How do we compute the gradient of the end-effector vector? (this is called the Jacobian)

$$\frac{\partial}{\partial \vec{\theta}} \left(\vec{F}(\vec{\theta}) \begin{bmatrix} \vec{t} \\ 1 \end{bmatrix} \right) = \left[\frac{\partial}{\partial \theta_0} \left(\vec{F}(\vec{\theta}) \begin{bmatrix} \vec{t} \\ 1 \end{bmatrix} \right) \quad \cdots \quad \frac{\partial}{\partial \theta_n} \left(\vec{F}(\vec{\theta}) \begin{bmatrix} \vec{t} \\ 1 \end{bmatrix} \right) \right]$$

Using our homogenous coordinates we have

$$\frac{\partial}{\partial \theta_j} \left(\vec{F}(\vec{\theta}) \begin{bmatrix} \vec{t} \\ 1 \end{bmatrix} \right) = \frac{\partial}{\partial \theta_j} \left(\mathbf{T}_0 \cdots \mathbf{T}_n \begin{bmatrix} \vec{t} \\ 1 \end{bmatrix} \right)$$

From the product rule we have

$$\frac{\partial}{\partial \theta_{j}} \left(\vec{F}(\vec{\theta}) \begin{bmatrix} \vec{t} \\ 1 \end{bmatrix} \right) = \frac{\partial}{\partial \theta_{j}} \left(\mathbf{T}_{0} \cdots \mathbf{T}_{j} \cdots \mathbf{T}_{n} \begin{bmatrix} \vec{t} \\ 1 \end{bmatrix} \right) \\
= \left(\left(\frac{\partial}{\partial \theta_{j}} \mathbf{T}_{0} \right) \cdots \mathbf{T}_{j} \cdots \mathbf{T}_{n} \begin{bmatrix} \vec{t} \\ 1 \end{bmatrix} \right) \\
+ \cdots \\
+ \left(\mathbf{T}_{0} \cdots \left(\frac{\partial}{\partial \theta_{j}} \mathbf{T}_{j} \right) \cdots \mathbf{T}_{n} \begin{bmatrix} \vec{t} \\ 1 \end{bmatrix} \right) \\
+ \cdots \\
+ \left(\mathbf{T}_{0} \cdots \mathbf{T}_{j} \cdots \left(\frac{\partial}{\partial \theta_{j}} \mathbf{T}_{n} \right) \begin{bmatrix} \vec{t} \\ 1 \end{bmatrix} \right) \\
+ \cdots \\
+ \left(\mathbf{T}_{0} \cdots \mathbf{T}_{j} \cdots \mathbf{T}_{n} \left(\frac{\partial}{\partial \theta_{j}} \begin{bmatrix} \vec{t} \\ 1 \end{bmatrix} \right) \right)$$

Using calculus we have

$$\frac{\partial}{\partial \theta_{j}} \begin{bmatrix} \cos \theta_{k} & -\sin \theta_{k} & l_{k,x} \\ \sin \theta_{k} & \cos \theta_{k} & l_{k,y} \\ 0 & 0 & 1 \end{bmatrix} = \begin{cases} \begin{bmatrix} -\sin \theta_{k} & -\cos \theta_{k} & 0 \\ \cos \theta_{k} & -\sin \theta_{k} & 0 \\ 0 & 0 & 0 \end{bmatrix} & j = k \\ \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} & j \neq k \end{cases}$$

Apply knowledge about terms that become zero

$$\frac{\partial}{\partial \theta_{j}} \left(\vec{F}(\vec{\theta}) \begin{bmatrix} \vec{t} \\ 1 \end{bmatrix} \right) = \frac{\partial}{\partial \theta_{j}} \left(\mathbf{T}_{0} \cdots \mathbf{T}_{j} \cdots \mathbf{T}_{n} \begin{bmatrix} \vec{t} \\ 1 \end{bmatrix} \right) \\
= \left(\left(\frac{\partial}{\partial \theta_{j}} \mathbf{T}_{0} \right) \cdots \mathbf{T}_{j} \cdots \mathbf{T}_{n} \begin{bmatrix} \vec{t} \\ 1 \end{bmatrix} \right) \\
+ \cdots \\
+ \left(\mathbf{T}_{0} \cdots \left(\frac{\partial}{\partial \theta_{j}} \mathbf{T}_{j} \right) \cdots \mathbf{T}_{n} \begin{bmatrix} \vec{t} \\ 1 \end{bmatrix} \right) \\
+ \cdots \\
+ \left(\mathbf{T}_{0} \cdots \mathbf{T}_{j} \cdots \left(\frac{\partial}{\partial \theta_{j}} \mathbf{T}_{n} \right) \begin{bmatrix} \vec{t} \\ 1 \end{bmatrix} \right) \\
+ \cdots \\
+ \left(\mathbf{T}_{0} \cdots \mathbf{T}_{j} \cdots \mathbf{T}_{n} \left(\frac{\partial}{\partial \theta_{j}} \begin{bmatrix} \vec{t} \\ 1 \end{bmatrix} \right) \right)$$

