

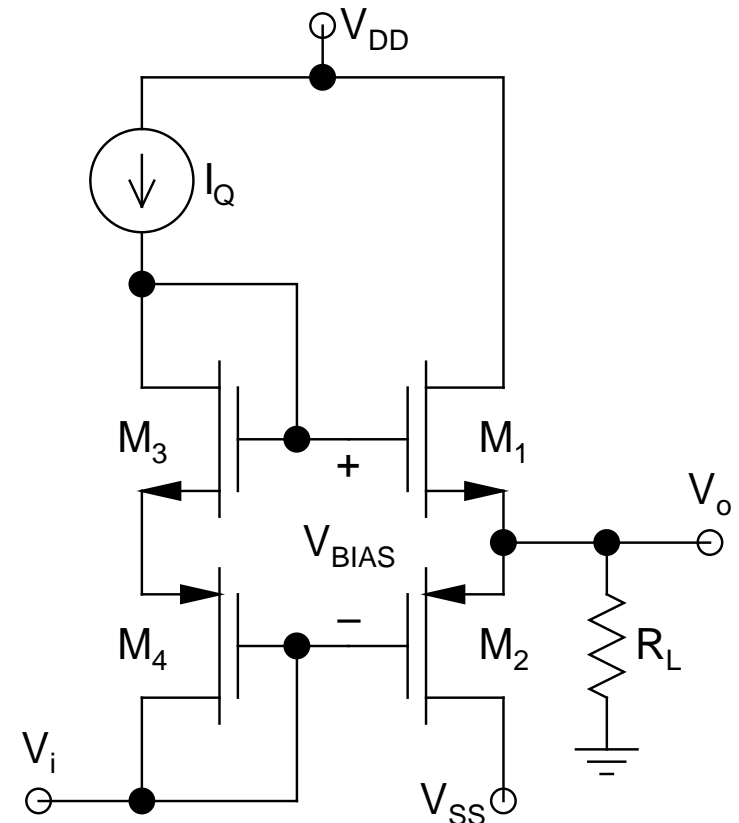
➤ *Summary:*

- *Quite small standby power*
- *Large current driving capability*
- *Almost linear VTC*
- *Very low distortion at the output*
- $A_v \sim 1$
- *No phase shift between input and output*
- *Very low output resistance*

*Thus, this stage is a superb one and is highly popular!*

- ***MOS Implementation:***

- *Biased using dual symmetric power supplies  $V_{DD}/V_{SS}$*
- *$M_1$ - $M_2$  in push-pull configuration*
  - *$M_1$  supplying current to load ( $R_L$ ) during the positive half cycle*
  - *$M_2$  pulling current away from load during the negative half cycle*



**Circuit Schematic**

- $M_1$ - $M_2$  *prebiased* by the *series combination* of  $M_3$ - $M_4$  (*both diode-connected*) *biased with  $I_Q$*
- *Develops  $V_{BIAS}$  across the gates of  $M_3$ - $M_4$* , which is *same as that between the gates of  $M_1$ - $M_2$*
- *$V_{BIAS}$  chosen to be slightly less than  $(V_{TN} + |V_{TP}|)$*
- *Crossover Distortion eliminated completely*, at the cost of *introducing standby power* into the system
- *Rest of the operation of the circuit exactly similar to that of a BJT Class AB Push-Pull Output Stage*

