

Please work on this sheet and the reverse. No extra sheet would be given.

Total marks: 10 Name:

Roll No.:

- (1) An R-C coupled amplifier is shown in fig. 1, which uses a BJT transistor of current gain (β) of 50. The d.c. collector current is 2mA. Assume that a conducting diode voltage is 0.7V and the thermal voltage is $V_T = 0.025V$.

- [2] (a) Find the values of R_1 and R_2 that would bias the transistor in the forward active mode.
[2] (b) Calculate the voltage gain of the amplifier $A_v = (v_o/v_i)$. *mid band.*
[2] (c) What is the lower cut-off frequency of the amplifier?

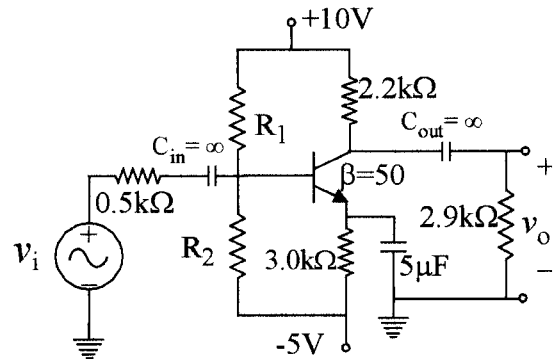


Figure 1.

- (2) For the OpAmp circuit shown in fig. 2, supplied with a $\pm 10V$ sources, where it is required to plot the output voltage V_o as a function of the potentiometer position of the variable resistor R_g . The OpAmp can be assumed to be ideal.

- [2] (i) Hence find an expression of V_o , as a function of α .
[2] (ii) What is V_o , at $\alpha = 0$, $\alpha = 0.5$, and $\alpha = 1$?

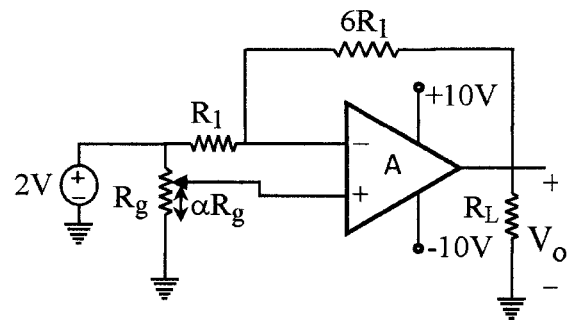


Figure 2.

1) (a) $I_{CQ} = 2 \text{ mA}$, $\beta = 50 \therefore I_B = (2/50) \text{ mA} = 0.04 \text{ mA} = 40 \mu\text{A}$.
 \therefore Choose $I_{R1} = 10 I_B = 0.4 \text{ mA}$.
 $V_C = 10 - 2.2 \text{ k} \times 2 \text{ m} = 5.6 \text{ V}$, $V_E \approx 3 \text{ k} \times 2 \text{ m} - 5 \text{ V} = +1 \text{ V}$. $\therefore V_B = 1 + 0.7 = 1.7 \text{ V}$.
 $V_{R1} = 10 - 1.7 = 8.3 \text{ V} \therefore R_1 = \frac{V_{R1}}{I_{R1}} = \frac{8.3}{0.4 \text{ m}} = 20.75 \text{ k}\Omega$
 Similarly $V_{R2} = 1.7 - (-5) = 6.7 \text{ V} \therefore R_2 = \frac{6.7}{9 \times 0.04 \text{ m}} = 18.61 \text{ k}\Omega$
 (b) For the a.c. model $R_B = R_1 \parallel R_2 = 20.75 \parallel 18.61 = 9.81 \text{ k}\Omega$
 a.c. model.

 $r_e = \frac{V_T}{I_C} = \frac{0.025}{2 \text{ m}} = 0.0125 \text{ k}\Omega$
 $r_\pi = (\beta + 1) r_e = 51 \times 0.0125 = 0.6375 \text{ k}\Omega$
 Since R_E is bypassed by CE $g_m = \frac{I_C}{V_T} = \frac{2 \text{ m}}{25 \text{ mV}} = 0.08 = 80 \text{ mS}$.
 $R_L = 2.2 \text{ k} \parallel 2.9 \text{ k} = 1.251 \approx 1.25 \text{ k}\Omega$, $A_v = \frac{v_o}{v_i} = -g_m R_L \times \frac{R_B \parallel r_\pi}{0.5 \text{ k} + R_B \parallel r_\pi}$
 $\therefore R_B \parallel r_\pi = 9.8 \text{ k} \parallel 0.6375 \text{ k} = 0.5986 \approx 0.6 \text{ k}\Omega$
 $\therefore A_{v_{mid}} = -80 \text{ m} \times 1.25 \text{ k} \times \frac{0.6}{0.5 + 0.6} = -100 \times 0.545 = -54.5$
 Approximate: Neglect R_B with respect to $r_\pi \rightarrow A_{v_{mid}} = -100 \times \frac{0.6375}{1.1375} = -56$

