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Lecture 13 - PowerPoint (Product Activation Failed)

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2.00

EE 250: Control Systems Analysis  
Module III: s-plane analysis  
Lecture 15: Time Response

Dr Laxmidhar Behera  
Professor, Department of EE, IIT Kanpur

SLIDE 13 OF 20

ENGLISH (INDIA)

NOTES COMMENTS

70%

# EE 250: Control Systems Analysis

## Module III: s-plane analysis

### Lecture 15: Time Response

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### 3 Physical systems vs Simulators

All physical devices are causal by nature. An aircraft, an automobile, and a DC servo motor are examples of physical devices. By definition, an input  $u$  at time  $t = \tau$ , can have influence on the response of the system  $y$  only at  $t \geq \tau$ . All these systems will have transfer functions  $G(s) = \frac{N(s)}{D(s)}$ , where the denominator order is greater than or equal to numerator order.

Any system whether causal or non-causal can be simulated using analogue circuits or digital circuits - respectively called as analogue computer or digital computer. In the class, we have shown how to simulate following transfer functions:

$$G(s) = \frac{s + 2}{s^3 + 2s^2 + 3s + 2} \quad (4)$$

$$G(s) = \frac{s^2 + 2s + 3}{s + 1} \quad (5)$$

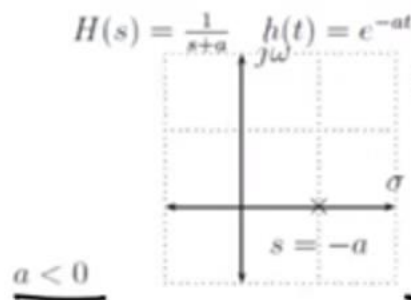


- 13 EE 250: Control Systems Analysis Module III: s-plane analysis Lecture 13: Time Response
- 14 Physical systems in the s-plane
- 15
- 16
- 17
- 18

### First order response

$$H(s) = \frac{1}{s+a}$$

$$h(t) = e^{-at}$$



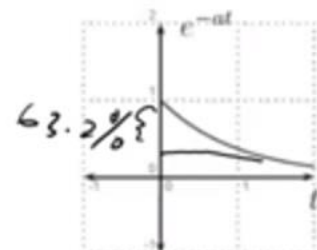
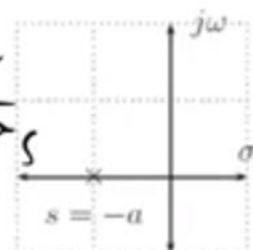
unstable

$(1 - K e^{-at})$

$$H(s) = \frac{1/a}{1 + \tau s} = \frac{\tau}{1 + \tau s}$$

$$\tau = 1/a$$

$a > 0$



$-a$  is positive

$\tau = 1/a$  is called time constant

$-a$  is negative

$$H(s) = 1/s$$

$$h(t) = 1$$

$a = 0$



$a = 0$

$\tau = \frac{1}{a}$  is the time constant, the time when the response is 63.2% of the initial value.





## Response of a Standard 2nd order System

The transfer function of a second order system is often given as follows:

$$K = \omega_n^2$$

$$a = 2\zeta\omega_n$$

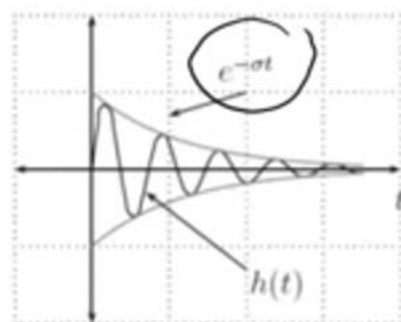
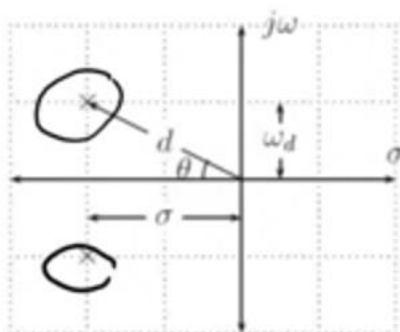
$$H(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2} = \frac{K}{s^2 + as + K}$$

It has two poles,  $s_{1,2} = -\zeta\omega_n \pm j\omega_n\sqrt{1-\zeta^2}$ . Here  $\omega_n$  is termed as natural frequency while  $\zeta$  is known as damping ratio or damping coefficient. Taking inverse Laplace transform, we get the following *impulse* response:

$$h(t) = \mathcal{L}^{-1}H(s) = \frac{\omega_n}{\sqrt{1-\zeta^2}} e^{-\sigma t} \sin(\omega_d t) u(t)$$

$$\omega_d = \frac{\sigma}{\zeta} = \frac{\zeta\omega_n}{\zeta} = \omega_n$$

where  $\sigma = \zeta\omega_n$  and  $\omega_d = \omega_n\sqrt{1-\zeta^2}$ .  $\omega_d$  is also called as frequency of transient oscillation.



