Research on Google's Monet

Style Data (Since Android 13 Beta 3)

| STYLE | ATTRIBUTE | A1 | A2 | A3 | N1 | N2 |
|------------|-----------|-----------|----------------------|----------------------|-----------------------|----------------------|
| TONAL | Chroma | 36 | 16 | 24 | 4 | 8 |
| SPOT | Hue shift | | | +60° | | |
| SPRITZ | Chroma | 12 | 8 | 16 | 2 | 2 |
| SFRIIZ | Hue shift | | | +30° | | |
| VIBRANT | Chroma | 48 | 24 | 32 | 10 | 12 |
| VIBRANI | Hue shift | | [1] | [2] | | |
| EXPRESSIVE | Chroma | 40 | 24 | 32 | 15 | 12 |
| EAFRESSIVE | Hue shift | +240° | [3] | [4] | +15° | +15° |
| CONTENT | Chroma | ×1 | $\times \frac{1}{3}$ | $\times \frac{2}{3}$ | $\times \frac{1}{12}$ | $\times \frac{1}{6}$ |
| | Hue shift | | | | | |

| HUE ROTATION |
|---------------------|
|---------------------|

| [1] | (0,18) | (41,15) | (61,10) | (101,12) | (131,15) | (181,18) | (251,15) | (301,12) | (360,12) |
|-----|---------|----------|---------|----------|----------|----------|----------|-----------|-----------|
| [2] | (0,120) | (21,120) | (51,20) | (121,45) | (151,20) | (191,15) | (271,20) | (321,120) | (360,120) |
| [3] | (0,45) | (21,95) | (51,45) | (121,20) | (151,45) | (191,90) | (271,45) | (321,45) | (360,45) |
| [4] | (0,120) | (21,120) | (51,20) | (121,45) | (151,20) | (191,15) | (271,20) | (321,120) | (360,120) |

Hue baseline

Vibrant secondary hue rotation



Vibrant tertiary hue rotation



Expressive secondary hue rotation

| + | +9 | +95 | | +45 | +2 | 20 | +45 | +90 | +45 | +45 | |
|---|----|-----|----|-----|-----|-----|-----|-----|-----|-----|-----|
| 0 | 21 | | 51 | | 121 | 151 | 191 | | 271 | 321 | 360 |

Expressive tertiary hue rotation



Appendices

Appendix A: The Simplified CAM16 Model

Define

$$F = 3.8848145378003529E - 3$$

$$R = 29.482183021342301$$

$$d = 1.3173270022537199$$

$$M_{16} \equiv \begin{pmatrix} 0.401288 & 0.650173 & -0.051461 \\ -0.250268 & 1.204414 & 0.045854 \\ -0.002079 & 0.048952 & 0.953127 \end{pmatrix}$$

$$\mathbf{D} \equiv \begin{pmatrix} 1.0211774459482703 \\ 0.98630789117685210 \\ 0.93396137406301061 \end{pmatrix}$$

$$\Re \equiv \begin{pmatrix} 2 & 1 & \frac{1}{20} \\ 1 & -\frac{12}{11} & \frac{1}{11} \\ \frac{1}{9} & \frac{1}{9} & -\frac{2}{9} \end{pmatrix}$$

$$\mathcal{F}(v) \equiv \left\{ 400 \operatorname{sign}(v_i) \frac{(Fv_i)^{0.42}}{(Fv_i)^{0.42} + 27.13} \right\}$$

$$\mathcal{F}^{-1}(\boldsymbol{v}) \equiv \left\{ \frac{\operatorname{sign}(\boldsymbol{v}_i)}{F} \left(\frac{27.13|\boldsymbol{v}_i|}{400 - |\boldsymbol{v}_i|} \right)^{\frac{1}{0.42}} \right\}$$

$$\varepsilon(h) \equiv 1 - 0.0582 \cos h - 0.0258 \cos 2h$$
$$- 0.1347 \cos 3h + 0.0289 \cos 4h$$
$$- 0.1475 \sin h - 0.0308 \sin 2h$$
$$+ 0.0385 \sin 3h + 0.0096 \sin 4h$$