Only one term survive

$$\frac{\partial}{\partial \theta_j} \left(\vec{F}(\vec{\theta}) \begin{bmatrix} \vec{t} \\ 1 \end{bmatrix} \right) = \mathbf{T}_0 \cdots \mathbf{T}_{j-1} \frac{\partial \mathbf{T}_j}{\partial \theta_j} \mathbf{T}_{j+1} \cdots \mathbf{T}_n \begin{bmatrix} \vec{t} \\ 1 \end{bmatrix}$$

A little mathematical exercise The permutation is the "hat" operation in 2D

$$\frac{\partial}{\partial \theta_j} \begin{bmatrix} \cos \theta_j & -\sin \theta_j & l_{j,x} \\ \sin \theta_j & \cos \theta_j & l_{j,x} \\ 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} -\sin \theta_j & -\cos \theta_j & 0 \\ \cos \theta_j & -\sin \theta_j & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

$$\begin{bmatrix} -\sin\theta_{j} & -\cos\theta_{j} & 0 \\ \cos\theta_{j} & -\sin\theta_{j} & 0 \\ 0 & 0 & 0 \end{bmatrix} = \begin{bmatrix} 0 & -1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} \cos\theta_{j} & -\sin\theta_{j} & l_{j,x} \\ \sin\theta_{j} & \cos\theta_{j} & l_{j,y} \\ 0 & 0 & 1 \end{bmatrix}$$

Using the re-write we have

$$\frac{\partial}{\partial \theta_j} \left(\vec{F}(\vec{\theta}) \begin{bmatrix} \vec{t} \\ 1 \end{bmatrix} \right) = \mathbf{T}_0 \cdots \mathbf{T}_{j-1} \frac{\partial \mathbf{T}_j}{\partial \theta_j} \mathbf{T}_{j+1} \cdots \mathbf{T}_n \begin{bmatrix} \vec{t} \\ 1 \end{bmatrix}$$

$$\frac{\partial}{\partial \theta_j} \left(\vec{F}(\vec{\theta}) \begin{bmatrix} \vec{t} \\ 1 \end{bmatrix} \right) = \mathbf{T}_0 \cdots \mathbf{T}_{j-1} \begin{bmatrix} 0 & -1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \mathbf{T}_j \cdots \mathbf{T}_n \begin{bmatrix} \vec{t} \\ 1 \end{bmatrix}$$

This allows us to easily make a geometric re-interpretation

$$\frac{\partial}{\partial \theta_{j}} \left(\vec{F}(\vec{\theta}) \begin{bmatrix} \vec{t} \\ 1 \end{bmatrix} \right) = \underbrace{\mathbf{T}_{0} \cdots \mathbf{T}_{j-1}}_{\vec{F}(\theta_{0}, \dots, \theta_{j-1})} \underbrace{\begin{bmatrix} 0 & -1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}}_{\hat{\tau}} \underbrace{\mathbf{T}_{j} \cdots \mathbf{T}_{n} \begin{bmatrix} \vec{t} \\ 1 \end{bmatrix}}_{\left[\Delta\right]_{j}}$$

The hat of the difference between tool position and link i origin as seen from world coordinate frame...

Using the geometric re-interpretation allow for a simpler computation

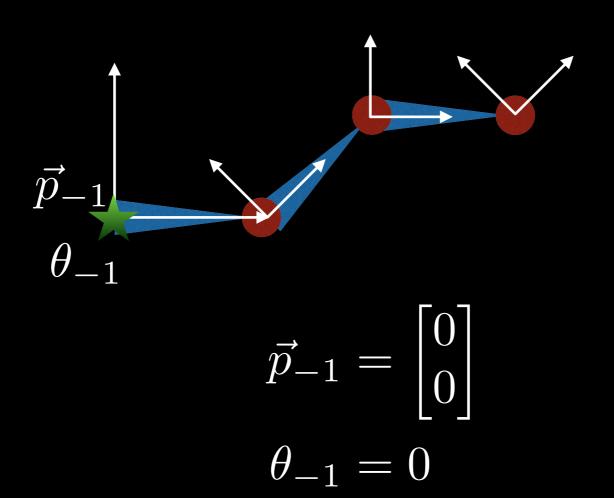
$$ec{\Delta} = ec{e} - ec{p}_j$$
 Origin of link j frame in WCS

$$\frac{\partial}{\partial \theta_j} \left(\vec{F}(\vec{\theta}) \begin{bmatrix} \vec{t} \\ 1 \end{bmatrix} \right) = \begin{bmatrix} -\Delta_y \\ \Delta_x \\ 0 \end{bmatrix}$$

