

Department of Mechanical and Aeronautical Engineering

**Simulation-based design MOW 323**

**Exercises - Dynamic loading conditions**

October 22, 2021

**Shigley's:**

- **Chapter 3** (Loads and stress)
- **Chapter 4** (Deflection and stiffness)
- **Chapter 5** (Failure modes for static loading)
- **Chapter 6** (Failure modes for dynamic loading)
- **Chapter 19** (Finite element analysis)

# 1 Static analysis

Consider the following beam:

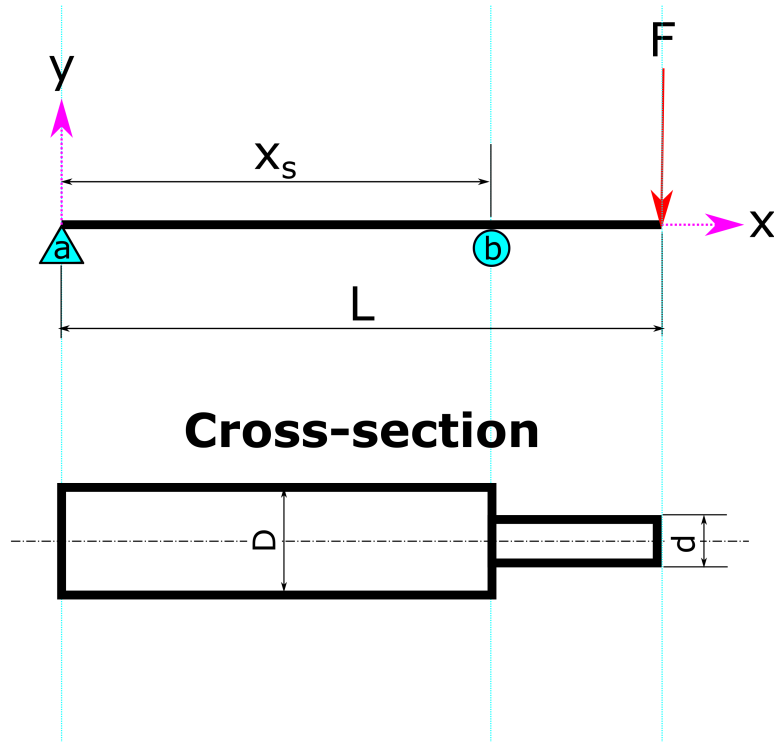


Figure 1: Problem 1

The beam has the following properties:

- Young's modulus: 200 GPa.
- Length of the beam: 2 m.
- Cross-sectional area: Circular.
- Diameters:  $D = 10$  mm,  $d = 5$  mm
- Density:  $7800 \text{ kg/m}^3$
- $F = 50\text{N}$ .
- $x_s = 0.75 \cdot L$

Answer the following questions:

- (a) Calculate the area moment of inertia of the two sections of the beam.
- (b) Prepare the following sanity checks:
  - (i) Calculate the reaction forces.
  - (ii) Calculate the bending moment diagram.
  - (iii) Calculate the normal stress  $xx$  at the top of the beam as a function of  $x$ .
  - (iv) Estimate the displacement at  $x = L$  by assuming the beam has a uniform thickness equal to  $D$ . If you were concerned about large displacements, would this approximation be conservative or not?
- (c) Implement the model in `engmod`:
  - (i) Calculate the reaction forces.
  - (ii) Calculate the bending moment diagram.
  - (iii) Calculate the normal stress  $xx$  at the top of the beam as a function of  $x$ .
  - (iv) Calculate the displacement at  $x = L$ .
  - (v) Use the displacement plot to read the estimate of the displacement at  $x = 0.3 \cdot L$ . Hint: Use the `%matplotlib notebook` magic, and use the cursor.
  - (vi) Verify the correctness of the results.
- (d) The beam needs to be designed to adhere to the following requirements:
  - (i) The safety factor against yielding is at least 2. The yield strength is 300 MPa.
  - (ii) The magnitude of the vertical displacement at  $x = L$  is less than 1mm.

Parametrise the design so that:

$$d = 0.5 \cdot D \tag{1}$$

This means you only have one unknown  $D$  (or  $d$ ).

Specify a feasible  $D$  and  $d$ .

