

Gautebøye - Instrument Response

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Introduction

Here is presented the theoretical derivation and analysis of the analog instrument response of the digitizer. The digital filtering during AD conversion is briefly discussed, but its properties are well defined in the manual of the ADC[ads1282's ds].

1 Hydrophone decoupling

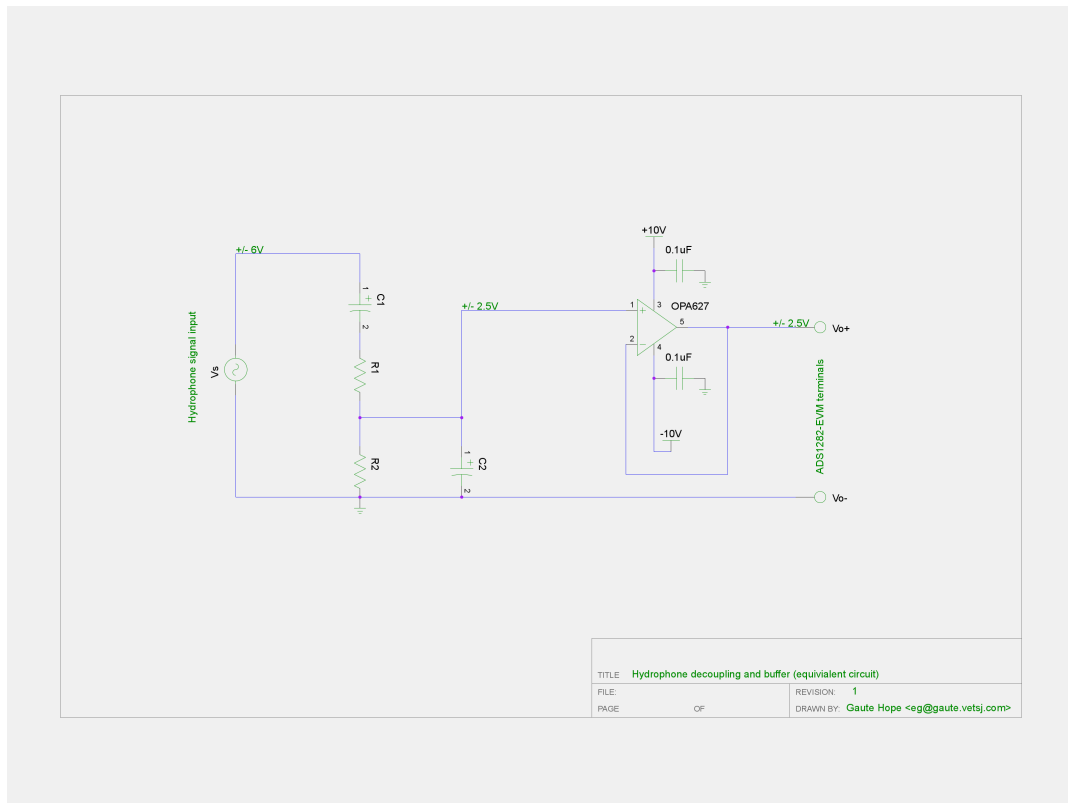


Figure 1: Hydrophone decoupling circuit

The figure above (1) shows an equivalent circuit of the deployed input decoupling to the hydrophone. decouples, and high-passes, the signal at frequency f_{HP} .

$$C_1 = 47\mu F$$

$$C_2 = 330pF$$

$$R_1 = 58.33k\Omega$$

$$R_2 = 41.67k\Omega$$

The circuit was based on the suggested decoupling in figure 2 seen below, it was designed to have the same properties, but also low-pass the signal at cutoff frequency f_{LP1} . The original design already

SUGGESTED PRE AMPLIFIER DECOUPLING
AND WIRING FOR AQ-11, AQ-12, AQ-17, AQ-18.

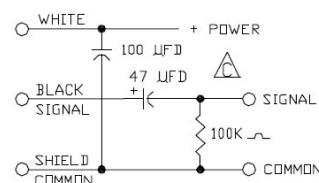


Figure 2: AQ-18 suggested decoupling and wiring T_- .
[aq-18'decoupling].

