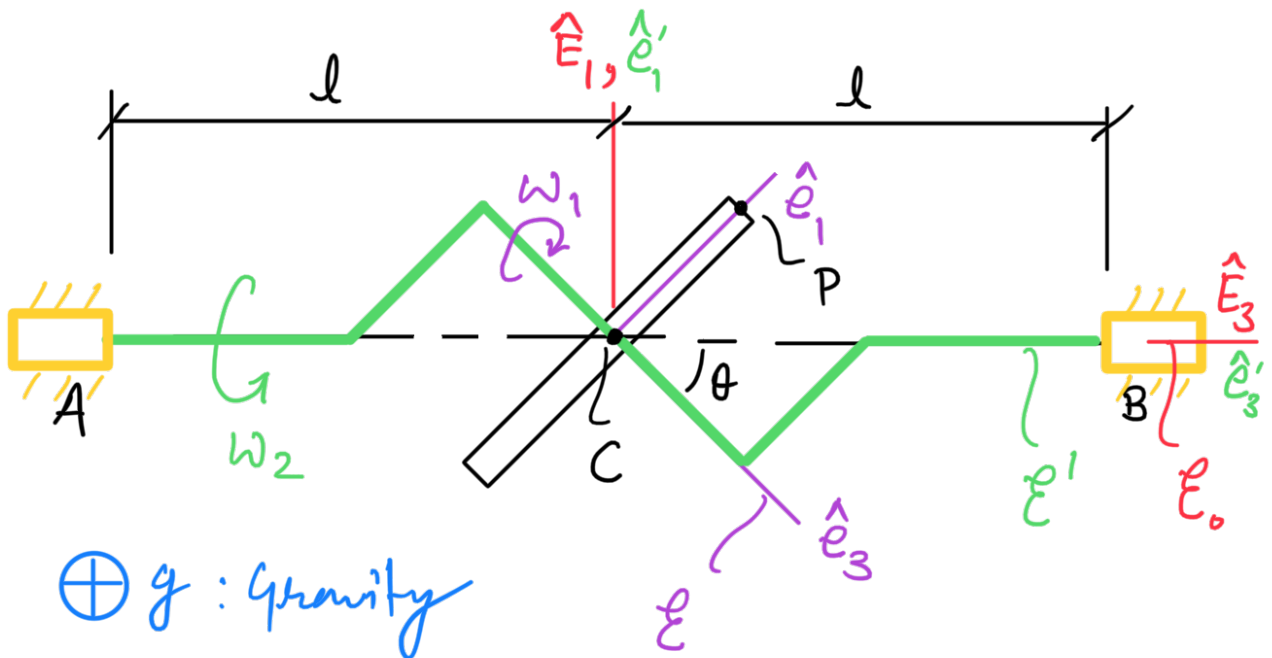


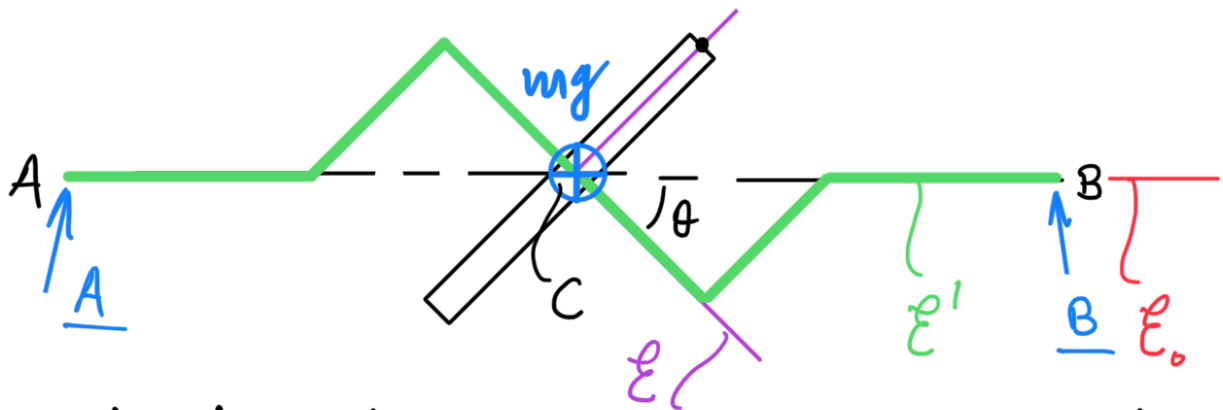
TOP VIEW



There are three frames:

