Validering af model

Voltage drop calculation

Windfarm

$$\begin{split} S_{wind} \coloneqq 5.51 \cdot 10^{3} & \textit{kV} \cdot \textit{A} \qquad V_{wind} \coloneqq 33 & \textit{kV} \qquad \chi'_{dwind} \coloneqq 0.33 \qquad pf_{wind} \coloneqq 0.9 \\ c \coloneqq 1.1 & X''Rratio \coloneqq 10 \\ \phi_{wind} \coloneqq \arccos \left(pf_{wind} \right) = 0.451 \\ Kg_{wind} \coloneqq 1 \cdot \frac{c}{1 + \chi'_{dwind} \cdot \sin \left(\phi_{wind} \right)} = 0.962 \\ X'_{dwind} \coloneqq \chi'_{dwind} \cdot Kg_{wind} \cdot \frac{V_{wind}}{S_{wind}} = 62.721 \; \Omega \qquad \qquad R_g \coloneqq \frac{X'_{dwind}}{X''Rratio} = 6.272 \; \Omega \end{split}$$

Synkron generator

$$\begin{split} S_{pp} &\coloneqq 6.01 \cdot 10^{3} \ \textit{kV} \cdot \textit{A} \qquad V_{pp} \coloneqq 33 \ \textit{kV} \qquad \chi'_{dpp} \coloneqq 0.232 \qquad pf_{pp} \coloneqq 0.8 \\ \phi_{pp} &\coloneqq \arccos \left(pf_{pp} \right) = 0.644 \\ Kg_{pp} &\coloneqq 1 \cdot \frac{c}{1 + \chi'_{dpp} \cdot \sin \left(\phi_{pp} \right)} = 0.966 \\ X'_{dpp} &\coloneqq \chi'_{dpp} \cdot Kg_{pp} \cdot \frac{V_{pp}^{-2}}{S_{pp}} = 40.591 \ \textit{\Omega} \qquad \qquad R_{pp} \coloneqq \frac{X'_{dpp}}{X''Rratio} = 4.059 \ \textit{\Omega} \\ Z_{pp} &\coloneqq R_{pp} + X'_{dpp} \cdot 1i = \left(4.059 + 40.591i \right) \ \textit{\Omega} \end{split}$$

Transformer 15MVA 33/150kV

$$\begin{split} S_{T1} &\coloneqq 15 \cdot 10^{3} \ \textit{kV} \cdot \textit{A} \qquad V_{T1HV} \coloneqq 150 \ \textit{kV} \qquad V_{T1LV} \coloneqq 33 \ \textit{kV} \qquad U_{kT1} \coloneqq 0.0802 \\ P_{T1} &\coloneqq 50 \ \textit{kW} \\ Z_{T1} &\coloneqq U_{kT1} \cdot \frac{V_{T1HV}^{2}}{S_{T1}} = 120.3 \ \textit{\Omega} \qquad \qquad I_{T1} \coloneqq \frac{S_{T1}}{V_{T1HV} \cdot \sqrt{3}} = 57.735 \ \textit{A} \\ R_{T1} &\coloneqq \frac{P_{T1}}{3 \cdot I_{T1}^{2}} = 5 \ \textit{\Omega} \qquad \qquad X_{T1} \coloneqq \sqrt{Z_{T1}^{2} - R_{T1}^{2}} = 120.196 \ \textit{\Omega} \\ Z_{T1} &\coloneqq R_{T1} + X_{T1} \cdot 1i = (120.3 \angle 87.618^{\circ}) \ \textit{\Omega} \end{split}$$

Transformer 15MVA 150/60kV

$$S_{T2} \coloneqq 15 \cdot 10^3 \ kV \cdot A$$
 $V_{T2HV} \coloneqq 150 \ kV$ $V_{T2LV} \coloneqq 60 \ kV$ $U_{kT2} \coloneqq 0.0802$

$$V_{T2HV} = 150 \ kV$$

$$V_{T2LV} = 60 \ kV$$

$$U_{kT2} = 0.0802$$

$$P_{T2} = 50 \ kW$$

$$Z_{T2} \! \coloneqq \! U_{kT2} \! \cdot \! \frac{{V_{T2HV}}^2}{S_{T2}} \! = \! 120.3 \; \Omega$$

$$Z_{T2} \coloneqq U_{kT2} \cdot \frac{{V_{T2HV}}^2}{S_{T2}} = 120.3 \; \Omega \qquad \qquad I_{T2} \coloneqq \frac{S_{T2}}{V_{T2HV} \cdot \sqrt{3}} = 57.735 \; A$$

