



NORTH SOUTH UNIVERSITY

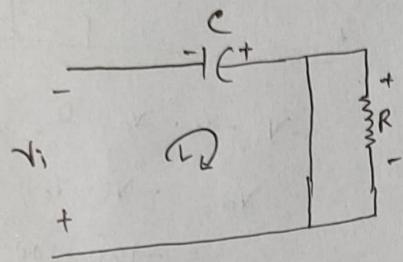
Department of Electrical and Computer Engineering

Assignment – 01

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Course No. : EEE 111
Course Title : Analog Electronics
Section : 11
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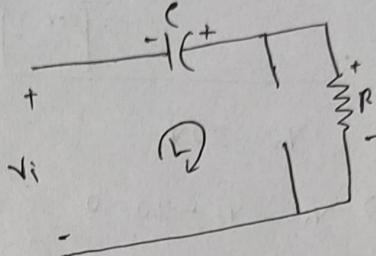
Ans. to the ques. no. 01

a)



$$kV_L, \quad -Vi + Vc = 0$$

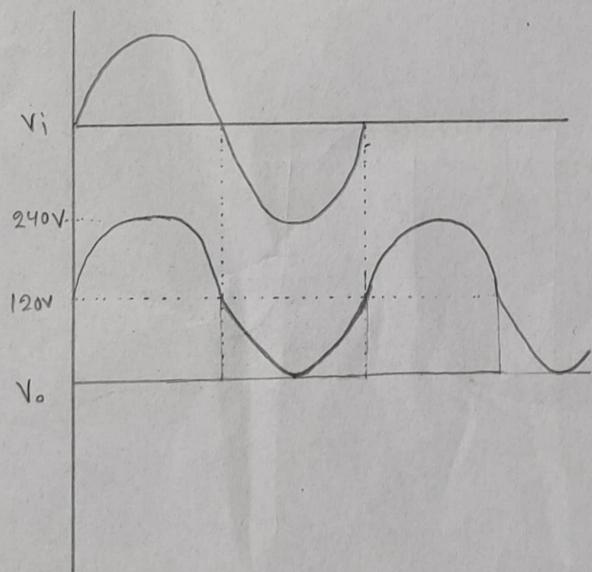
$$\therefore Vc = Vi = 120V$$



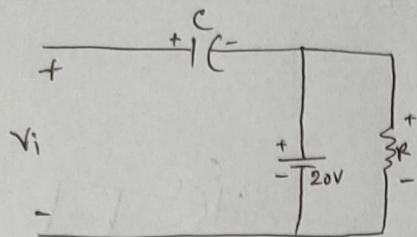
$$kV_L, \quad Vi + Vc - Vo = 0$$

$$Vo = Vi + Vc$$

$$= 240V$$



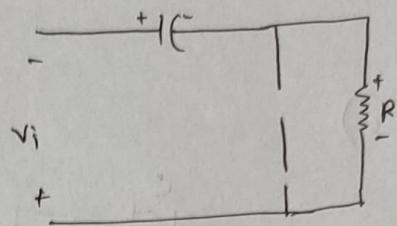
b)



