

EE 210
Soln to HA #1

①

- i) a) $V_D = 50 \text{ mV} \Rightarrow \text{comparable to } V_T \Rightarrow I_D = I_0 (e^{V_D/V_T} - 1)$
 $= 10 \text{ pA} \times (e^{50/26} - 1) = \underline{58.42 \text{ pA}}$ (from p to n)
 b) $V_D = 500 \text{ mV} \Rightarrow \gg V_T \Rightarrow I_D \approx I_0 e^{V_D/V_T} = 10 \text{ pA} \times e^{500/26} = \underline{2.25 \text{ mA}}$ (p to n)
 ii) a) $V_D = -50 \text{ mV} \Rightarrow I_D = 10 \text{ pA} \times (e^{-50/26} - 1) = \underline{-8.54 \text{ pA}}$
 (-ve sign implies that the current is flowing from n to p)
 b) $V_D = -500 \text{ mV} \Rightarrow I_D \approx -I_0 = \underline{-10 \text{ pA}}$ (n to p)

2. $\because D_2$ is rev. biased, major part of V_{AP} will drop across it, &
 $I_D \approx I_0(D_2) = \underline{1 \text{ nA}}$. The same current also flows thru D_1 .
 $\Rightarrow I_D = I_0(D_1) (e^{V_{D1}/V_T} - 1) \Rightarrow V_{D1} = V_T \ln \left(\frac{I_D}{I_0(D_1)} + 1 \right)$
 $\because I_D (= 1 \text{ nA})$ is 10^3 times $I_0(D_1) (= 1 \text{ pA})$
 $\Rightarrow V_{D1} \approx V_T \ln \frac{I_D}{I_0(D_1)} = 26 \text{ mV} \times \ln \frac{1 \text{ nA}}{1 \text{ pA}} = \underline{179.6 \text{ mV}}$
 & $V_{D2} = V_{AP} - V_{D1} = 5 \text{ V} - 179.6 \text{ mV} = \underline{4.82 \text{ V}}$

3. 2 defining relations $\Rightarrow I_D = \frac{10 - V_D}{1 \text{ k}} \quad \& \quad I_D = 10 \text{ pA} \times e^{V_D/26 \text{ mV}}$
 Rearrange $V_D = 26 \text{ mV} \times \ln \frac{I_D}{10 \text{ pA}}$ choose $V_D = 0.7 \text{ V}$ as initial
 guess, \because this set of eqns. can be solved only thru iterations.
 Gives $I_D = \underline{9.3 \text{ mA}} \Rightarrow V_D = \underline{0.537 \text{ V}} \Rightarrow I_D = \underline{9.463 \text{ mA}} \Rightarrow V_D = \underline{0.537 \text{ V}}$
 \Rightarrow Convergence in just 2 iterations.
 $\Rightarrow \boxed{V_D = 0.537 \text{ V}} \quad \& \quad \boxed{I_D = 9.463 \text{ mA}}$

4 Abrupt $j_n \Rightarrow m = 1/2$ $C_{dep} = \frac{C_{dep0}}{(1 - \frac{V_D}{V_0})^{1/2}}$ (2)

$\Rightarrow \frac{1}{C_{dep}^2} = \frac{1}{C_{dep0}^2 V_0} (V_0 - V_D)$ Compare with the given expression

$\frac{1}{C_{dep}^2} = 1.5625 \times 10^6 (0.64 - V_D) \Rightarrow V_0 = 0.64V$

Also, $C_{dep0}^2 V_0 = 6.4 \times 10^{-7}$ which gives $C_{dep0} = 10^{-3} \mu F = 1nF$

And $C_{dep0} = \frac{\epsilon_s A}{W} \Rightarrow W = \frac{\epsilon_s A}{C_{dep0}} = \frac{11.7 \times 8.854 \times 10^{-14} \times 10 \times 10^{-2}}{10^{-9}} \approx 1\mu m$

5 $I_{DQ} = 9.463mA \Rightarrow r_D = \frac{V_T}{I_{DQ}} = \frac{26mV}{9.463mA} = 2.75\Omega$

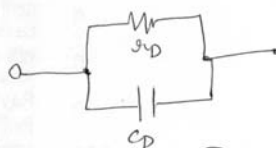
J_n is linearly graded $\Rightarrow C_{dep} = \frac{C_{dep0}}{(1 - \frac{V_D}{V_0})^{1/3}} = \frac{1pF}{(1 - \frac{0.537}{0.8})^{1/3}} = 1.45pF$

$C_{diff} = j_n \tau = \frac{\tau}{r_D} = \frac{1\mu s}{2.75\Omega} = 0.364\mu F$

* Note that in general for a forward biased diode, $C_{diff} \gg C_{dep}$.

$\Rightarrow C_D = C_{diff} + C_{dep} \approx C_{diff} = 0.364\mu F$

Small-Signal Model:



$r_D = 2.75\Omega$
 $C_D = 0.364\mu F$

Diode time constant $\tau_D = r_D C_D = 1\mu s$