

➤ ***Minimization of the Total Capacitance:***

- From the previous analysis, we note that C_E *sees the least Thevenin resistance across its two terminals*

⇒ *Let's choose C_E to contribute the DP f_d , and let C_C and C_B each contribute poles at $f_d/10$*

$$\Rightarrow 48.8 = \sqrt{f_d^2 + 2(f_d/10)^2}$$

$$\Rightarrow f_d = 48.3 \text{ Hz and } f_d/10 = 4.83 \text{ Hz}$$

- Thus:

$$C_E = 1/(2\pi f_d R_E^\infty) = 101.1 \text{ } \mu\text{F}$$

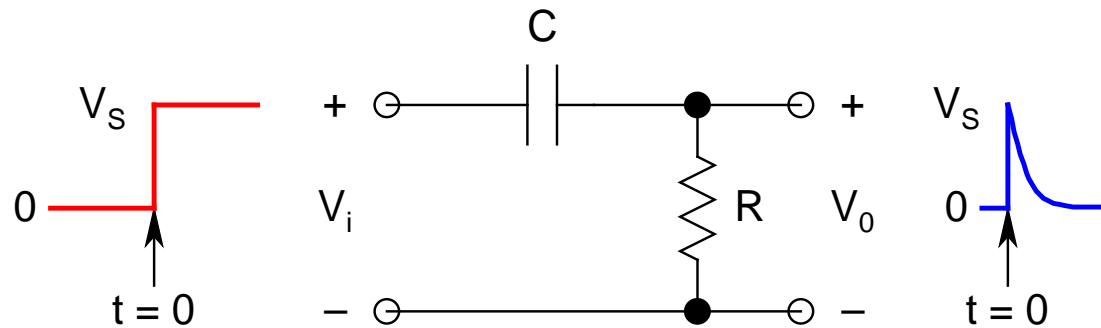
$$C_B = 1/[2\pi(f_d/10)R_B^\infty] = 11 \text{ } \mu\text{F}$$

$$C_C = 1/[2\pi(f_d/10)R_C^\infty] = 4.7 \text{ } \mu\text{F}$$

- Thus, the *total capacitance* requirement comes out to be *116.8 μF* , for the *same f_L of 48.8 Hz*
- The *original circuit* had a *total capacitance* of *200 μF*
- Thus, this approach gave a *cost saving* of almost *42%* in terms of the *capacitors*
- As an *exercise*, you can pick *either C_C or C_B* to *contribute f_d* , and find the *total capacitance* requirement for each case
- Finally, after all, this is a *heuristic*
- To get the *absolute minimum value* of the *total capacitance*, we need to *formulate the problem*, and *find the minima of the function mathematically*

- **Tilt/Sag:**

- For **pulse/square wave excitation**, f_L dictates the amount of **tilt/sag** present in the **output**
- **Due to f_L** , the circuit effectively behaves like a **HPF**, represented by a simple **RC circuit**
- Under **step input**, the **output** would be a **spike**



➤ Thus:

$$V_0 = V_S \exp(-t/\tau_L)$$

$$\tau_L = RC = 1/\omega_L \quad (\omega_L = 2\pi f_L)$$

➤ For $t \ll \tau_L$:

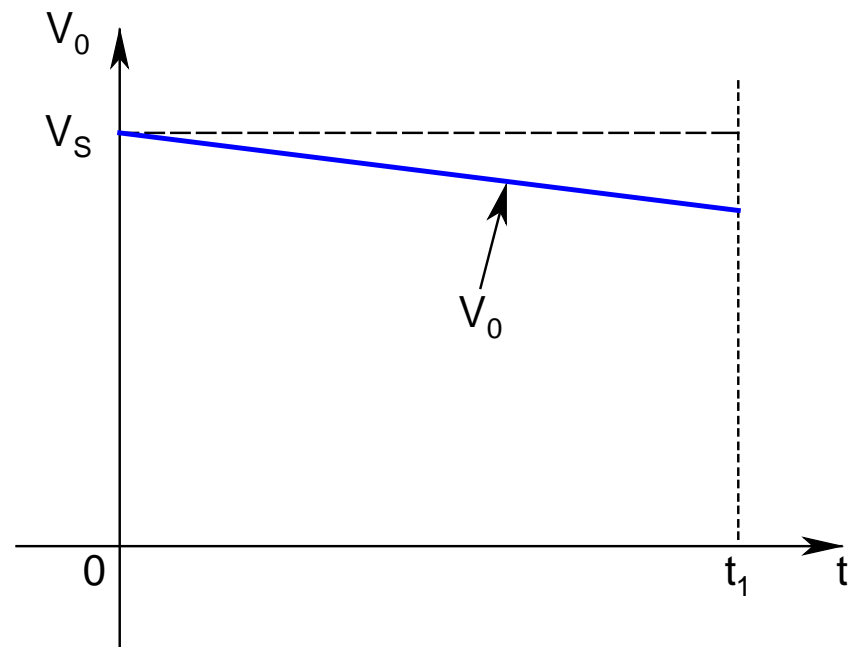
$$V_0 \approx V_S(1 - t/\tau_L)$$

$$= V_S(1 - \omega_L t)$$

$$= V_S(1 - 2\pi f_L t)$$

➤ Thus, *V_0 drops linearly with time*

➤ *Quantified by percent tilt/sag (P)*



$$\begin{aligned} \text{➤ } P &= [(V_S - V_0)/V_S] \times 100\% \\ &= (t_1/\tau_L) \times 100\% \end{aligned}$$

