$. This is about one order higher than in the case of vibrating wire.

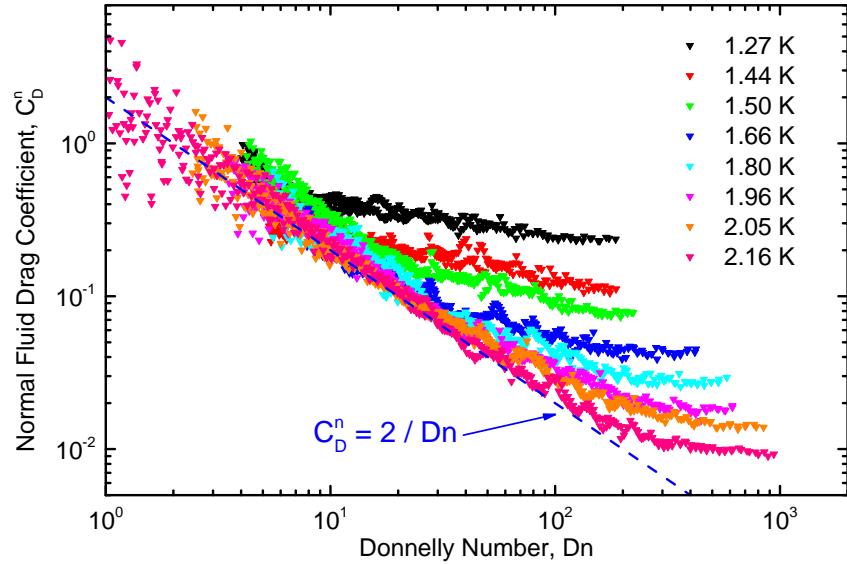


Figure 3.6: Plot of re-defined fluid drag coefficient C_D^n against the dimensionless Donnelly number (D_n) for the torsionally oscillating disc at several temperatures. The blue dashed line shows the expected theoretical dependence [16] for viscous drag. The temperature-dependent and temperature-ascending starting points of non-linearities are a clear sign of the onset of quantum turbulence by the superfluid component.

3.1.3 Tuning fork

As the last oscillator, we used quartz tuning fork with geometry and resonant specifics as they were described in **Experimental approach** chapter. the resonant response was experimentally measured in the same way as was with vibrating wire - by a real-time analysis of the in-phase current and quadrature response. Electrical quantities are then converted into physical attributes according to mentioned relations (2.2), which are dependent on fork constants $a_{f0} = 3.665 \times 10^{-7} \text{ Cm}^{-1}$, $a_{f1} = 14.094 \times 10^{-7} \text{ Cm}^{-1}$ for the fundamental and overtone mode, respectively.

In order to measure the fork constants, we had to perform a series of frequency sweeps in low-temperature vacuum. We estimate the uncertainty of fork constants to be of 10% since velocity calculation errors were proven using optical experiments. [33]

In **Figure 3.7** we plot the peak velocity response U_0 of the top of the fork prong, against the applied peak force F_0 at various temperatures from two-fluid regime ($T > 1.0$ K). We sketched the theoretical laminar $F_0 \propto U_0$ and classical turbulent dependencies $F_0 \propto U_0^2$ as guides for the eye.

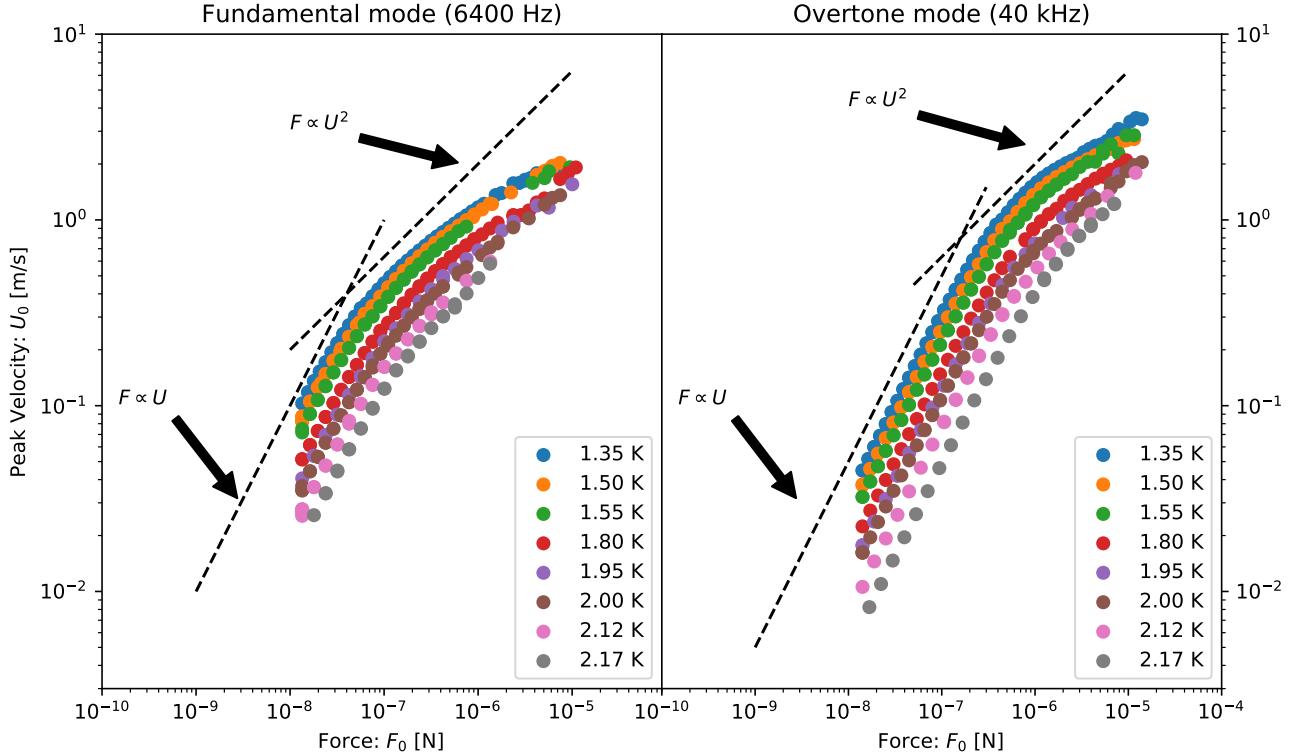


Figure 3.7: Plot of peak velocity U_0 against the applied peak force F_0 for the oscillating tuning fork submerged in superfluid ${}^4\text{He}$ at several temperatures.
 Left image: Measurements in fork's fundamental mode, Right image: Measurements in fork's overtone mode, Black dashed lines mark the theoretical laminar and classical turbulent regime dependencies.

We note that the linear sketched dependency describe the laminar regime very well, whereas the quadratical (classical turbulence regime) seems to be a weak fit to the situation, especially for the lower temperatures from the studied range.

Next, we plot in **Figure 3.8** the classical drag coefficient C_D against the peak velocity U_0 . Both oscillating modes are visualized as a paired plot in order to show their shared asymptote (as sketched with the black dashed line) in the area of big velocities. Also, we sketched the laminar regime fit as a demonstration.

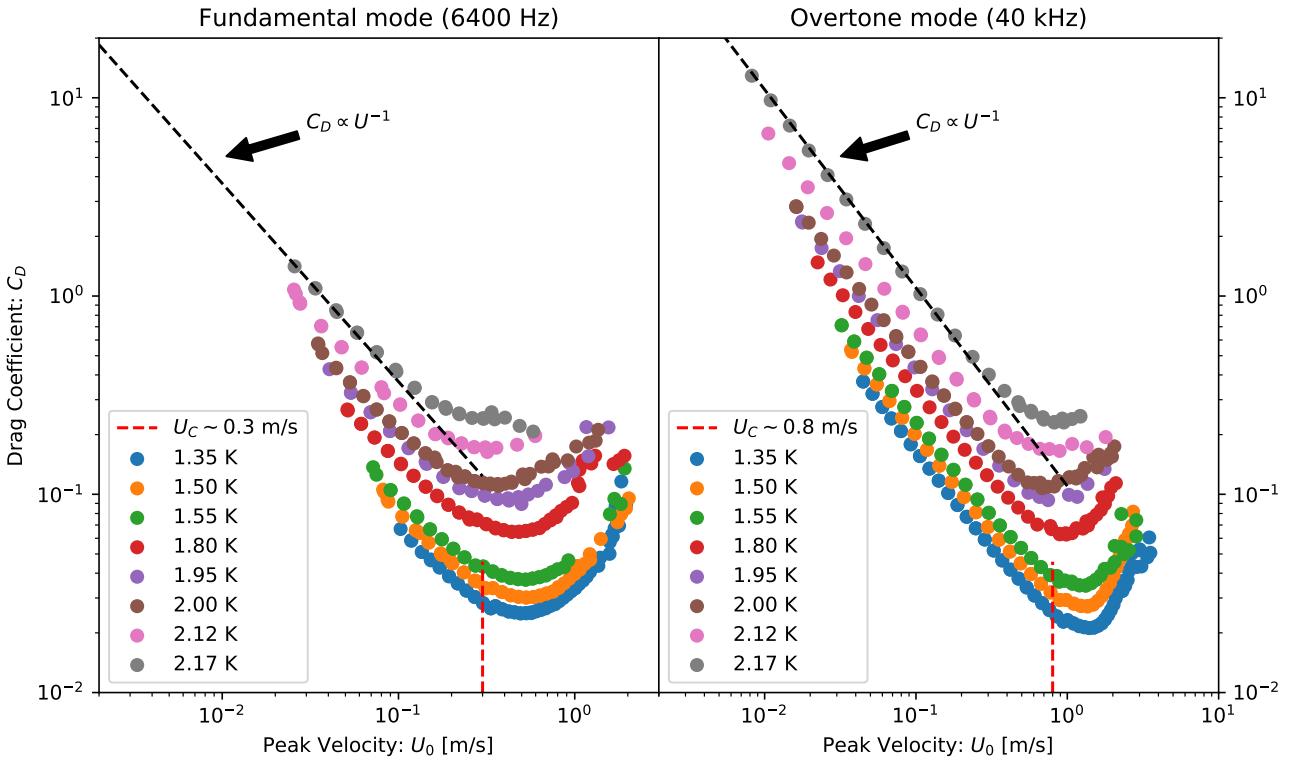


Figure 3.8: Plot of drag coefficient C_D against the velocity peak response U_0 for the oscillating tuning fork submerged in superfluid ^4He at several temperatures. Left image: Measurements in fork's fundamental mode, Right image: Measurements in fork's overtone mode, black dashed line fits the theoretical laminar regime dependency, red dashed line marks the critical velocity value U_C above which an onset of quantum turbulence appears. The clear sign of this effect can be seen for a group of curves with $T < 1.6\text{ K}$.