From CIE XYZ to CAM16

Input: CIE XYZ vector **X**

Output: CAM16 (JCh) vector M

$$\begin{pmatrix} A \\ a \\ h \end{pmatrix} = \Re \mathcal{F}(\text{Diag}(\mathbf{D})M_{16}\mathbf{X})$$

$$h' = \arctan\left(\frac{b}{a}\right)$$

$$\mathbf{M} = \begin{pmatrix} 100 \left(\frac{A}{R}\right)^d \\ \frac{1505}{R} \varepsilon(h') \sqrt{a^2 + b^2} \\ \frac{180^{\circ}}{\pi} h' \end{pmatrix}$$

From CAM16 to CIE XYZ

Input: CAM16 (JCh) vector $(J, C, h)^T$

Output: CIE XYZ vector X

$$h' = \frac{\pi}{180^{\circ}} h$$

$$\gamma = \frac{C}{1505 \, \varepsilon(h')}$$

$$\boldsymbol{X} = M_{16}^{-1} \operatorname{Diag}(\boldsymbol{D}^{\circ - 1}) \mathcal{F}^{-1} \left(\Re^{-1} R \begin{pmatrix} \left(\frac{J}{100} \right)^{\frac{1}{d}} \\ \gamma \cos h' \\ \gamma \sin h' \end{pmatrix} \right)$$

Notes on Appendix A

- 1. All the numbers were rounded to 17 significant digits (which was done in the last steps, but the intermediate values were arithmetically exact) except those defined in specifications.
- 2. The inverse of M_{16}

$$M_{16}^{-1} \equiv \begin{pmatrix} 1.8620678550872327 & -1.0112546305316844 & 0.14918677544445172 \\ 0.38752654323613716 & 0.62144744193147536 & -0.0089739851676125183 \\ -0.015841498849333855 & -0.034122938028515564 & 1.0499644368778494 \end{pmatrix}$$

3. The reference white W_{D65} used throughout the calculation

$$\boldsymbol{W}_{D65} \equiv \begin{pmatrix} 95.047055865428191 \\ 100 \\ 108.88287363958874 \end{pmatrix}$$

4. The Hadamard inverse (of a vector)

$$(\boldsymbol{v}^{\circ -1})_i = \frac{1}{\boldsymbol{v}_i}$$

Appendix B: Conversions between CIE XYZ and sRGB

$$M \equiv 100 \begin{pmatrix} 0.41245744558236514 & 0.35757586524551642 & 0.18043724782640035 \\ 0.21267337037840703 & 0.71515173049103283 & 0.072174899130560142 \\ 0.019333942761673366 & 0.11919195508183881 & 0.95030283855237520 \end{pmatrix}$$

$$M^{-1} \equiv \frac{1}{100} \begin{pmatrix} 3.2404462546477561 & -1.5371347618200895 & -0.49853019302273171 \\ -0.96926660624467829 & 1.8760119597883673 & 0.041556042214430008 \\ 0.055643503564352598 & -0.20402617973595953 & 1.0572265677226994 \end{pmatrix}$$

$$\mathcal{F}(v) \equiv \left\{ \begin{cases} \left(\frac{v_i + 0.055}{1.055}\right)^{2.4}, & v_i \ge \frac{11}{280} \\ \frac{v_i}{12.923210180787861}, & otherwise \end{cases} \right\}$$

$$\mathcal{F}^{-1}(\boldsymbol{v}) \equiv \begin{cases} \begin{cases} 1.055 \, \boldsymbol{v}_i^{\frac{1}{2.4}} - 0.055, & \boldsymbol{v}_i \geq 0.0030399346397784300 \\ 12.923210180787861 \, \boldsymbol{v}_i, & otherwise \end{cases}$$

From sRGB to CIE XYZ

From CIE XYZ to sRGB

Input: sRGB vector **R**

Output: CIE XYZ vector X

 $X = M\mathcal{F}(R)$

Input: CIE XYZ vector **X Output:** sRGB vector **R**

 $\mathbf{R} = \mathcal{F}^{-1}(M^{-1}\mathbf{X})$