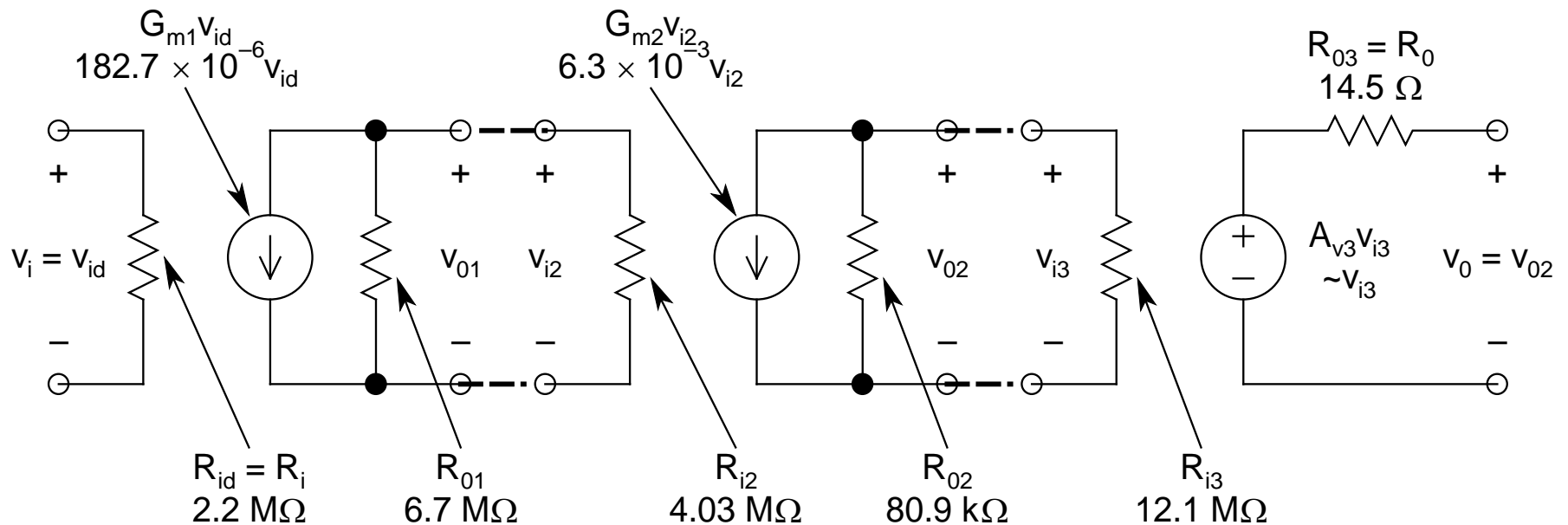


## ➤ *Overall Performance:*

- Just *cascade* the *2-port equivalents* of the *three stages*



## Complete 2-Port Representation of 741 Op-Amp

- *Voltage gain of the input stage:*

$$A_{v1} = v_{01}/v_{id} = -G_{m1}(R_{01}||R_{i2}) = -459.7$$

- *Voltage gain of the gain stage:*

$$A_{v2} = v_{02}/v_{01} = -G_{m2}(R_{02}||R_{i3}) = -506.3$$

- *Voltage gain of the output stage:*

$$A_{v3} \sim 1$$

- Thus, the *overall voltage gain* of *741 op-amp*:

$$\begin{aligned} A_{vOL} &= v_0/v_{id} = (v_0/v_{i3}) \times (v_{i3}/v_{i2}) \times (v_{i2}/v_{id}) \\ &= 2.33 \times 10^5 \text{ (107.3 dB)} \end{aligned}$$

*Note:*  $v_{i3} = v_{02}$ , and  $v_{i2} = v_{01}$

- This is an *excellent value*, in spite of the *significant loading effect* of the *gain stage* on the *input stage*

