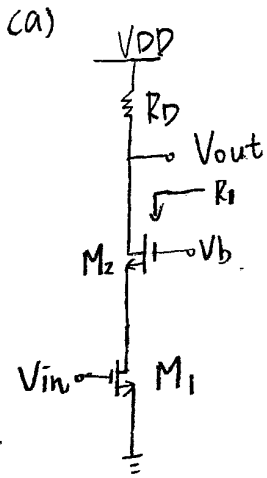
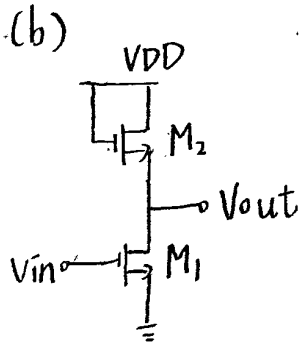


Q1:



$$R_i = g_{m1} r_{o1} r_{o2} + r_{o1} + r_{o2}$$

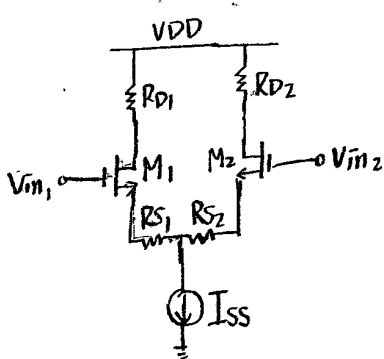
$$A_v = -g_{m1} (R_1 \parallel R_D) \quad (10\%)$$



$$R_{out} = r_{o1} \parallel r_{o2} \parallel \left(\frac{1}{g_{m2} + g_{mb2}} \right)$$

$$A_v = -g_{m1} R_{out} = -g_{m1} \left[r_{o1} \parallel r_{o2} \parallel \left(\frac{1}{g_{m2} + g_{mb2}} \right) \right] \quad (10\%)$$

Q2:



(a) for $R_{S1} = R_{S2} = 0$ $v_{in1} - v_{in2} = v_{in}$

$$v_{in1} - v_{in2} = V_{GS1} - V_{GS2}, \quad V_{GS} = \sqrt{\frac{2I_D}{k_n}} + V_{th}$$

$$\Rightarrow v_{in1} - v_{in2} = \sqrt{\frac{2I_{D1}}{k_{n1}}} - \sqrt{\frac{2I_{D2}}{k_{n2}}} \quad \text{if } v_{th1} = v_{th2}$$

$$(v_{in1} - v_{in2})^2 = \frac{2}{k_n} (I_{SS} - 2\sqrt{I_{D1} I_{D2}}) \quad \text{if } k_{n1} = k_{n2}$$

$$\frac{1}{2} k_n (v_{in1} - v_{in2})^2 - I_{SS} = -2\sqrt{I_{D1} I_{D2}}$$

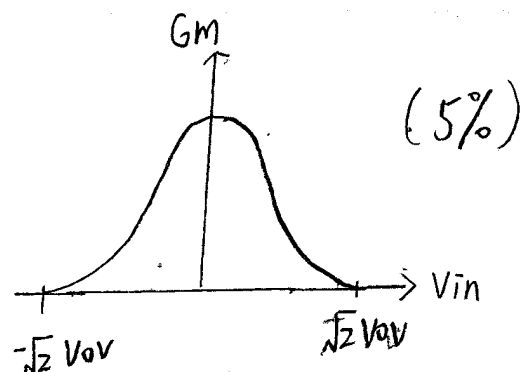
$$\left(\frac{1}{2} k_n v_{in}^2 - I_{SS} \right)^2 = 4 I_{D1} I_{D2}$$

$$\text{and } 4 I_{D1} I_{D2} = (I_{D1} + I_{D2})^2 - (I_{D1} - I_{D2})^2 = I_{SS}^2 - (I_{D1} - I_{D2})^2$$

$$\Rightarrow (I_{D1} - I_{D2})^2 = -\frac{1}{4} k_n^2 v_{in}^4 + I_{SS} k_n v_{in}^2$$

$$I_{D1} - I_{D2} = \sqrt{k_n I_{SS}} v_{in} \sqrt{1 - \frac{k_n}{4 I_{SS}} v_{in}^2}$$

$$G_m = \frac{\partial I_{D1}}{\partial V_{in1}} = \frac{1}{2} k_n \cdot \frac{\frac{4I_{SS}}{k_n} - 2V_{in1}^2}{\sqrt{\frac{4I_{SS}}{k_n} - V_{in1}^2}}$$