$$d = \sqrt{\zeta^2\omega_n^2 + \omega_n^2(1-\zeta^2)}$$

$$= \sqrt{\omega_n^2} = \omega_n$$

$$\cos \theta = \frac{\zeta\omega_n}{\omega_n} = \zeta$$

$$\theta = \cos^{-1}\zeta$$



Step response: The output of the system with above transfer function is given by

$$Y(s) = H(s) \frac{1}{s} = \frac{\omega_n^2}{s(s^2 + 2\zeta\omega_n s + \omega_n^2)}$$

$$y(t) = 1 - e^{-\zeta\omega_n t} \left( \cos \omega_d t + \frac{\zeta\omega_n}{\omega_d} \sin \omega_d t \right)$$

$$= 1 - \frac{e^{-\zeta\omega_n t}}{\sqrt{1-\zeta^2}} \sin(\omega_d t + \theta)$$

$$\text{where } \theta = \cos^{-1} \zeta$$

rise time:  $t_r$

peak time =  $t_p$

Peak overshoot  $= M_p$

$t_s$  = settling time

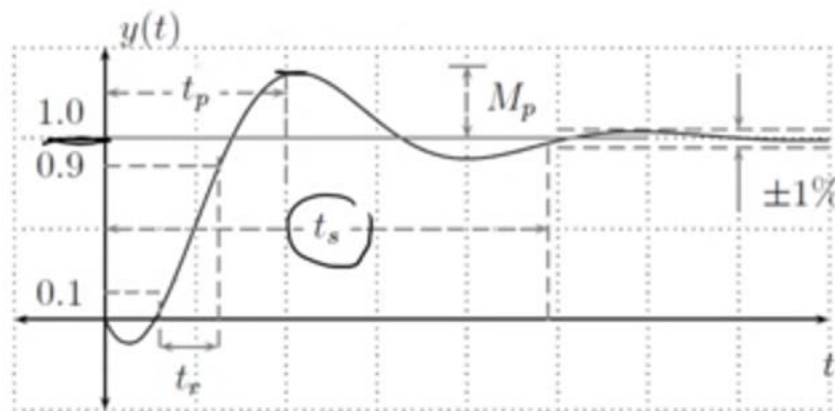
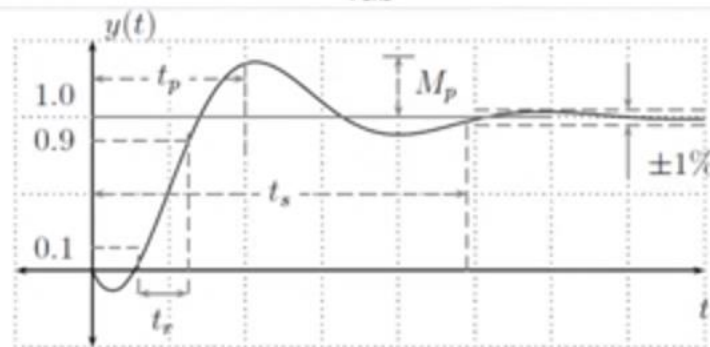


Figure 1: Time response of a second order system



- 16
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**Rise time ( $t_r$ ):** It is the time required by the output to go from 10% to 90% of the final value. The time it takes the response to reach the value 1 can be considered to be upper bound of  $t_r$ . This value can be obtained by making the sin term of the response vanish (zero).

$$1 - e^{-\zeta\omega_n t_r} \left( \cos \omega_d t_r + \frac{\zeta\omega_n}{\omega_d} \sin \omega_d t_r \right) = 1$$

$$\sin(\omega_n \sqrt{1-\zeta^2} t_r + \theta) = \sin \pi = 0$$

$$\omega_n \sqrt{1-\zeta^2} t_r + \theta = \pi$$

$\omega_n t_r + \theta = \pi$

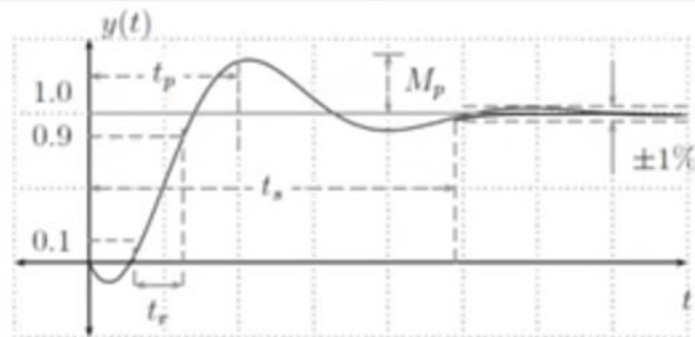
$$t_r = \frac{\pi - \cos^{-1} \zeta}{\omega_n \sqrt{1-\zeta^2}} \quad (\text{maximum value})$$

This is an upperbound. The actual value is obtained through empirical observation. For a system with  $\zeta = 0.5$ ,  $t_r$  can be approximated as  $t_r = \frac{1.8}{\omega_n}$ .