## ➤ *Observations:*

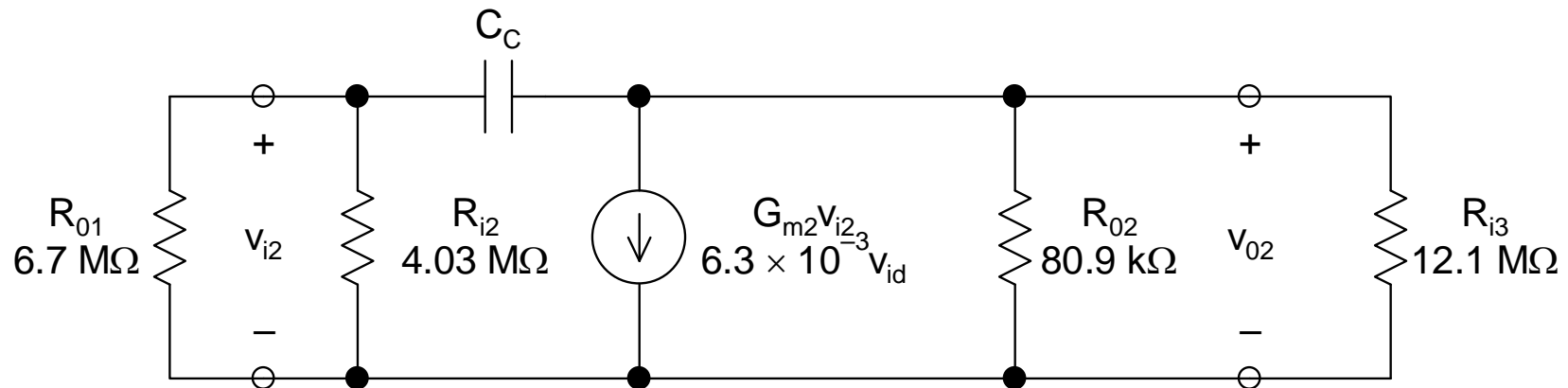
- $A_{vOL}$  is actually the *differential-mode gain* ( $A_{dm}$ )
- It is *positive*
  - ❖ *Positive  $v_{id}$*  produces *positive  $v_o$*
  - ❖ *Bases* of  $Q_1$  and  $Q_2$  are termed as *non-inverting (+)* and *inverting (-)* terminals respectively
- *Input and output resistances* are  $2.2\text{ M}\Omega$  and  $14.5\text{ }\Omega$  respectively, both of which are *excellent values*
- The *exact value* of  $A_{cm}$  is *slightly difficult to evaluate*, however, an *estimate of CMRR can be made*
- Using the *result* of our *simple analysis* of *DA*:  
$$CMRR \approx 2g_{m1}r_{o8} = 1923\text{ (66 dB)}$$
- This is not too bad!
  - ❖ *Actual value is much higher than this*

- *Compensation:*

- Actual evaluation of the *frequency response* characteristic of 741 is a *huge task*, even with the *ZVTC technique*
- There will be *numerous poles and zeros*, out of which, some will be *important*, while others will be *inconsequential*
- However, there will of course be a *Dominant Pole* (DP), and rough calculation shows that it is  $\sim 1\text{ MHz}$ , which is the *bandwidth* of the *uncompensated op-amp*

- Now, ~ *100 dB open-loop gain* with *1 MHz bandwidth* is a *ready recipe for disaster* as far as the *stability of the system* is concerned
- Hence, for *unconditional stability* under *unity negative feedback*, e.g., *voltage follower*, *compensation is imperative*
- In 741, this task is accomplished by the technique of *Dominant Pole Compensation* (DPC) through the use of the *compensation capacitor*  $C_C$ , *connected between the input and output of the gain stage*

- To obtain the *required value* of  $C_C$ , we use the cascade of the *2-port networks*, as was done earlier to compute the *overall voltage gain*



- Denote  $R' = R_{01} \parallel R_{i2} = 2.5 \text{ M}\Omega$   
and  $R'' = R_{02} \parallel R_{i3} = 80.4 \text{ k}\Omega$

- The *simplified circuit* can be easily identified as the *three-legged creature*, and using the *ZVTC technique*:

$$R_C^0 = R' + R'' + G_{m2} R' R'' = 1.27 \text{ G}\Omega$$

- Now, to get an estimate of the *DPF*  $f_d$ , we assume that the *open-loop gain* is exactly 100 dB, and the *first pole* of the *uncompensated op-amp* is *exactly 1 MHz*

$$\Rightarrow f_d = 10 \text{ Hz}$$

- Also,  $f_d = \omega_d / (2\pi)$ , with  $\omega_d = 1/\tau$ , and  $\tau = R_C^0 C_C$