The *simplified circuit* can be easily identified as the *three-legged creature*, and using the *ZVTC technique*:

$$R_C^0 = R' + R'' + G_{m2}R'R'' = 1.27 G\Omega$$

Now, to get an estimate of the *DPF* f<sub>d</sub>, we assume that the *open-loop gain* is exactly 100 dB, and the *first pole* of the *uncompensated op-amp* is *exactly 1 MHz* 

$$\Rightarrow$$
 f<sub>d</sub> = 10 Hz

Also,  $f_d = \omega_d/(2\pi)$ , with  $\omega_d = 1/\tau$ , and  $\tau = R_C^0 C_C$ 

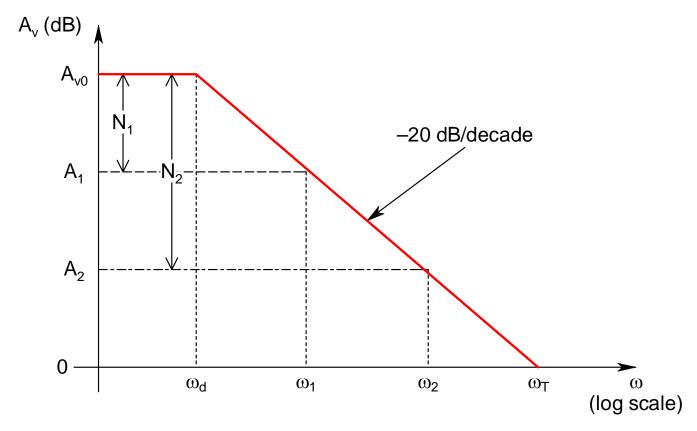
## > Thus:

$$C_{\rm C} = \tau / R_{\rm C}^0 = 12.5 \text{ pF}$$

- ➤ Note that with this *compensation scheme*, the *open-loop bandwidth* of the *compensated op-amp* drops all the way down to *10 Hz*, from *1 MHz*
- ➤ However, this is not really a *limitation*, since the *open-loop gain* is *so high*, that even with *negative feedback*, *sufficiently high values of gain can be achieved*

## $\succ$ Unity-Gain Bandwidth $(f_T)$ :

- Product of the dominant pole frequency and the open-loop gain
- This is also the *bandwidth* of the system when the *gain is unity* (hence the name!)
- Also known as the gain-bandwidth product (GBP)
- It is *1 MHz* for this case
- Note that under *DPC*, it's also the *first pole* of uncompensated system
- With negative feedback, the GBP remains constant  $\Rightarrow$  As gain  $\checkmark$ , bandwidth  $\uparrow$ , and vice-versa



A<sub>v0</sub>: Midband Gain,  $\omega_d$ : Compensated Bandwidth,  $\omega_T$ : Unity-Gain Bandwidth N<sub>1</sub> and  $\omega_1$ , N<sub>2</sub> and  $\omega_2$ : Amount of Feedback and Corresponding Bandwidth A<sub>1</sub>, A<sub>2</sub>: Gain With Feedback N<sub>1</sub>, N<sub>2</sub>  $A_{v0}\omega_d = A_1\omega_1 = A_2\omega_2 = \omega_T$ 

## • Protection Circuits:

- $ightharpoonup Q_{15}$ -R<sub>6</sub>: *Overload protection circuit* for  $Q_{14}$
- ➤ Similar to that discussed in the chapter on Output Stages
- R<sub>6</sub> senses the current being sourced by Q<sub>14</sub> to load
- When the *drop* across  $R_6$  *approaches*  $V_{\gamma}$  of  $Q_{15}$ , it starts to *bypass* the *base current* of  $Q_{14}$ 
  - ⇒ The current does not increase indefinitely
- $\triangleright$  Protection scheme of  $Q_{20}$  is slightly different

- For the *previous case* of  $Q_{14}$ , the *load current* was *flowing out* of the circuit
- $\succ$  However, for  $Q_{20}$ , the *load current* is *flowing* into the circuit
- Thus, the circuit should be *protected* by *limiting* the amount of this *current*
- $\triangleright$  Here, R<sub>7</sub> senses the current being sunk by Q<sub>20</sub>
- As soon as the *drop* across  $R_7$  *approaches*  $V_{\gamma}$  of  $Q_{21}$ , it *turns on* and starts to *bypass* the *current* through  $Q_{20}$

- ► Values of  $R_6$  and  $R_7$  are slightly different to account for the difference in  $V_{\gamma}$  for npn and pnp BJTs
- $\succ$  Initially, this *shunted current* starts to *flow* through the *unnumbered* 50 kΩ resistor to  $-V_{CC}$
- When the *drop* across this 50 k $\Omega$  resistor *approaches*  $V_{\gamma}$  of  $Q_{24}$ , it starts to *turn on*, which makes  $Q_{22}$  to *turn on* too (note that  $Q_{22}$  and  $Q_{24}$  form a *mirror*)
- Now, the *collector* of  $Q_{22}$  is *connected* to the *base* of  $Q_{16}$

- Thus, Q<sub>16</sub> starts to *lose* its *base drive*, since a *part of it* is *shunted away* by Q<sub>22</sub>
- ➤ Hence, Q<sub>16</sub> conducts less, and produces a chain reaction, which limits the current sinking capability of the output stage
- > Thus, the *circuit gets protected*
- $\triangleright$  Now, about the *role played by Q*<sub>23B</sub>
- > *Note*:  $V_{B16} = V_{E23B}$ , and  $V_{C17} = V_{B23B}$

$$\Rightarrow$$
 V<sub>EB23B</sub> = V<sub>B16</sub> - V<sub>C17</sub>

$$ightharpoonup$$
 Also,  $V_{C17} = V_{B17} + V_{CB17}$ 

 $\triangleright$  Noting that  $V_{B17} = V_{E16}$ :

$$V_{EB23B} = V_{B16} - V_{E16} - V_{CB17} = V_{BE16} - V_{CB17}$$

- $\triangleright$  Under *normal operating condition*,  $V_{BE16} \sim 0.7 \text{ V}$
- ➤ If  $Q_{17}$  also is in the *FA mode*, which is the *desired mode of operation*, then the *CB junction* of  $Q_{17}$  will be *reverse biased* 
  - $\Rightarrow$  V<sub>CB17</sub> is *positive*
  - $\Rightarrow$  V<sub>EB23B</sub> < V<sub>BE16</sub>, and Q<sub>23B</sub> would *remain off*
- Now, if for any reason whatsoever,  $Q_{17}$  moves towards saturation, then  $V_{CB17}$  would decrease