

Soln. to HA #2

$$1 \quad R_C = \frac{V_{CC} - V_{CE}}{I_C} = \frac{5 - 3}{0.5 \text{ mA}} = \underline{4 \text{ k}\Omega} \quad I_B = \frac{I_C}{\beta} = \frac{0.5 \text{ mA}}{100} = \underline{5 \mu\text{A}}$$

$$R_B = \frac{V_B - V_{BE}}{I_B} = \frac{5 - 0.7}{5 \mu\text{A}} = \underline{860 \text{ k}\Omega}$$

At onset of sat., $V_{CE} = \underline{0.7 \text{ V}} \Rightarrow$ With I_B unchanged, I_C will remain unchanged $\Rightarrow R_C = \frac{5 - 0.7}{0.5 \text{ mA}} = \underline{8.6 \text{ k}\Omega}$

With R_C further doubled to $\underline{17.2 \text{ k}\Omega}$, the pot. drop across it will drive Q into hard sat., with $V_{CE}(\text{sat}) = \underline{0.1 \text{ V}}$ (assumed).

$$\Rightarrow I_{C,\text{sat}} = \frac{5 - 0.1}{17.2 \text{ k}\Omega} = \underline{284.9 \mu\text{A}} \quad (\text{note the reduction in } I_C)$$

V_{BE} will adjust itself to $\underline{0.8 \text{ V}}$ in hard sat.

$$\therefore I_{B,\text{sat}} = \frac{5 - 0.8}{860 \text{ k}\Omega} = \underline{4.88 \mu\text{A}} \Rightarrow \beta_{\text{sat}} = \frac{I_{C,\text{sat}}}{I_{B,\text{sat}}} = \frac{284.9}{4.88} = \underline{58.4}$$

$$\text{Degree of sat. (Dos)} = \frac{\beta}{\beta_{\text{sat}}} = \frac{100}{58.4} = \underline{1.7}$$

$$2 \quad C_{\pi} = C_{je} + \tau_F g_m \Rightarrow C_{\pi 2} - C_{\pi 1} = \tau_F (g_{m2} - g_{m1}) \quad \because C_{je1} = C_{je2}$$

$$\Rightarrow 8 - 6 = \tau_F \left(\frac{2}{26} - \frac{1}{26} \right) \Rightarrow \tau_F = \underline{52 \text{ pS}} \quad \& \quad C_{je} = 6 \text{ pF} - 52 \text{ pS} \times \frac{1}{26} = \underline{4 \text{ pF}}$$

\because EB jn. is forward biased, apply thumb rule $C_{je} \approx 2 C_{je0}$, which gives $C_{je0} = \underline{2 \text{ pF}}$.

$$3 \quad \text{For both } I_C = 1 \text{ mA} \& 10 \text{ mA}, V_{CB} \text{ is held constant at } 10 \text{ V} \Rightarrow C_{\mu} \text{ remains constant. } f_T = \frac{g_m}{2\pi(C_{\pi} + C_{\mu})} = \frac{1}{2\pi\tau} \quad \text{where } \tau \text{ is an effective time} = \frac{C_{\pi} + C_{\mu}}{g_m}$$

\therefore for $I_C = 1 \text{ mA}$, $\tau_1 = \frac{1}{2\pi f_{T1}} = \underline{0.265 \text{ ns}}$, & for $I_C = 10 \text{ mA}$, $\tau_2 = \frac{1}{2\pi f_{T2}} = \underline{0.159 \text{ ns}}$. Thus, $0.265 \text{ ns} = \tau_F + \frac{C_{je} + C_{\mu}}{g_{m1}}$ ($\because \tau_F, C_{je}, \& C_{\mu}$ are constants) with $g_{m1} = \frac{1}{26} \text{ S}$, & $0.159 \text{ ns} = \tau_F + \frac{C_{je} + C_{\mu}}{g_{m2}}$ with $g_{m2} = \frac{1}{2.6} \text{ S}$. $C_{\mu} = 0.15 \text{ pF}$ is given. Solving, we get $C_{je} = \underline{4.38 \text{ pF}} \quad \& \quad \tau_F = \underline{147.22 \text{ pS}}$

Also, $C_{\mu} = \frac{C_{\mu 0}}{(1 - \frac{V_{BC}}{V_0})^{1/2}}$ (assumed that the jn. is abrupt) (2)

with $V_{BC} = -10V$, $C_{\mu} = 0.15 pF$, & $V_0 = 0.55V$ (given) $\Rightarrow C_{\mu 0} = \underline{0.657 pF}$

\therefore with $V_{BC} = -2V$ $C_{\mu} = \frac{0.657 pF}{(1 + \frac{2}{0.55})^{1/2}} = \underline{0.305 pF}$

$r_o = 50 k\Omega$ at $I_C = 1 mA \Rightarrow V_A = I_C r_o = \underline{50V}$

Now, we have all the reqd. parameters to obtain the small-signal model.