## 2 Dynamic analysis

Consider the following structure:

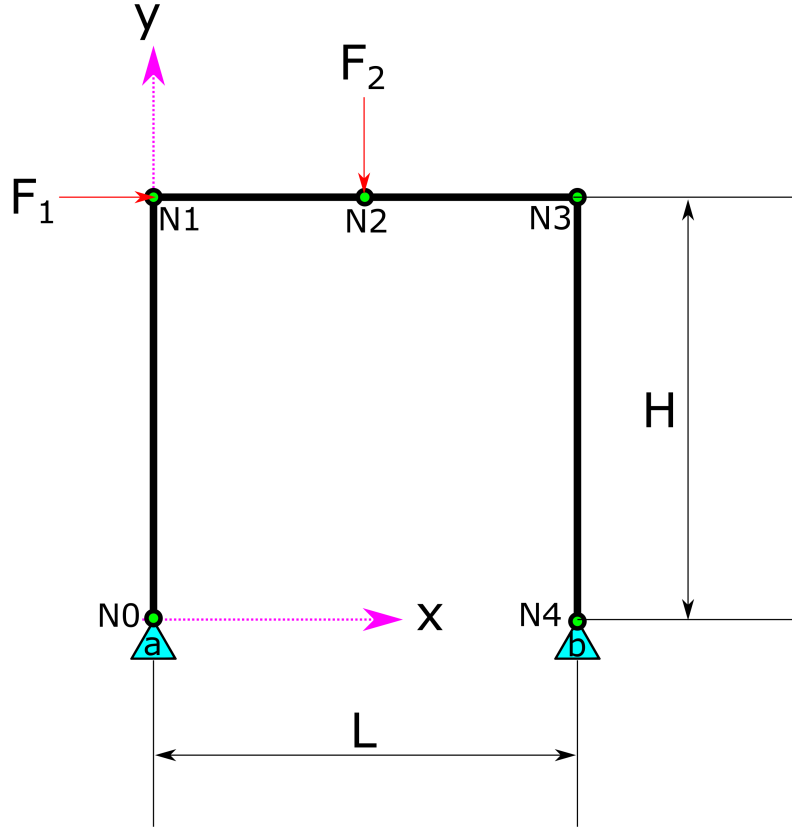


Figure 2: Geometry layout

- Material: Steel.
  - Young's modulus: 200 GPa.
  - Density: 7800 kg/m<sup>3</sup>.
  - Yield strength: 300 MPa.
  - $H = 2\text{m}$ .
  - $L = 1\text{m}$ .
  - Cross-sectional area: Square with a side length of 100mm, i.e. the cross-sectional area is 100<sup>2</sup>mm<sup>2</sup>
- (a) Perform a modal analysis and plot the first five mode shapes. Reflect on the symmetry of the mode shapes and the order of the modes.
- Which excitation frequency do you expect is most dangerous for  $F_1$ ?
  - Which excitation frequency do you expect is most dangerous for  $F_2$ ?
- (b) Apply a static load to node 2 of 1000N in the same direction as the figure. Assume  $F_1 = 0$ . Calculate:

- The vertical displacement at node 2.
- The stiffness for a vertical force at node 2 and a vertical displacement measured at node 2.
- Plot bending moment in the frame.
- Plot the stress in the frame due to bending only. Since the geometry is constant, you can easily parametrise the stress as:

$$\sigma(M) = M \cdot \gamma \quad (2)$$

where the constant  $\gamma = y/I$ .

- Plot the normal stress in the frame in element 0.
- (c) Perform a dynamic analysis by assuming the damping is zero and assuming that the particular solution is equal to the steady-state solution. Calculate the (i) largest absolute bending moment in the structure and (ii) the vertical displacement at node 2<sup>1</sup> for the following excitation forces:
- (a)  $F_2 = 1000 \cdot \cos(\omega \cdot t)$  [N],  $\omega = 1$  rad/s.
  - (b)  $F_2 = 1000 \cdot \cos(\omega \cdot t)$  [N],  $\omega = 2 \cdot \pi \cdot 10$  rad/s.
  - (c)  $F_2 = 1000 \cdot \cos(\omega \cdot t)$  [N],  $\omega = 2 \cdot \pi \cdot 50$  rad/s.
  - (d)  $F_2 = 1000 \cdot \cos(\omega \cdot t)$  [N],  $\omega = 2 \cdot \pi \cdot 81$  rad/s.
  - (e)  $F_2 = 1000 \cdot \cos(\omega \cdot t)$  [N],  $\omega = 2 \cdot \pi \cdot 120$  rad/s.
- (d) Repeat the same process where the magnitude of  $F_1$  is equal to 50 N and  $F_2 = 0$ .
- (e) Repeat the step (c), but use proportional damping of the form  $\mathbf{C}_{ff} = 0.1 \cdot \mathbf{K}_{ff}$ .

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<sup>1</sup>You can access this with  $U[7]$  where  $U$  is the global displacement vector.