- (i) $(\mathcal{E}; C; \hat{e}_i)$: Fixed to the disc (P dirⁿ)
- (ii) $(\mathcal{E}'; C; \hat{e}'_i)$: Fixed to the bent shaft
- (iii) $(\mathcal{E}_0; C; \hat{E}_i)$: Ground fixed

Step-1 Draw FBD



At this time we are assuming that the bearings at A and B are offering resistance in all three directions. Therefore, we have taken A and B in arbitrary directions.

Step-2 Applying balance laws

(i) LMB : $\Sigma \underline{F}_{ext} = m \underline{a}_c$

$$\Rightarrow \underline{A} + \underline{B} - mg \hat{E}_2 = \underline{0} \quad \text{--- (1)} \quad \left| \begin{array}{l} \text{Aside} \\ C \text{ is fixed} \\ \therefore \underline{a}_c = \underline{0}. \end{array} \right.$$

$$\text{OR } (A_1 + B_1) \hat{E}_1 + (A_2 + B_2) \hat{E}_2 + (A_3 + B_3) \hat{E}_3 = mg \hat{E}_2$$

$$\Rightarrow A_1 + B_1 = 0 \quad \text{--- (2a)}$$

$$A_2 + B_2 = mg \quad \text{—————} (2b)$$

$$A_3 + B_3 = 0 \quad \text{—————} (2c)$$

(ii) AMB : About pt. C. (fixed)

Note : shaft's mass is ignored.

$$\begin{aligned} \underline{M}/_C = \underline{I}_{cm} \cdot \underline{\alpha}_{E/E_0} + \underline{\omega}_{E/E_0} \times \underline{I}_{cm} \cdot \underline{\omega}_{E/E_0} \\ + \underline{r}_{C/G} \times m \underline{\underline{a}}_G \end{aligned}$$

$$\therefore \underline{M}/_C = \underline{I}_{cm} \cdot \underline{\alpha}_{E/E_0} + \underline{\omega}_{E/E_0} \times \underline{I}_{cm} \cdot \underline{\omega}_{E/E_0}$$

$$\begin{aligned} \underline{r}_{A/C} \times \underline{A} + \underline{r}_{B/C} \times \underline{B} = \underline{I}_{cm} \cdot \underline{\alpha}_{E/E_0} + \\ \underline{\omega}_{E/E_0} \times \underline{I}_{cm} \cdot \underline{\omega}_{E/E_0} \end{aligned} \quad \text{—————} (3)$$

Step - 3 Kinematics

$$\underline{r}_{A/C} = -l \hat{E}_3 ; \underline{r}_{B/C} = l \hat{E}_3 \quad \text{————} (4)$$

CP = R (radius of the disc)

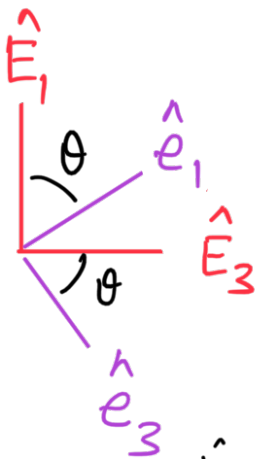
$$\underline{\omega}_{E/E_1} = -\omega_1 \hat{e}_3 ; \underline{\omega}_{E'/E_0} = \omega_2 \hat{E}_3$$

$$\therefore \underline{\omega}_{\mathcal{E}/\mathcal{E}_0} = -\omega_1 \hat{e}_3 + \omega_2 \hat{E}_3 \quad \text{————— (5)}$$

Note: ω_1 and ω_2 are constants.