As expected, the tuning fork exhibits a linear drag in the area of low velocities regardless on the temperature from the studied range. Then, approximately above the critical velocity U_C , a synchronized increased drag was observed for a group of curves with temperature $T < 1.6\text{ K}$, which is a clear sign of onset of quantum turbulence. The critical velocities differ for oscillating modes:

$$U_{C0} \sim 0.30 \pm 0.05 \text{ m/s} \quad U_{C1} \sim 0.80 \pm 0.12 \text{ m/s}, \quad (3.4)$$

which is expected from the scaling relation (1.33) and roughly proven since the critical dimensionless velocities $\hat{U}_{C0} = U_{C0}/\sqrt{\kappa\omega_0} \approx 4.7$ and $\hat{U}_{C1} = U_{C1}/\sqrt{\kappa\omega_1} \approx 5.0$ are similar.

Curves with higher temperature seem to transit to non-linear regime earlier, which indicates the classical turbulence of the normal component instead.

To characterize the normal component flow, we plot in **Figure 3.9** the normal drag coefficient against the dimensionless Donnelly number. The conversions were done as we stated in (3.1).

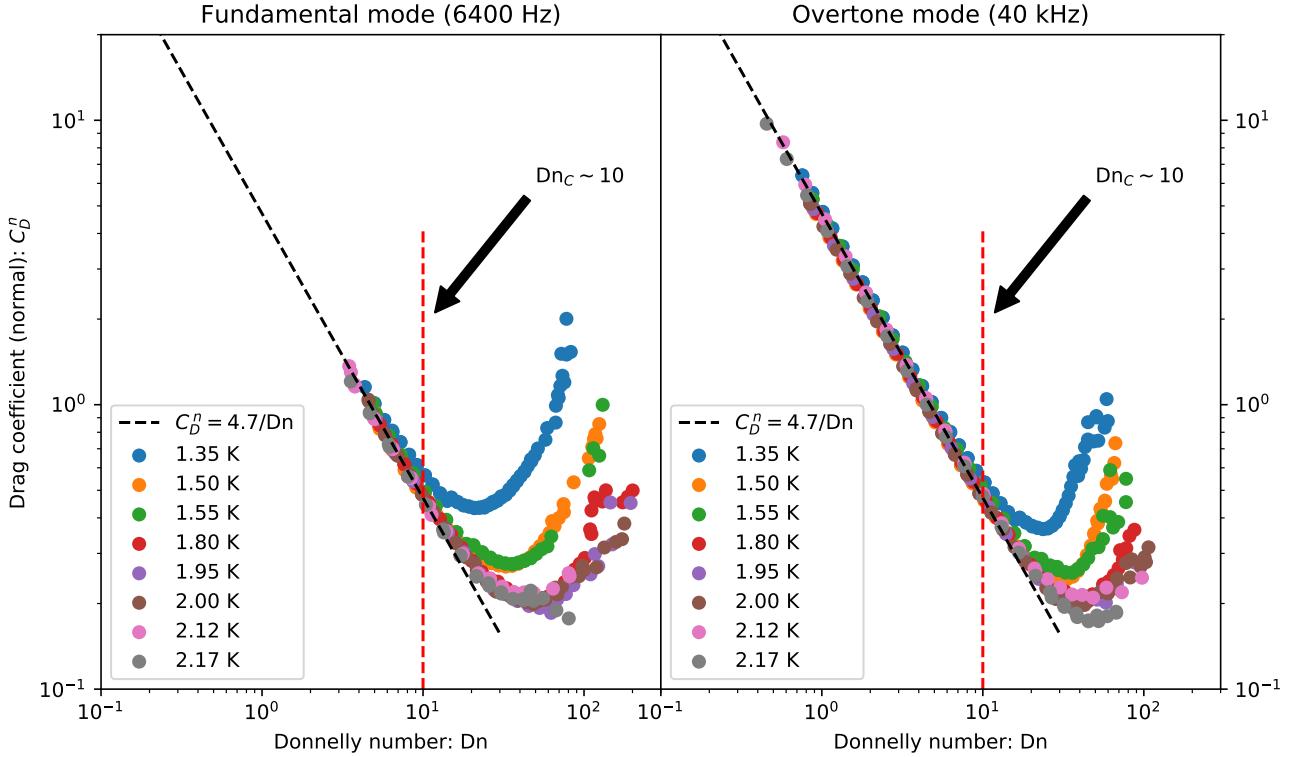


Figure 3.9: Normal fluid drag coefficient C_D^n as a function of the Donnelly number Dn . Left image: Measurements in fork's fundamental mode, Right image: Measurements in fork's overtone mode, Black dashed line fits the theoretical laminar regime dependency, with the same pre-factor $C_D^n = 4.7/Dn$ for both oscillation modes, Red dashed line: the estimated critical value of Dn , above which the onset of classical turbulence occurs for the group of temperature curves $T > 1.6$ K.

With no doubt, in the area of low Donnelly values, the dependencies collapse to a single line as expected, representing the laminar regime with the shared pre-factor $\Phi \sim 4.7$. In contrast to the results obtained with the vibrating wire or oscillating disc, we also recognize, additionally to the critical velocity \hat{U}_C , a critical value of Donnelly number Dn_C , above which the rest group of temperature curves $T > 1.6$ K non-linearly deviate. The onset of turbulence for these curves is governed by a single value of Donnelly number Dn_C and thus dominated by the classical turbulence of the normal component.

We note that it is interesting to find the laminar pre-factor $\Phi \sim 4.7$ to be same for both oscillation modes. The shared critical Dn_C was expected from the dynamical similarity principle, but the shared Φ is a result of different principle - the fact that both modes have the same effective mass m_{eff} (see [16]).

We found the approximate value for the shared critical Donnelly number Dn_C again using *error plot*, where the *error* is here defined via the normalized deviation rate from the laminar fit $f : C_D^n Dn - \Phi$, where $\Phi = 4.7$ as:

$$\text{Error} = \frac{\text{abs}(C_D^n Dn - \Phi)}{C_D^n Dn} \in (0, 1) \quad (3.5)$$

We plot these errors in **Figure 3.10** in order to mark more clearly the position of Dn_C , where the group of temperatures $T > 1.6$ K starts to deviate.

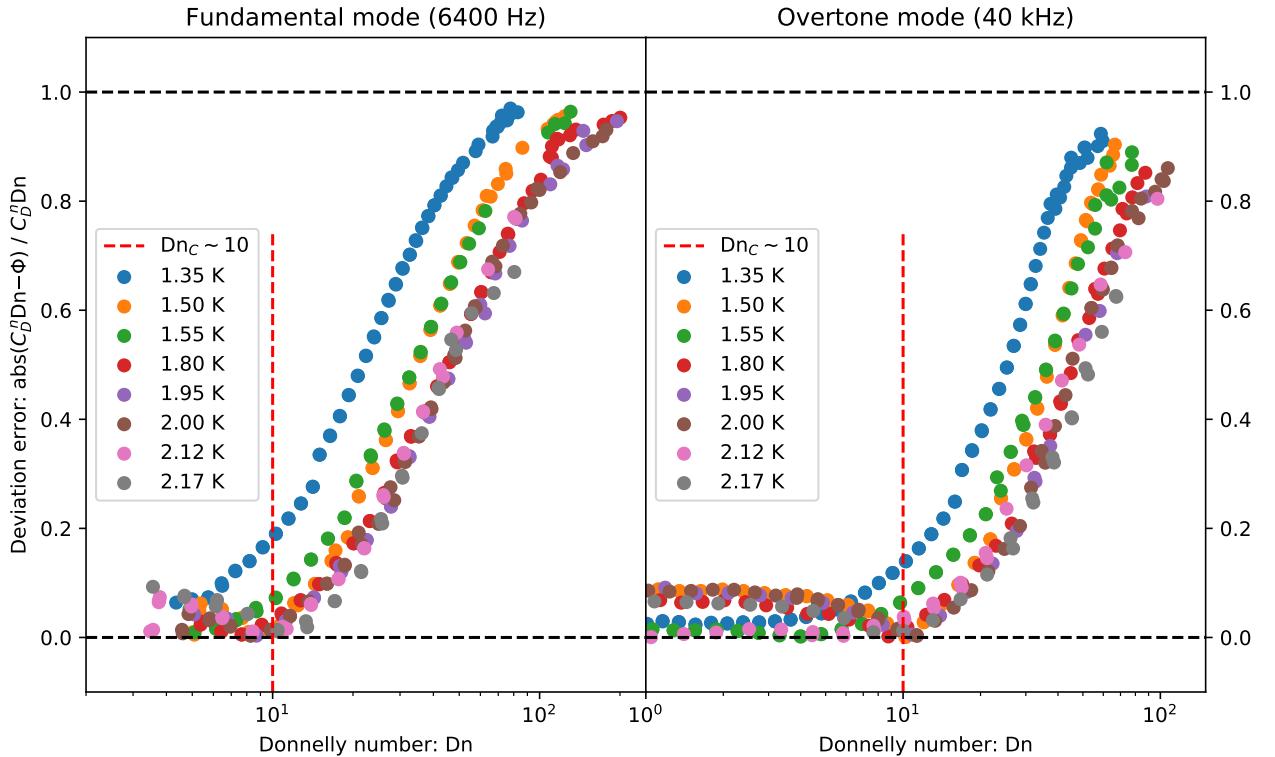


Figure 3.10: Plot of normalized deviations from the linear fit $C_D^n = \Phi/Dn$ with $\Phi = 4.7$ as a function of the Donnelly number. Left image: Errors in fork's fundamental mode, Right image: Errors in fork's overtone mode, Black dashed lines mark the boundaries and red dashed lines our estimations for the values of Dn_C .

