

Determine the junction resistance/Voltage bias ratio and find that the resistance of the junctions can increase a few % over their room temperature values when cooled to dilution temperatures. As such, if you're really gungho about having a 50  $\Omega$  junction, you'll do best to start with something like 48 or 49. Since the goal for these devices is an accurate assessment of the noise temperature, getting close to 50  $\Omega$  is important, but how close is close? If your source impedance (junction impedance) is 41  $\Omega$ , then the fraction of noise power that can propagate out is

$$\eta = 1 - |\Gamma|^2 = 0.99$$

so you'll only end up with a 1

This is the number that you'll use for your  $t$ . It's important to get this right since the noise temperatures that you will infer will scale with your measurement of the junction voltage through  $k_B$ . Figure 0.1: Bias resistor configuration for determining the ratio between the applied bias  $V_B$  and the junction bias  $V_J$ . If you use a current source in place of  $V_B$  you can determine the resistance and convince yourself that your reflection loss will probably be good enough.

How do you set the bias resistance values?

If you're after noise temperature and your SNTJ is cold enough to be well into the quantum regime, then you'll be happy if you have something like  $10hf/e$ , that is, something that well exceeds the corners on the quantum noise at bottom. If you're at 6GHz, then this turns out to be something like 25V. Since I like to have my bias sources scaled so that they swing about 1V for the range of interest, this means a divider ratio of something like 1:40,000. If you don't use any room temperature dividers, you can use a single bias resistor value of 2 M $\Omega$ . I usually end up using a divider at room temperature and using something like 100k so that I can measure temperature at higher temperatures as a sanity check.

Although you can, in principle, demodulate the output of your amp chain using a diode rectifier, you'll have to play games setting the filtering of the room temperature mixer output and you'll have to think about one more thing. I think that it's far easier to demodulate the output of the SNTJ at a given frequency by using a standard spectrum analyzer in a triggered, zero span acquisition at the frequency that you care to measure. I use the Agilent E4407B for this purpose. Make sure to set it to sample each bin and not pull the max/min at each point. The E4407B also lets you set the display to linear Watts. Open up the resolution bandwidth as wide as you need to, usually less than 10 MHz on a typical instrument. This will yield the

noise curve integrated over this bandwidth, so if you're interested in getting the noise over a narrower bandwidth then you can crank it down, but be prepared to wait longer. Anyhow, with the trace averaging in the instrument you can accumulate averaged shot noise mustache traces quickly and easily by syncing a triangle sweep on the bias. Output the data however you like and perform your  $t$  using the scaling ratio  $V_J/V_B$  that you found with your 3 probe measurement above. Since these automated spectrum analyzers do a lot under the hood, you have to make sure that however it configures its own internal attenuators to level its incoming signals, that its noise floor is dominated by your amplification chain. Set up your bias sweep so that you can see a good noise mustache, sweeping out something like  $10 k_B T$  and setting the power scale on your analyzer so that the max noise fills out the y-scale. If you shut off your cryogenic HEMT, then the noise power shown on the analyzer should be very close to zero. This is an indication that the cryogenic HEMT is dominating your system noise. If it doesn't reach zero, then you have other stuff later in the chain that is contributing significant noise and you have some troubleshooting to do.

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