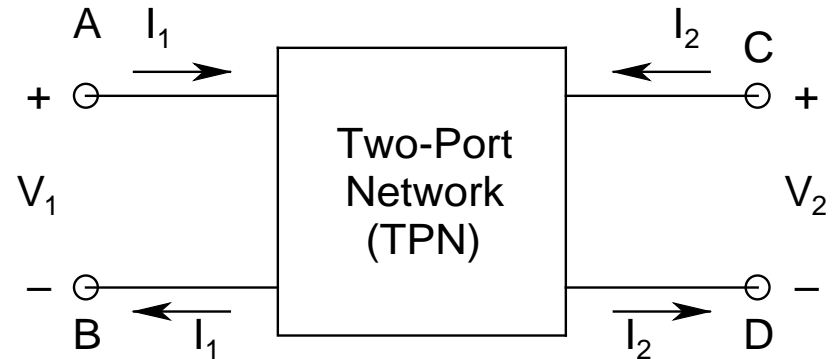


Two-Port Network (TPN)

* *Four Variables:*

- Input voltage V_1
- Input current I_1
- Output voltage V_2
- Output current I_2



- * The network within the box is known as the ***TPN***
- * It must be a ***linear*** network, i.e., it should contain only linear elements, so that ***superposition*** principle can be applied
- * There should be ***no connection*** between A/B and C/D

- * Current *entering* the TPN through terminal A must *equal* the current *leaving* through terminal B
- * Similarly, current *entering* through terminal C must *equal* the current *leaving* through terminal D
- * The TPN must *not* contain any *independent source*
- * It may contain *dependent sources*, however, the *controlling parameter* of the dependent source must be *within* the TPN
- * The TPN is treated as a *black box* with the external current-voltage relations expressed by a set of TPN *parameters*

- * There are various types of *representations* of *TPN parameters*
- * We will discuss the *three* most important ones:
 - *Admittance Parameter (y-Parameter)*
 - *Impedance Parameter (z-Parameter)*
 - *Hybrid Parameter (h-Parameter)*
- * Typically expressed in a *matrix form*:

$$[X] = \begin{bmatrix} X_{11} & X_{12} \\ X_{21} & X_{22} \end{bmatrix}, \text{ where } x \text{ is } y, z, \text{ or } h$$

y-Parameters:

* I-V relations expressed as:

$$I_1 = y_{11} V_1 + y_{12} V_2$$

$$I_2 = y_{21} V_1 + y_{22} V_2$$

V_1, V_2 : ***Independent*** variables

I_1, I_2 : ***Dependent*** Variables

$$y_{11} = \text{short-circuit input admittance} = \left. \frac{I_1}{V_1} \right|_{V_2=0}$$

y_{12} = ***short-circuit (output to input) transfer***

$$\text{admittance} = \left. \frac{I_1}{V_2} \right|_{V_1=0}$$

$y_{21} = \text{short-circuit (input to output) transfer}$

$$\text{admittance} = \left. \frac{I_2}{V_1} \right|_{V_2=0}$$

$$y_{22} = \text{short-circuit output admittance} = \left. \frac{I_2}{V_2} \right|_{V_1=0}$$

- * **Note:** $y_{12} = y_{21}$ is not a *necessary* condition
- * Networks with $y_{12} = y_{21}$ are known as *bilateral*
- * Generally *purely resistive* networks are *bilateral*
- * Networks with $y_{12} \neq y_{21}$ are known as *unilateral*
- * Generally *unilateral* networks have *active elements* and/or *dependent sources* within the network

Example: To find *y*-parameters for the resistive network (known as the *π*-network)

$$y_1 = 1/R_1 = 0.2 \text{ } \mathfrak{U}$$

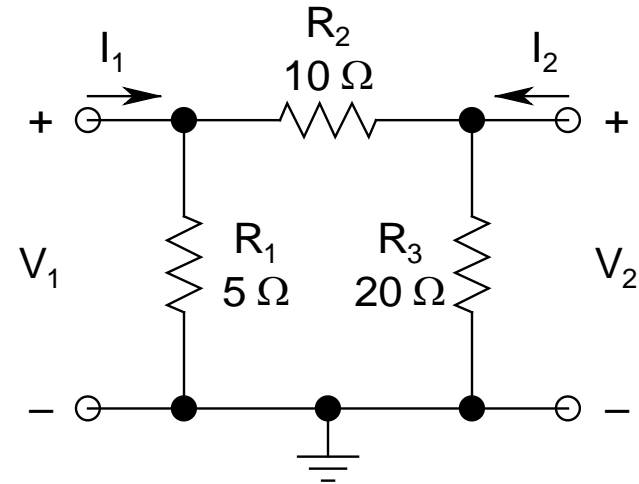
$$y_2 = 1/R_2 = 0.1 \text{ } \mathfrak{U}$$

$$y_3 = 1/R_3 = 0.05 \text{ } \mathfrak{U}$$

$$\begin{aligned} I_1 &= y_1 V_1 + y_2 (V_1 - V_2) \\ &= (y_1 + y_2) V_1 - y_2 V_2 \end{aligned}$$

$$I_2 = y_2 (V_2 - V_1) + y_3 V_2 = -y_2 V_1 + (y_2 + y_3) V_2$$

$$\text{Thus, } [y] = \begin{bmatrix} y_1 + y_2 & -y_2 \\ -y_2 & y_2 + y_3 \end{bmatrix} = \begin{bmatrix} 0.3 & -0.1 \\ -0.1 & 0.15 \end{bmatrix} \mathfrak{U}$$



z-Parameters:

* I-V relations expressed as:

$$V_1 = z_{11}I_1 + z_{12}I_2$$

$$V_2 = z_{21}I_1 + z_{22}I_2$$

I_1, I_2 : ***Independent*** Variables

V_1, V_2 : ***Dependent*** Variables

$$z_{11} = \textit{open-circuit input impedance} = \left. \frac{V_1}{I_1} \right|_{I_2=0}$$

$z_{12} = \textit{open-circuit (output to input) transfer}$

$$\textit{impedance} = \left. \frac{V_1}{I_2} \right|_{I_1=0}$$

$z_{21} = \textit{open-circuit (input to output) transfer}$

$$\textit{impedance} = \left. \frac{V_2}{I_1} \right|_{I_2=0}$$

$$z_{22} = \textit{open-circuit output impedance} = \left. \frac{V_2}{I_2} \right|_{I_1=0}$$

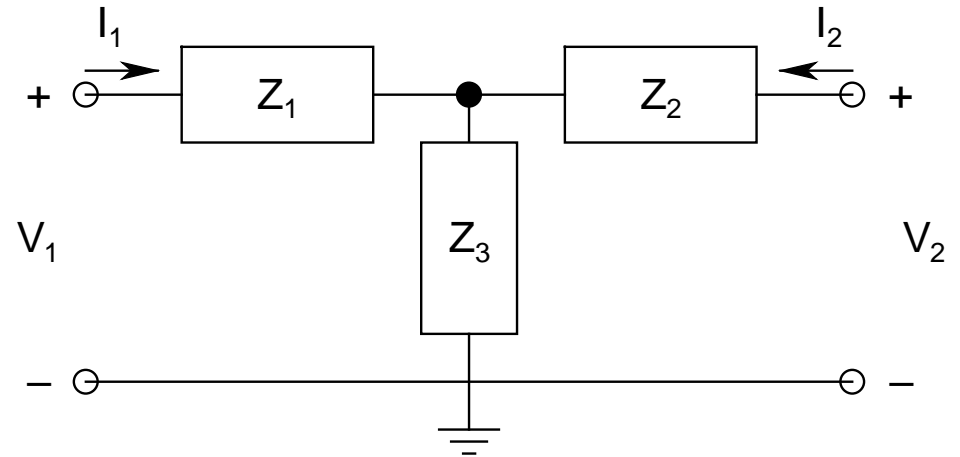
- * Again, only for a ***bilateral*** network, $z_{12} = z_{21}$, otherwise not
- * Also, ***caution*** that for a given network $z_{ij} \neq 1/y_{ij}$

Example: To find *z*-parameters for the network
(known as the ***T*-network**)

$$\begin{aligned} V_1 &= Z_1 I_1 + Z_3 (I_1 + I_2) \\ &= (Z_1 + Z_3) I_1 + Z_3 I_2 \\ V_2 &= Z_2 I_2 + Z_3 (I_1 + I_2) \\ &= Z_3 I_1 + (Z_2 + Z_3) I_2 \end{aligned}$$

$$\text{Thus, } [z] = \begin{bmatrix} Z_1 + Z_3 & Z_3 \\ Z_3 & Z_2 + Z_3 \end{bmatrix}$$

All T-networks are bilateral



Transformation Relations Between y - and z -Parameters:

$$* \ y_{11} = \frac{Z_{22}}{\Delta Z}, \ y_{12} = -\frac{Z_{12}}{\Delta Z}, \ y_{21} = -\frac{Z_{21}}{\Delta Z}, \ y_{22} = \frac{Z_{11}}{\Delta Z}$$

$$\text{with } \Delta Z = \begin{vmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{vmatrix}$$

$$* \ z_{11} = \frac{Y_{22}}{\Delta Y}, \ z_{12} = -\frac{Y_{12}}{\Delta Y}, \ z_{21} = -\frac{Y_{21}}{\Delta Y}, \ z_{22} = \frac{Y_{11}}{\Delta Y}$$

$$\text{with } \Delta Y = \begin{vmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{vmatrix}$$

* **Note:** While *y -parameter* representation is preferred for *π -networks*, *z -parameter* representation is the choice for *T -networks*

h-Parameters:

* I-V relations expressed as:

$$V_1 = h_{11}I_1 + h_{12}V_2$$

$$I_2 = h_{21}I_1 + h_{22}V_2$$

I_1, V_2 : ***Independent*** Variables

V_1, I_2 : ***Dependent*** Variables

$$h_{11} = \textit{short-circuit input impedance} = \left. \frac{V_1}{I_1} \right|_{V_2=0}$$

$$h_{12} = \textit{open-circuit reverse voltage gain} = \left. \frac{V_1}{V_2} \right|_{I_1=0}$$

$$h_{21} = \textit{short-circuit forward current gain} = \left. \frac{I_2}{I_1} \right|_{V_2=0}$$

$$h_{22} = \textit{open-circuit output admittance} = \left. \frac{I_2}{V_2} \right|_{I_1=0}$$

- * These are known as *hybrid* parameters, since they involve both *voltages and currents*, with h_{12} and h_{21} being *dimensionless* quantities, while h_{11} and h_{22} have units of Ω and \mathcal{U} respectively
- * In contrast, note that all *y-parameters* are expressed in \mathcal{U} , while all *z-parameters* are expressed in Ω

Example: To find *h*-parameters for the *transistor* (*BJT*) equivalent circuit (*low-frequency hybrid- π*):

r_{π} : **Input Resistance**

r_o : **Output Resistance**

β : **Current Gain**

$$V_1 = r_{\pi} I_1$$

$$I_2 = \beta I_1 + g_o V_2$$

$g_o = 1/r_o$ = **Output Conductance**

$$\text{Thus, } [h] = \begin{bmatrix} r_{\pi} & 0 \\ \beta & g_o \end{bmatrix}$$