$$V_o = 20V$$

$$\Rightarrow V_i - V_c - 20 = 0$$

$$\therefore V_c = 120 - 20 = 100V$$

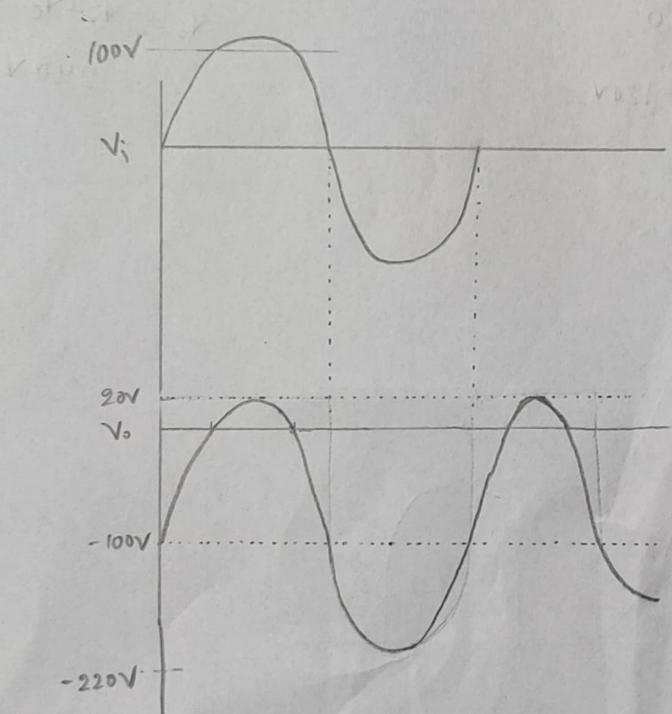


$$-V_i - V_c - V_o = 0$$

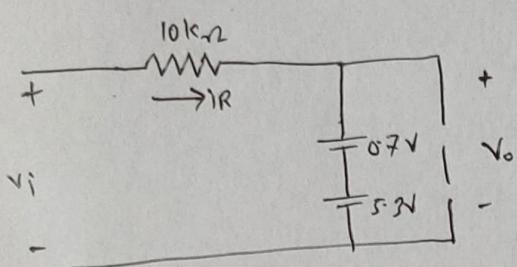
$$V_o = -V_i - V_c$$

$$= -120 - 100$$

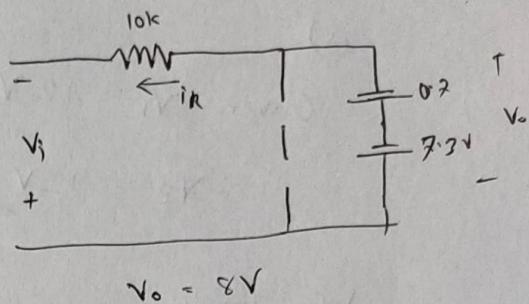
$$= -220V$$



Ans. to the ques. no. 02

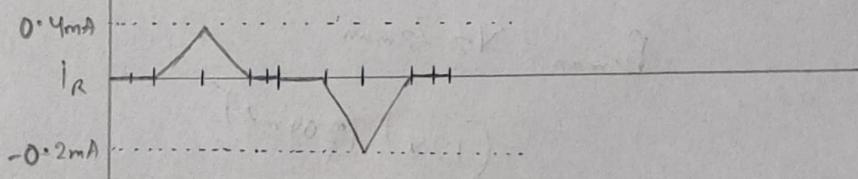
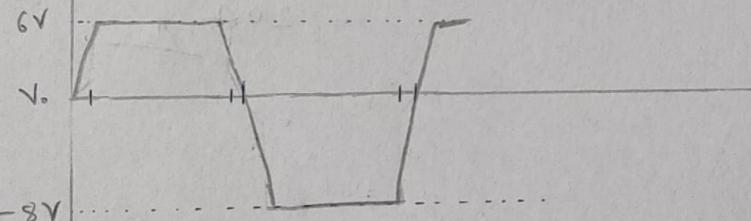
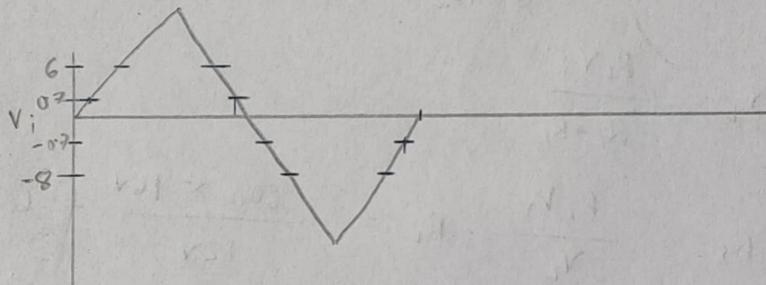


$$\begin{aligned} V_o &= (5.3 + 0.7)V \\ &= 6V \end{aligned}$$



$$V_o = 8V$$

~~ER~~



Ans. to the ques. no. 03

a)

$$\text{Given } V_L = 12 \text{ V}$$

$$\therefore V_2 = 12 \text{ V} \quad A$$

We know,

$$R_L = \frac{V_L}{I_L}$$

$$= \frac{12 \text{ V}}{200 \text{ mA}}$$

$$= 60 \Omega$$

Where, $I_L = 200 \text{ mA}$

$$\text{Again, } V_L = \frac{R_L V_i}{R_L + R_s}$$

$$\therefore R_s = \frac{R_L V_i}{V_L} - R_L = \frac{60 \Omega \times 16 \text{ V}}{12 \text{ V}} - 60 \Omega$$

$$= 20 \Omega \quad A$$

b)