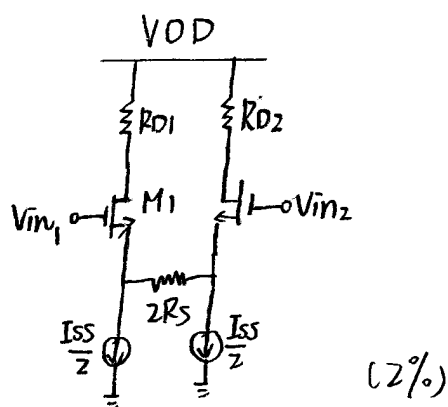
for $G_m = 0$, assume $I_{SS} = I_{D1}$, $V_{in} = V_{in1}$

$$\frac{4I_{SS}}{k_n} - 2V_{in1}^2 = 0$$

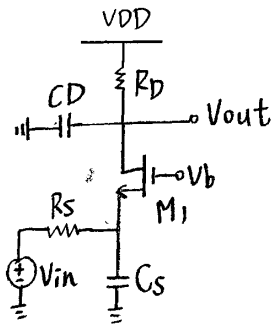
$$\frac{2I_{SS}}{k_n} = V_{in1}^2 \quad V_{in1} = \sqrt{\frac{2I_{SS}}{k_n}} = \sqrt{2} V_{ov} \quad (5\%)$$

(b) If $R_{S1} = R_{S2} = R_S \neq 0$, then the input linear region will increase from $\sqrt{2} V_{ov}$ to $\sqrt{2} V_{ov} + I_{SS} R_S$ and improve the non-linear effect (4%)
disadvantage: $G_m \downarrow$, V_{ICM} level \nearrow (4%)

How to improve:

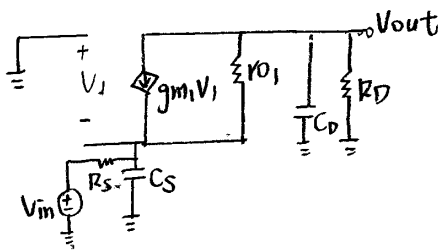


Q3



$$g_m = g_{m1} + g_{mb1}$$

$$A_v(s) = \frac{V_{out}(s)}{V_{in}(s)} = A_0 \times \frac{1}{(1 + \frac{s}{\omega_{in}})(1 + \frac{s}{\omega_{out}})}$$



$$\frac{V_{in} + V_1}{R_s} + V_1 s C_s + g_m V_1 + \frac{V_{out} + V_1}{r_{o1}} = 0 \quad \dots (1)$$

$$g_m V_1 + \frac{V_{out} + V_1}{r_{o1}} + V_{out} \left(\frac{1}{R_D \parallel \frac{1}{s C_D}} \right) = 0 \quad \dots (2)$$

As the above (1), (2) we can get

$$A_v(s) = \frac{V_{out}(s)}{V_{in}(s)} = \frac{1 + g_m r_{o1}}{s^2 C_s C_D R_s r_{o1} + s \left[C_s R_s \left(1 + \frac{1}{R_D} \right) + C_D R_s (1 + g_m r_{o1}) + C_D r_{o1} R_D \right] + 1 + \frac{(1 + g_m r_{o1}) R_s + 1}{R_D}}$$

$$\text{DC gain} \Rightarrow s=0 \Rightarrow \frac{1 + g_m r_{o1}}{1 + \frac{(1 + g_m r_{o1}) R_s + 1}{R_D}} = \frac{(1 + g_m r_{o1}) R_D}{R_D + R_s + (1 + g_m r_{o1}) R_s} \quad (10\%)$$

$$\text{for } \lambda \neq 0, \omega_{p1} \approx \left[\frac{C_s R_s (R_D + 1) + C_D R_D R_s (1 + g_m r_{o1}) + C_D r_{o1} R_D}{R_D + R_s + (1 + g_m r_{o1}) R_s} \right]^{-1}$$

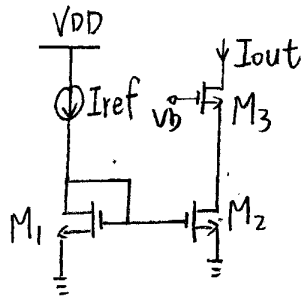
if $\omega_{p1} \gg \omega_{p2}$

$$\omega_{p2} = \frac{R_D + R_s + (1 + g_m r_{o1}) R_s}{\omega_{p1} \cdot C_s C_D R_s r_{o1} R_D}$$