### 3 Compliance minimization

Consider the following beam:

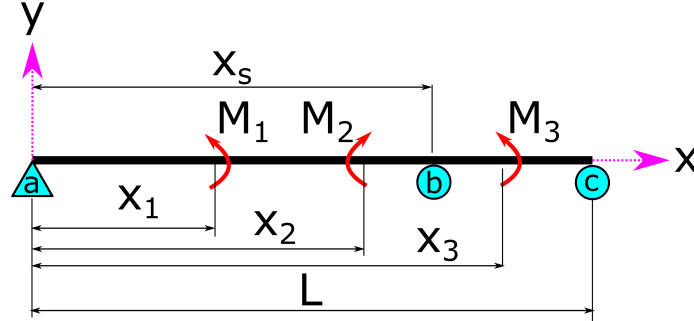


Figure 3: Problem 3

The beam has the following properties:

- Young's modulus: 70 GPa.  $\rho = 2700 \text{ kg/m}^3$ .
- Length of the beam: 1m.
- Cross-sectional area: Rectangular. Cross-sectional dimensions:  $y \times z = 0.020 \times 0.010 \text{ m}^2$ .
- $M_1 = 50 \text{ N.m}$  is applied to Node 4 with the same direction shown in the figure.
- $M_2 = -100 \text{ N.m}$  is applied to Node 10 with the same direction shown in the figure.
- $M_3 = 100 \text{ N.m}$  is applied to Node 15 with the same direction shown in the figure.

Twenty-one node positions are defined: Node 0 has an  $x$ -position of 0m and the last node, Node 20, has a  $x$  position of  $L$ .

- Calculate the compliance of the structure for  $x_s = 0.5 \cdot L$ .
- Calculate the first five natural frequencies of the structure for  $x_s = 0.5 \cdot L$ .
- Perform the following calculation in a for loop: Calculate the compliance, the maximum absolute vertical displacement and the natural frequencies of the structure for the different node positions.
  - Plot the compliance vs. the support position.
  - Plot the natural frequencies vs. the support position.
  - Plot the maximum absolute vertical displacement of the beam vs. the support position.
- What should  $x_s$  be to minimize the compliance?
- What benefits would there be to refine the mesh in this calculation?

## 4 Design

Consider the structure in Figure 4. Each element is connected via truss joints (i.e. cannot transfer moments). Each element should be made from the same cross-sectional geometry (e.g. the cross-sectional properties are the same). The parts will be machined.

The steel has a yield strength of 580MPa and an ultimate strength of 690MPa.  $E = 200$  GPa.  $\rho = 7800$  kg/m<sup>3</sup>.

The following force is applied to the system:

$$f(t) = A_f \cdot \cos(\omega \cdot t) \text{ [N]} \quad (3)$$

The structure is operated in two load cases:

- $A_f = 3000$ ,  $\omega = 2 \cdot \pi$  rad/s.
- $A_f = 2000$ ,  $\omega = 2 \cdot \pi \cdot 100$  rad/s.

- Perform a modal analysis using  $h = 0.01$ m. Are the modes sensitive to  $h$ ?
- Use  $h = 0.01$ m, calculate the stresses in the structure for the two load cases.
- The system must be designed to adhere to the following specifications: The cross-section must be square, i.e.  $A = h^2$ . The structure must have a safety factor of five against buckling using Euler's theory, a safety factor of two against yielding and a safety factor of one against fatigue failure using the modified Goodman theory. All elements have a notch radius of 3mm and a stress concentration factor of 3.0 that needs to be incorporated. Assume that the temperature factor is  $k_d = 1.0$  and use a reliability of 99%.

Does  $h = 0.01$ m satisfy the specifications? If it does not, choose a suitable  $h$ .

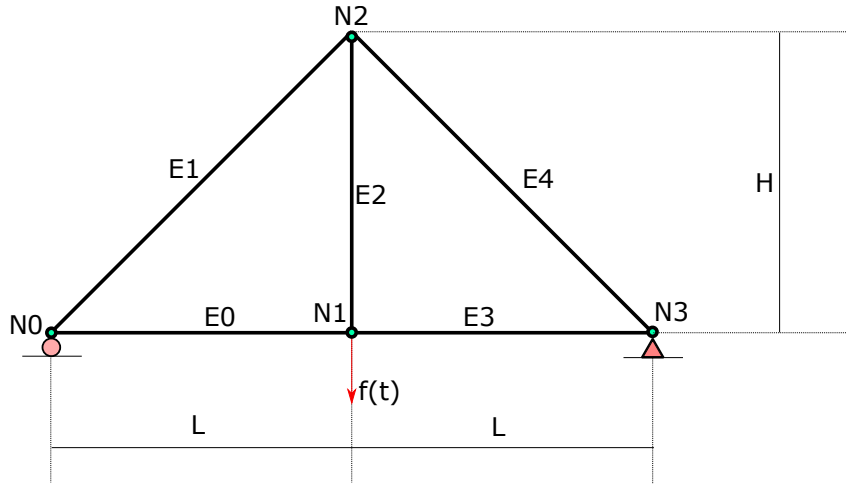


Figure 4: Truss system:  $L = 2$ m;  $H = 2$ m