



# Airbrake Integration

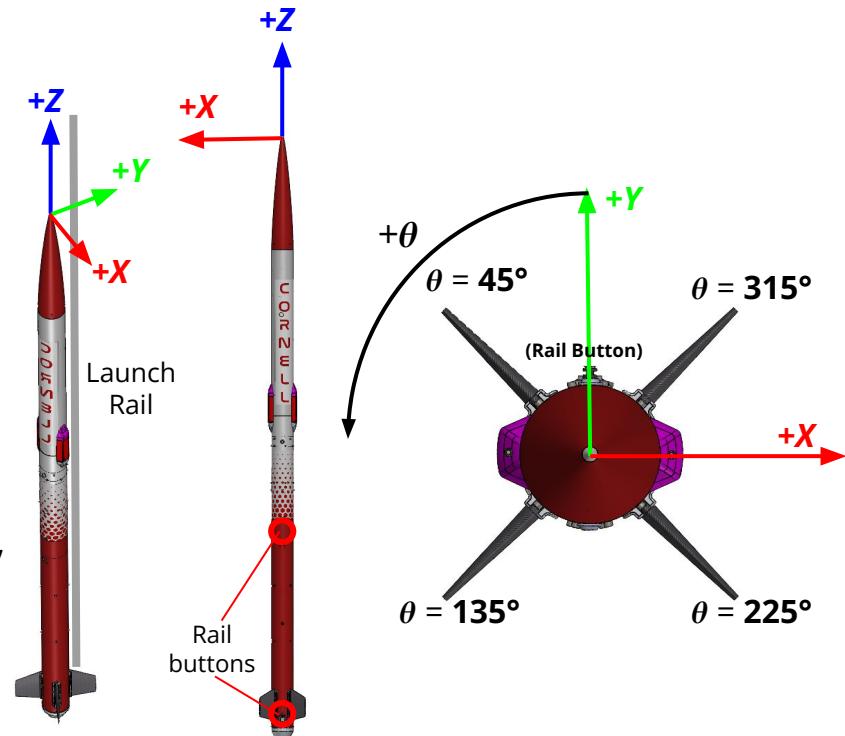
**Final Design Review  
Saturday, November 15, 2025  
Langston Johnson**

# Address Action Items from IDR

- Action Items from IDR
  - Bulkhead Mass Reductions
    - Ansys to Verify
  - Electrical Pass Through
    - Using Notches Instead of Amphenol Pass Throughs
    - Bottom Bulkhead No Longer Sealed
  - Mechanism Integration
    - New Motor Retaining Ring
    - Lintech Rail Integration
    - Mechanical Clearances

