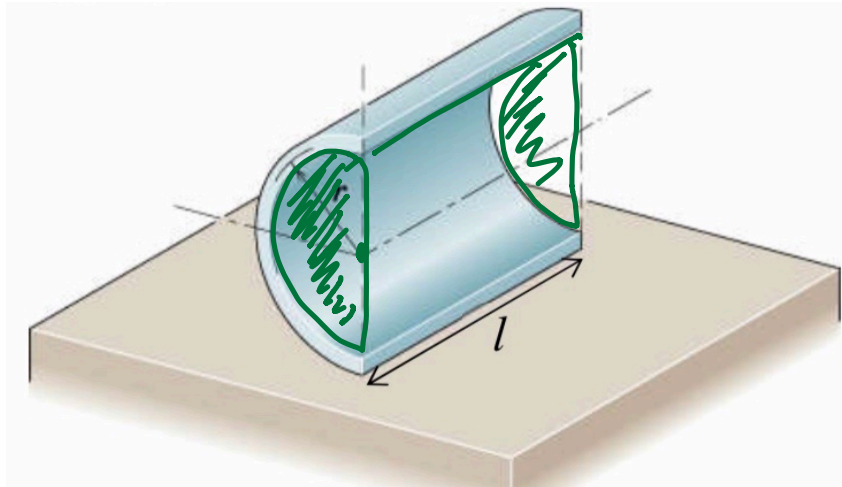
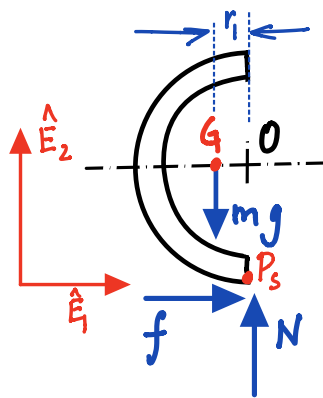


(2) A uniform thin semi-cylindrical shell of mass 10 kg, length  $l = 1$  m and mean radius  $r = 0.5$  m, is released from the rest position as shown. Determine the minimum coefficient of friction necessary to prevent any initial slipping of the shell.



FBD



- While the object is 3D  
the KINETICS is 2D  
(You show this)

- CM  $G$  is NOT at  $O$ . By symmetry  
 $G$  must be as shown  
(We will compute  $r_1$  below)

LMB:  $\Sigma \underline{F} = m \underline{a}^G \Rightarrow f \hat{e}_1 + (N - mg) \hat{e}_2 = m \underline{a}^G \quad (1)$

AMB about G:  $\underline{M}^G = \underline{\omega}^B \times (\underline{I}^G \cdot \underline{\omega}^B) + \underline{I}^G \cdot \underline{\alpha}^B$

(2D KINETICS:  $\underline{\alpha}^B = \alpha \hat{e}_3$ ,  $\underline{\omega}^B = \omega \hat{e}_3$ )  $\Rightarrow (f r + N r_1) \hat{e}_3 = \underline{I}_3^G \alpha \hat{e}_3$   
(2)

THREE equations, FIVE ( $\alpha, \underline{a}^G, f, N$ ) unknowns.

The remaining TWO equations will be found by KINEMATIC ANALYSIS.

KINEMATIC ANALYSIS: Assume shell rolls without slipping

- let  $\underline{a}^G = a_1 \hat{E}_1 + a_2 \hat{E}_2$  — (3)

- Rolling condition #2:  $\underline{a}^{P_s} \cdot \hat{E}_1 = \underline{a}^{P_g} \cdot \hat{E}_1 = 0$  (4)