2) For ideal OpAmp $i_- = i_+ = 0$, $V_- = V_+$

$$\therefore V_+ = \frac{2V}{R_g} \times \alpha R_g = 2\alpha V = V_-$$

KCL at node V_- gives $\frac{V_- - 2}{R_1} + \frac{V_- - V_o}{6R_1} = 0$.

$$\text{or } 6V_- - 12 + V_- = V_o. \text{ or } V_o = 7V_+ - 12$$

$$\therefore V_o = 7 \times 2\alpha - 12 = 14\alpha - 12.$$

$\alpha = 0$, $V_o = -12$, but supply is only $-10V$
 \therefore due to saturation $V_o = -10V$

$$\alpha = 0.5, V_o = 14 \times 0.5 - 12 = 7 - 12 = \underline{\underline{-5V}}$$

$$\alpha = 1, V_o = 14 - 12 = \underline{\underline{+2V}},$$

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(1) An R-C coupled amplifier is shown in fig. 1, which uses a BJT transistor of current gain (β) of 80. The d.c. collector current is 2mA. Assume that a conducting diode voltage is 0.7V and the thermal voltage is $V_T = 0.025V$.

- [2] (a) Find the values of R_1 and R_2 that would bias the transistor in the forward active mode.
 [2] (b) Calculate the voltage gain of the amplifier $A_v = (v_o/v_i)$. *mid band*
 [2] (c) What is the lower cut-off frequency of the amplifier?

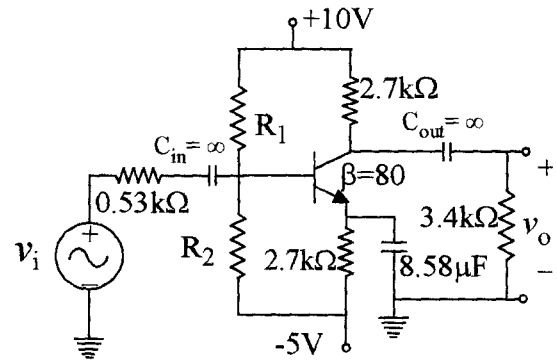


Figure 1.

(2) For the OpAmp circuit shown in fig. 2, supplied with a $\pm 8V$ sources. It is required to know the output voltage V_o as a function of the potentiometer position of the variable resistor R_g . The OpAmp can be assumed to be ideal.

- [2] (i) Hence find an expression of V_o , as a function of α .
 [2] (ii) What is V_o , at $\alpha = 0$, $\alpha = 0.5$, and $\alpha = 1$?

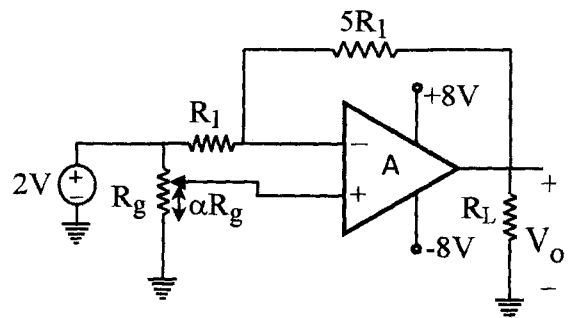
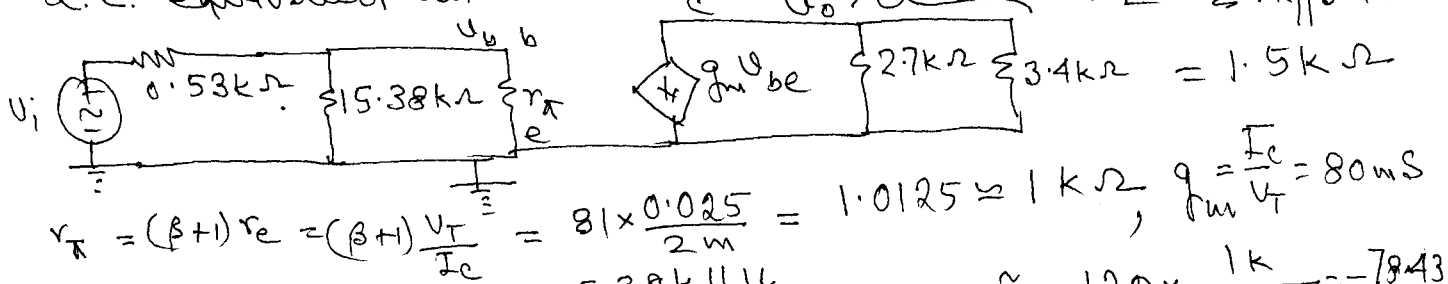