# CRT Launch Vehicle Frame

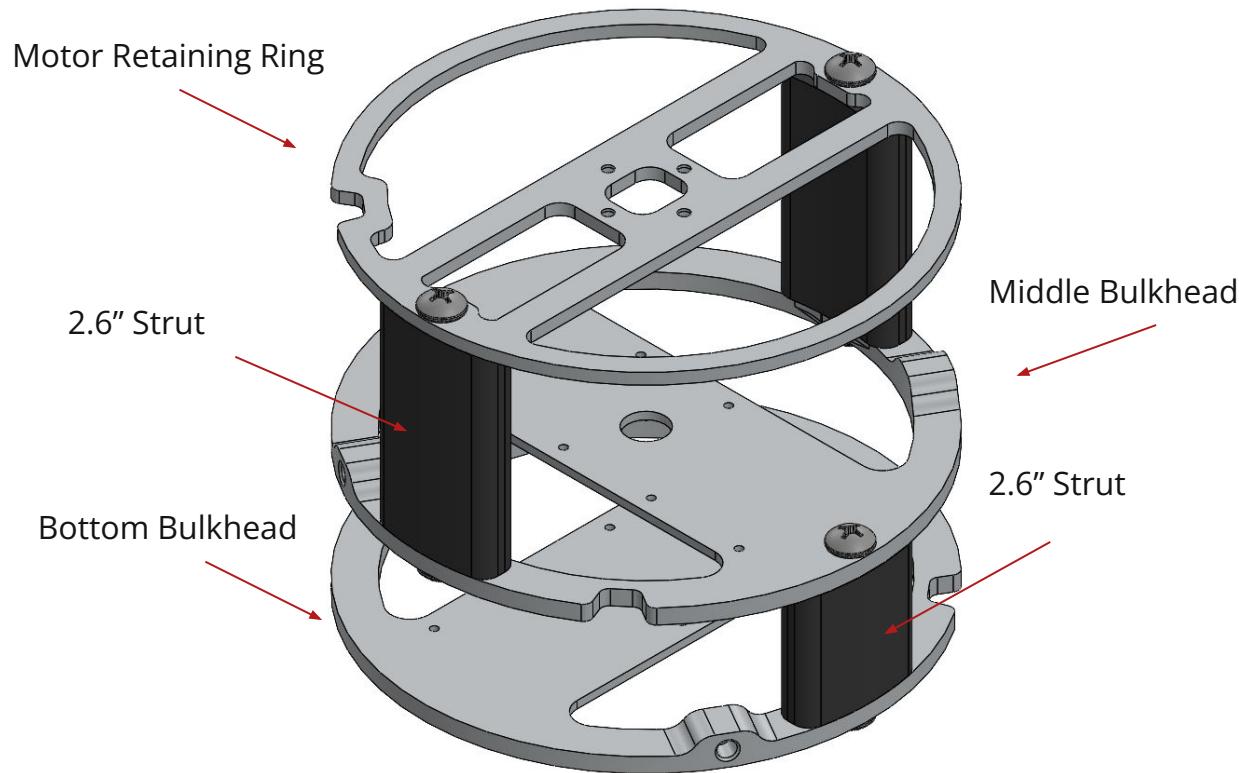
- The CRT LV frame is a right handed Cartesian coordinate system located at the theoretical nose termination (TNT), or tip of the nose cone.
- The orientation of this coordinate system is based on the position of the launch rail prior to lift off, with rail buttons located in line with **+Y**.
- The **+Z** axis points forward out of the nose of the vehicle.
- The **+Y** axis points outward in the direction of the rail buttons and launch rail.
- The **+X** axis is rotated 270° in the **+Z** direction from **+Y**, completing a right handed coordinate system.
- The angle  $\theta$  is defined as the angle counterclockwise from the **+Y** axis when viewed from the **+Z** direction.
- To aid with LV integration, subsystem CAD assemblies should be oriented to fit this coordinate system in Solidworks.



# System Overview

- Parents: Launch Vehicle (LV)
- Airbrake Mechanism
- Function: Transfer Aerodynamic Load from Airbrakes to LV

# System Overview

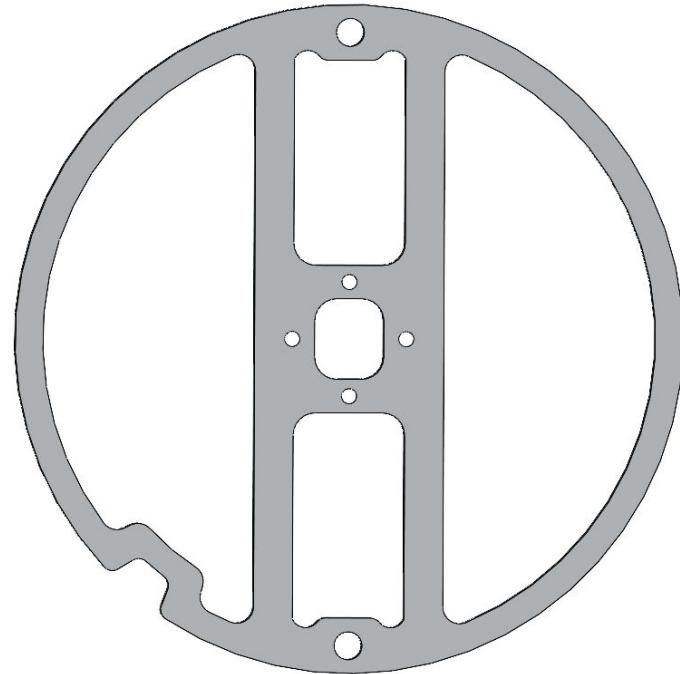
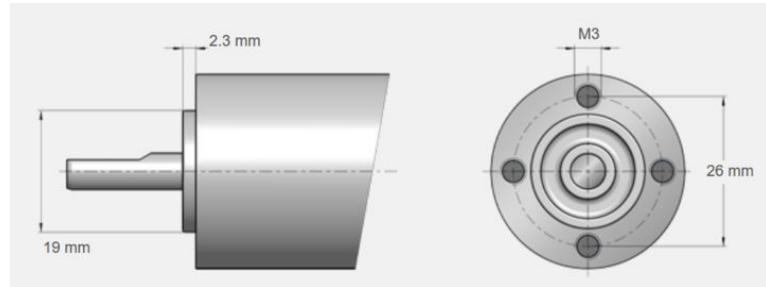


