

- ***Voltage Divider (or 4-Resistor) Bias:***

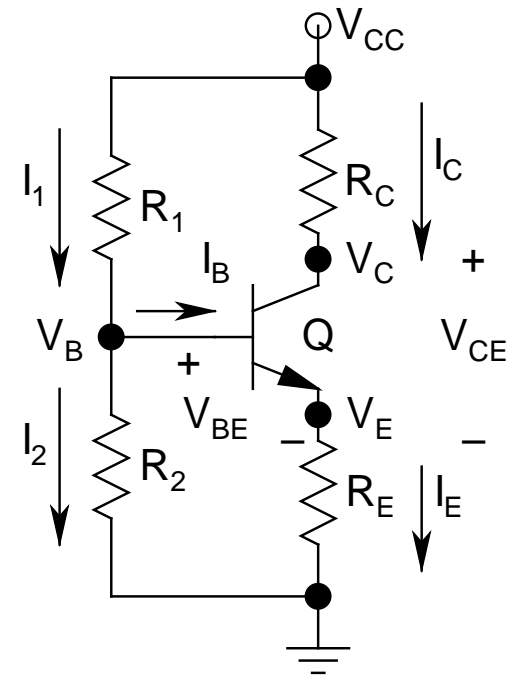
- *The best: Extremely robust and versatile*

- If properly designed, *almost  $\beta$  independent*

- If  $I_1 \geq 10I_B$ ,  $I_1 \approx I_2$

$$\Rightarrow V_B \approx \frac{R_2}{R_1 + R_2} V_{CC}$$

$$\Rightarrow V_E = V_B - V_{BE} \text{ and } I_C \approx I_E = V_E / R_E$$



- **Example:** Let  $V_{CC} = 5\text{ V}$ ,  $R_1 = 40\text{ k}\Omega$ ,  $R_2 = 10\text{ k}\Omega$ ,  $R_C = 2\text{ k}\Omega$ , and  $R_E = 300\text{ }\Omega$ 
  - **Quick estimate:** Assume  $\beta \geq 100$ 
    - $\Rightarrow V_B = 1\text{ V}$ ,  $V_E = 0.3\text{ V}$ ,  $I_C \approx I_E = 1\text{ mA}$ ,  $V_{CE} = 2.7\text{ V}$ , and  $P_D = 5.5\text{ mW}$
    - $\Rightarrow$  Done! Piece of cake, isn't it?
  - $I_1 = 100\text{ }\mu\text{A}$  and  $I_B \leq 10\text{ }\mu\text{A}$  (for  $\beta \geq 100$ ):  
Assumption of  $I_1 \geq 10I_B$  validated
  - Actually, *as  $I_1$  and  $\beta$  go down*, this *analysis becomes more and more inaccurate!*

- *Exact Analysis:*

- *Sufficiently more complicated*

- *Open the base lead and*

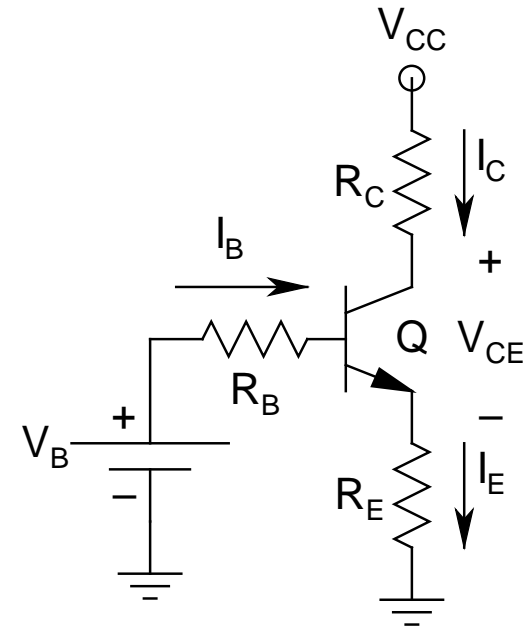
- Thevenize the left branch*

$$\Rightarrow V_B = \frac{R_2}{R_1 + R_2} V_{CC} = 1 \text{ V}$$

$$R_B = R_1 \parallel R_2 = 8 \text{ k}\Omega$$

- Also,  $V_B = I_B R_B + V_{BE} + I_E R_E$

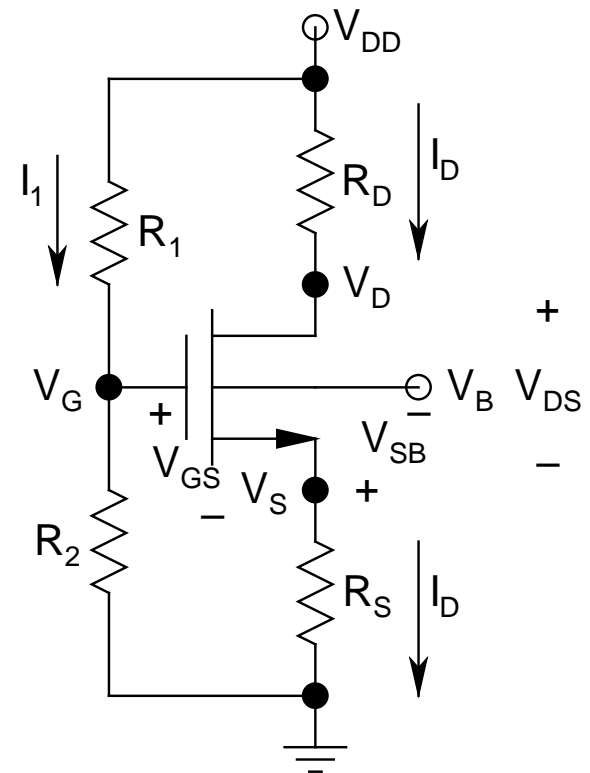
$$\Rightarrow I_B = \frac{V_B - V_{BE}}{R_B + (\beta + 1) R_E}$$



- Gives:
  - $I_B = 7.83 \mu\text{A}$ ,  $I_C = 0.78 \text{ mA}$ , and  $V_{CE} = 3.2 \text{ V}$  for  $\beta = 100$  (*quite off from quick estimate!*)
  - $I_B = 3.6 \mu\text{A}$ ,  $I_C = 0.9 \text{ mA}$ , and  $V_{CE} = 2.93 \text{ V}$  for  $\beta = 250$  (*within  $\pm 10\%$  error band*)
- Thus, *as  $\beta \uparrow$ , accuracy of quick estimate  $\uparrow$*
- Also, *as  $R_B \downarrow$ , accuracy  $\uparrow$*
- *$R_B$  should not be too small, since  $P_D \uparrow\uparrow$*
- Thus, there are *various design constraints*

# Discrete Stage Biasing: MOSFET

- *Almost universally biased using 4-Resistor Bias*
- *Significantly more complicated than BJT biasing, since there is no quick estimate*
- *Also, body effect and CLM complicate matters*



- **No  $I_G$**   $\Rightarrow$   *$R_1$ - $R_2$  combination provides a perfect voltage division*

$$\Rightarrow V_G = \frac{R_2}{R_1 + R_2} V_{DD}$$

- $V_S = I_D R_S$  and  $V_D = V_{DD} - I_D R_D$

$$\Rightarrow I_D = \frac{k_N}{2} (V_G - I_D R_S - V_{TN})^2 \times \\ \left( 1 + \lambda [V_{DD} - I_D (R_S + R_D)] \right)$$