2 Derivation of transfer function

i_1 and i_2 signify the current loops passing through respectively left and right loop. Using Kirchoff's equation:

$$V_s = i_1(Z_{C_1} + Z_{R_1}) + (i_1 - i_2) \cdot Z_{R_2} \quad (1)$$

$$0 = (i_2 - i_1) \cdot Z_{R_2} + i_2 \cdot Z_{C_2} \quad (2)$$

V_s is the signal source, the hydrophone. See separate data sheet for hydrophone frequency response. V_o , output, is measured at the terminals T_+ and

$$V_o = i_2 \cdot Z_{C_2} \quad (3)$$

$$H(s) = \frac{V_o}{V_s}, s = i\omega \quad (4)$$

Solving for $H(s)$ gives:

$$H(s) = \frac{51951s}{(s + 1.2470 \times 10^5)(s + 0.2128)} \quad (5)$$

A bode plot of the transfer function (instrument response) is shown in figure 3 below.

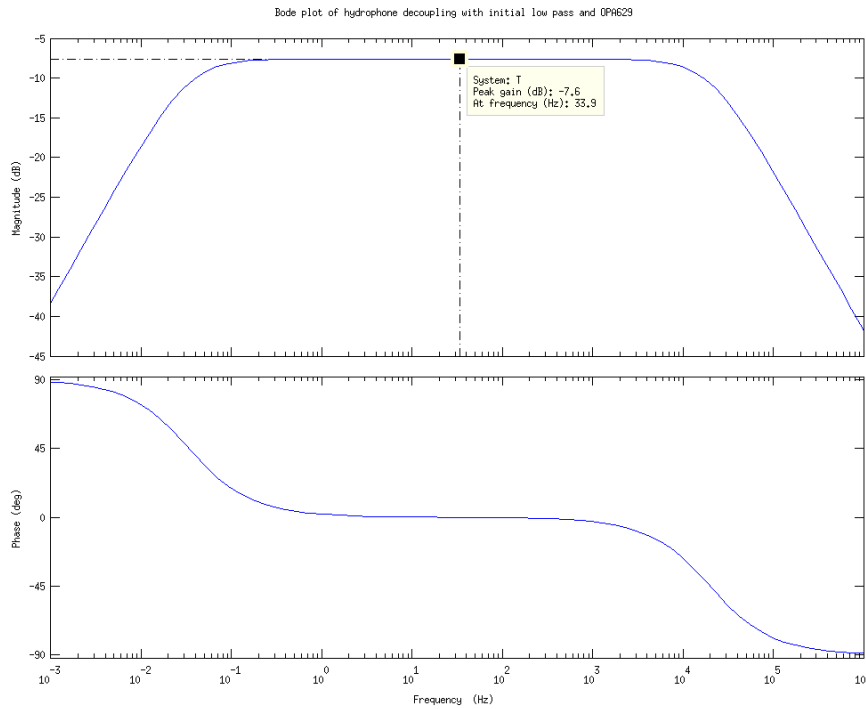


Figure 3: Bode plot of transfer function, showing peak response at 33.9 Hz.

Equation 5 can be solved by using the MATLAB script response.m (listing 1), the Bode plot in figure 3 was created with the same script.

2.1 Analysis

The initial frequency band of interest reaches from periods of 20 s (0.05 Hz) to approximately 100 Hz. The analog input part as well as the configuration of the analog-digital converter has been configured to as best and simple as possible to record the signal within this frequency band.

2.1.1 Decoupling and analog high pass filter

The transfer function is a bandpass filter with the suggested decoupling creating a high-pass filter with corner frequency at $f_{HP} = 0.0339$ Hz or a period of 29.4985 s.