# Motor Retaining Ring

Updated Holes - ECX Flat 32S

Notch 140° CCW from y+

Mass: .145 lbs



# Middle Bulkhead

Lintech Rail 14.mm spacing

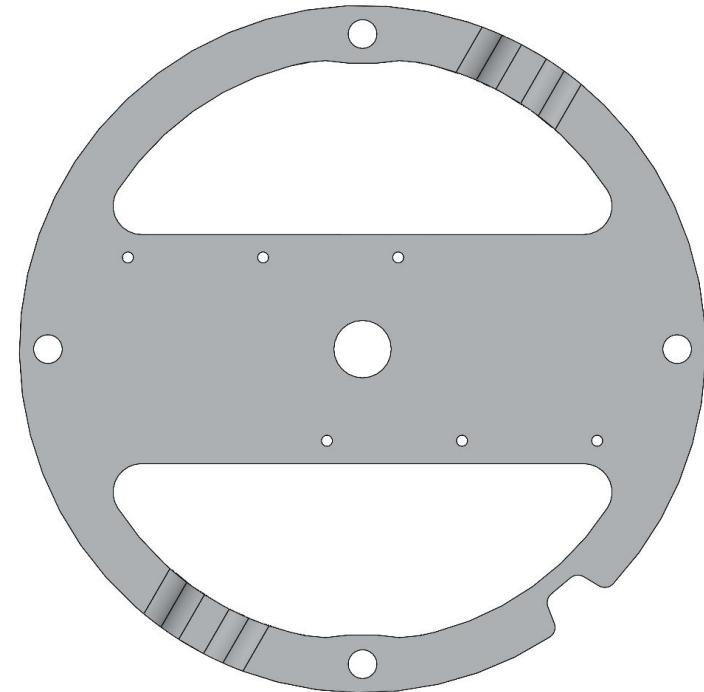
Axel Pass Through

Notch 220° CCW from y+

Mass: .267 lbs

Outer thickness: 0.2"

Base Thickness: 0.1"



