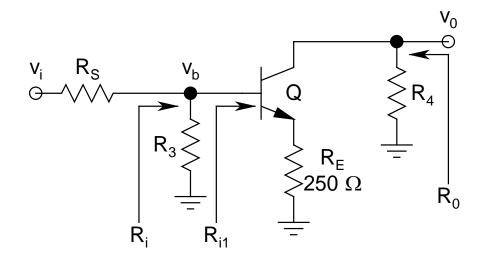
- Now let's explore what happens if C_E were absent, i.e., R_E unbypassed
- > Redraw the *ac schematic*:

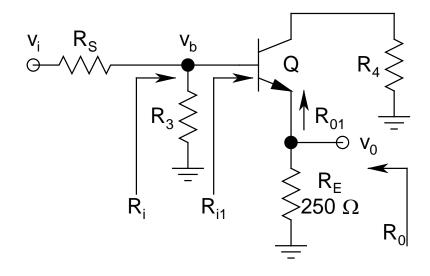


ac Midband Schematic for R_F unbypassed

- Note: Degeneration Factor = $(1 + g_m R_E) \approx (1 + R_E/r_E) = 20.23$
- $ightharpoonup R_{i1} = r_{\pi} + (\beta + 1)R_{E} = 26.55 \text{ k}\Omega$
 - Exactly 20.23 times of the previous case $(1.3 \text{ k}\Omega)$
- $ightharpoonup R_i = R_{i1} || R_3 = 6.72 \text{ k}\Omega$
- \triangleright Total resistance *seen* by $v_i = R_S + R_i = 7.72 \text{ k}\Omega$
- $v_0/v_b = -R_4/(r_E + R_E) = -7.6 \ [CE(D) \ Stage]$
 - Reduced by exactly 20.23 times of the previous case (-153.85)
- $v_b/v_i = R_i/(R_i + R_S) = 0.87$
 - *Improvement as compared to previous case* (0.533)

- $A_{\rm v} = -6.6$
 - Compare with −82 obtained in previous case (significant reduction)
- $ightharpoonup R_0 \approx R_4 = 2 \text{ k}\Omega \text{ (if } r_0 \text{ is neglected)}$
- > If r_0 is considered, analysis becomes significantly complicated, since the Golden Rule can't be applied due to the presence of resistance (apart from r_{π}) in the base of Q
- > Summary:
 - $A_v = -6.6$
 - $R_i = 6.72 \text{ k}\Omega$
 - Resistance *seen* by $v_i = 7.72 \text{ k}\Omega$
 - $R_0 = 2 k\Omega$

- > What if the output is taken from emitter?
- > Redraw the *ac schematic*:



ac Midband Schematic for Output Taken from Emitter

- $ightharpoonup R_4$ actually redundant for this case (collector of Q could have been connected to V_{CC} directly)
- $ightharpoonup R_{i1} = 26.55 \text{ k}\Omega$, $R_i = 6.72 \text{ k}\Omega$, and resistance seen by $v_i = 7.72 \text{ k}\Omega$ (same as before)
- $v_0/v_b = R_E/(r_E + R_E) = 0.95 (CC Stage)$
- $> v_b/v_i = R_i/(R_i + R_S) = 0.87$ (same as before)
- $ightharpoonup A_v = 0.827$ (<1, as expected, but *could have* been made closer to unity by better design!)
- $> R_0 = R_E ||R_{01}||$
- \succ Computation of R_{01} is slightly more involved, but quite easy if the trick is understood!