Figure 2.

1) (a) $V_c = 10.2m \times 2.7k = 10.5.4 = 4.6V$
 $V_E = 2.7k \times 2m - 5 = 0.4V$ $V_B = 0.4 + 0.7 = 1.1V$ $V_{R1} = 10 - 1.1 = 8.9V$
 $V_{R2} = 1.1 + 5 = 6.1V$
 Choose $I_{R1} = 10I_B$ & $I_{R2} = 9I_B$ where $I_B = \frac{2m}{80} = 0.025m = 25\mu A$.
 $\therefore R_1 = \frac{8.9}{250\mu} = 35.6k\Omega$, $R_2 = \frac{6.1}{9 \times 25\mu} = 27.1k\Omega$, $R_B = R_1 || R_2 = 15.38k\Omega$

(b) As R_E is by-passed by C_E everywhere except at low frequencies, a.c. equivalent is:



$r_{\pi} = (\beta + 1)r_e = (\beta + 1)\frac{V_T}{I_c} = 81 \times \frac{0.025}{2m} = 1.0125 \approx 1k\Omega$, $g_m = \frac{I_c}{V_T} = 80ms$
 $A_{v_{mid}} = -80m \times 1.5k \times \frac{15.38k || 1k}{0.53k + 15.38k || 1k} \approx -120 \times \frac{1k}{1.53k} = -78.43$

Exact: $= -120 \times \frac{0.94}{0.53 + 0.94} = -120 \times 0.64 = -76.8$

(c) C_{in} & C_{out} capacitors have no effect. $\therefore f_L = \frac{1}{2\pi C_E R_{C_{E_{short}}}}$ with C_E shorted.
 $R_{C_{E_{short}}} = R_E || \left(\frac{r_{\pi} + R_B || R_1}{\beta + 1} \right) = 2.7k || \frac{1.51k}{81} = 2.7k || 0.0185k = 0.0184k$
 $R_B || R_1 = 15.38k || 0.53k \approx 0.51k$
 $f_L = \frac{1}{2\pi \times 8.58 \times 0.0184} = 9736Hz$

Approx: neglect 15.38k with respect to 0.53k
 $(1 + 0.53/81) \approx 0.019k$ neglect 2.7k with respect to this
 $\therefore R_{C_{E_{short}}} \approx 0.019k$
 $f_L \approx \frac{1}{2\pi \times 8.58 \times 0.019} = 9736Hz$

2) For ideal OpAmp $i_- = i_+ = 0$, $V_- = V_+$

$$V_+ = \frac{2V}{R_g} \times \alpha R_g = 2\alpha V = V_-$$

\therefore KCL at V_- node gives $\frac{V_- - 2}{R_1} + \frac{V_- - V_o}{5R_1} = 0$

$$\text{or } 5V_- - 10 = -V_- + V_o \therefore V_o = 6V_- - 10$$

$$\text{or } V_o = 6V_+ - 10 = 6 \times 2\alpha - 10 = 12\alpha - 10.$$

$$\alpha = 0, V_o = -10 \text{ but supply is at } -8. \therefore V_o(\alpha=0) = \underline{\underline{-8V}}$$

$$\alpha = 0.5, V_o = 12 \times 0.5 - 10 = 6 - 10 = \underline{\underline{-4V.}}$$

$$\alpha = 1, V_o = 12 - 10 = \underline{\underline{+2V.}}$$