# Middle Bulkhead

Lintech Rail [14.mm](#) spacing

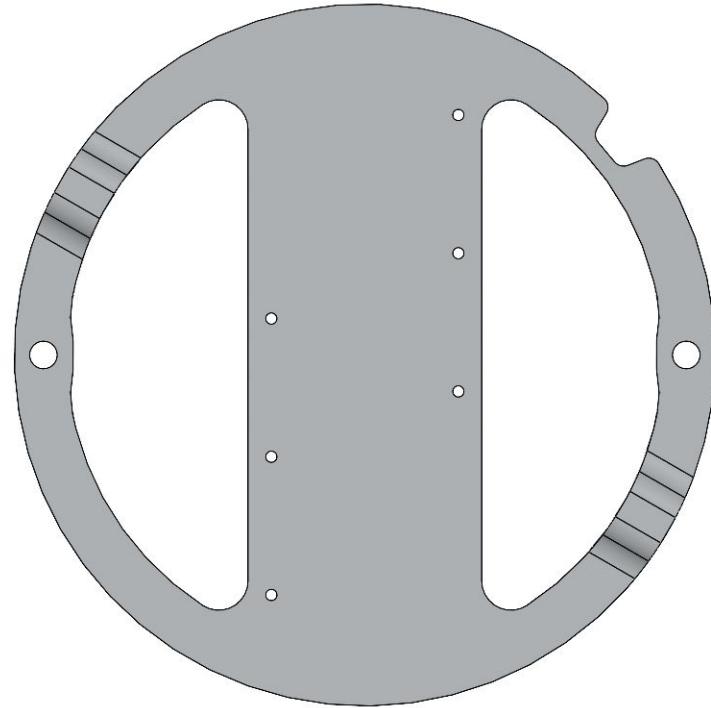
Not Sealed

Notch 220° CCW from y+

Mass: .27 lbs

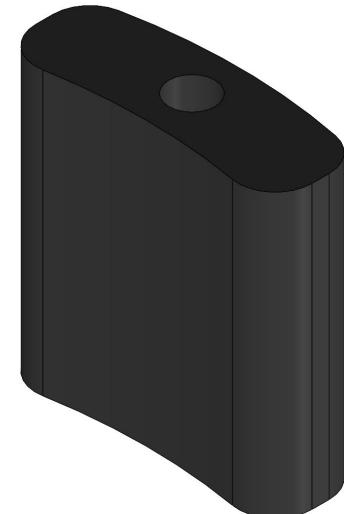
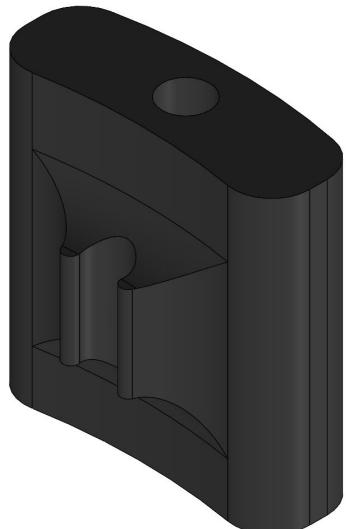
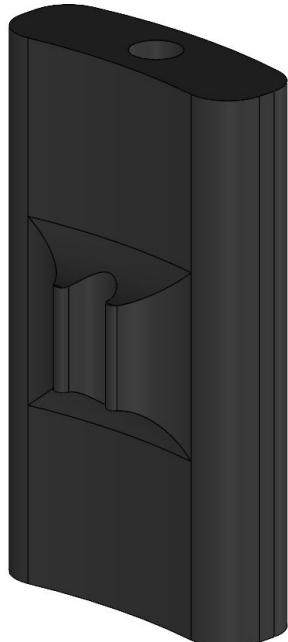
Outer thickness: 0.2"

Base Thickness: 0.1"



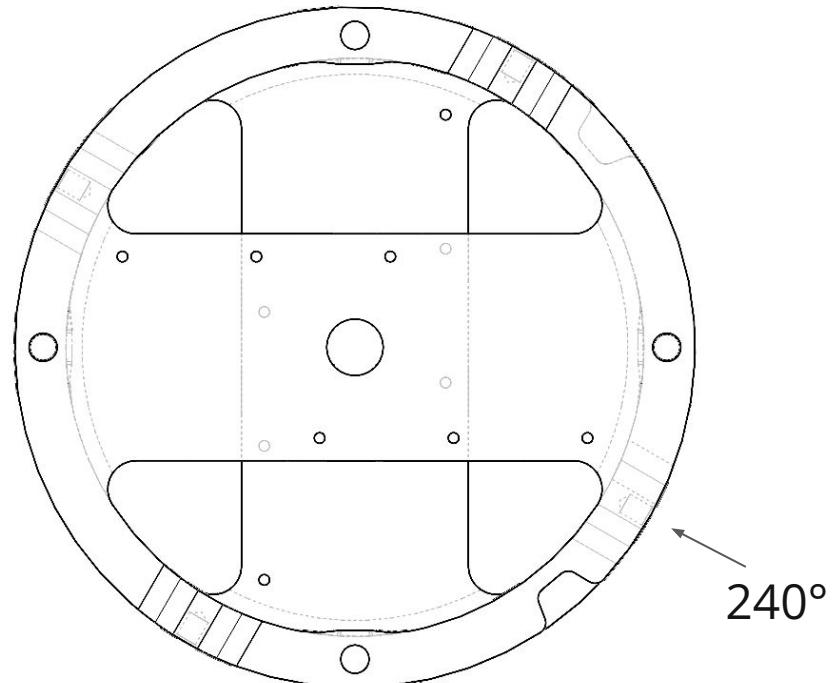
# PETG Struts

1.6" and 2.6"



# Clocking

- Bottom Right Hole 240° CCW from y+
- Holes are clocked 90° relative to one another
- Clocked to maximize the distance from the fastener hole and the airbrake apertures, without interfering with struts and electrical pass through.



# Bill of Materials

## Airbrake Integration Bill of Materials

Product	Link	Vendor	System(s)	Package Quantity	Quantity per Package	Package Price	Total Price	In Stock ?
Brass Tapered Heat-Set Inserts	<a href="#">Link</a>	McMaster	Struts	1	25	\$15.76	\$15.76	Y
Black-Oxide 18-8 Hex Pan Head Phillips Screws	<a href="#">Link</a>	McMaster	Struts	1	50	\$16.61	\$16.61	Y
¼-20 Key Inserts		Mc Master	Bulkheads	1	4	\$3.51	\$14.04	Y
PETG Filament					On Hand			Y
6" Round Stock								



# Requirements + Verification Plan

- See System Requirements Review document [here](#)
- The LV and the Payload have functional requirements for successful flight and mission. The linked document lists requirements mandated by the competition.
- **FULLY** review all LV and Payload competition and determine which requirements apply to you.
- Provide a table of the requirements and verification plans that apply to your system in the FDR presentation. Make sure to include the tests you intend to conduct.

