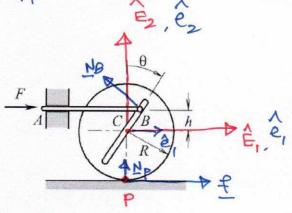
ESO 209 - Tutorial 11

(2) Horizontal force F causes the actuating rod to move to the left at the constant speed v. This rod is connected to the wheel by pin B, which may slide F through the groove. The mass of the wheel is m, the radius of gyration is κ, and μ_s and μ_k are the coefficients of static and kinetic friction, respectively, between the wheel and the ground. Friction between the pin and the groove is negligible, as is the mass of the rod. Consider the instant when θ = 30°. Derive expressions for the acceleration of center C, the angular acceleration of the gear, and the force F under the assumption that (a) the wheel rolls without slipping. (b) there is slippage by



that (a) the wheel rolls without slipping, (b) there is slippage between the wheel and the ground.

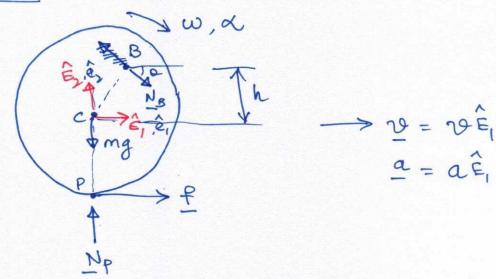
Choosing Observer CS {Fo, C, Êi} } Wheel BFCS {F, C, êi}

Assuming reaction NB at pin B, friction force of and reaction at point P (contact between whell & ground) as NP,

Considering only the \vec{E}_i direction components, $\vec{E}_i = \vec{E}_i = \vec{E}_i$ (Since mans is negligible)

 $F - N_B \cos \alpha = 0$ $\Rightarrow \left[N_B = F/\cos \alpha \right] - 0$

FBD of wheel



LMB & wheel

EF = mag

Note: ê, WE, and ê, WE, are aligned at instant of interest.

LHS = $\Xi F \equiv N_B \cos \alpha \hat{E}_1 - N_B \sin \alpha \hat{E}_2 - m_B \hat{E}_2 + N_P \hat{E}_2 + \xi \hat{E}_1$ RHS = $m \alpha^G \equiv m i \alpha \hat{E}_1$ Equating the components $\xi \hat{E}_1 \& \hat{E}_2$

Fi: NBCOSO+P= mie Using EgnD, we get

Ez: - NBSina - mg + Np = 0

again Rubstituting for NB Room equal.

- Ftand -mg + Np = 0

$$\Rightarrow [N_p = Ftand + mg] - (3)$$

AMB of wheel.

Recognizing that this is a planar 2-D problem, we can write the E3 components of AMB egn as.

EMa = Ig. XE/GO

EMq in Ê3 = FR - NB: h
cosa

 $\begin{bmatrix} \exists q \end{bmatrix}_{E} = \begin{bmatrix} mk^2 & 0 & 0 \\ 0 & mk^2 & 0 \\ 0 & 0 & 2mk^2 \end{bmatrix}$

The unknowns are f, 20, x and we have

equations (2) & (4)

The missing equation is that of Kinematics that of

the wheel solling without

slipping, which by now can be easily coniten as

Note: Eqn (3) is not very helpful here. However, Eqn. (3) helps in determining the value of F at which the wheel begins to ship.

(2D-planax problem: att rector)

Eliminating
$$f$$
 from Equs (2) & (4), we get
 $(mre-F)R - \frac{Fh}{cos^2a} = -mk^2x$

$$(mRx-F)R-\frac{Fh}{\cos^2 \theta}=-mk^2x$$

$$\frac{1}{2} mR^2 x - FR - \frac{Fh}{\cos^2 \theta} = -mk^2 x$$

$$\Rightarrow m(R^2+k^2)\alpha = F(R+\frac{h}{\cos^2\alpha})$$

$$\Rightarrow \sqrt{x} = \frac{F}{m} \frac{(R + h/co²o)}{(R² + K²)} - 6$$

From (5) &(6), we get
$$\frac{1}{a^{G}} = \frac{1}{2^{G}} = \frac{FR(R + h/\cos^{2}a)}{(R^{2} + K^{2})} - \frac{1}{2^{G}}$$
The condition the coheel starts slipping the

Case 2 when the wheel starts slipping, the Kinematic relation is no longer applicable.

and
$$f = -\mu_K N_P$$

Using Equation (3)

 $f = -\mu_K (Ftand + mg)$

Using the AMB eqr(4), we get
$$fR - \frac{Fh}{\cos^2 a} = -mk^2 \alpha$$

$$\left[-Mk \left(F \tan \alpha + mg\right)\right]R - \frac{Fh}{\cos^2 a} = -mk^2 \alpha$$

$$\Rightarrow \int x = \frac{1}{mk^2} \left[\mu_{K} FR \tanh + \mu_{E} mgR + \frac{Fh}{\cos^2 \theta} \right] - 6$$

(8) & (9) are the expressions for acceleration of centre C & angular acceleration & (in the negative \hat{E}_3 direction) for the wheel slipping condition.