We know,

$$P_{Z_{\max}} = V_2 I_{Z_{\max}}$$

$$= (12 \text{ V}) (200 \text{ mA})$$

$$= 2.4 \text{ W}$$

A

Ans. to the ques. no. 04

a)

Given,

$$\alpha_{dc} = 0.980$$

We know,

$$\beta_{dc} = \frac{\alpha_{dc}}{1 - \alpha_{dc}} = \frac{0.980}{1 - 0.980} = 49$$

Therefore, $\beta_{dc} = 49$.

b)

Given,

$$\beta_{dc} = 120$$

We know,

$$\alpha_{dc} = \frac{\beta_{dc}}{1 + \beta_{dc}} = \frac{120}{1 + 120} = 0.9917$$

Therefore, $\alpha = 0.9917$.

c)

Given

$$\beta_{dc} = 120$$

$$I_c = 2.0 \text{ mA}$$

We know,

$$I_c = \beta_{dc} \times I_B$$

$$\therefore I_B = \frac{I_c}{\beta_{dc}} = \frac{2 \text{ mA}}{120}$$

$$= 16.67 \text{ mA}$$

Again,

$$I_E = I_c + I_B$$

$$= 2 \text{ mA} + 16.67 \text{ mA}$$

$$= 2.0167 \text{ mA}$$

Therefore,

$$I_E = 2.0167 \text{ mA}$$

$$I_B = 16.67 \text{ mA}$$

Ans. to the ques. no. 05

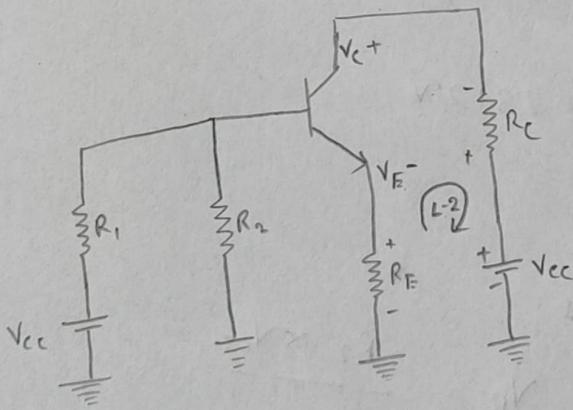
a)

From the given circuit, we can say that,

$$\begin{aligned} V_C &= V_{CC} - I_C R_C \\ \therefore I_C &= \frac{V_{CC} - V_C}{R_C} \\ &= \frac{(18 - 12) \text{ V}}{4.7 \text{ k}\Omega} \\ &= 1.2766 \text{ mA} \end{aligned}$$

Where,
 $V_C = 12 \text{ V}$
 $V_{CC} = 18 \text{ V}$
 $R_C = 4.7 \text{ k}\Omega$

b)



Applying KVL in Loop-2,

$$\begin{aligned} V_{CC} - I_C R_C - V_{CE} - I_E R_E &= 0 \\ \Rightarrow V_{CC} - I_C R_C - I_C R_E &= V_{CE} = V_C - V_E \quad [\because I_C \approx I_E] \\ \Rightarrow V_C - V_E &= V_C - V_{CC} + I_C R_C + I_C R_E \end{aligned}$$

$$\therefore V_E = 12V - 18V + 6V + 1.2766mA \times 1.2k\Omega \\ = 1.5319V$$

Therefore, $V_E = 1.5319V$

c)

We know,

$$V_{BE} = V_B - V_E$$

$$\therefore V_B = V_{BE} + V_E \\ = 0.7V + 1.5319V \\ = 2.2319V$$

Therefore,

$$V_B = 2.2319V$$

d)

We know that,

$$V_B = \frac{R_2 \times V_{CC}}{R_1 + R_2}$$

$$\therefore R_1 = \frac{R_2 \times V_{CC}}{V_B} - R_2$$

$$= \frac{5.6k\Omega \times 18V}{2.2319V} - 5.6k\Omega$$

$$= 39.56k\Omega \quad \underline{\text{Ans}}$$

Ans. to the ques. no. 06

a)