# Requirements + Verification Plan

Launch Vehicle Requirements		
Requirement	Verification Plan	Verified? (T/F)
<b>SYS 1</b> All components on the LV that interface with the airframe shall have at least .005" clearance with the ID of the airframe	Design, Integration	T
<b>SYS 4</b> Structural components shall be designed to a minimum MoS of 0.5. (Designed to Mos of 1.5)	Design, Ansys	T
<b>STRUC 2</b> Launch vehicles shall be constructed to withstand the operating stresses and retain structural integrity under the conditions encountered during handling as well as rocket flight.	Design, Ansys. Stand on it.	T

# Failure Mode Effect Analysis

Failure Mode Effects Analysis (FMEA)						
Hazard	Causes	Effects	Mitigation Plan	Verification Plan	Risk Level	Verified? (T/F)
Bolt Shear/ Deform during flight	Excess aerodynamic load  Manufacturing defects	Mechanism fails to deploy  Possible airframe structural failure	-Hand Calcs -Structural Analysis	Manual Testing. Applying Axial Loads	Low	T
Electrical Passthrough Difficulty	Overly stiff wiring / strain  Incorrect bend radius	Damage during integration  Higher assembly time	CAD routing refinement  Add strain relief	Routing Test	Medium	F
Mechanism Integration Difficulty	Misaligned mounting holes  Inaccessible screws	Excessive integration time  Incorrect assembly	CAD Tolerancing	Integration	Low	F

# Safety Hazards

It's completely safe :D

Fill in this chart for your system.



# Safety Hazards

Safety Hazards						
Hazard	Causes	Effects	Mitigation Plan	Verification Plan	Risk Level	Verified? (T/F)
Sharp Edges During Assembly	Improper deburring of CNC / 3D printed parts	Physical Harm	Deburr & chamfer all edges	Visual inspection	Low	F
Heat Insert Installation	Hot	Burn	Lock tf in	<=	Low	F

# Fastener Calcs

Fastener: Black Oxide:  $\frac{1}{4}$ " 20.

Maximum Aerodynamic Load + System

Mass: 142.6 lbf

1x Screw can support the maximum loading experienced by the system with a FoS of 34.7.

