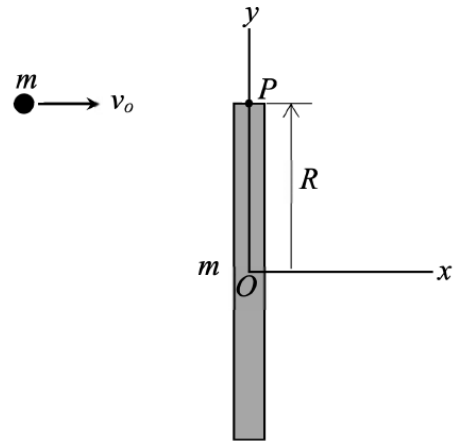


Problem:

- (1) A thin uniform circular disc-type satellite of mass m and radius R is spinning at a constant angular rate of ω_0 in space about its body-fixed x -axis, as shown. A space debris of equal mass but of a point size hits the satellite normal to its plane with the velocity v_0 as shown. Subsequently, the debris gets embedded into it at point P . Find the angular velocity vector immediately after the collision. What impact model is being used here? The figure shows the side view of the satellite.



Solution: we have attached the ground fixed CS: $\{\mathcal{E}_o, O, \hat{E}_i\}$ and satellite BFCs: $\{\mathcal{E}_1, O, \hat{e}_i\}$.

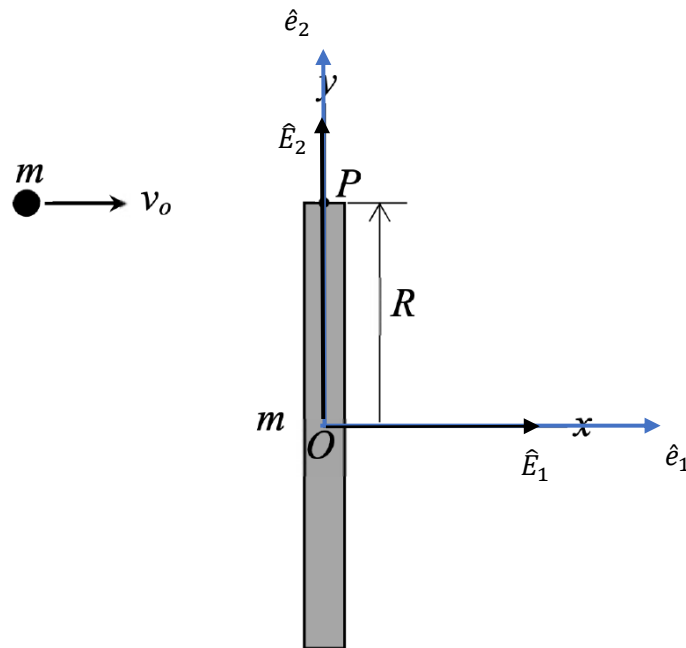


Fig. 1

FBD: as given in problem that debris gets embedded into satellite therefore, $e = 0$. Weights are not shown as they are bounded forces.

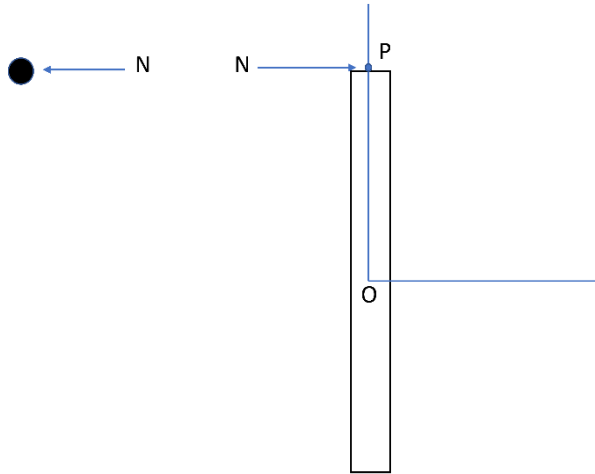


Fig.2

Let mass of debris as m_d and mass of satellite as m_s and other parameters are given as

\underline{v}_b^s : velocity of satellite just before impact.