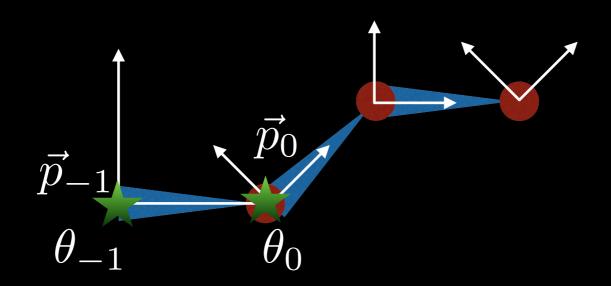
We need to compute origin of link frames to apply this

How do we compute link frame origins?

Let us use a forward sweep approach



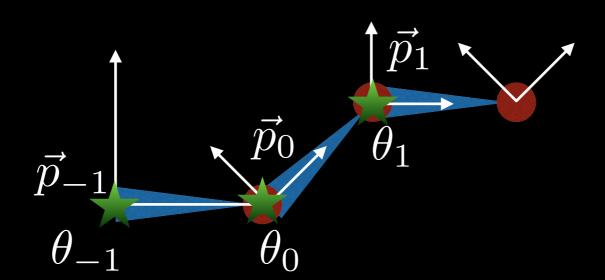
First link



$$\beta_0 = \theta_{-1}$$

$$\vec{p}_0 = \vec{p}_{-1} + \begin{bmatrix} \cos \beta_0 & -\sin \beta_0 \\ \sin \beta_0 & \cos \beta_0 \end{bmatrix} \vec{l}_0$$

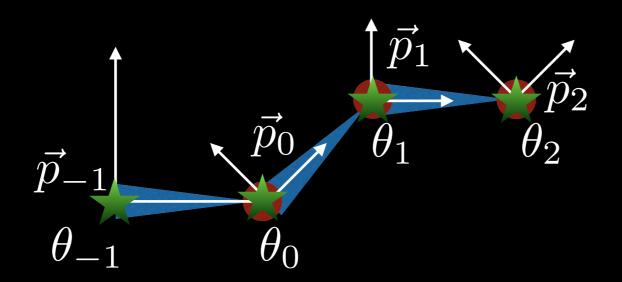
Second link



$$\beta_1 = \beta_0 + \theta_0$$

$$\vec{p}_1 = \vec{p}_0 + \begin{bmatrix} \cos \beta_1 & -\sin \beta_1 \\ \sin \beta_1 & \cos \beta_1 \end{bmatrix} \vec{l}_1$$

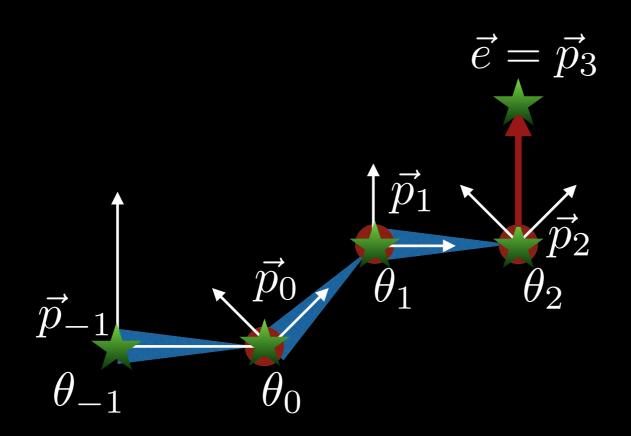
Third Link



$$\beta_2 = \beta_1 + \theta_1$$

$$\vec{p}_2 = \vec{p}_1 + \begin{bmatrix} \cos \beta_2 & -\sin \beta_2 \\ \sin \beta_2 & \cos \beta_2 \end{bmatrix} \vec{l}_2$$

End-Effector if non-zero tool position



$$\beta_3 = \beta_2 + \theta_2$$

$$\vec{e} = \vec{p}_3 = \vec{p}_2 + \begin{bmatrix} \cos \beta_3 & -\sin \beta_3 \\ \sin \beta_3 & \cos \beta_3 \end{bmatrix} \vec{t}$$

By construction we have found the incremental update rule for a forward sweep

$$\beta_i = \beta_{i-1} + \theta_{i-1}$$

$$\vec{p}_i = \vec{p}_{i-1} + \begin{bmatrix} \cos \beta_i & -\sin \beta_i \\ \sin \beta_i & \cos \beta_i \end{bmatrix} \vec{l}_i$$

The Final Algorithm

- Step 1 Compute end-effector vector and link frame origins
- Step 2 Fill in the Jacobian column-wise