x4 Fasteners

Black Oxide Alloy Steel

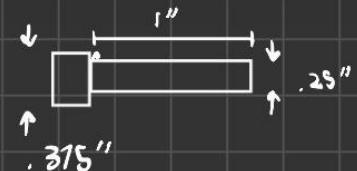
$$\sigma_u = 170 \text{ ksi}$$

$$T_u = (.6) \sigma_u = 102 \text{ ksi}$$

$$A = \pi (\frac{.25}{2})^2 = \frac{\pi}{64} \approx 0.05 \text{ in}^2$$

$$V_{max} = T_u A$$

$$V_{max} = \underline{5007 \text{ lbf}}$$

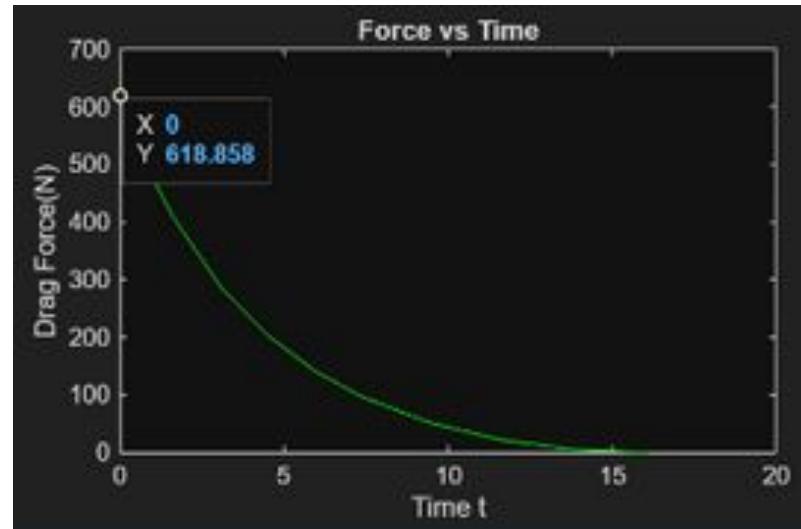


# Integrated Load Bearing Structural Analysis

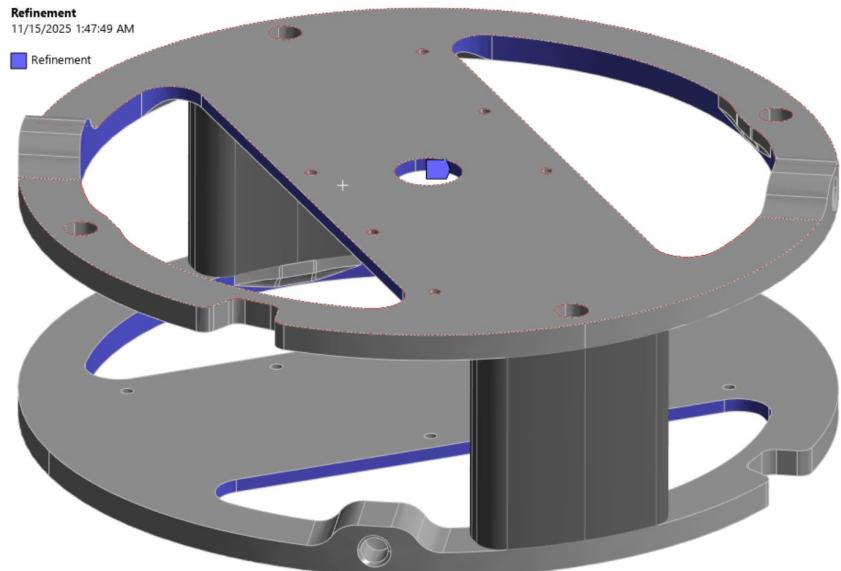
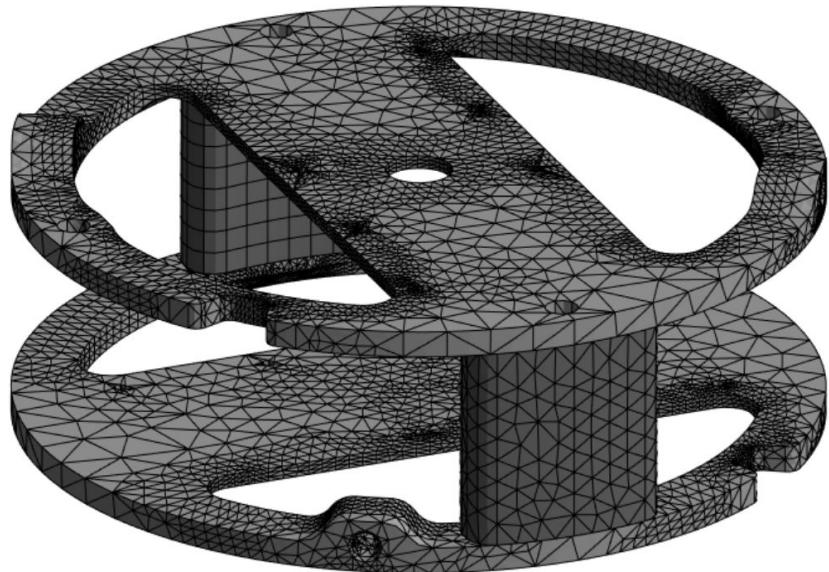
- Estimated max load is around 620 (aerodynamic drag at MAV close), testing with FOS = 2.5, so loading with 1550 N ramped with 7075-T6 bulkheads

AL 7075-T6 [FIXED]	
Equation of State and Strength Properties of Selected Materials", Steinberg D.J. LLNL, Feb 1991	
Density	2804 kg/m <sup>3</sup>
Structural	
Isotropic Elasticity	
Derive from	Young's Modulus and Poisson's Ratio
Young's Modulus	7.17e+10 Pa
Poisson's Ratio	0.33
Bulk Modulus	7.0294e+10 Pa
Shear Modulus	2.6955e+10 Pa

PETG	
Rough Approximation of PETG	
Density	1270 kg/m <sup>3</sup>
Structural	
Isotropic Elasticity	
Derive from	Young's Modulus and Poisson's Ratio
Young's Modulus	2.4e+09 Pa
Poisson's Ratio	0.4
Bulk Modulus	4e+09 Pa
Shear Modulus	8.5714e+08 Pa