Our estimated value for critical Donnelly number Dn_C for temperature curves $T > 1.6$ K and for both oscillation modes is $Dn_C \sim 10$. This shared value of Dn_C proves the high-frequency regime validity and thus the possible domination of classical turbulence from normal component.

3.2 Ballistic regime

In this section, we demonstrate the limits of universal scaling validity. In **Figure 3.11** we plot the scaling function of Weissenberg number $f(Wi)$, as derived in [34] and introduced in the **Theoretical Background** in (1.34). In order to validate the derivation, we add the experimental results obtained with a tuning fork in two-fluid regime (presented in previous section) and also in ballistic regime ($T < 0.6$ K). Again, these regimes represent the Newtonian hydrodynamics ($Wi \ll 1$), governed by Navier-Stokes equations, and a non-Newtonian gas dynamics. [16]

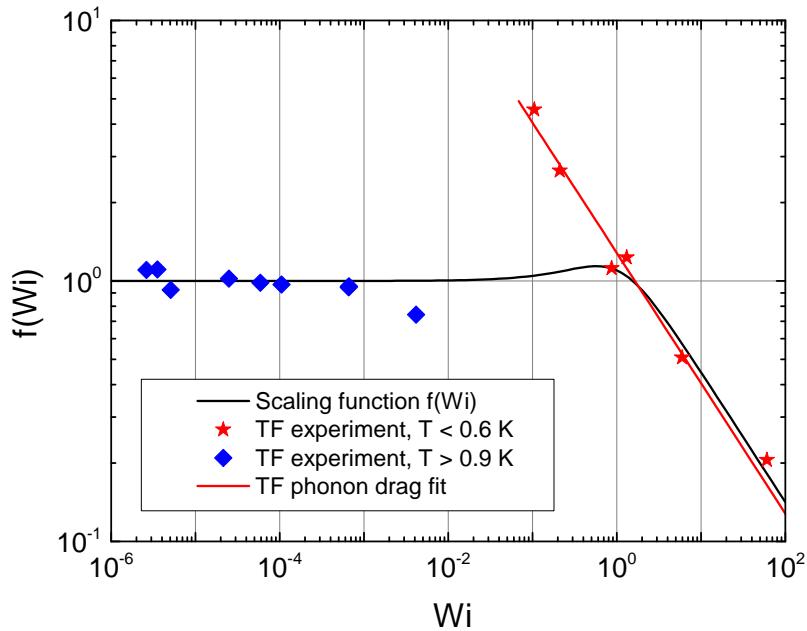


Figure 3.11: Plot of scaling function $f(Wi)$ as proposed in Eq.(1.35) compared with the experimental results of tuning fork in both low and ultra-low temperatures.

Black line is the scaling function, red line fits the phonon drag [16], blue squares mark the data collected from the mentioned experiments and red stars: mark the data collected from an ultra-low temperature range. In all experiments we used the same tuning fork on both oscillation modes.

The derived behavior of scaling function ($f(Wi) \sim 1$ for $Wi \ll 1$ and $f(Wi) \propto 1/\sqrt{Wi}$ for $Wi \gg 1$) reflects the experimental data, except for the transitional area $Wi \sim 0.1$, where emerged a bigger peak than expected.

However, according to **Figure 1.7**, this is the range where the fluid has already reached the ballistic regime ($Kn \sim 1$) earlier than the non-Newtonian one ($Wi \sim 1$). Hence, the assumptions for the scaling function derivation (that the situation $Wi \sim 1$ happens before, or at the same time, as $Kn \sim 1$) are no more valid and thus our prediction $f(Wi) \propto 1/\sqrt{Wi}$ for the problematic area $Wi \sim 0.1$ does not hold. In this case, the apparent scaling $f(Wi) \propto 1/\sqrt{Wi}$ simply means a frequency-independent drag force, as is expected for the ballistic regime.

3.3 Flow phase diagram

The last plot we show in **Experimental results** is the *flow phase diagram*, summarizing the achieved hydrodynamical states by the oscillating tuning fork at various temperatures and modes. In **Figure (3.12)** we also mark the estimated areas ("CT" for classical turbulence and "QT" for quantum turbulence), where the transitions to non-linear regimes emerge, separately for the normal and superfluid component.

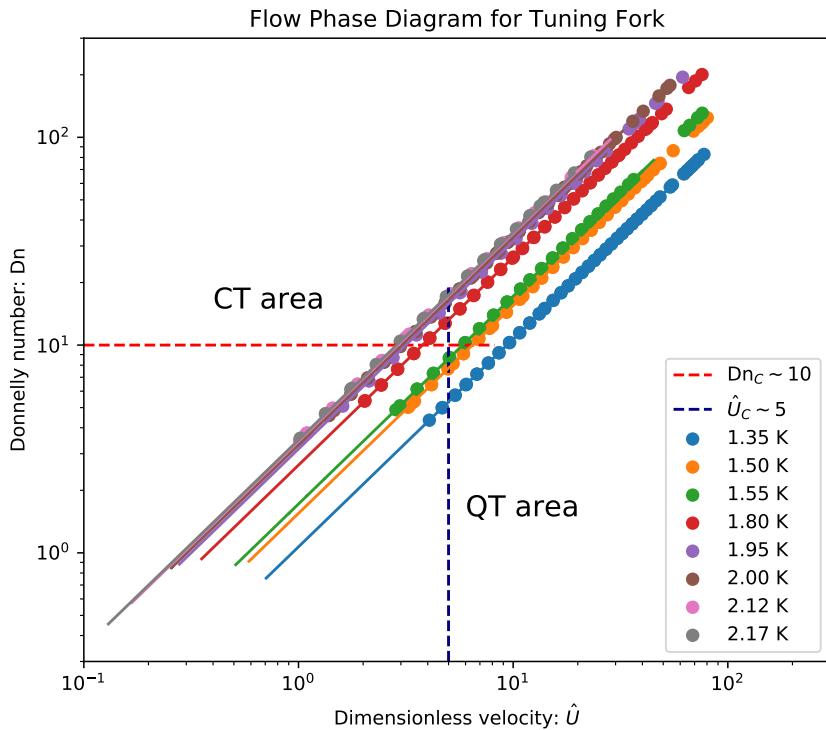


Figure 3.12: Plot of Donnelly numbers against dimensionless velocities for both fork's oscillation modes. Full lines fit the overtone mode data and dashed lines the estimated areas of transition from laminar/potential regimes to the non-linear ones, both for normal and superfluid components.

It is worth to note that the *CT area* and *QT area* are not so sharp as it may seem from the graph. First of all, the most of the graph is covered by *mixed turbulence* area since we already hinted that QT probably directly triggers CT.

Also, there could not be any more data above the $T = 2.17\text{ K}$ curve since it is the natural limitation for the warmest Helium-II system.

4. Simulations

This part of Thesis serves as a general description of the **PyVort** codebase, a new platform to simulate quantum vortices. The code is written in well commented **Python 3**, arranged in a modular structure. The primary aim of this chapter is to highlight which modules are involved and how they work. On GitHub, one can find a table of the parameters (user's options) which can be set in the `config.py` file to run the simulation.

At present, we use infinite boundary conditions. Therefore, only closed-loop vortices can be realized in simulation. However, the codebase is flexible and supports the potential implementation of unclosed loops.

4.1 Vortex filament model

The **PyVort** code is based on vortex filament (VF) model, a technique pioneered by Schwarz [26] in the early 1980s. Superfluid vortex filament is represented by a series of mesh points (segments) distributed along the centerline of the filament (**Figure 4.1**). The motion of the whole VF is summed up by the motion of each mesh point.

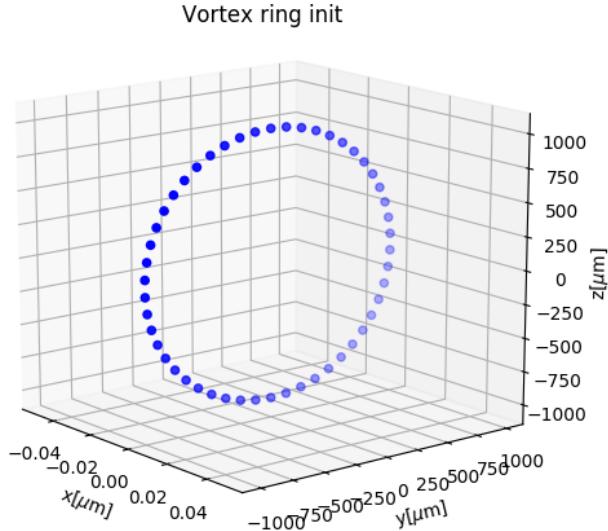


Figure 4.1: Visualisation of vortex ring segments right after their initialization.

As introduced in **Theoretical Background** chapter, we define the VF more precisely as a three dimensional curve $\mathbf{s}(\xi, t)$, where ξ represents an arc-lengths and t the time. Each segment, indexed as (i) (i is increasing as we move along the VF) is localized by its assigned coordinates \mathbf{s}_i and direct neighbors indices: *previous* $(i - 1)$ and *next* $(i + 1)$.