2.1.2 Low pass filter and operational amplifier

To avoid aliasing due to the speed of the opamps (operational amplifiers) in the signal path; the

OPA627 (see [opa627'ds] and figure 1) acting as buffer with unity gain and then the OPA1632 [opa1632'ds] at the input terminals of the ADS1282EVM [ads1282evm'ds]. An additional low pass stage is added with a corner frequency of $f_{LP_1} = 17.189$ kHz. The speed of the opamp is in the order of Mhz so this corner frequency should be well within their capabilities.

OPA1632

The OPA1632 [opa1632'ds] is set up with a 1 nF capacitor in its feedback loop on the ADS1282EVM [ads1282evm'ds], this low passes the signal with a cut off frequency at $f_{LP_2} = 151.99$ kHz. Its gain bandwidth is specified to be 180 MHz, given that the gain is 1 and the load is large it should have a well behaved and near ideal response. The OPA1632-setups simplified transfer function is [fully'diff'opamps]:

$$H_{OPA1632}(s) = \frac{9.551 \times 10^5}{(s + 9.551 \times 10^5)} \quad (6)$$

OPA627

The OPA627 is used as a buffer with gain 1 to provide a high impedance input and low impedance output. It has a gain bandwidth product of 16 MHz at this gain [opa627'ds]. With the first low pass filter, f_{LP_1} , well below this it should be able to relay the signal without problems. The transfer function would simply be 1 for this step. It is important that the OPA627 has well mounted bypass capacitors to

avoid oscillations when configured for this low gain. An buffer designed for unity gain, like the OPA633 [opa633'ds] or BUF634 [buf634'ds] could prove a better choice.

OPA633

The OPA633 [opa633'ds] is a strong candidate for an drop-in replacement of the OPA627, it is specifically designed to be a buffer working at unity gain. The feedback loop is internally connected. But otherwise the same wiring scheme applies. Closely mounted and well chosen bypass capacitors are still needed on the power supplies to ensure stability. The input impedance of the ADS1282EVM should be sufficient for the gain to approach unity. The OPA633 has a gain bandwidth of 260 MHz, however it requires ± 15 mA current, which is about twice that of the OPA627.

2.1.3 Stability

The system, $H(s)$ from equation (5), is passive and has all its poles in the left half plane and is stable.

2.1.4 Analog-Digital Converter (ADC)

The ADS1282EVM equips its ADS1282 with a crystal with the recommended clock frequency of $f_{clk} = 4.096$ Mhz [ads1282evm'ds]. This results in a modulator output speed of $f_s = f_{clk}/4 = 1.024$ Mhz [ads1282'ds]. The Nyquist frequency is then:

$$f_{Nq} = 1.024 \times 10^6 / 2 = 512 \text{ kHz} \quad (7)$$

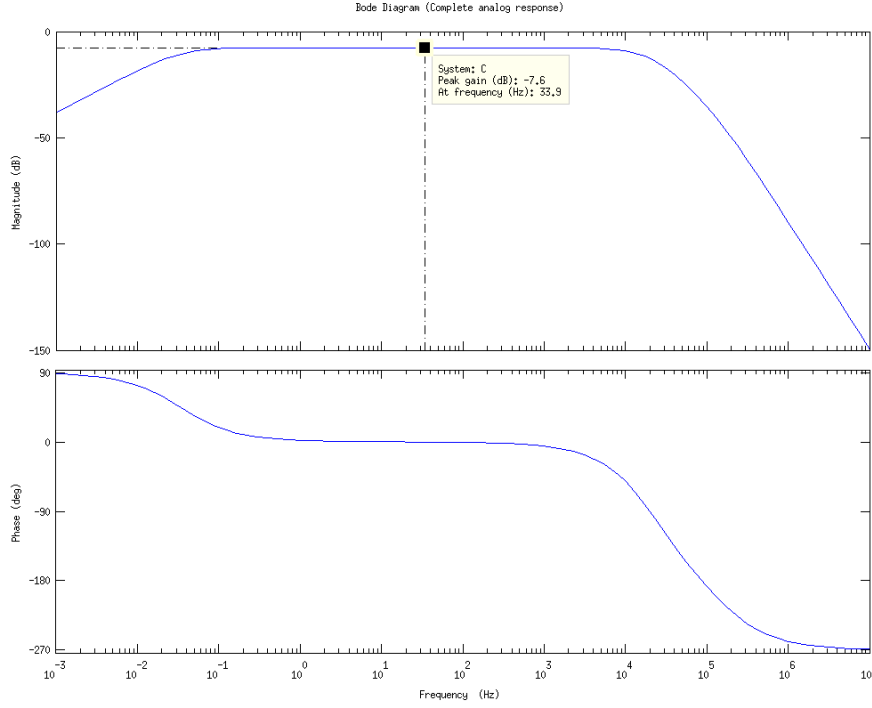


Figure 4: Frequency response of complete analog system, equation (9).

2.1.5 Anti-alias filter

The 10 nF capacitor used on the ADS1282EVM [ads1282evm.ds], results in a low-pass filter with an upper corner frequency of $f_{LP_3} = \frac{1}{2\pi \times 600 \times 10 \times 10^{-9}} = 26525.82 \text{ Hz}$ ¹. f_{LP_3} is thus well below f_{Nq} and any signal component above f_{LP_3} should be almost completely damped before it reaches f_{Nq} , resulting in no or very small aliasing effects.

This equation represents the upper low pass filter:

$$H_{UL}(s) = \frac{1 \div 600 \times 10 \times 10^{-9}}{(s + 1 \div 600 \times 10 \times 10^{-9})} = \frac{1.667 \times 10^5}{(s + 1.667 \times 10^5)} \quad (8)$$

The complete analog transfer function is then:

$$H_a = \frac{8.2698 \times 10^{15} s}{(s + 9.551 \times 10^5) \times (s + 1.667 \times 10^5)} \times \frac{1}{(s + 1.247 \times 10^5) \times (s + 0.2128)} \quad (9)$$

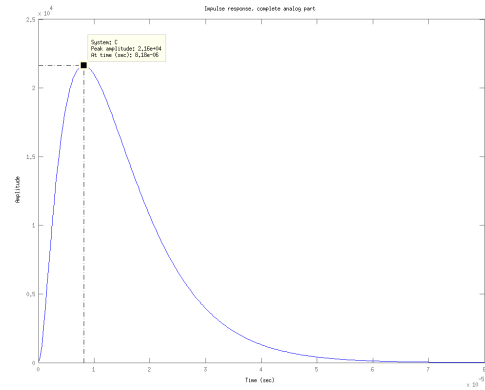
The frequency response is illustrated in figure (4).

¹Equation (3), p.15, [ads1282.ds]; ads1282.ds

2.1.6 Output of decoupling and buffer

The output is scaled by $-7.6 \text{ dB} = 0.4169 \frac{V}{V}$ which is to scale the input from $\pm 6V$ to $\pm 2.5V$, $0.4169 \approx 5/12 = 0.4167$, which is the input range of the ADS1282EVM ([ads1282evm.ds] and [ads1282.ds]) in bipolar mode. The slightly inaccurate scaling is due to the available (high precision) resistor values.

The impulse response of the system is plotted in figure 5:



interface, although it would come at an cost of resolution and would require adaption of the firmware of the buoy to handle the higher data rate.

High Pass Filter (HPF) The ADS1282 is configured to have an high pass corner frequency as close to 20 seconds as possible, the built in IIR HPF is set according to p. 22 in **ads1282's**

$$HPF[1 : 0] = 65,536 \times \left[1 - \sqrt{1 - 2 \frac{\cos(\omega_n) + \sin(\omega_n) - 1}{\cos(\omega_n)}} \right] \quad (11)$$

with:

$$\omega_n = 2\pi f_{HP}/f_{DATA} \quad (12)$$

An $f_{HP} = 1/20 = 0.05$ Hz gives an $\omega_n = 0,001256637$ normalized radians. And an $HPF[1 : 0] = 82.3550098$ truncated to $HPF[1 : 0] = 82_{10} = 52_{16}$.