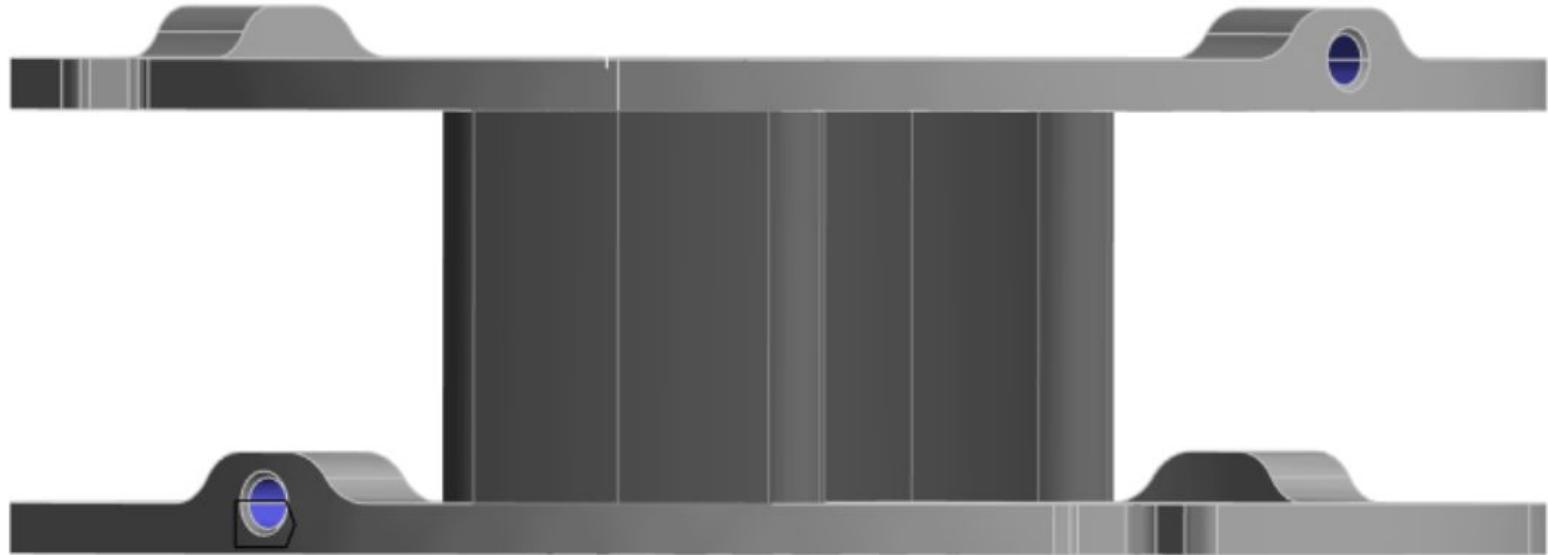


# Integrated Load Bearing Structural Analysis



# Integrated Load Bearing Structural Analysis

 Fixed Support



# Integrated Load Bearing Structural Analysis

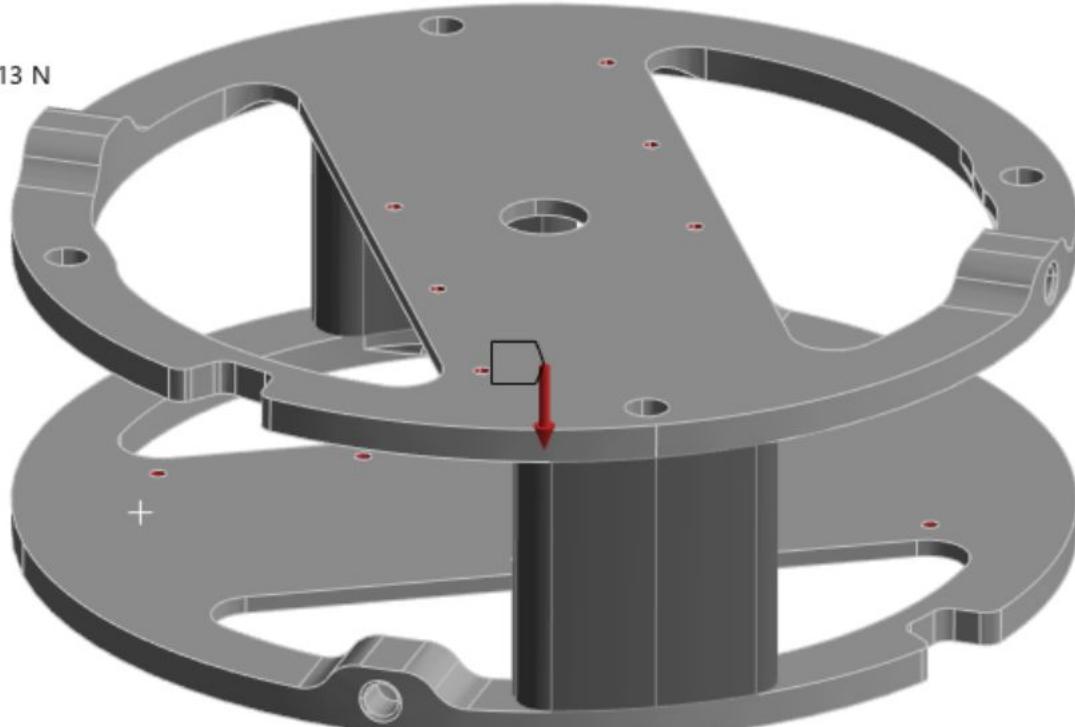
Remote Force: 1550. N

Components: 1.2484e-012, -1550., -5.8782e-013 N

Location: 0.705, 0.92765, 1.3388 m



Adding Force where  
rails transmits load  
to bulkheads



# Integrated Load Bearing Structural Analysis

Maximum Eq Stress(7075): 2.2MPa MoS: 227 ( $\sigma_y = 503$  MPa)

With FoS 2.5 Loading

## B: Integration Structure

Equivalent Stress

Type: Equivalent (von-Mises) Stress

Unit: Pa

Time: 1 s

11/15/2025 2:05:21 AM

2.2063e8 Max

1.9612e8

1.7161e8

1.4709e8

1.2258e8

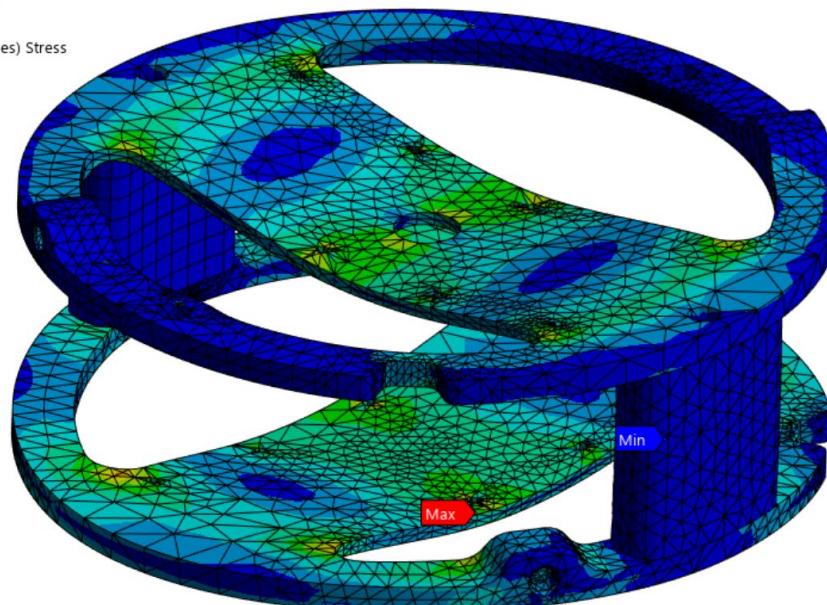
9.8069e7

7.3556e7

4.9044e7

2.4531e7

18955 Min



# Manufacturing Plan (Machining)

Composites						
Part Description	Quantity	Prereqs	Machine	Time (hours)	Status	Responsible Engineer
Motor Retaining Ring	1	CAM	Haas	6	Incomplete	Johan K
Middle Bulkhead	1	CAM	Haas 4th axis?	7	Incomplete	Johan K
Bottom Bulkhead	1	CAM	Haas 4th axis?	6.7	Incomplete	Johan K

# Testing Plan

- Airbrakes Mechanism Integration is primary test
- Then electrical pass through
- For Strength testing axial compression of the loading bearing sub-assembly

# Next Steps

- Finalize remaining integration hurdles with mechanism
- Confirm wire bend radius is feasible
- Integration Meetings during the next few airbrake standing meets



2025

Cornell Rocketry Team