This leads to a data structure called *directed digraph*, which we found as an useful array structure for vortex segments and thus was implemented.

Next we define the tangent vector \mathbf{s}' , then normal vector \mathbf{s}'' , and the binormal vector $\mathbf{s}' \times \mathbf{s}''$, as depicted in **Figure 1.3**, by taking numerical derivatives. Note $\mathbf{s}' = d\mathbf{s}/d\xi$ and $\mathbf{s}'' = d\mathbf{s}'/d\xi$. Numerical derivatives are achieved using *Finite Differences* method, as introduced in next subsection.

Finite differences

In order to properly calculate the numerical derivatives \mathbf{s}' and \mathbf{s}'' , belonging to the directed 3D curve, we need to use a sophisticated numerical method. At a particular segment (i) with position \mathbf{s}_i , we define the distance to the next point \mathbf{s}_{i+1} as $l_i = |\mathbf{s}_{i+1} - \mathbf{s}_i|$ and the distance to the previous point \mathbf{s}_{i-1} as $l_{i-1} = |\mathbf{s}_i - \mathbf{s}_{i-1}|$ (**Figure 4.2**).

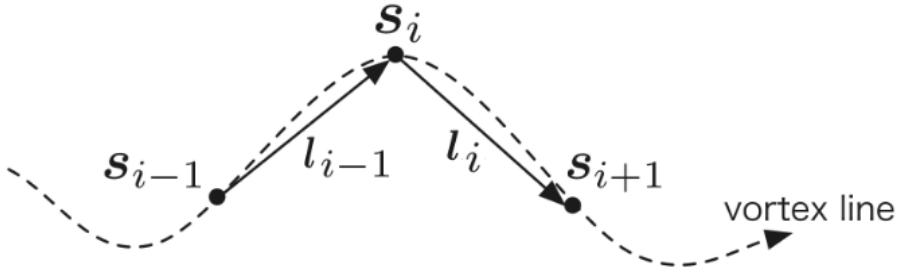


Figure 4.2: Depiction of i -th segment vector and its corresponding lengths. Source: [27]

For accuracy, we approximate all the spatial derivatives \mathbf{s}'_i , \mathbf{s}''_i by a fourth-order finite difference method (FD), which can also account for the varying distances along the vortex filament. With this, the first and second derivatives can be obtained based on coordinates of 2 closest neighbors (on each side).

Using FD theorem, we can construct the approximations by taking the Taylor's series expansions. We can then write:

$$\frac{d^n \mathbf{s}_i}{d\xi^n} \approx A_i \mathbf{s}_{i-2} + B_i \mathbf{s}_{i-1} + C_i \mathbf{s}_i + D_i \mathbf{s}_{i+1} + E_i \mathbf{s}_{i+2} \quad \text{for } n \in \{1, 2\} \quad (4.1)$$

Calculation of coefficients A, B, C, D, E can be done using analytical solution of *Vandermonde matrix* inversion. This inversion can be done also numerically, which is a more scalable way of implementation, however, this method often meets with problems when the Vandermonde matrix becomes singular. In code, there is implemented both the analytical solution (closed form) and the solution by inverting the Vandermonde matrix.

The closed form works for exactly our form of approximation (4.1) and is more described in [28], whereas the numerical method works generally for any approximation level.

Biot-Savart discretization

We denote the dynamic external sources of velocity fields (which can be set in `config.py`) as $\mathbf{v}_{n,ext}(\mathbf{r}, t)$ and $\mathbf{v}_{s,ext}(\mathbf{r}, t)$. The equation of motion for a given segment is then given directly by Schwarz's equation(1.13):

$$\frac{d\mathbf{s}_i}{dt} = \mathbf{v}_{s,ext} + \mathbf{v}_{\text{ind}}^{(i)} + \mathbf{v}_{\text{drive}}^{(i)} \quad (4.2)$$

The first difficulty in the VF model comes from the calculation of term \mathbf{v}_{ind} . As we shown previously in (1.6), this advection term can be split into the LIA part and a Biot-Savart integral:

$$\mathbf{v}_{\text{ind}}^{(i)} = \mathbf{v}_{\text{LIA}}^{(i)} + \mathbf{v}_{\text{BIOT}}^{(i)} = \frac{\kappa}{4\pi} (\mathbf{s}'_i \times \mathbf{s}''_i) \ln \left(\frac{2\sqrt{l_{i-1}l_i}}{a} \right) \quad (4.3)$$

$$+ \frac{\kappa}{4\pi} \int_{\mathcal{L}'} \frac{(\mathbf{r}' - \mathbf{s}_i) \times d\mathbf{r}'}{|\mathbf{r}' - \mathbf{s}_i|^3}, \quad (4.4)$$

where l_{i-1} and l_i are the arc lengths of the curve between points \mathbf{s}_{i-1} and \mathbf{s}_i and between \mathbf{s}_i and \mathbf{s}_{i+1} respectively, and \mathcal{L}' is the original vortex line without the two segment lines between \mathbf{s}_{i-1} and \mathbf{s}_{i+1} .

Using the segment discretization, the Biot-Savart integral can be rewritten [29] into the sum of single-line contributions (**Figure 4.3**) between each j -th and $j + 1$ -th segment (except for the ones attached to the i -th point):

$$\mathbf{v}_{\text{BIOT}}^{(i)} \approx \frac{\kappa}{4\pi} \sum_{j \notin \{i-1, i\}} \frac{(R_j + R_{j+1})(\mathbf{R}_j \times \mathbf{R}_{j+1})}{R_j R_{j+1}(R_j R_{j+1} + \mathbf{R}_j \cdot \mathbf{R}_{j+1})}, \quad (4.5)$$

where $\mathbf{R}_j = \mathbf{s}_j - \mathbf{s}_i$ and $\mathbf{R}_{j+1} = \mathbf{s}_{j+1} - \mathbf{s}_i$ are the relative vectors from the given point.

Note that, if one takes into account the Biot-Savart law for N mesh points, the computational time is proportional to $\mathcal{O}(N^2)$, while, if one uses just the LIA term, it is only $\mathcal{O}(N)$. Numerical simulations based on Biot-Savart are therefore significantly more computationally expensive.

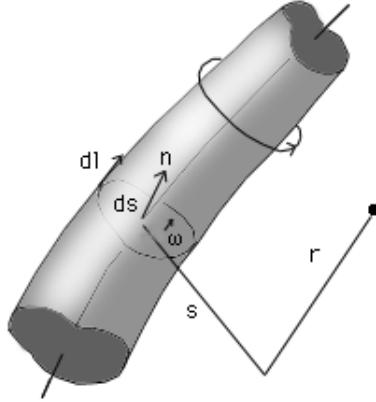


Figure 4.3: An infinitesimal contribution of a j -th segment line between two points \mathbf{s}_j and \mathbf{s}_{j+1} at a given point \mathbf{r} . Source: [30]

One way to get around this difficulty is to update the LIA term. In this method we neglect completely the non-local Biot-Savart integral and keep just the local term. This is typically done with a minor adjustments within the log term:

$$\mathbf{v}_{\text{LIA}}^{*(i)} = \frac{\kappa}{4\pi} (\mathbf{s}'_i \times \mathbf{s}''_i) \ln \left(\frac{2R_i}{a} \right), \quad (4.6)$$

where R_i is a i -th segment local length scale - may be taken [13] as a local curvature: $R_i = 1/|\mathbf{s}''_i|$. Updated LIA approach (4.6) is a very convenient approximation and works very well for calculating the motion of a single vortex ring.

4.2 Implementation

In code, a system consisting of flow sources and a single vortex ring object is represented using several `class` structures. These structures are updated after each time step. We will call them as a *state* of the system and it is defined (and initialized) with following properties:

Environment class

- external normal component - defines an external source of normal component flow
- external superfluid component - defines an external source of superfluid component flow

Ring class

This class is initialized only when the purpose of simulation is to collect physical and statistical data about vortex rings.

- center - an array of ring center coordinates
- radius - current radius R of the ring object
- direction - a normal vector $\hat{\mathbf{n}}$ pointing in a direction toward which the ring is moving
- velocity - measured velocity of the ring center \mathbf{v}_{ring}

Vortex class

- number of active segments - number of active segments N the vortex ring is composed of
- segments - an array of all segments, each one with following attributes:
 - activity - a logical value whether a particular segment should be considered as a part of vortex object
 - coordinates - an array of segment coordinates $\mathbf{s}_i = [x_i, y_i, z_i]$
 - previous/next neighbor - array localization indices of the *previous* ($i - 1$) and the *next* ($i + 1$) segment within the context of the directed vortex
 - tangent/curvature - a tangential and normal vectors \mathbf{s}'_i and \mathbf{s}''_i
 - LIA velocity - a self-induced velocity $\mathbf{v}_{\text{LIA}}^{(i)}$ driven by the local curvature. (4.3) or (4.6)
 - BIOT velocity - a self-induced velocity driven by the farther segment lines of the vortex ring $\mathbf{v}_{\text{BIOT}}^{(i)}$ (4.4)
 - Drive velocity - a velocity given by the mutual friction force $\mathbf{v}_{\text{drive}}^{(i)}$ (1.14)
 - Full velocity - the sum of external sources $\mathbf{v}_{s,\text{ext}}$, LIA velocity $\mathbf{v}_{\text{LIA}}^{(i)}$, BIOT velocity $\mathbf{v}_{\text{BIOT}}^{(i)}$ and the drive velocity $\mathbf{v}_{\text{drive}}^{(i)}$, resulting in $d\mathbf{s}_i/dt$

All functions that are manipulating with segments' attributes are implemented as Vortex class methods. Before each time step, all attributes have to be updated and tested. We used numerical methods already introduced in previous section and tests that are described in next section.