4 Hydrophone characteristics

The hydrophone used, Benthos AQ-18, is specified to have an flat frequency response within ± 1.5 dB at the band 7 Hz - 10 kHz [**benthos'hydrophone'brochure**]. With a sensitivity of -171 dBv re 1 uPa at 20° C.

The frequency response for the AQ-18 is plotted in figure 10:

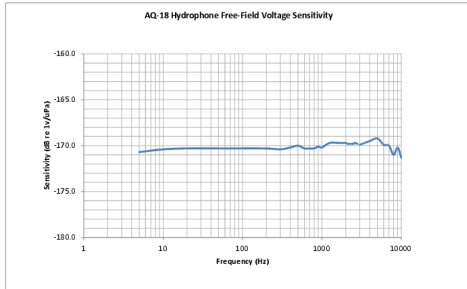


Figure 10: Frequency response plot of hydrophone, AQ-18 [**communication'benthos'aq18'freq**].

A simplified transfer function for the hydrophone in the flat band (7 Hz - 10 kHz):

$$H_{Hyd} = -171 \text{ dBv re 1 uPa} = 10^{8.55} \frac{\text{V}}{\text{uPa}} \quad (13)$$

5 Response of Digitizer

The AD converter, ADS1282, includes very sharp digital filters (section 3). The output is 32 bit integers, with a range of $[-2^{31}, 2^{31} - 1]$. The result is a near approximately flat frequency response from 0.05 Hz up to 125 Hz.

$$H_D = \frac{2^{32} \text{ counts}}{5 \text{ V}} \quad (14)$$

6 Response compared to output of a seismometer

The hydrophone measures pressure (uPa) while the seismometer measures displacement (nm), to be able to compare these some relation has to be figured out.

Considering that a force is exerted proportional to the pressure the hydrophone is measuring and that acceleration is proportional to force the simplest is to consider the hydrophone an accelerometer.

7 Attachments

7.1 response.m

Listing 1: response.m, MATLAB code for calculating instrument response

```
1 % Calculates instrument response
2 r1 = 58.33e3; % ohm
3 r2 = 41.67e3; % ohm
4
5 c1 = 47e-6; % farad
6 c2 = 330e-12; % farad
7
8 %% Transfer function of Hydrophone decoupling, including first high pass and low
9 % pass filters and OPA629.
10
11 syms s i1 i2 vs;
12 zc1 = 1/(s*c1);
13 zr1 = r1;
14 zc2 = 1/(s*c2);
15 zr2 = r2;
16
17 [i1, i2] = solve ('vs = i1*(zc1 + zr1) + (i1 - i2)*zr2', ...
18                 '0 = (i2 - i1)*zr2 + i2*zc2', 'i1', 'i2');
19 %i2 = solve ('vs = i2*(zc1 + zr1 + zr2)', 'i2');
20
21 vo = i2*sym('zc2');
22 H = vo/vs;
23 H = simplify(subs (H));
24
25 [n, d] = numden (H);
26
27 Tn = sym2poly(n);
28 Td = sym2poly(d);
29 T = tf(Tn, Td);
30
31
32 P = bodeoptions;
33 P.FreqUnits = 'Hz';
34 figure(1); clf('reset');
35 bodeplot (T, P);
36 title ('Bode plot of hydrophone decoupling with initial low pass and OPA629');
37
38 disp ('Hydrophone decoupling up to OPA629:');
39 zpk(T)
40 if isstable(T)
41     disp ('System is stable.');
```

```

64 bodeplot (C, P);
65 title ('Bode Diagram (Complete analog response)');
66
67 % Stable
68 if isstable(C)
69     disp ('System is stable. ');
70 else
71     disp ('System is unstable. ');
72 end
73 figure(5);
74 [p, z] = pzmap(C);
75 pzmap(C);
76 disp ('Poles: ')
77 disp(p)
78
79 % attenuation at nyquist
80 disp ('Attenuation at Nyquist: ');
81 a = abs(freqresp(C, 512e3*2*pi))
82 adb = 20*log10(a)

```