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- 19
- 20



$$y(t) = 1 - e^{-\sigma t} \sqrt{1 + \frac{\sigma^2}{\omega_d^2}} \cos(\omega_d t - \beta)$$

$\dot{y} = 0$   
 $t = t_p$

**Settling time ( $t_s$ ):** It is the time taken by the output to enter  $\pm 1\%$  band around the final value.

$$t_s = \frac{4.6}{\zeta \omega_n} \text{ for } \pm 1\% \text{ band}$$

$$= \frac{4}{\zeta \omega_n} \text{ for } \pm 2\% \text{ band}$$

**Peak Time ( $t_p$ ):** The time taken by the output to reach the maximum overshoot point.

$$t_p = \frac{\pi}{\omega_d}$$

$$\dot{y} = \frac{\zeta \omega_n}{\sqrt{1 - \zeta^2}} e^{-\zeta \omega_n t} \sin(\omega_n \sqrt{1 - \zeta^2} t + \theta) - \frac{e^{-\zeta \omega_n t}}{1 - \zeta^2} \cos(\omega_n \sqrt{1 - \zeta^2} t + \theta)$$

$$= \omega_n \frac{e^{-\zeta \omega_n t}}{1 - \zeta^2} (\sin(\omega_d t + \theta) \cos(\theta) - \cos(\omega_d t + \theta) \sin(\theta)) = 0$$

$$\Rightarrow \omega_n \frac{e^{-\zeta \omega_n t}}{1 - \zeta^2} (\sin(\omega_d t)) = 0$$

which gives

$$\omega_d t_p = \pi$$

$$\Rightarrow t_p = \frac{\pi}{\omega_d}$$



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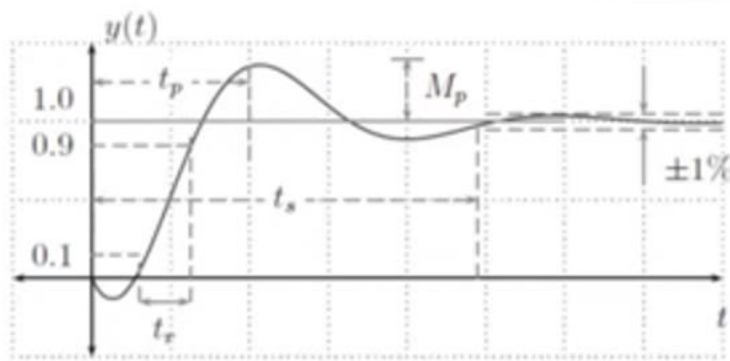


16

$$\begin{aligned} y(t_p) &= \left. 1 - e^{-\sigma t} \left( \cos \omega_d t + \frac{\sigma}{\omega_d} \sin \omega_d t \right) \right|_{t=t_p} \\ &= 1 - e^{-\frac{\pi \zeta}{\sqrt{1-\zeta^2}}} \left( \cos \pi + \frac{\sigma}{\omega_d} \sin \pi \right) \\ &= 1 + e^{-\frac{\pi \zeta}{\sqrt{1-\zeta^2}}} \end{aligned}$$

Thus, the maximum overshoot is given as

$$M_p = \frac{y(t_p) - 1}{1} = e^{-\frac{\pi\zeta}{\sqrt{1-\zeta^2}}}$$



Please note that the peak overshoot is ONLY a function of damping coefficient  $\zeta$ .

$$y(t) = 1 - \left( \frac{-\bar{a}b}{e^{\bar{a}-b^2}} \right) \sin(\omega_d t + \theta) \quad b=1$$

$\eta_1 = 0$  or  $h'$  is ally damped





First order System

Impulse response  $e^{-at}$

Step response  $(1 - e^{-at})$

$$\tau = 1/a \rightarrow 63.2\%$$

2<sup>nd</sup> order System step response

$$t_r \approx \frac{1.8}{\omega_n} \quad \zeta = 0.5 \quad \pm 1\%$$

$$t_p = \frac{\pi}{\omega_d} = \frac{\pi}{\omega_n \sqrt{1-\zeta^2}} \quad \pm 2\%$$

$$M_p = e^{-\frac{\pi \zeta}{\sqrt{1-\zeta^2}}}, \quad t_s = \frac{4.6}{\zeta \omega_n} \approx \frac{4}{\zeta \omega_n}$$

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Typically any  $n$ th  
order system after ~~the~~ being integrated  
with a compensator should behave  
~~like~~ like an ideal 2nd order system

$$G(s) = \frac{n(s)}{d(s)}, \quad C(s), \quad \text{and} \quad \text{Block Diagram}$$

Block Diagram: A feedback control system. The reference input  $C(s)$  is summed with the feedback signal. The error signal is then passed through a compensator block  $G(s)$ . The output  $Y(s)$  is fed back through a feedback path with gain  $\omega_n$  to the summing junction.

$$\frac{C(s)G(s)}{1 + C(s)G(s)}$$

18

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21

22