( $P_s$  is the point on shell in contact with point  $P_g$  on the ground)

$$\underline{a}^{P_s} = \underline{a}^G + \underline{\omega}^B \times (\underline{\omega}^B \times \underline{r}^{P_s/G}) + \underline{\alpha}^B \times \underline{r}^{P_s/G}$$

$$\underline{r}^{P_s/G} = r_1 \hat{E}_1 - r_2 \hat{E}_2$$

$$= a_1 \hat{E}_1 + a_2 \hat{E}_2 - \omega^2 (r_1 \hat{E}_1 - r_2 \hat{E}_2) + \alpha (r_1 \hat{E}_2 + r_2 \hat{E}_1)$$

0 as given that shell is released from rest.

$$\therefore \underline{a}^{P_s} = a_1 \hat{E}_1 + a_2 \hat{E}_2 + \alpha (r_1 \hat{E}_2 + r_2 \hat{E}_1) \text{ — (5)}$$

Equations (4) & (5)  $\Rightarrow a_1 + \alpha r = 0$  — (6)

Need one more equation.

- Consider the motion of  $O$ . Think of  $O$  as a part of the cylindrical shell. This is because  $O$  remains at the same distance from all points on the shell

Clearly  $\underline{a}^O \cdot \hat{E}_2 = 0$  ————— (7)

as  $O$  remains at a distance  $r$  from the ground.

As  $O$  &  $G$  are on the rigid shell:

$$\underline{a}^O = \underline{a}^G + \underline{\omega}^B \times (\underline{\omega}^B \times \underline{r}^{O/G}) + \underline{\alpha}^B \times \underline{r}^{O/G}$$

from (3)  $\swarrow$   $\nwarrow$   $O$

$$\Rightarrow \underline{a}^O = a_1 \hat{E}_1 + a_2 \hat{E}_2 + \alpha r_1 \hat{E}_2$$

Using (7):  $a_2 + \alpha r_1 = 0$  ————— (8)

Equations (6) & (8) are the required TWO more equations.

Collecting (1), (2), (6) & (8)

$$\underbrace{f = m a_1; N - mg = m a_2}_{LMB}; \quad \overbrace{f r + N r_1}^{AMB/G} = I_3^G \alpha$$

KINEMATIC ANALYSIS:  $a_1 + \alpha r = 0$ ;  $a_2 + \alpha r_1 = 0$

Solving for  $f$  &  $N$ :

$$(9) \quad f = \frac{mg(m r r_1)}{I_3^G + m(r^2 + r_1^2)} \quad N = mg \left( 1 - \frac{m r_1^2}{I_3^G + m(r^2 + r_1^2)} \right)$$

Now we must have  $f \leq \mu N$

$$\Rightarrow \mu_{\min} = f/N = \frac{m r r_1}{I_3^G + m r^2} \quad (10)$$

All we need now is  $r_1$  &  $I_3^G$ .

• From  $\underline{r}^{G/O} = \frac{\int \underline{r} dV}{m}$  we obtain

$$-r_1 \hat{E}_1 = -\frac{\int_0^\pi r \sin \theta \rho r d\theta \hat{E}_1 L}{m} = -\frac{\int_0^\pi r^2 (-\cos \theta) d\theta}{m} \hat{E}_1 L$$

$$\Rightarrow r_1 = \frac{2 \int_0^\pi r^2 L}{m} = \frac{2 \int_0^\pi r^2 L}{r \int_0^\pi L} = 2r/\pi \quad (11)$$

•  $I^0 = I^G + m(|\underline{r}^{G/O}|^2 - \underline{r}^{G/O} \otimes \underline{r}^{G/O})$  (11 axis theorem)

It is easy to guess/compute that  $\hat{E}_3 = \hat{E}_3^0$  is the principal axis of  $I^0$  &  $I^G$

$$\Rightarrow I_3^0 = I_3^G + m r_1^2$$

$$\Rightarrow m r^2 = I_3^G + m r_1^2$$

$$\Rightarrow I_3^G = m(r^2 - r_1^2) = m r^2 (1 - 4/\pi^2) \quad (12)$$

Combine (10)-(12) to get

$$\mu_{\min} = \frac{\pi}{\pi^2 - 2}$$