We know,

$$I_B = \frac{V_{CC} - V_{BE}}{R_B + \beta(R_E + R_E)}$$

$$= \frac{16V - 0.7V}{270\text{k}\Omega + 120(7.6\text{k}\Omega + 1.2\text{k}\Omega)}$$

$$= 18.0851 \text{ mA}$$

Where,

$$V_{CC} = 16V$$

$$V_{BE} = 0.7V$$

$$R_B = 270 \text{ k}\Omega$$

$$R_C = 7.6 \text{ k}\Omega$$

$$R_E = 1.2 \text{ k}\Omega$$

$$\beta = 120$$

Therefore,

$$I_B = 18.0851 \text{ mA}$$

b)

We know,

$$I_C = \beta I_B$$

$$= 120 \times 18.0851 \text{ mA}$$

$$= 2.1702 \text{ mA}$$

Therefore, $I_C = 2.1702 \text{ mA}$.

c)

According to circuit, we can write that,

$$V_c = V_{cc} - V_{Re}$$

$$= V_{cc} - I_{Re} \times R_e$$

$$= V_{cc} - (I_B + I_c) \times R_e \quad [KCL]$$

$$= 16V - (2.1702mA + 18.0851mA) \times 3.6k\Omega$$

$$= 8.1222V$$

Therefore,

$$V_c = 8.1222V.$$

Ans. to the que. no. 07

a)

We know,

$$R_e = \frac{26mV}{I_F}$$

Now,

$$V_B = \frac{R_2 \times V_{CC}}{R_1 + R_2} = \frac{4.7 \text{ k}\Omega \times 16V}{39 \text{ k}\Omega + 4.7 \text{ k}\Omega}$$

$$= 1.72V$$

Again,

$$V_{BE} = V_B - V_E$$

$$\therefore V_E = V_B - V_{BE}$$

$$= 1.72V - 0.7V$$

$$= 1.02V$$

$$\therefore I_E = \frac{V_E}{R_E} = \frac{1.02V}{1.2 \text{ k}\Omega}$$

$$= 0.85 \text{ mA}$$

Therefore

$$r_{e\text{op}} = \frac{26 \text{ mV}}{0.85 \text{ mA}}$$

$$= 30.59 \text{ }\mu\Omega$$

b)

We know,

$$Z_i = R_1 \parallel R_2 \parallel r_{e\text{op}}$$

$$= \left(\frac{1}{39 \text{ k}\Omega} + \frac{1}{4.7 \text{ k}\Omega} + \frac{1}{100 \times 30.59 \mu\Omega} \right)^{-1}$$

$$= 1.77 \text{ k}\Omega$$

From the circuit,

$$Z_o = R_c \parallel r_o$$

Since, $R_c \ll r_o$

we can write, $Z_o \approx R_c = 3.9 \text{ k}\Omega$

Therefore,

$$Z_i = 1.22 \text{ k}\Omega$$

$$Z_o = 3.9 \text{ k}\Omega$$

c)

We know,

$$A_v = - \frac{Z_o}{r_o} = - \frac{3.9 \text{ k}\Omega}{30.59 \text{ }\Omega}$$

$$= -127.49$$

Therefore

$$A_v = -127.49$$

d)

As Z_i not dependent on π_0 ,

$$\therefore Z_i = 1.77 \text{ kN}$$

Now,

$$\begin{aligned} Z_0 &= R_e \parallel \pi_0 && \left| \text{where, } \pi_0 = 25 \text{ kN} \right. \\ &= \left(\frac{1}{R_e} + \frac{1}{\pi_0} \right)^{-1} \\ &= 3.37 \text{ kN} \end{aligned}$$

$$\text{Then, } A_r = - \frac{Z_0}{R_e} = - \frac{3.37 \text{ kN}}{30.59 \text{ N}} \\ = -110.29$$

Therefore,

$$Z_i = 1.77 \text{ kN}$$

$$Z_0 = 3.37 \text{ kN}$$

$$A_r = -110.29$$

Ans. to the quer no. 18

a)