$$\text{for } \lambda = 0, \omega_{p1} = \frac{1 + g_m R_s}{R_s C_s}$$

$$\omega_{p2} = \frac{1}{R_D C_D} \quad (10\%)$$

Q4

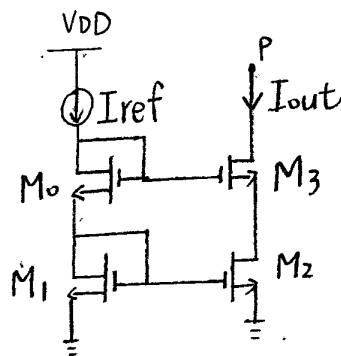


(a)

$$\frac{I_{out}}{I_{ref}} = \frac{\frac{1}{2} \mu_n C_{ox} \left(\frac{W}{L}\right)_2 (V_{GS2} - V_{th1})^2 (1 + \lambda V_{DS2})}{\frac{1}{2} \mu_n C_{ox} \left(\frac{W}{L}\right)_1 (V_{GS1} - V_{th2})^2 (1 + \lambda V_{DS1})}$$

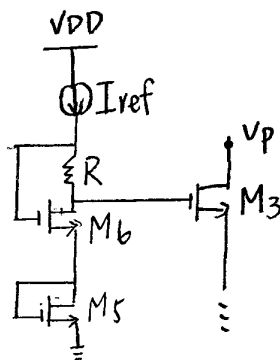
$$= \frac{\left(\frac{W}{L}\right)_2 (1 + \lambda V_{DS2})}{\left(\frac{W}{L}\right)_1 (1 + \lambda V_{DS1})} \quad (10\%)$$

(b)



The gate voltage of M_3 is $V_{GS1} + V_{GS0} = 2V_{OV} + 2V_{th}$
the output swing (V_p) \downarrow (5%)

How to improve



The gate voltage of M_3 is $V_{GS5} + V_{GS6} - I_{ref}R$

$$= 2V_{OV} + 2V_{th} - I_{ref}R$$

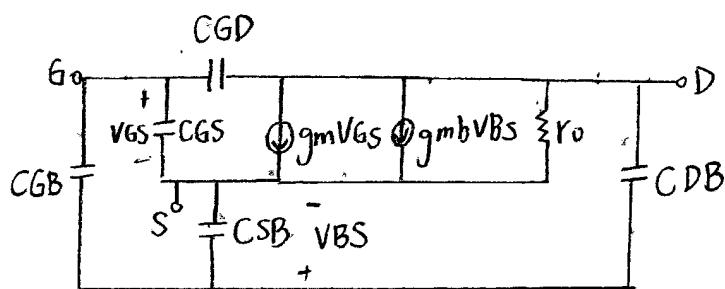
$$\text{If } I_{ref} \cdot R = V_{th}$$

$$V_{G, M3} = 2V_{OV} + V_{th}$$

the output swing (V_p) \nearrow (5%)

Q5

(a)

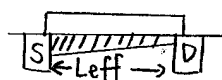


(10%)

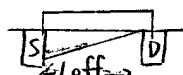
(b)

channel length modulation

⇒ Mos 通道實際長度會隨著閘極和汲極間的電位差降低而逐漸減少，當 mos 在飽合區時， L_{eff} 長度縮小，電流就會相對上升



$V_{DS} < V_{GS} - V_{th}$



$V_{DS} > V_{GS} - V_{th}$

$$\frac{1}{L_{eff}} = \frac{1}{L - \Delta L} = \frac{1}{L(1 - \frac{\Delta L}{L})} = \left(\frac{1 + \frac{\Delta L}{L}}{L}\right) \quad \frac{\Delta L}{L} = 1 + \lambda V_{DS}$$

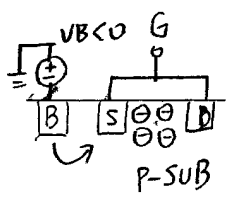
$$I = \frac{1}{2} \mu n C_{ox} \left(\frac{W}{L}\right)_n (V_{GS} - V_{th})^2 (1 + \lambda V_{DS}) \quad (3\%)$$

↳ 修正項

設計上當 I_D 在飽合區時， V_{DS} 增減會對 r_o 造成變化，在公式上有非線性變化 (2%)

body effect

⇒ 當 $V_B < 0$ 時，body 端電壓會吸引更多電洞到基板，產生更多的負電荷到 gate 端下方，gate 端需施加更大的正電壓來形成 inversion layer



(3%)

設計上當 $V_{BS} \neq 0$ 時，則 $V_{th} = V_{th0} + \gamma (\sqrt{2\phi_F - V_{BS}} - \sqrt{2\phi_F})$ (2%)