$I_C = 0.1 mA$: $g_m = 3.846 mV$, $r_{\pi} = 26 k\Omega$, $r_o = 500 k\Omega$, $r_{\mu} = 250 M\Omega$,

$C_b = \tau_F g_m = 0.566 pF$, $C_{\pi} = C_{je} + C_b = 4.946 pF$, $C_{\mu} = 0.305 pF$.

$I_C = 1 mA$: $g_m = 38.46 mV$, $r_{\pi} = 2.6 k\Omega$, $r_o = 50 k\Omega$, $r_{\mu} = 25 M\Omega$, $C_b = 5.66 pF$,

$C_{\pi} = 10.04 pF$, $C_{\mu} = 0.305 pF$.

$I_C = 5 mA$: $g_m = 192.3 mV$, $r_{\pi} = 520 \Omega$, $r_o = 10 k\Omega$, $r_{\mu} = 5 M\Omega$, $C_b = 28.31 pF$,

$C_{\pi} = 32.69 pF$, $C_{\mu} = 0.305 pF$.

* Check all these nos. for their correctness. *

The small-signal model will be identical to that given in class.

$\beta = \frac{\beta_0}{1 + j f / f_{\beta}}$ Now, with $\beta_0 = 100$ & β at only 9 at $f = 50 MHz$,
it is prudent to assume that $f \gg f_{\beta}$.

$\Rightarrow |\beta| = \frac{\beta_0 f_{\beta}}{f} = \frac{f_T}{f} \Rightarrow f_T = f |\beta| = \underline{450 MHz}$

Now, $f_T = \frac{g_m}{2\pi(C_{\pi} + C_{\mu})} \Rightarrow C_{je} + \tau_F g_m + C_{\mu} = \frac{g_m}{2\pi f_T}$

We have $g_m = \frac{1}{26} V$, $\tau_F = 0.25 ns$, & $C_{\mu} = 0.6 pF$

$\Rightarrow C_{je} = \frac{1}{26 \times 2\pi \times 450 \times 10^6} - 0.25 ns \times \frac{1}{26} - 0.6 pF = \underline{3.4 pF}$

Small-Signal model parameters for $I_C = 2 mA$:

$g_m = \frac{I_C}{V_T} = \frac{2 mA}{26 mV} = \underline{76.923 mV}$, $r_{\pi} = \beta_0 / g_m = \underline{1.3 k\Omega}$, $r_o = \frac{V_A}{I_C} = \underline{20 k\Omega}$,

$C_{je} = \underline{3.4 pF}$, $C_b = \tau_F g_m = 19.23 pF$, $C_{\pi} = C_{je} + C_b = \underline{22.63 pF}$,

& $C_{\mu} = \underline{0.6 pF}$

(3)

$$5 \quad C_{\pi} = C_{je} + \tau_F g_m = 5 \text{ pF} + 26 \text{ pS} \times \frac{2}{26} = \underline{7 \text{ pF}} \quad C_{\mu} = \underline{0.5 \text{ pF}} \quad (\text{given})$$

$$f_T = \frac{g_m}{2\pi(C_{\pi} + C_{\mu})} = \frac{2}{26} \times \frac{1}{2\pi(7 \text{ pF} + 0.5 \text{ pF})} = \underline{1.63 \text{ GHz}}$$

$$f_{\beta} = \frac{f_T}{\beta_0} = \underline{16.32 \text{ MHz}} \quad (\text{Note how small } f_{\beta} \text{ is as compared to } f_T, \\ \& \text{ of course, the difference depends on } \beta_0)$$

$$f_{\alpha} = (\beta_0 + 1) f_{\beta} = \underline{1.65 \text{ GHz}} \quad (\text{Note that } f_{\alpha} \text{ is so very slightly larger than } f_T)$$

$$f_{\max} = \frac{1}{2\pi \tau_F} = \underline{6.12 \text{ GHz}} \quad (\text{way higher than } f_{\beta}, \& \text{ almost 4 times that of } f_T \& f_{\alpha})$$

The transistor cannot be operated for any freq. higher than f_{\max} .

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