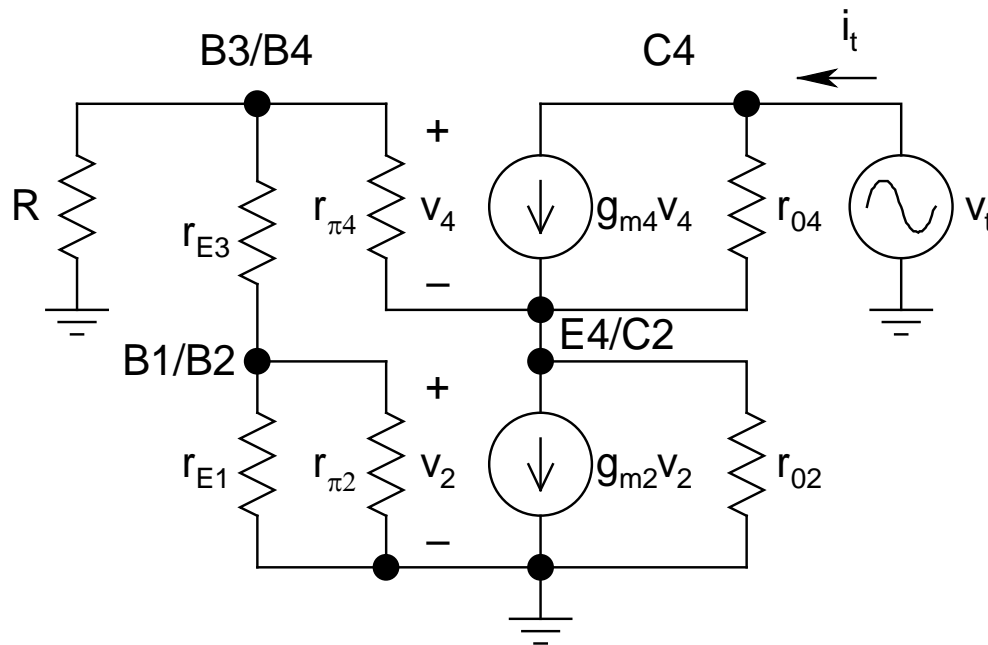


➤ *Calculation of R_o :*

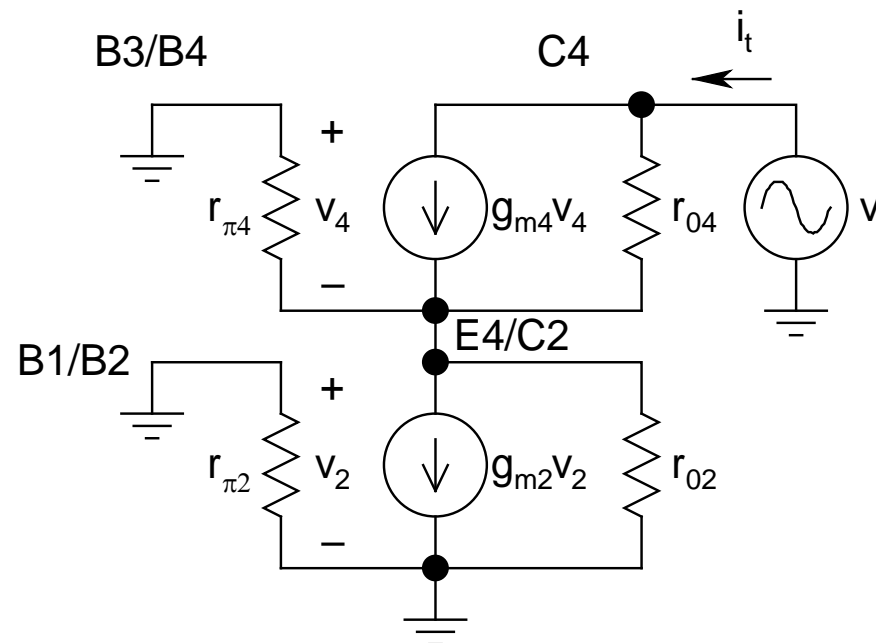


Exact Equivalent

- *Q_1 and Q_3 diode-connected $\Rightarrow r_{E1}$ and r_{E3}*

➤ ***Simplification:***

- *Bases of Q_1 - Q_2 and Q_3 - Q_4 can be approximated to be at ac ground (a first-order estimate)*