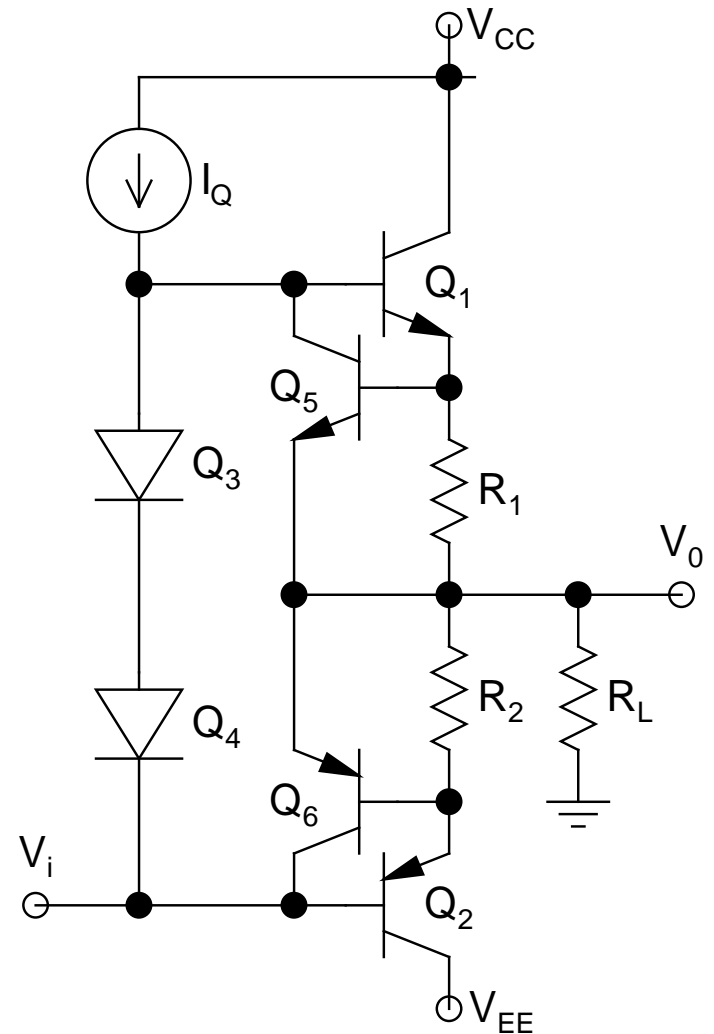
- *All transistors suffer from body effect problem*  
⇒ *More distortion at the output*
- *The linearity of the VTC is not that good*
- *Low current drive capability*
- *Biasing itself becomes tricky*, due to the *body effect of  $M_3$ - $M_4$*
- The *output resistance not that low*, since *MOSFETs have lower  $g_m$  than BJTs*
- Overall, the stage *suffers from quite a few problems* and is *not used much*
- We will explore this through an assignment

- **Overload Protection:**

- *Protects the output stage from accidental short-circuits*

- *Needs 4 more components:*

- **2 BJTs** ( $Q_5, Q_6$ )
- **2 Resistors** ( $R_1, R_2$ )  
 $R_1, R_2 \sim 25\text{-}50\ \Omega$



**Circuit Schematic**

- During *normal operation*, these *extra circuits* play absolutely *no role*, and come *into picture* only under *accidental short-circuit* of the *output terminal to ground*
- *Numerical Example:*
  - Assume  $V_i$  at its *positive peak*, the *maximum drive current* to the base of  $Q_1 = 1 \text{ mA}$ , and  $\beta_1 = 100$
  - Now output gets *accidentally shorted to ground* ( $V_o = 0$ )  
 $\Rightarrow I_{c1} = 100 \text{ mA}$  and  $V_{ce1} = 5 \text{ V}$   
 $\Rightarrow P_1 = 500 \text{ mW}$
  - This may be *way above* the *maximum power rating* of the transistor ( $\sim 100\text{-}150 \text{ mW}$ ) and the transistor would *burn out*  $\Rightarrow$  *potentially dangerous situation!*

➤ *Principle of Operation of the Protection Circuit:*

- Assume *positive*  $V_i$  with  $Q_1$  *supplying current to load*
- *$Q_2$  is off during this time*
- As  $R_L \downarrow$ ,  $I_{c1} \uparrow$  (since  $I_{c1} = V_o/R_L$ )  
 $\Rightarrow V_{be5} (= I_{c1}R_1)$  *also*  $\uparrow$
- As  $V_{be5} \rightarrow V_\gamma$  of  $Q_5$ , it starts to *turn on*  
 $\Rightarrow$  A *part of base drive current* of  $Q_1$  starts to get *shunted away* by  $Q_5$ , and *appears at the output* almost *without any gain* ( $1/\alpha_5$ )
- This acts as a *limit of the rate* at which the *output current can increase*, and thus, *protects the circuit*

- Thus, the *current can't increase indefinitely*
- Assume  $R_1 = 30\ \Omega$  and  $V_\gamma = 0.6\ V$   
 $\Rightarrow$  As soon as  $I_{c1}$  reaches about  $20\ mA$ ,  $Q_5$  cuts in, shunts current away from the base of  $Q_1$ , and protects the circuit
- Due to the exponential dependence of this shunted current on  $V_{be5}$ , the maximum output current will saturate near around  $20\ mA$  itself
- Thus, under this case, if the output is accidentally shorted to ground, then  $P_1(max)$  will be around  $100\ mW$ , which is well within limit, and protection will be achieved