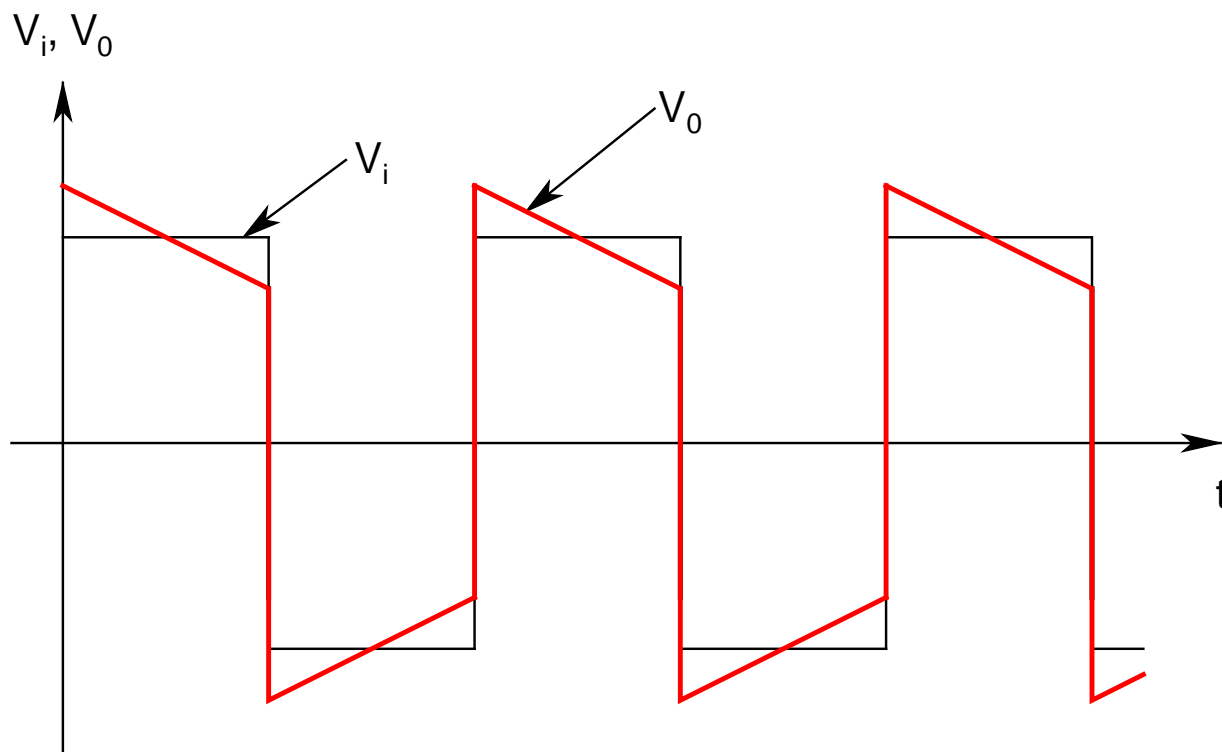
t_1 = *Time at which the tilt is measured*

➤ For *square wave input*, $t_1 = T/2$ (T = *period* = $1/f$, f = *cycle frequency*)

$$\begin{aligned} \Rightarrow P &= [T/(2\tau_L)] \times 100\% = [\omega_L/(2f)] \times 100\% \\ &= (\pi f_L/f) \times 100\% \end{aligned}$$

➤ *Note: P is directly proportional to f_L and inversely proportional to f*

\Rightarrow *Circuits having low f_L , will show significant amount of tilt/sag at low frequencies*



Tilt/Sag

High-Frequency Response

- Will consider *3 methods*:
 - *Exact Analysis*:
 - The *most accurate* and the *most rigorous*
 - *Gives information about all poles and zeros of the system*
 - *Miller Effect Approximation*:
 - *One level of approximation*
 - *Gives information about the Dominant Pole (DP) and one Non-Dominant Pole (NDP)*

➤ *Zero-Value Time Constant (ZVTC)*

Technique:

- *The easiest one*
- *Information regarding only the DP*
- *Suppresses information about all other poles and zeros of the system*
- *Reasonable accuracy*
- *Underestimates f_H slightly (better than overestimating and not achieving it!)*
- *Based on heuristic*
- *Similar to the IVTC technique, based on an algorithm*