Initialization

The proper initialization of the *state* in the very beginning of simulation requires several physical inputs. This is done in following steps:

0. Symbolically, we expect as a *0-th step* the environmental setup of the system - *external sources, temperature, time-step,....*
1. If interested in quantized ring simulation, we expect several ring inputs from user: *center, radius, direction* and *resolution*. Resolution parameter is the initial desired distance δ between each two neighboring segments. This set of 4 inputs makes an unambiguous ring object, ready for next updates.
2. After creation, we initialize neighbor indices (to an i -th element in segment array will be assigned $i - 1$ index as the *previous* and $i + 1$ index as the *next* neighbor index)
3. Next we calculate all \mathbf{s}' and \mathbf{s}'' using Finite differences method
4. Final step is the calculation of all segment velocities using motion equations and their approximative forms.

After these four steps, we obtain a fully updated ring object that can be propagated in time.

4.3 Time evolution

After we defined and ran all the necessary calculations leading to the vortex ring's *state* fulfillment, we can start to propagate it in time (visualized example in **Figure 4.4**).

Time stepping

Time evolution is based on an explicit iterative method: the fourth-order Runge-Kutta (RK4) scheme. When we consider the Schwarz's equation $d\mathbf{s}_i/dt \equiv \mathbf{v}_{\text{full}}^{(i)}$, the stepping algorithm is given as:

$$\mathbf{s}_i(t + dt) = \mathbf{s}_i(t) + \frac{dt}{6}(\mathbf{v}_1^{(i)} + 2\mathbf{v}_2^{(i)} + 2\mathbf{v}_3^{(i)} + \mathbf{v}_4^{(i)}), \quad (4.7)$$

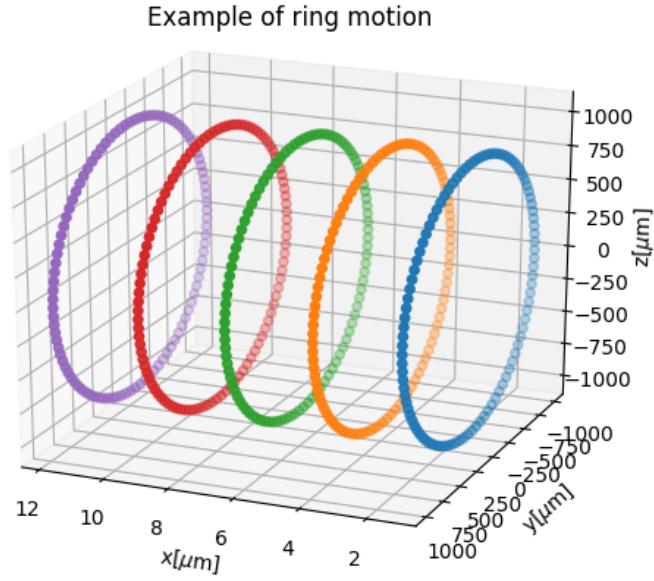


Figure 4.4: Example of a moving vortex ring

where dt is the time step and the velocities $\mathbf{v}_1^{(i)}, \mathbf{v}_2^{(i)}, \mathbf{v}_3^{(i)}, \mathbf{v}_4^{(i)}$ are the induced velocities of partial steps:

$$\mathbf{v}_1^{(i)} = \mathbf{v}_{\text{full}}^{(i)}(\mathbf{s}_i, t), \quad (4.8)$$

$$\mathbf{v}_2^{(i)} = \mathbf{v}_{\text{full}}^{(i)}(\mathbf{s}_i + \mathbf{v}_1^{(i)} dt/2, t + dt/2), \quad (4.9)$$

$$\mathbf{v}_3^{(i)} = \mathbf{v}_{\text{full}}^{(i)}(\mathbf{s}_i + \mathbf{v}_2^{(i)} dt/2, t + dt/2), \quad (4.10)$$

$$\mathbf{v}_4^{(i)} = \mathbf{v}_{\text{full}}^{(i)}(\mathbf{s}_i + \mathbf{v}_3^{(i)} dt, t + dt) \quad (4.11)$$

Lower-order schemes such as basic Euler method is also implemented in code, however, not recommended to use. More on this is discussed in Results part of thesis.

The time step dt is adaptively changing so that the vortex ring cannot move faster than a 1% of its size in a single step. As we will see later in Results, in case of vortex rings with changing radius, the time step dt has to be iteratively changing after each break of the above rule:

$$dt \leftarrow \frac{0.01R}{|\mathbf{v}_{\text{ring}}|} \quad (4.12)$$

4.4 Re-segmentation of vortex

To obtain the most realistic simulation (to capture effects on any length scale), the natural tendency would be to set the resolution parameter δ as low as possible. However, the CPU time cost rises rapidly as the number of segments N increases, so there is need to find the best trade-off.

As the distance between neighboring segments is reduced/enlarged with time due to the physics and numerical inaccuracies, there is need to remove/add segments (*re-segment*) in order to conserve the vortex resolution δ . The closeness (in terms of arclength) of neighboring segments is therefore measured after each simulation time-step.

We used the simplest re-segmenting criteria - keeping an approximately *uniform distance* between the segments. To ensure this, two boundary conditions were implemented:

1. The segment \mathbf{s}_{j+1} would be removed if:

$$|\mathbf{s}_{j+1} - \mathbf{s}_j| < \delta_{\min}, \quad (4.13)$$

where δ_{\min} is the minimal distance between two segments. Also, the segment \mathbf{s}_j would take place somewhere between \mathbf{s}_{j-1} and \mathbf{s}_{j+2} so that it will conserve the curvature of vortex. Such result can be obtained using any spline interpolation along nearest neighbors. We worked with 3D local spline using 4 points (in our context they would be $\mathbf{s}_{j-2}, \mathbf{s}_{j-1}, \mathbf{s}_{j+1}, \mathbf{s}_{j+2}$) and create another 11 interpolated knots. Consequently, the new position of \mathbf{s}_j will be the position of the 6-th knot (the middle one).

2. We add a new segment \mathbf{s}_{new} between \mathbf{s}_j and \mathbf{s}_{j+1} if:

$$|\mathbf{s}_{j+1} - \mathbf{s}_j| > \delta_{\max}, \quad (4.14)$$

where δ_{\max} is the maximal allowed distance between two segments.

This method keeps all the distances along the vortex roughly in the range $\delta \in \langle \delta_{\min}, \delta_{\max} \rangle$ and also keeps the geometrical properties.

Real-time tests

After each time step is done, a few tests are performed, to ensure that vortex itself is behaving according to our expectations. The tests are following:

- Length test - This test calculates the segmented vortex circumference as $l = \sum_j |\mathbf{s}_j - \mathbf{s}_{j+1}|$ and compare it with the theoretical one $2\pi R$, where radius R has to be measured as well. If the deviation from the theoretical value is too high $> 1\%$, the segments are noisy and the process is killed. In case of deviation below $< -1\%$, there are clearly too few segments and re-segmentation process is called.
- Segmentation test - Here we check the value $l_j = |\mathbf{s}_j - \mathbf{s}_{j+1}|$ for each j and ask whether $l_j \in \langle \delta_{\min}, \delta_{\max} \rangle$. If not, re-segmentation process is called.
- Smallness test - If the vortex ring radius would decrease below $R < \delta_{\min}$, the ring is deleted from the simulation.

4.5 Future implementations

To make Pyvort a full-fledged quantum vortex simulation, there should be implemented following improvements:

Complexity speedup

Recent numerical research presented [31] a new numerical method to compute the evolution of vortex filament. The method is based on an N-body cosmological simulation by Barnes and Hut [32], a *tree algorithm* which considerably speeds up the calculation of Biot-Savart integrals - computational cost scales as $\mathcal{O}(N \log(N))$ rather than N^2 . Properties of the tree method were tested for a variety of vortex configurations, ranging from simple vortex rings to a counterflow vortex tangle and compared with the LIA approach and the exact Biot-Savart's law.

Implementation of such algorithm is not easy, but definitely worth due to the gain in efficiency.

Re-connection process

If any lines of two vortices (or even the single one) become very close, the filaments can re-connect, changing the topology of the system. Many researchers experimentally reported this is happening and also found analogies with vortex dynamics in the Navier–Stokes equation.

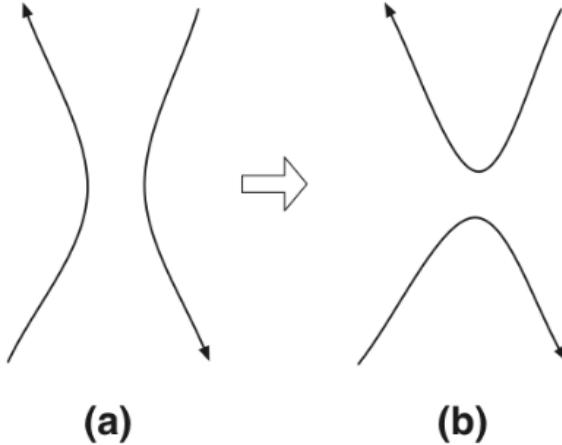


Figure 4.5: Reconnection of quantized vortices. (a) Two vortices before reconnection, about to contact each other. (b) The new vortices after reconnection.

The VF model itself cannot describe the reconnection process because the vortex core structure is neglected. Hence, some artificial procedures must be introduced to simulate such process. For instance, when two vortices approach within a critical distance δ_{\min} , we will artificially reconnect the vortices.

The main criteria for reconnection is that the total length (this is corresponding with energy) will decrease. Self-reconnection (e.g. caused by a twist of vortex) would be treated in the same way. Since reconnection involves only anti-parallel vortices, one has to check using the inner product whether two vortices could physically reconnect or not.

High-order tests

Once the code of interacting vortex filaments is developed, the data analysis needs to be improved. The simplest measurable quantity is the total length of all vortex lines. In a finite volume this would be $L = (1/V) \int d\xi$ for the vortex length per unit volume.

