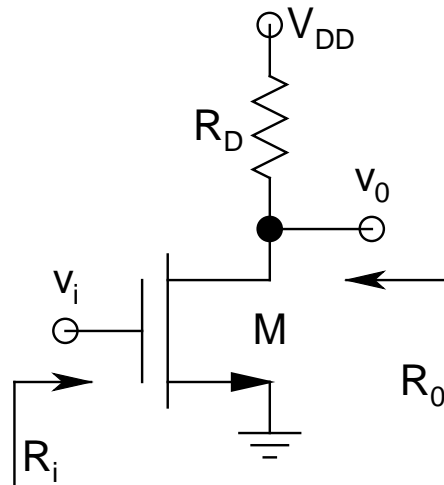
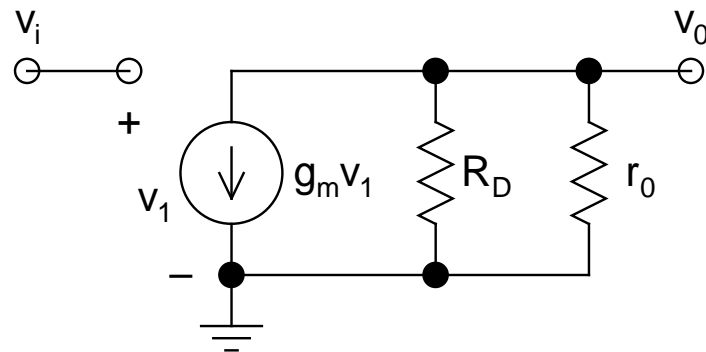


- **Common-Source (CS):**



ac Schematic



ac Low-Frequency Equivalent

- **Biasing circuit not shown**
- **Body at ground \Rightarrow No body effect**

- By inspection, ***Voltage Gain***:

$$A_v = \frac{V_o}{V_i} = \frac{-g_m V_1 (R_D \parallel r_o)}{V_i} = -g_m (R_D \parallel r_o)$$

- The ***negative sign*** in front implies ***180° phase shift*** between v_i and v_o
- ***v_i and v_o are exactly out of phase***
- For ***discrete circuits***, in general, $R_D \ll r_o$
- $\Rightarrow A_v = -g_m R_D$ (***moderate***)
- ***Input Resistance***: $R_i \rightarrow \infty$
- ***Output Resistance***: $R_o = R_D \parallel r_o \approx R_D$
- ***Note the remarkable similarity with CE stage***

➤ If $R_D \gg r_0$:

$$A_v = -g_m r_0 = -k_N V_{GT}/(\lambda I_D) = -2/[\lambda(\Delta V)]$$

(*assuming $\lambda V_{DS} < 0.1$*)

➤ Thus, *for small λ and small ΔV , A_v can be large*

▪ Keep in mind that $\Delta V(\min) = 3V_T$

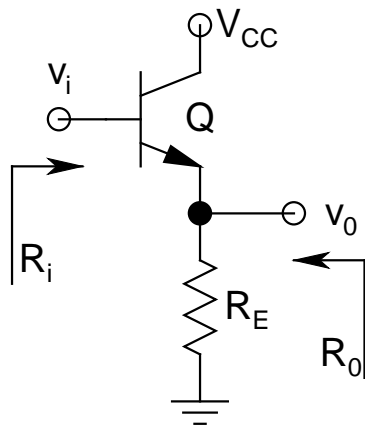
➤ Also, $A_v \propto 1/\sqrt{I_D}$

\Rightarrow *Lower I_D , higher A_v*

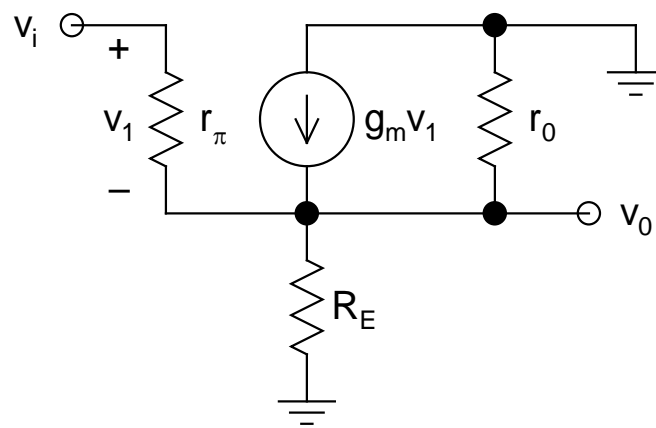
➤ **Recall:** For *CE stage*, $A_v(\max)$ was *independent of I_C* , and *dependent only on T*

- **Common-Collector (CC):**

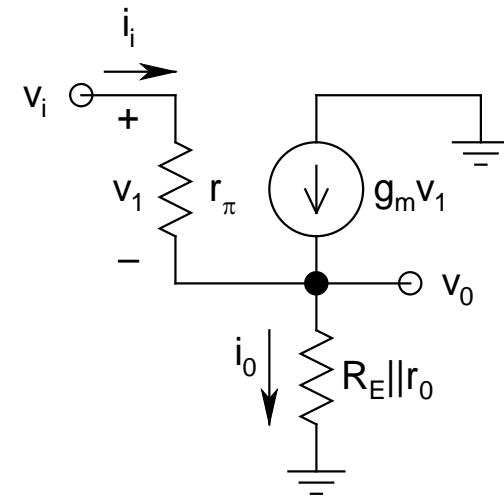
➤ Also known as **Emitter-Follower**



ac Schematic



ac Low-Frequency Equivalent



Simplified ac
Low-Frequency Equivalent

➤ **Biasing circuit not shown**

➤ *Voltage Gain:*

$$\begin{aligned} A_v &= \frac{v_o}{v_i} = \frac{i_o (R_E \parallel r_o)}{v_1 + v_o} = \frac{(\beta + 1) i_i (R_E \parallel r_o)}{i_i r_\pi + (\beta + 1) i_i (R_E \parallel r_o)} \\ &= \frac{R_E \parallel r_o}{r_\pi / (\beta + 1) + (R_E \parallel r_o)} = \frac{R_E \parallel r_o}{r_E + (R_E \parallel r_o)} \end{aligned}$$

➤ Now, in general, $r_o \gg R_E$

$$\Rightarrow A_v = R_E / (r_E + R_E)$$

➤ *Two important observations:*

- $A_v \leq 1$
- *No phase shift between v_i and v_o*