Computation of $\underline{\omega}_{\mathcal{E}/\mathcal{E}_0}$:

$$\begin{aligned} \underline{\omega}_{\mathcal{E}/\mathcal{E}_0} &= \frac{d}{dt} (\underline{\omega}_{\mathcal{E}/\mathcal{E}_0}) \\ &= \frac{d}{dt} (-\omega_1 \hat{e}_3 + \omega_2 \hat{E}_3) \\ &= -\omega_1 \frac{d\hat{e}_3}{dt} + \underline{0} \quad \left| \begin{array}{l} \text{Aside} \\ \omega_2: \text{const.} \\ \hat{E}_3: \text{fixed} \end{array} \right. \\ &= -\omega_1 (\underline{\omega}_{\mathcal{E}/\mathcal{E}_0} \times \hat{e}_3) \\ &= -\omega_1 (-\omega_1 \hat{e}_3 + \omega_2 \hat{E}_3) \times \hat{e}_3 \\ &= -\omega_1 \omega_2 \hat{E}_3 \times \hat{e}_3 \\ &\quad \underline{\text{Aside}} \end{aligned}$$



$$\left. \begin{aligned} \hat{E}_3 &= \hat{e}_1 \sin \theta + \hat{e}_2 \cos \theta \\ \hat{E}_1 &= \hat{e}_1 \cos \theta - \hat{e}_2 \sin \theta \end{aligned} \right\} \text{--- (6)}$$

$$\begin{aligned} \therefore \underline{\omega}_{\mathcal{E}/\mathcal{E}_0} &= -\omega_1 (\omega_2 \sin \theta \hat{e}_1 \times \hat{e}_3) \\ &= \omega_1 \omega_2 \sin \theta \hat{e}_2 \quad \text{————— (7)} \end{aligned}$$

Further, using transformations ⑥

$$\begin{aligned}\underline{\omega}_{\mathcal{E}/\mathcal{E}_0} &= -\omega_1 \hat{e}_3 + \omega_2 (\hat{e}_1 \sin \theta + \hat{e}_3 \cos \theta) \\ &= \omega_2 \sin \theta \hat{e}_1 + (\omega_2 \cos \theta - \omega_1) \hat{e}_3\end{aligned}\quad \text{--- ⑧}$$

Now we will write ③ in \mathcal{E} , because \underline{I}_{cm} in \mathcal{E} is diagonal and fixed.

This eliminates computation of

$\frac{d}{dt} \underline{I}_{cm}$ when calculating $\dot{\underline{h}}$.

RHS of ③ in \mathcal{E}

$$\begin{aligned}&= \left(\frac{mR^2}{4} \hat{e}_1 \otimes \hat{e}_1 + \frac{mR^2}{4} \hat{e}_2 \otimes \hat{e}_2 + \frac{mR^2}{2} \hat{e}_3 \otimes \hat{e}_3 \right) \cdot \\ &\quad (\omega_1 \omega_2 \sin \theta \hat{e}_2) \\ &+ (\omega_2 \sin \theta \hat{e}_1 + (\omega_2 \cos \theta - \omega_1) \hat{e}_3) \times \\ &\left(\frac{mR^2}{4} \hat{e}_1 \otimes \hat{e}_1 + \frac{mR^2}{4} \hat{e}_2 \otimes \hat{e}_2 + \frac{mR^2}{2} \hat{e}_3 \otimes \hat{e}_3 \right) \cdot \\ &\quad (\omega_2 \sin \theta \hat{e}_1 + (\omega_2 \cos \theta - \omega_1) \hat{e}_3)\end{aligned}$$