Of course, one may define more complicated metrics, measuring the isotropy of the vortex tangle. One of them is the length of line projected along a given vector $\hat{\mathbf{r}}$, given as:

$$J(\hat{\mathbf{r}}) = \frac{1}{VL} \int_L \sqrt{1 - (\mathbf{s}'(\xi) \cdot \hat{\mathbf{r}})^2} d\xi \quad (4.15)$$

5. Simulation Results

In this chapter, we analyze the functionality of new codebase. We made several tests on energy conservation, precision of numerical methods and stability, to ensure that simulation is reliable and stable for further development.

All presented measurements and optimizations were conducted in order to recommend the best simulation parameters for future investigations, which is ensured by the correct setup of the `config` file. We performed tests with physical motivation and also tests focused on precision and stability. With presented findings, the reliability and stability of any further large-scale simulation should be ensured.

5.1 Zero-temperature test

In case of zero temperature $T = 0\text{ K}$, the *normal component* in superfluid He-II is not present anymore and therefore also no mutual friction. Even the mutual friction is not the only present dissipation process (we neglect phonon emissions), we expect for our numerical model to conserve the velocity and energy of the vortex ring.

We plotted in **Figure 5.1** the ring velocity $|\mathbf{v}_{\text{ring}}|$ and energy E_{ring} evolving in time, for the case of temperature $T = 0$ (pure superfluid, no normal component) and $T = 1.5\text{ K}$ (considerable ratio of present normal and superfluid component $\rho_s/\rho_n \approx 8$).

We tested the mutual friction effect during 1000 time-steps (referred to as *epochs*) with adapting time-step dt according to (4.12).

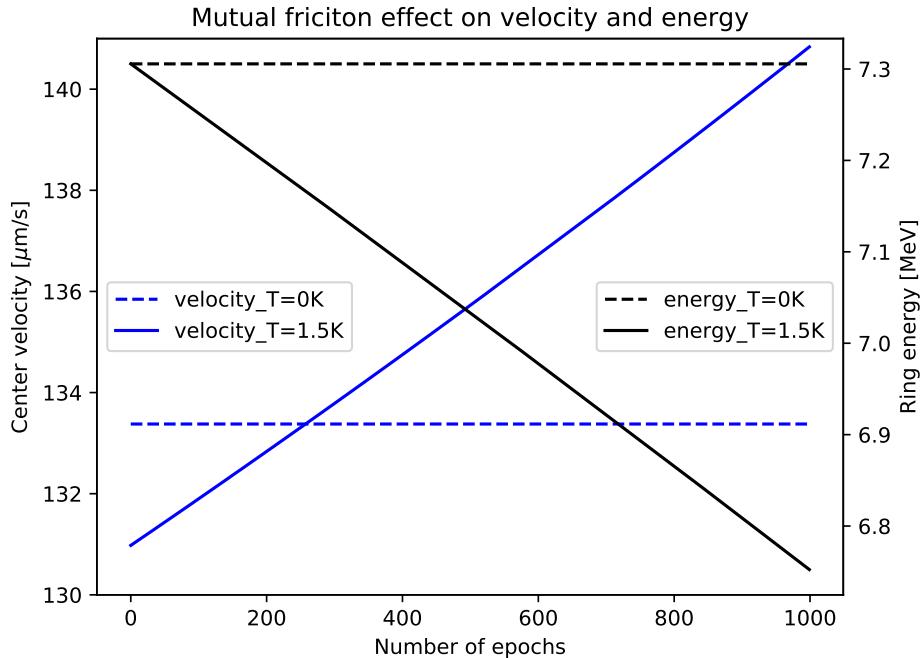


Figure 5.1: Evolution of ring velocity and energy in time. Blue lines - measured velocity data, Black lines - measured energy data, Dashed lines - the constant behavior for temperature $T = 0\text{ K}$, Full lines - the dissipative process for temperature $T = 1.5\text{ K}$.

On x axis, we plot the number of elapsed epochs (time steps) and on y axis the velocity of the ring center $|\mathbf{v}_{\text{ring}}|$ and ring energy E_{ring} .

As we see, at $T = 0\text{ K}$ the velocity and energy is conserved even after 1000 epochs of simulation due to missing dissipation process (mutual friction). In case of $T = 1.5\text{ K}$, energy is decreasing as expected, whereas the velocity is increasing. This increase is physically well-explained by the fact that the radius is decreasing with time due to the non-dissipative term of mutual friction. Also, it can be seen directly from the theoretical formula (1.16).

5.2 Velocity precision test

Our first velocity test compares the various approaches how can the ring velocity $|\mathbf{v}_{\text{ring}}|$ be calculated. Here, we compare four approaches, recognizing their theoretical motivation, computational complexity and precision:

- LIA (4.3): motivated [13], computationally cheap, not precise
- LIA + BIOT (4.3 + 4.4): motivated [13], but computationally expensive
- updated LIA (4.6): not well motivated [29], but computationally cheap and precise
- Theoretical (1.16): well motivated [9] and most precise

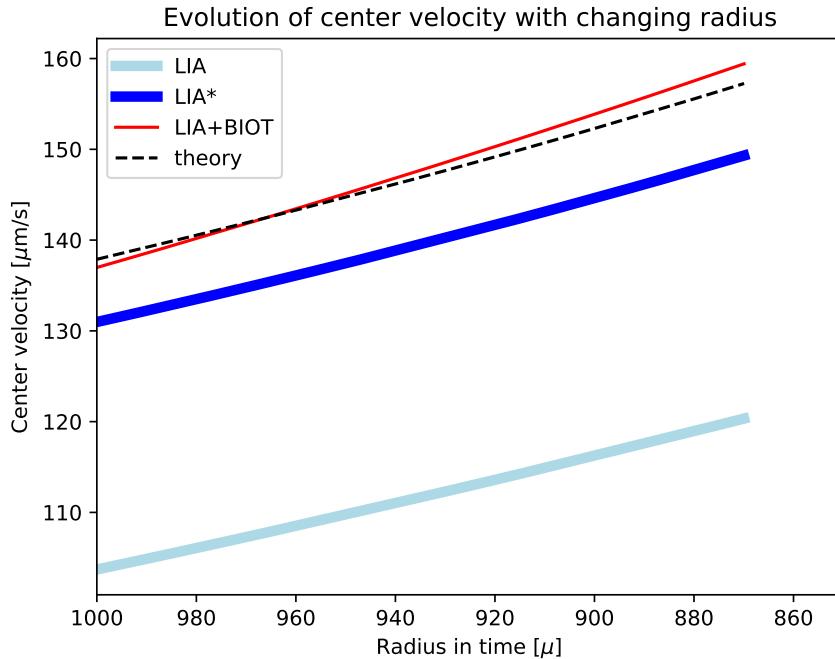


Figure 5.2: Comparison of all implemented velocity approaches (full lines) with the theoretical one (black dashed line) according to (1.16), with decreasing radius in time.

Velocity values $|\mathbf{v}_{\text{ring}}|$ on y axis are computed always using the measured decreasing radius value (x axis)

The theoretical values of ring velocity from (1.16) are taken as a baseline that other velocity calculations are compared with. All velocities were measured and evolved over a few thousands epochs (time steps), during which the radius was dissipative decreasing, as is plotted in **Figure 5.2**.

We see that the theoretically most precise (LIA + BIOT) approach grows a bit faster than it should according to theory. This inconsistency is caused by too big resolution

parameter, which was set at $\delta \approx 70\mu\text{m}$

Therefore, for all further measurements we used the updated LIA velocity (LIA*) approach due to its time-scale consistency and computational speed.

5.3 Velocity convergence test

Next, we investigated the magnitude of the ring velocity $|\mathbf{v}_{\text{ring}}|$ for various resolutions $\delta \in \langle 50, 200\rangle\mu\text{m}$, immediately after initialization and then after 100 epochs. Ring radius was always set at $R = 1000\mu\text{m}$ (this is usual working radius [27] [28]), so the number of discretization points along the vortex was given by R and δ as $N \approx 2\pi R/\delta \in \langle 30, 120\rangle$.

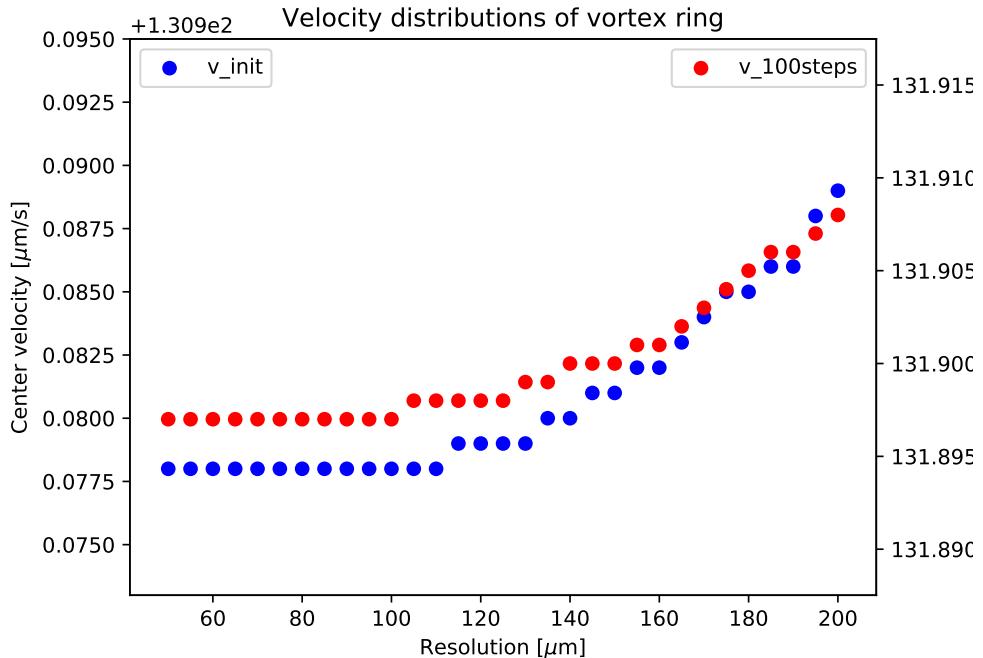


Figure 5.3: The distribution of ring velocity values $|\mathbf{v}_{\text{ring}}|$ for a range of resolution parameters δ in two situations. Blue dots - Velocity values immediately after initialization, Red dots - velocity values after 100 time-steps.

