

# Manipulator Kinematics Jacobians

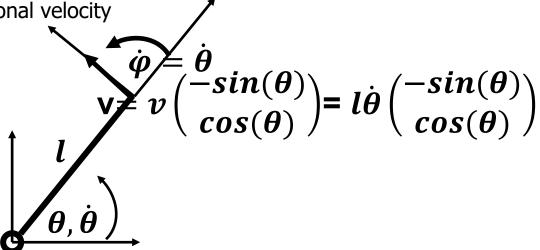


#### Kinematics and Velocities

- Forward kinematics deals with the transformation of internal robot configurations to locations in space of the end-effector
  - Note: Forward kinematics can also be derived for other points on the manipulator but is most often used for the end-effector
- There are situations where we are interested in how the end-effector is movine (i.e. its velocity)
  - When playing a ball game, the velocity at which a robot hits the ball is important
  - When performing interaction tasks (such as painting),
     velocity of the interaction is important

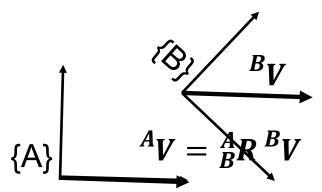


- Joint rotations produce translational and rotational velocities in the subsequent frames/links
  - The rotational velocity of a revolute joint produces both translational and rotational velocities at the end of the link
    - Direction of translational velocity depends on joint angle, magnitude on rotational velocity





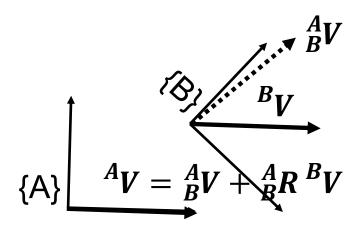
- Translational velocities in a frame can be transformed into another frame in the same way as positions as long as the frames do not rotate or move
  - Velocities are vectors and thus only have magnitude and direction but no position (can draw them at frame origin)



- In homogeneous transformations this would be achieved by making the 4<sup>th</sup> element in the velocity vector (the one we added) equal to 0
  - Remember, adding a 1 means it is a position, adding a 0 means it is a vector



 Translational velocities between frames simply add to the velocity of the point





- Rotational velocities of frames are more complex as they affect translational and rotational velocities
  - We can express the rotational velocity of a frame using a vector of rotational velocities around all the axes

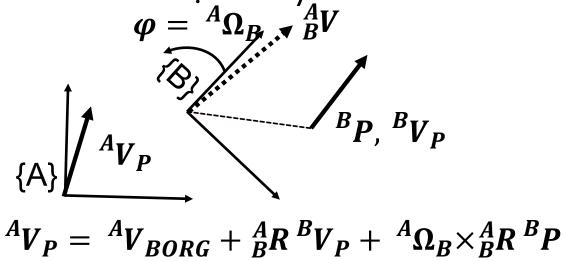
$$^{A}\Omega_{B}=egin{pmatrix} m{\omega}_{X} \ m{\omega}_{Y} \ m{\omega}_{Z} \end{pmatrix}$$

 Effect of frame rotational velocity on translational velocity is more complex and depends on the location of the moving point in the second frame (point at the origin of B will not move due to rotation of frame B)

$$^{A}V_{P} = {^{A}\Omega_{B}} \times {^{A}_{B}}R^{B}P$$



Using both translational and rotational velocities we can express the velocity as seen from frame A due to the rotational and translational velocities of a frame B and the translational velocity in that frame



Represents the effect of the movement of one proximal joint (in A) on the end-effector velocity (in B)

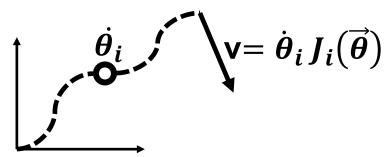


- Using the previous result, we could perform something akin to outward inward iteration
  - Starting from the base frame, use the kinematic relations to derive the rotational and translational effects form one joint frame to the next  $\binom{A}{B}V$ ,  $\binom{A}{B}Q_B$ )
  - Starting from the tool frame ( ${}^TP_{TORIG} = 0$ ,  ${}^TV_{TORIG} = 0$ ) we can now work backward towards the base and compute the resulting velocities
    - We also have to estimate the location of the end-effector for each frame (as in the forward kinematics)

$${}^{A}V_{T} = {}^{A}V_{BORG} + {}^{A}_{B}R {}^{B}V_{T} + {}^{A}\Omega_{B} \times {}^{A}_{B}R {}^{B}P_{T}$$
$${}^{A}P_{T} = {}^{A}P_{BORG} + {}^{A}_{B}R$$



- Another way to derive the end-effector velocities is to realize their relation to the forward kinematics
  - If we move only one joint and keep all others fixed as we change the corresponding joint velocity we can see that
    - The direction of the velocity vector of the end-effector is not affected by the joint speed, only the joint angles
    - The magnitude of the velocity vector of the end-effector scales linearly with the joint angle speed (i.e. twice the joint angle speed yields twice the end-effector speed





