

EE 210
Solⁿ to HA #3

①

1 i) $V_{SB} = 0 \Rightarrow V_{TN} = V_{TNO} = \underline{1V}$

ii) $V_{SB} = +1V \Rightarrow V_{TN} = V_{TNO} + \gamma(\sqrt{2\phi_F + V_{SB}} - \sqrt{2\phi_F})$
 $= 1 + 0.4(\sqrt{0.6+1} - \sqrt{0.6}) = \underline{1.2V}$

iii) $V_{SB} = +5V \Rightarrow V_{TN} = 1 + 0.4(\sqrt{0.6+5} - \sqrt{0.6}) = \underline{1.64V}$

If body were tied to a +ve potential, then the SB jn. would become forward biased, & the jn. would carry large forward current, totally overshadowing the surface current due to field effect. \Rightarrow MOS operation will be lost.

2 a) i) $V_{DS} = 1V$ $V_{GS} - V_{TN} = 2 - 0.7 = \underline{1.3V} \Rightarrow V_{DS} < V_{GS} - V_{TN} \Rightarrow \underline{\text{non-saturation}}$
 $\therefore I_D = \frac{K_n'}{2} \left(\frac{W}{L}\right) [2(V_{GS} - V_{TN})V_{DS} - V_{DS}^2] = \frac{40 \times 10^{-6}}{2} \times \frac{20}{1} \times [2(2-0.7)1 - 1^2]$
 $= \underline{0.64mA}$

ii) $V_{DS} = 5V$ $V_{GS} - V_{TN} = \underline{1.3V} \Rightarrow V_{DS} > V_{GS} - V_{TN} \Rightarrow \underline{\text{saturation}}$

$\therefore I_D = \frac{K_n'}{2} \left(\frac{W}{L}\right) (V_{GS} - V_{TN})^2 = \underline{0.676mA}$

b) i) With $\lambda = 0.1V^{-1}$, the result of part i) will remain unaltered, $\because \lambda$ has no meaning in non-saturation region (as the channel is yet to pinch off).

ii) $I_D = 0.676mA \times (1 + \lambda V_{DS}) = \underline{1.014mA}$

Note: I_D increases significantly in saturation region due to the channel length modulation effect, compounded by a high value of λ .

3 $V_{TNO} = -1V \Rightarrow$ Depletion mode device, operated with $V_G = V_S = 0 \Rightarrow V_{GS} = 0$
 & $V_{DS} = 0.5V$.

a) If $V_B = 0$, $V_{BS} = 0$, $V_{TN} = V_{TNO} = -1V$, $V_{GS} - V_{TN} = 1V$, $V_{DS} = 0.5V \Rightarrow \underline{\text{non-sat}}$
 $\therefore I_D = \frac{K_n'}{2} \left(\frac{W}{L}\right) [2(V_{GS} - V_{TN})V_{DS} - V_{DS}^2] = \underline{0.3mA}$

b) V_B can only be -ve, $\because V_S = 0$, & the device is n-channel (p-substrate).
 With V_{BS} becoming more -ve, V_{TN} would keep on increasing due to body effect.
 When V_{TN} equals $-0.5V$, $V_{GS} - V_{TN} = 0.5V = V_{DS}$, & the device would be at the cross-over point betⁿ non-sat. & sat. regions.

$\therefore V_{TN} = -0.5V = -1 + \gamma(\sqrt{2\phi_F + V_{SB}} - \sqrt{2\phi_F}) \Rightarrow 0.5 = 0.4(\sqrt{0.6+V_{SB}} - \sqrt{0.6})$

which gives $V_{SB} = 3.5V \Rightarrow V_B = \underline{-3.5V}$

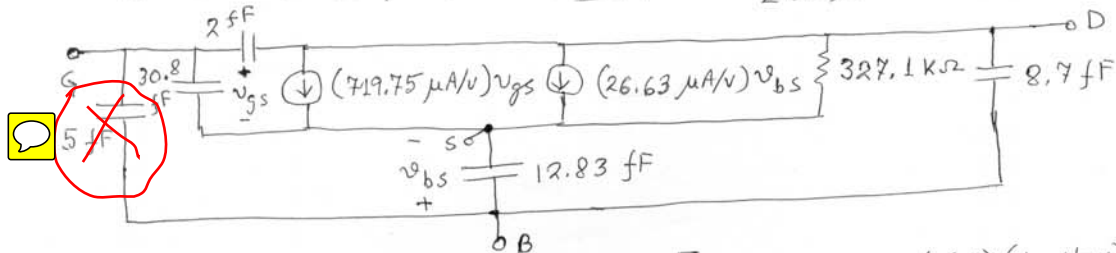
& $I_D = \frac{K_n'}{2} \left(\frac{W}{L}\right) (V_{GS} - V_{TN})^2 = \underline{0.1mA}$