On x axis, we plot the resolutions δ of vortex segments and on y axis the ring velocity $|\mathbf{v}_{\text{ring}}|$.

We see in **Figure 5.3** the expected convergent behavior of both measured velocities in the range of good resolutions (small values of δ). It seems that below $\delta < 100\mu\text{m}$ (corresponding to ≈ 60 segments along the ring of radius $R = 1000\mu\text{m}$) the velocities are converged, which provides the upper boundary for a *good-chosen* resolution.

Even if it is intuitive that good resolutions (small δ -s) lead to more precise velocities, the high number of vortex segments $N \propto 1/\delta$ worsens the stability of simulation in time.

The reason behind this effect is the assumption of $RK4$ stepping method that functions, which $RK4$ is approximating, are smooth. With higher number of segments, there is higher chance for the ring to be non-smooth, which leads to exponential errors in $RK4$ algorithm.

Therefore, we propose also a lower boundary for δ , ensuring the stability, in a following test in next subsection.

5.4 Stability test

Stability of simulation in time was measured for a range of resolutions $\delta \in \langle 10, 100 \rangle \mu\text{m}$ and three values of vortex radius $R \in \{500, 1000, 2000\} \mu\text{m}$ using *Euler* and *RK4* stepping method. In all cases, the stability is measured by the maximal number of elapsed epochs, till the simulation was forced to stop. This enforcement was determined by the violation of length condition, as was described in **Real-time tests** subsection- the real vortex circumference $l = \sum_j |\mathbf{s}_j - \mathbf{s}_{j+1}|$ cannot deviate more than 1% from the geometrical value $2\pi R$, where R is the measured radius in current state.

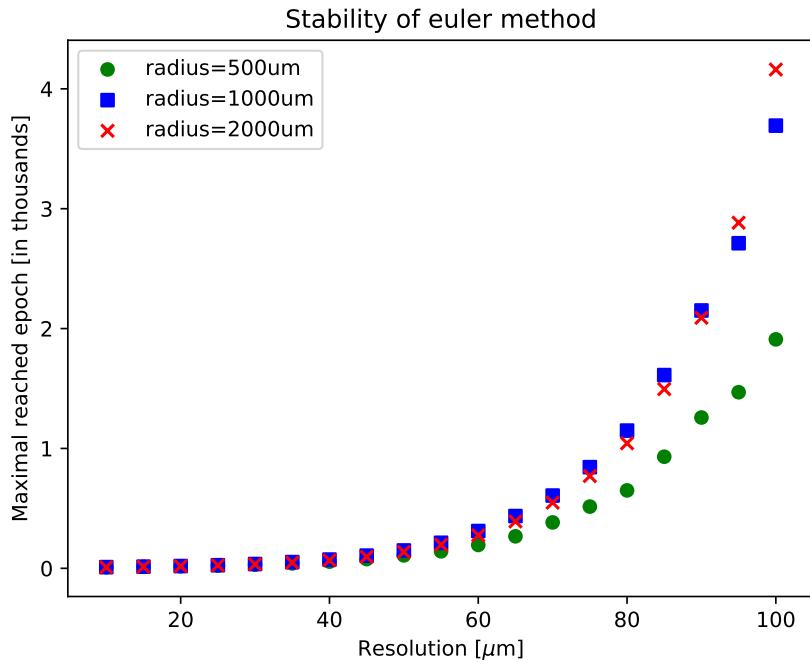


Figure 5.4: Plot of maximal elapsed epoch (time step) of simulation with a given resolution δ , radius R and *Euler* stepping method, till the simulation was forced to stop by violating the length condition.

From the plot in **Figure 5.4**, the *Euler* method seems to be unstable for all resolutions $\delta \in \langle 10, 100 \rangle \mu\text{m}$. Such behavior was expected and simulated only as an example of

inappropriately chosen stepping method.

The next experiment was conducted with *RK4* method, a much more stable method comparing with the *Euler* one, but also suffering from strong assumptions (smoothness of evolving function). After the same experiment with changed time-step method was performed, we measured a stronger stability:

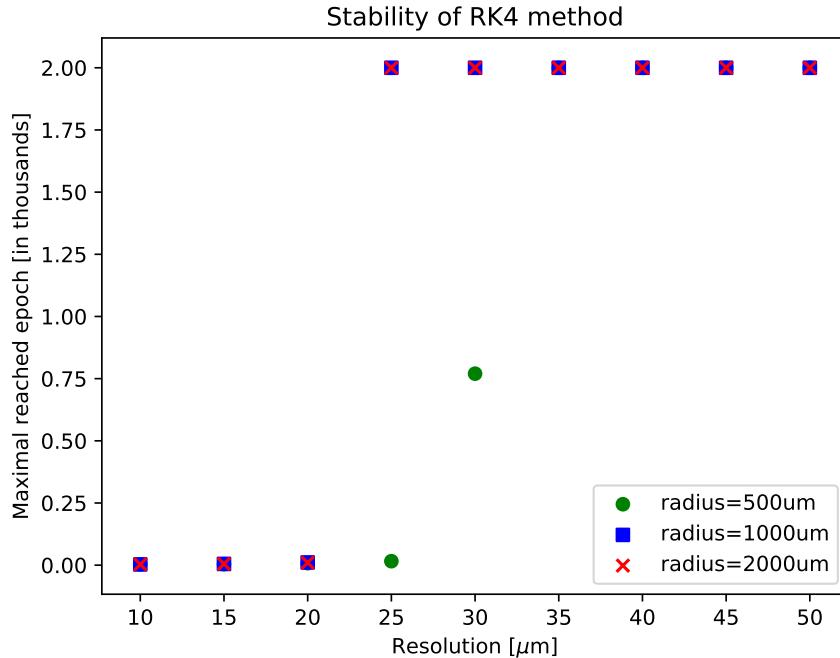


Figure 5.5: Plot of maximal elapsed epoch (time step) of simulation with a given resolution δ , radius R and *RK4* stepping method, till the simulation was forced to stop by violating the length condition. A threshold is set on 2000 epochs.

The plot in **Figure 5.5** suggests the minimal resolution to be at least $\delta > 30\mu\text{m}$. This boundary estimate is still quite conservative, since the radius of vortex is decreasing in time and re-segmentation processes will happen. Re-segmentation process significantly contributes to the stability of simulation since the deletion of some segments behaves as a *smoothing effect* which supports the *RK4* method to be stable.

6. Conclusions

In this chapter we summarize the findings of analyzed experiments from **Experimental Results** chapter and of numerical experiments from the **Simulation** chapter.

6.1 Experimental conclusions

We investigated systematic high-Stokes flows of Helium-II at a range of temperatures $T \in \langle 1.35\text{ K}, 2.17\text{ K} \rangle$ generated by several types of oscillators - *vibrating wire, torsionally oscillating disc and tuning fork*. All of them were kept in high-frequency limit to ensure the Stokes number to be $\text{St} \gg 1$.

Within the area of low peak velocities, we showed the normal component behaving laminar ($C_D^n \propto \text{Dn}^{-1}$) and superfluid component remaining potential (or stationary in case of torsional disc).

When we consider only a negligible amount of remnant quantized vortices attached to the oscillator body, the normal and superfluid components have independent velocity fields, so the measured drags can be analyzed separately as well. In this limit we treat the normal component as a classical viscous fluid, resulting naturally in inverse scaling of measured normal drag coefficient with the Donnelly number: $C_D^n \propto \text{Dn}^{-1}$.

Assuming that superfluid component doesn't contribute to the drag, the universal scaling holds until a critical velocity U_C for a given oscillator geometry is reached. Or, generalizing it for all oscillator modes $\{\omega_i\}$, until a critical dimensionless velocity $\hat{U}_C = U_{C_i}/\sqrt{\kappa\omega_i}$ is reached.

In general, we distinguish between 4 types of hydrodynamical states of Helium-II. We label the instabilities formed due to normal component as "CT" (classical turbulence) and due to superfluid component as "QT" (quantum turbulence):

- No CT nor QT present: laminar regime as described above, working universal scaling on normal component, superfluid component is potential or not moving at all, observed with all used oscillators ($\text{Dn} \lesssim 1$ for vibrating wire, $\text{Dn} \lesssim 5$ for oscillating disc and $\text{Dn} \lesssim 10$ for both oscillation modes of tuning fork).
- CT present without QT: normal component expected to start exhibiting a classical non-linear behavior after reaching critical value of Donnelly number Dn_C (thus universal scaling still holds), superfluid component expected to remain potential or

motionless, observed only with tuning fork at both oscillation modes for temperatures higher than $T > 1.6$ K with low Donnelly numbers between $10 \lesssim Dn \lesssim 100$.

- QT present without CT: occurs if critical velocity U_C given by Donnelly-Glaberson instability (reconnection of remnant vortices) is achieved sooner than the critical Donnelly number Dn_C . Generally it is hard to prove whether such situation occurred since the CT is usually triggered almost immediately due to the mutual friction, but the data obtained with the wire and the disc show a very strong indication.
- Both CT and QT present: both normal and superfluid components are expected to contribute to the drag, occurring when both critical velocity U_C and Donnelly number Dn_C are reached (or triggered), observed with all used oscillators.