We know,

$$\begin{aligned} I_E &= \frac{V_{EE} - V_{BE}}{R_E} \\ &= \frac{6V - 0.7V}{6.8k\Omega} \\ &= 0.779 \text{ mA} \end{aligned}$$

Therefore,

$$\begin{aligned} r_{le} &= \frac{0.26 \text{ mV}}{0.779 \text{ mA}} \\ &= 0.3338 \Omega \end{aligned}$$

b)

We know,

$$\begin{aligned} Z_i &= R_E \parallel r_{le} \\ &= \left(\frac{1}{6.8k\Omega} + \frac{1}{33.38\Omega} \right)^{-1} \\ &= 33.22 \Omega \end{aligned}$$

And, $Z_o = R_C = 4.7k\Omega$

Ans

c)

We know,

$$A_v = \frac{\alpha R_c}{R_e}$$

$$= \frac{(0.998)(4.7\text{ k}\Omega)}{33.38 \Omega}$$

$$= 140.52$$

Therefore,

$$A_v = 140.52$$

Ans. to the que. no. 10

a)

We know,

$$V_B = \frac{R_2 V_{CC}}{R_1 + R_2} = \frac{(8.2\text{ k}\Omega)(20\text{ V})}{(8.2\text{ k}\Omega + 56\text{ k}\Omega)}$$

$$= 2.55 \text{ V}$$

Again,

$$I_E = \frac{V_E}{R_E} = \frac{V_B - V_{BE}}{R_E} = \frac{2.55 \text{ V} - 0.7 \text{ V}}{2 \text{ k}\Omega}$$

$$= 0.925 \text{ mA}$$

Therefore,

$$I_B = \frac{I_E}{\beta + 1} = \frac{0.925 \text{ mA}}{200 + 1}$$

$$= 4.60 \text{ mA}$$

A

And $I_C = \beta I_B$

$$= 200 \times 4.60 \text{ mA}$$

$$= 0.92 \text{ mA}$$

A

b)

We know,

$$\pi_e = \frac{26 \text{ mV}}{Z_E} = \frac{26 \text{ mA}}{0.925 \text{ mA}}$$

$$= 28.11 \text{ n}$$

A

c)

We know,

$$Z_i = R_B \parallel Z_b$$

And,

$$Z_b = \beta \pi_e + (\beta + 1) R_E$$

$$= (200 \times 28.11 \text{ n}) + (200 + 1) 2 \text{ k}\Omega$$

$$= 407.62 \text{ k}\Omega$$

Therefore

$$Z_i = \left(\frac{1}{R_1 + R_2} \parallel Z_b \right)$$

$$= \left(\frac{1}{56\text{k}\Omega} + \frac{1}{8.2\text{k}\Omega} + \frac{1}{407.62\text{k}\Omega} \right)^{-1}$$

$$= 7.029 \text{ k}\Omega \quad \underline{\Delta}$$

And,

$$Z_o = R_e \parallel r_e$$

$$= \left(\frac{1}{2\text{k}\Omega} + \frac{1}{28.11\text{m}} \right)^{-1}$$

$$= 27.72 \text{ m} \quad \underline{\Delta}$$

d)

We know,

$$A_v = \frac{R_E}{R_E + R_e}$$

$$= \frac{2\text{k}\Omega}{2\text{k}\Omega + 28.11\text{m}}$$

$$= 0.986$$

Δ

Ans. to the ques. no. 09

a)

I_G is effectively 0 A in a JFET due to its unique operation. The gate-source junction is reverse-biased, creating a depletion region that prevents current flow. As the gate-source voltage is adjusted, the width of this region changes. When the voltage surpasses a certain threshold, the depletion region blocks current entirely, making I_G practically 0 A.

b)

The input impedance of a JFET is extremely high due to its reverse-bias gate-source junction. This reverse bias creates a depletion region around the gate, effectively narrowing the channel between the source and drain. As a result, it becomes very difficult for minority carriers to flow through the channel, resulting in a negligible gate current and a very high input impedance.

c)

The term "field effect transistor" (FET) is appropriate for this three-terminal device because the current flowing between its terminals is controlled by an electric field generated by the voltage applied to the gate terminal. This electric field, rather than an ~~extra~~ external current, modulates the conductivity of the channel between the source and drain terminals, hence the name "field effect."