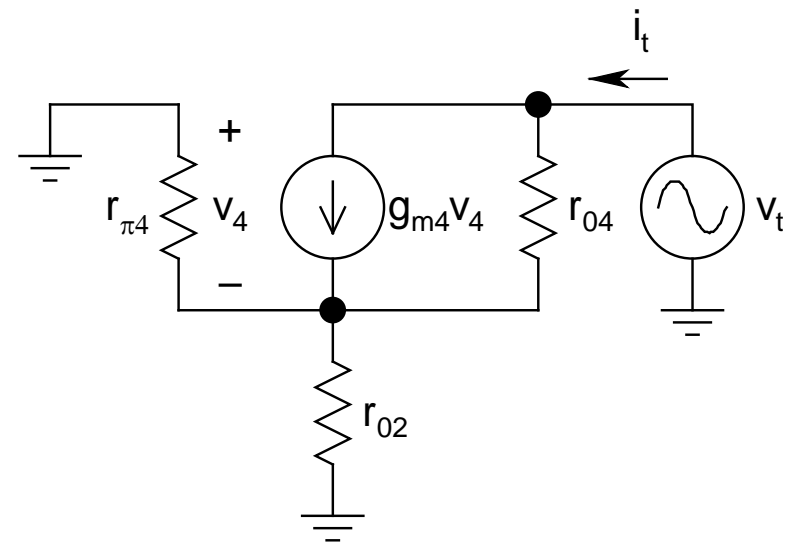


Equivalent after First-Order Simplification

- $\Rightarrow v_2 = 0 \Rightarrow g_{m2}v_2 = 0$
 \Rightarrow Leads to the *simplified equivalent* (looks familiar?)

- *By inspection:*
 $R_0 \approx r_{o4}(1 + g_{m4}r_{\pi4})$
 $\approx \beta_4 r_{o4}$
(assuming $r_{o2} \gg r_{\pi4}$)

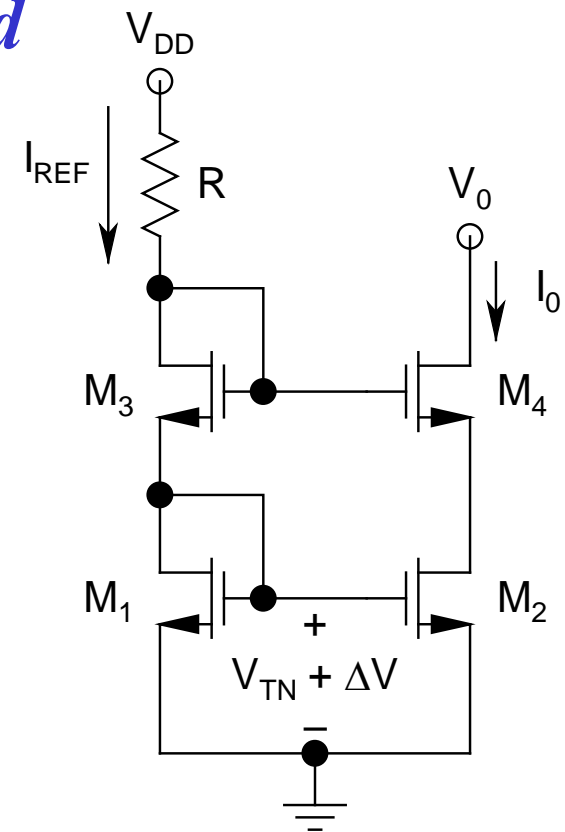
- *Actual analysis gives:*
 $R_0 = \beta_4 r_{o4}/2$ (*large error!*)



Simplified Equivalent

- **NMOS Cascode:**

- *All Ms perfectly matched*
- *All bodies connected to ground*
 - *M_1 - M_2 does not have body effect, but M_3 - M_4 does!*
 - *Makes hand analysis quite tedious*
 - ⇒ *Neglect body effect*
- *All Ms operate with same V_{GS}*
- Define $\Delta V = V_{GS} - V_{TN} = V_{GT}$
 - $\Delta V =$ *Gate Overdrive*



➤ *The reference current:*

$$I_{\text{REF}} = \frac{V_{\text{DD}} - 2V_{\text{GS}}}{R} = \frac{k_{\text{N}}}{2} V_{\text{GT}}^2 \quad (\text{neglecting } \lambda)$$

➤ *V_{GS} and I_{REF} can be found $\Rightarrow I_0 = I_{\text{REF}}$*

➤ $V_{\text{G1}} = V_{\text{G2}} = V_{\text{GS}} = V_{\text{TN}} + \Delta V$

➤ $V_{\text{G3}} = V_{\text{G4}} = 2V_{\text{GS}} = 2(V_{\text{TN}} + \Delta V)$

➤ $V_{\text{S4}} = V_{\text{D2}} = V_{\text{TN}} + \Delta V$

$$\Rightarrow V_{\text{GS2}} = V_{\text{DS2}}$$

$\Rightarrow M_2$ can never enter linear region

$$\Rightarrow V_{0,\text{min}} = V_{\text{DS2}} + V_{\text{DS4}} = V_{\text{TN}} + 2\Delta V$$