To summarize, Donnelly-Glaberson instability (launching QT) occurs upon reaching a **critical dimensionless velocity** \hat{U}_C , while the instability in the normal component is governed upon reaching a **critical Donnelly number** Dn_C . All of the phase states were observed during experiments on oscillating bodies as described in previous chapters.

We summarize all oscillators, once again in the *flow phase diagram* in **Figure 6.1**:

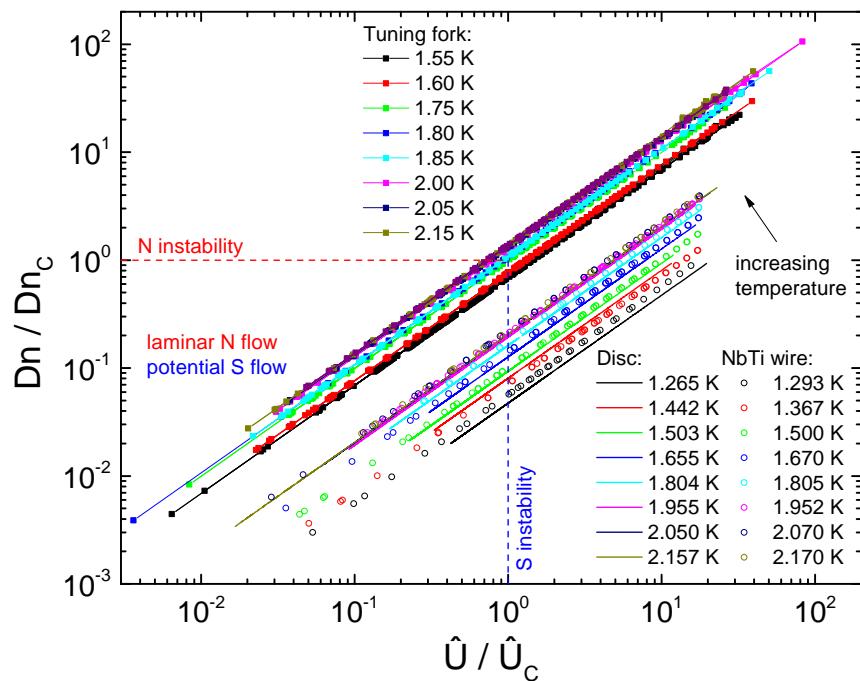


Figure 6.1: Plot of Donnelly numbers against dimensionless velocities for three oscillators - vibrating wire, oscillating disc and tuning fork - submerged in Helium-II.

Dashed lines mark the estimated areas of transition from laminar/potential regimes to the non-linear ones, both for normal and superfluid components. The data used as a tuning fork is sourced from a different experiment, exhibiting the same behavior.

Vibrating wire and oscillating disc reach QT as the first transition. From that, it is questionable when the CT was exactly triggered since the exact behavior of QT evolution with oscillation velocity is not yet known. However, the tuning fork was the only oscillator that encountered the CT earlier than QT for a certain temperatures $T \gtrsim 1.6$ K. Which instability occurs as the first depends both on geometry of the oscillator and temperature. Nevertheless, phase flow diagram proved itself as an useful visualization for such purpose.

Additionally, we presented a formalism allowing the comparison between measurements in hydrodynamical, ballistic and non-Newtonian regimes of Helium-II. We have confirmed the universal scaling concept suggested for laminar flows in high-frequency limit, using the scaling function $f(\text{Wi})$.

However, the transitional flow regime ($\text{Wi} \sim 0.1$) remains an open challenge to the theoretical and experimental investigation.

6.2 Simulation conclusions

We proposed an effective numerical method to compute the time evolution of vortex ring in superfluid He-II. All numerics is implemented in Python 3 and publicly uploaded on GitHub repository.

Performance of vortex filament model was improved by neglecting the Biot-Savart integral, showing that the percentage errors are small, and updating the LIA calculation instead. Simulation well replicates the physical processes and performs with sufficient stability when using testing vortex ring of radius $R \in \langle 500, 2000 \rangle \mu\text{m}$ in resolution $\delta \in (60 - 100) \mu\text{m}$.

7. Appendix

To run the code, there has to be installed only Python 3 (with various libraries) on any OS. All the Python code can be found in the directory `src/`. The entire project is open-source and can be found as a public GitHub repository. Pull requests of any further development would be appreciated.

Here we briefly present a few visualisations of observed instabilities and physical processes.

Instabilities in good and poor resolution

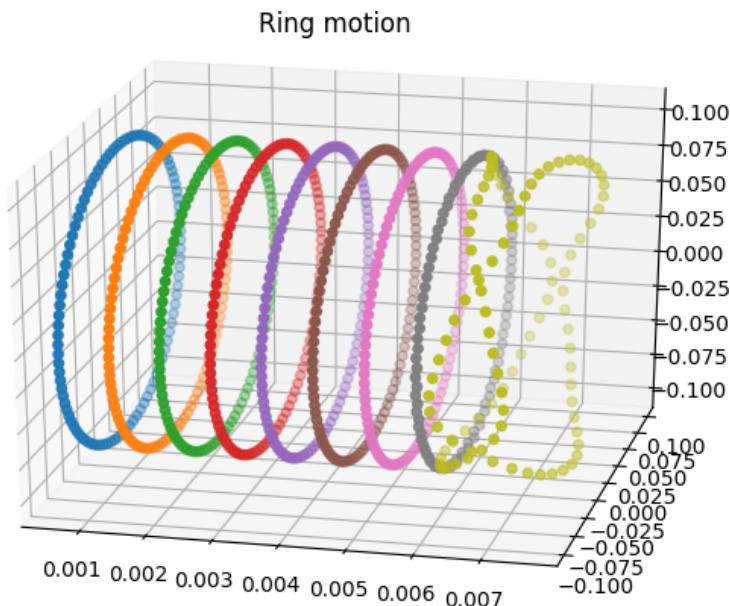


Figure 7.1: A graphical example of ring instability when Euler stepping was used with good resolution (small δ). Ring is moving from the left side to the right with exponentially forwarding error.

Mutual friction effects

Also, we present one of the bigger simulations (**Figure 7.3**) we tested. After we set the ring radius $R = 1000\mu\text{m}$, resolution $\delta = 60\mu\text{m}$ (resulting in around ≈ 100 mesh points), re-segmentation boundaries $\delta_{\min} = \delta/2 = 30\mu\text{m}$, $\delta_{\max} = 2\delta = 120\mu\text{m}$, the updated LIA calculation, RK4 stepping method and a temperature $T = 1.5\text{K}$, we obtained a stable simulation of vortex ring with a decreasing radius. More on particular physical processes can be found in [10].

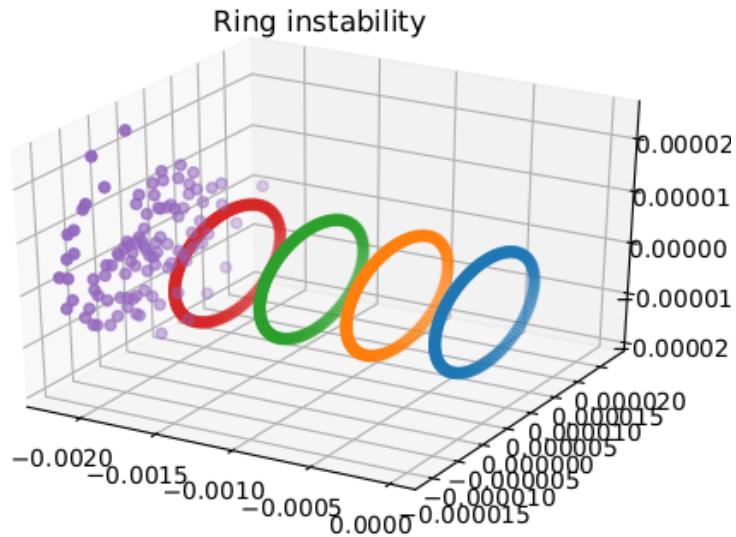


Figure 7.2: Another example of ring instability due to forwarded numerical error using Euler stepping. In this case, resolution δ is higher (worse resolution), so the instability itself is much more noisy.

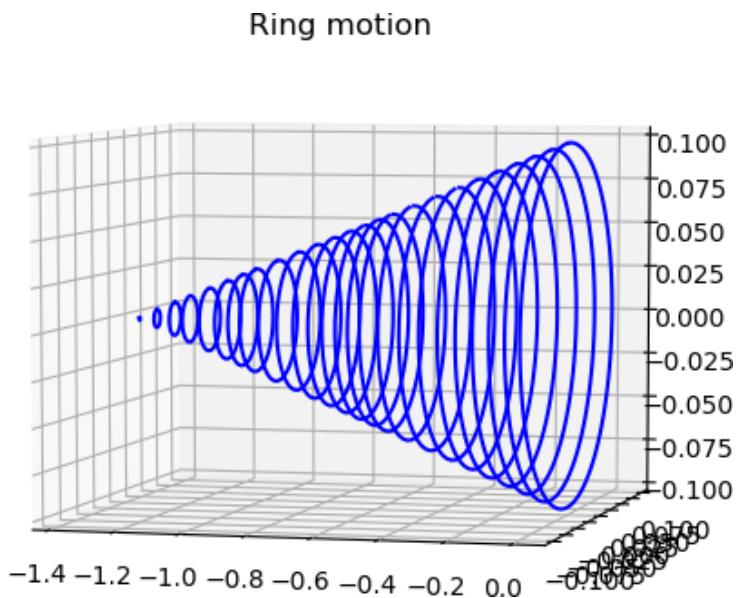


Figure 7.3: Here, a vortex ring is moving to the left, its energy is dissipating due to the mutual friction and therefore, the radius is decreasing in time. The ring re-segmented itself a few times (due to the violation of δ_{\min} condition and died (the simulation was stopped) when the length error was too high.

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