$$= \frac{mR^2}{4} \omega_1 \omega_2 \sin \theta \hat{e}_2 + (\omega_2 \sin \theta \hat{e}_1 + (\omega_2 \cos \theta - \omega_1) \hat{e}_3) \times \left(\frac{mR^2}{4} \omega_2 \sin \theta \hat{e}_1 + \frac{mR^2}{2} (\omega_2 \cos \theta - \omega_1) \hat{e}_3 \right)$$

$$= \frac{mR^2}{4} \omega_1 \omega_2 \sin \theta \hat{e}_2 - \omega_2 \sin \theta \frac{mR^2}{2} \cdot$$

$$(\omega_2 \cos \theta - \omega_1) \hat{e}_2 + \omega_2 \sin \theta \frac{mR^2}{4} \cdot$$

$$(\omega_2 \cos \theta - \omega_1) \hat{e}_2$$

$$= \left(\frac{mR^2}{4} \cancel{\omega_1 \omega_2 \sin \theta} - \frac{mR^2}{2} \omega_2^2 \sin \theta \cos \theta + \frac{mR^2}{2} \omega_1 \omega_2 \sin \theta + \frac{mR^2}{4} \omega_2^2 \sin \theta \cos \theta - \frac{mR^2}{4} \cancel{\omega_1 \omega_2 \sin \theta} \right) \hat{e}_2$$

$$= \frac{mR^2}{2} \omega_2 \sin \theta \left(\omega_1 - \frac{1}{2} \omega_2 \cos \theta \right) \hat{e}_2$$

We recall that $\hat{e}_2 = \hat{E}_2$

\therefore RHS of ③ in \mathcal{E}_0 is simply

$$= \frac{mR^2}{2} \omega_2 \sin \theta \left(\omega_1 - \frac{1}{2} \omega_2 \cos \theta \right) \hat{E}_2 \quad \text{⑨}$$

Now let us write LHS of (3) in \mathcal{E}_0

$$\begin{aligned} & -\mathcal{L} \hat{\mathbf{E}}_3 \times (A_1 \hat{\mathbf{E}}_1 + A_2 \hat{\mathbf{E}}_2 + A_3 \hat{\mathbf{E}}_3) + \mathcal{L} \hat{\mathbf{E}}_3 \times \\ & \quad (B_1 \hat{\mathbf{E}}_1 + B_2 \hat{\mathbf{E}}_2 + B_3 \hat{\mathbf{E}}_3) \\ &= \mathcal{L}(A_2 - B_2) \hat{\mathbf{E}}_1 + \mathcal{L}(B_1 - A_1) \hat{\mathbf{E}}_2 \quad \text{--- (10)} \end{aligned}$$

Equating (9) and (10) yields

$$(A_2 - B_2) \mathcal{L} = 0$$

$$\text{or } A_2 - B_2 = 0$$

$$\text{or } A_2 = B_2 \quad \text{--- (11a)}$$

and

$$\mathcal{L}(B_1 - A_1) = \frac{mR^2}{2} \omega_2 \sin \theta \left(\omega_1 - \frac{\omega_2}{2} \cos \theta \right)$$

$$\therefore B_1 - A_1 = \frac{mR^2}{2\mathcal{L}} \omega_2 \sin \theta \left(\omega_1 - \frac{\omega_2}{2} \cos \theta \right) \quad \text{--- (11b)}$$

Using $A_1 = -B_1$ from (2a) in (11b) we get

$$\boxed{B_1 = \frac{mR^2}{4\mathcal{L}} \omega_2 \sin \theta \left(\omega_1 - \frac{\omega_2}{2} \cos \theta \right)}$$

$$A_1 = -\frac{mR^2}{4L} \omega_2 \sin \theta \left(\omega_1 - \frac{\omega_2}{2} \cos \theta \right)$$

Using (11a) in (2b) results in

$$A_2 = B_2 = \frac{mg}{2}$$

From (2c) we have $A_3 = -B_3$. We need another equation to determine A_3 and B_3 . In the absence of any other information e.g. details of the bearing-shaft interaction etc. these two components of \underline{A} and \underline{B} will remain undetermined in "rigid body" world.