- c) for I_D to go to zero, the device must cutoff, i.e., $V_{GS} - V_{TN}$ must be zero, (2)
 or $V_{GS} = V_{TN} = 0$ (for this case) ($\because V_G = V_S = 0$ & $V_{GS} = 0$).
 $\therefore V_{TN} = 0 = -1 + 0.4(\sqrt{0.6 + V_{SB}} - \sqrt{0.6}) \Rightarrow V_{SB} = 10.12V \Rightarrow V_B = -10.12V$

$$4 \quad C_{ox}' = \frac{\epsilon_{ox}}{t_{ox}} = \frac{4.32 \times 10^{-7} \text{ F/cm}^2}{\text{cm}^2}, \quad \gamma = \frac{\sqrt{2q\epsilon_s N_A}}{C_{ox}'} = 0.094 \text{ V}^{1/2}$$

$$V_{TN} = V_{TN0} + \gamma(\sqrt{2\phi_F + V_{SB}} - \sqrt{2\phi_F}) = 0.646V, \quad V_{GS} - V_{TN} = 0.354V$$

$$V_{DS} = 2V \Rightarrow V_{DS} > V_{GS} - V_{TN} \Rightarrow \text{sat} \Rightarrow I_D = \frac{K_n'}{2} \left(\frac{W}{L}\right) (V_{GS} - V_{TN})^2 (1 + \lambda V_{DS}) = 127.4 \mu A$$



$$g_m = \sqrt{2K_n' \left(\frac{W}{L}\right) I_D (1 + \lambda V_{DS})} = 719.75 \mu A/V \quad \left[\text{Alternately, } g_m = K_n' \left(\frac{W}{L}\right) (V_{GS} - V_{TN}) (1 + \lambda V_{DS}) = 719.75 \mu A/V \right]$$

$$\chi = \frac{\gamma}{2\sqrt{2\phi_F + V_{SB}}} = 0.037, \quad g_{mb} = \chi g_m = 26.63 \mu A/V$$

$$r_o = \frac{1}{\lambda I_D} = 327.1 k\Omega, \quad C_{sb} = \frac{C_{sbo}}{\left(1 + \frac{V_{SB}}{V_0}\right)^{1/2}} = 12.83 \text{ fF} \quad V_{DB} = V_{DS} + V_{SB} = 3V$$

$$\therefore C_{db} = \frac{C_{dbo}}{\left(1 + \frac{V_{DB}}{V_0}\right)^{1/2}} = 8.7 \text{ fF}, \quad C_{gs0} = g_{gs0}' W = 2 \text{ fF} = C_{gd0} = C_{gdo}' W$$

$$\Rightarrow C_{gs} = \frac{2}{3} WL C_{ox}' + C_{gs0} = 30.8 \text{ fF}, \quad C_{gd} \approx C_{gd0} = 2 \text{ fF}, \quad C_{gb} = 5 \text{ fF}$$

Eqv. ckt. as shown. [Check all the calculations for correctness]

- 5 Note: C_{gs}, C_{gd}, C_{gb} are to a first-order, independent of V_{GS} , & for the given data, the device remains saturated for all values of V_{GS} .

$$f_T = \frac{g_m}{2\pi(C_{gs} + C_{gd} + C_{gb})} \quad \& \quad f_{max} = \frac{1.5 \mu_n}{2\pi L^2} (V_{GS} - V_{TN}) \quad \mu_n = \frac{K_n'}{C_{ox}'} = 449.1 \frac{\text{cm}^2}{\text{Vsec}}$$

$$V_{GS} = 1V: \quad g_m = K_n' \left(\frac{W}{L}\right) (V_{GS} - V_{TN0}) (1 + \lambda V_{DS}) = 831.87 \mu A/V$$

$$C_{gs} + C_{gd} + C_{gb} = 37.8 \text{ fF} \quad f_T = 3.5 \text{ GHz} \quad \& \quad f_{max} = 4.3 \text{ GHz}$$

$$V_{GS} = 1.5V: \quad g_m = 1.87 \text{ mA/V} \Rightarrow f_T = 7.87 \text{ GHz} \quad \& \quad f_{max} = 9.65 \text{ GHz}$$

$$V_{GS} = 2V: \quad g_m = 2.9 \text{ mA/V} \Rightarrow f_T = 12.2 \text{ GHz} \quad \& \quad f_{max} = 15 \text{ GHz}$$

[Check all calculations for correctness]