\underline{v}_b^d : velocity of debris just before impact.

\underline{v}_a^s : velocity of satellite just after impact.

\underline{v}_a^d : velocity of debris just before impact.

$\underline{\omega}_b^s$: angular velocity of satellite just before impact.

$\underline{\omega}_a^s$: angular velocity of satellite just after impact.

Now writing all *impulse-momentum relations*,

First writing conservation of Linear momentum

$$p_{sys}(t - \delta t) = p_{sys}(t + \delta t) \dots \dots (1)$$

Using Eq. (1)

$$m_s \underline{v}_b^s + m_d \underline{v}_b^d = m_s \underline{v}_a^s + m_d \underline{v}_a^d,$$

Given: $\underline{v}_b^d = v_o \hat{e}_1$, $\underline{v}_b^s = \underline{0}$ and $m_s = m_d = m$. Then

$$\underline{v}_a^s + \underline{v}_a^d = v_o \hat{e}_1 \dots \dots (2)$$

Using impact model, $e = 0$, as after impact debris get embedded into satellite at point P, therefore

$$\underline{v}_a^d = \underline{v}_a^s + \underline{\omega}_a^s \times \underline{r}_{P/O} \dots \dots (3)$$

where, $\underline{r}_{P/O} = R\hat{e}_2$ and let, $\underline{\omega}_a^s = \omega_1\hat{e}_1 + \omega_2\hat{e}_2 + \omega_3\hat{e}_3$. Then from Eq. (3) and (2)

$$\underline{v}_a^s = \left(\frac{v_o + \omega_3 R}{2}\right)\hat{e}_1 - \frac{\omega_1 R}{2}\hat{e}_3 \dots \dots (4)$$

From Eq. (4) and (2)

$$\underline{v}_a^d = \left(\frac{v_o - \omega_3 R}{2}\right)\hat{e}_1 + \frac{\omega_1 R}{2}\hat{e}_3 \dots \dots (4)$$

Now writing conservation of angular momentum about point O

$$\underline{h}_O^{sys}(t - \delta t) = \underline{h}_O^{sys}(t + \delta t) \dots \dots (5)$$

Using Eq. (5)

$$\begin{aligned}\underline{h}_O^{sys}(t - \delta t) &= \underline{h}_O^s(t - \delta t) + \underline{h}_O^d(t - \delta t), \\ \underline{h}_O^{sys}(t - \delta t) &= \underline{I}_O \cdot \underline{\omega}_b^s + \underline{r}_{O/O} \times m_s \underline{v}_b^s + \underline{r}_{P/O} \times m_d \underline{v}_b^d, \\ \underline{h}_O^{sys}(t + \delta t) &= \underline{h}_O^s(t + \delta t) + \underline{h}_O^d(t + \delta t), \\ \underline{h}_O^{sys}(t + \delta t) &= \underline{I}_O \cdot \underline{\omega}_a^s + \underline{r}_{P/O} \times m_d \underline{v}_a^d.\end{aligned}$$

This gives:

$$\underline{I}_O \cdot \underline{\omega}_b^s + \underline{r}_{P/O} \times m_d \underline{v}_b^d = \underline{I}_O \cdot \underline{\omega}_a^s + \underline{r}_{P/O} \times m_d \underline{v}_a^d \dots (6)$$

where

$$\begin{aligned}\underline{I}_O &= \frac{mr^2}{4} \begin{bmatrix} 2 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}, \\ \underline{\omega}_b^s &= \omega_o \hat{e}_1,\end{aligned}$$

From Eq. (6) and (4), and comparing components of \hat{e}_1, \hat{e}_2 and \hat{e}_3 , we get

$$\omega_1 = \frac{\omega_o}{2}, \omega_2 = 0, \text{ and } \omega_3 = -\frac{2v_o}{3R}$$

Then

$$\underline{\omega}_a^s = \frac{\omega_o}{2}\hat{e}_1 - \frac{2v_o}{3R}\hat{e}_3.$$