- This observation yields that the end-effector velocity is linear in terms of the joint velocities
  - It can thus be written (and computed) as:

$$V = J(\vec{\theta})\vec{\dot{\theta}}$$

 Since we also know that the end-effector velocity is the change of end-effector position over time, we know that it is the derivative of the forward kinematics

$$V = \frac{dP_T}{dt} = \begin{pmatrix} \frac{dx_T}{dt} \\ \frac{dy_T}{dt} \\ \frac{dz_T}{dt} \end{pmatrix}$$



• From this we can derive the Jacobian matrix  $J(\vec{\theta})$  for the manipulator  $\int \frac{d\theta_1}{dt} \sqrt{\frac{dx_T}{dt}}$ 

the manipulator
$$V = J(\vec{\theta})\vec{\theta} = J(\vec{\theta}) \begin{pmatrix} \frac{d\theta_1}{dt} \\ \vdots \\ \frac{d\theta_n}{dt} \end{pmatrix} = \begin{pmatrix} \frac{dx_T}{dt} \\ \frac{dy_T}{dt} \\ \frac{dz_T}{dt} \end{pmatrix}$$

The Jacobian has as many rows at there are end-effector velocities (usually 3) and as many columns as there are joints and is a matrix of partial derivatives expressing the relation between position and joint changes

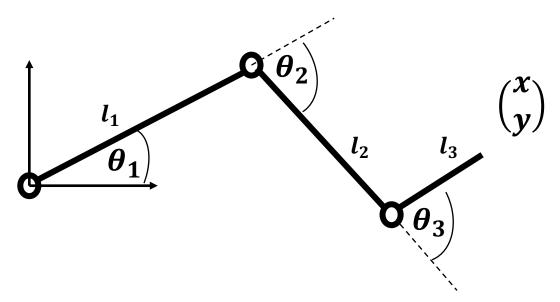
$$J(\vec{\theta}) = \begin{pmatrix} \frac{d\mathbf{x}_T}{d\theta_1} & \cdots & \frac{d\mathbf{z}_T}{d\theta_n} \\ \frac{d\mathbf{y}_T}{d\theta_1} & \cdots & \frac{d\mathbf{z}_T}{d\theta_n} \\ \frac{d\mathbf{z}_T}{d\theta_1} & \cdots & \frac{d\mathbf{z}_T}{d\theta_n} \end{pmatrix}$$



- Manipulator Jacobian expresses the relation between joint movements and end-effector movements
  - If an entry is 0 then the corresponding joint can not cause any movement in this direction
  - The larger a value, the more velocity the corresponding joint can produce in this direction
- The Manipulator Jacobian can be derived directly from the Forward Kinematic function
  - All entries are derivatives of the kinematics with respect to a single joint angle

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 To derive the Jacobian we first derive the Forward Kinematics



$$x = l_1 \cos(\theta_1) + l_2 \cos(\theta_1 + \theta_2) + l_3 \cos(\theta_1 + \theta_2 + \theta_3)$$
  
$$y = l_1 \sin(\theta_1) + l_2 \sin(\theta_1 + \theta_2) + l_3 \sin(\theta_1 + \theta_2 + \theta_3)$$



$$x = l_1 \cos(\theta_1) + l_2 \cos(\theta_1 + \theta_2) + l_3 \cos(\theta_1 + \theta_2 + \theta_3)$$
  
$$y = l_1 \sin(\theta_1) + l_2 \sin(\theta_1 + \theta_2) + l_3 \sin(\theta_1 + \theta_2 + \theta_3)$$

 Compute the partial derivatives of the spatial dimensions with respect to each of the joint angles

$$dx/d\theta_{1} = -l_{1}\sin(\theta_{1}) - l_{2}\sin(\theta_{1} + \theta_{2}) - l_{3}\sin(\theta_{1} + \theta_{2} + \theta_{3})$$

$$dx/d\theta_{2} = -l_{2}\sin(\theta_{1} + \theta_{2}) - l_{3}\sin(\theta_{1} + \theta_{2} + \theta_{3})$$

$$dx/d\theta_{3} = -l_{3}\sin(\theta_{1} + \theta_{2} + \theta_{3})$$

$$dy/d\theta_{1} = -l_{1}\cos(\theta_{1}) + l_{2}\cos(\theta_{1} + \theta_{2}) + l_{3}\cos(\theta_{1} + \theta_{2} + \theta_{3})$$

$$dy/d\theta_{2} = -l_{2}\cos(\theta_{1} + \theta_{2}) + l_{3}\cos(\theta_{1} + \theta_{2} + \theta_{3})$$

$$dy/d\theta_{3} = -l_{3}\cos(\theta_{1} + \theta_{2} + \theta_{3})$$

These are the entries in the Manipulator Jacobian



- Besides calculating end-effector velocity (or velocities of other point with a forward kinematic function), the Manipulator Jacobian is also used in other ways
  - Incrementally moving towards a position
    - Jacobian provides approximate joint velocities to move in a given direction

$$\vec{\dot{\theta}} \approx J(\vec{\theta})^T V_T$$

Note: While  $J(\vec{\theta})^{-1}$  would be the precise answer, we can not invert the Jacobian in general since it is not a square matrix

- Compute relation between joint torque  $\vec{\tau}$  and static endeffector force  $\vec{F}$  (forces not due to impact and movement)
  - Intuitively, the faster something can move, the less hard it can push

$$\vec{\tau} \approx J(\vec{\theta})^T \vec{F}$$