$$R_{T2} = \frac{P_{T2}}{3 \cdot I_{T2}^2} = 5 \ \Omega$$

$$X_{T2} \coloneqq \sqrt{{Z_{T2}}^2 - {R_{T2}}^2} = 120.196 \ \Omega$$

$$Z_{T2} := R_{T2} + X_{T2} \cdot 1i = (120.3 \angle 87.618^{\circ}) \Omega$$

Transformer 15MVA 60/10kV

$$S_{T3} \coloneqq 15 \cdot 10^3 \quad \textbf{kV} \cdot \textbf{A} \qquad V_{T3HV} \coloneqq 60 \quad \textbf{kV} \qquad V_{T3LV} \coloneqq 10 \quad \textbf{kV} \qquad U_{kT3} \coloneqq 0.0802$$

$$V_{T3HV} = 60 \ kV$$

$$V_{T2IV} = 10 \ kV$$

$$U_{kT3} = 0.0802$$

$$P_{T3} = 50 \ kW$$

$$Z_{T3} \coloneqq U_{kT3} \cdot \frac{{V_{T3HV}}^2}{S_{T3}} = 19.248 \text{ s.}$$

$$Z_{T3} \coloneqq U_{kT3} \cdot \frac{{V_{T3HV}}^2}{S_{T3}} = 19.248 \; \Omega \qquad \qquad I_{T3} \coloneqq \frac{S_{T3}}{V_{T3HV} \cdot \sqrt{3}} = 144.338 \; A$$

$$R_{T3} \coloneqq \frac{P_{T3}}{3 \cdot I_{T3}^2} = 0.8 \ \Omega$$

$$R_{T3} := \frac{P_{T3}}{3 \cdot I_{-}^{2}} = 0.8 \ \Omega$$
 $X_{T3} := \sqrt{Z_{T3}^{2} - R_{T3}^{2}} = 19.231 \ \Omega$

$$Z_{T3} := (R_{T3} + X_{T3} \cdot 1i) = (19.248 \angle 87.618^{\circ}) \Omega$$

Transformer 2.5MVA 10/0.4kV

$$S_{T4} \coloneqq 2.5 \cdot 10^3 \ \textbf{\textit{kV}} \cdot \textbf{\textit{A}} \qquad V_{T4HV} \coloneqq 10 \ \textbf{\textit{kV}} \qquad V_{T4LV} \coloneqq 0.4 \ \textbf{\textit{kV}} \qquad U_{kT4} \coloneqq 0.06$$

$$V_{T4HV} = 10 \ kV$$

$$V_{T4LV} = 0.4 \ kV$$

$$U_{1m4} = 0.06$$

$$P_{TA} = 19 \ kW$$

$$Z_{T4}\!\coloneqq\!U_{kT4}\!\cdot\!rac{{V_{T4HV}}^2}{S_{T4}}\!=\!2.4~\Omega$$

$$Z_{T4} \coloneqq U_{kT4} \cdot \frac{{V_{T4HV}}^2}{S_{T4}} = 2.4 \; \Omega \qquad \qquad I_{T4} \coloneqq \frac{S_{T4}}{V_{T4HV} \cdot \sqrt{3}} = 144.338 \; A$$

$$R_{T4} = \frac{P_{T4}}{3 \cdot I_{T4}^2} = 0.304 \ \Omega$$
 $X_{T4} = \sqrt{Z_{T4}^2 - R_{T4}^2} = 2.381 \ \Omega$

$$X_{T4} \coloneqq \sqrt{Z_{T4}^2 - R_{T4}^2} = 2.381 \text{ so}$$

$$Z_{T4} := (R_{T4} + X_{T4} \cdot 1i) = (0.304 + 2.381i) \Omega$$

Transmission cable 150kV

$$R_{150kV}\!\coloneqq\!0.194\;\frac{\it \Omega}{\it km} \qquad X_{150kV}\!\coloneqq\!0.4\;\frac{\it \Omega}{\it km} \qquad \quad L_{c150kV}\!\coloneqq\!50\;\it km$$

$$R_{c150kV} \coloneqq R_{150kV} \bullet L_{c150kV} = 9.7 \; \mathbf{\Omega} \qquad \qquad X_{c150kV} \coloneqq X_{150kV} \bullet L_{c150kV} = 20 \; \mathbf{\Omega}$$

$$Z_{c150kV} := R_{c150kV} + X_{c150kV} \cdot 1i = (22.228 \angle 64.127^{\circ}) \Omega$$

Transmission cable 60kV

$$R_{60kV} = 0.8342 \frac{\Omega}{km}$$
 $X_{60kV} = 0.43 \frac{\Omega}{km}$ $L_{c60kV} = 20 \text{ km}$

$$R_{c60kV} \coloneqq R_{60kV} \cdot L_{c60kV} = 16.684 \ \Omega \qquad \qquad X_{c60kV} \coloneqq X_{60kV} \cdot L_{c60kV} = 8.6 \ \Omega$$

$$Z_{c60kV} := R_{c60kV} + X_{c60kV} \cdot 1i = (18.77 \angle 27.269^{\circ}) \Omega$$

Windfarm cable 33kV

$$R_{33kV} \coloneqq 0.1021 \; \frac{\varOmega}{\pmb{km}} \quad X_{33kV} \coloneqq 0.1445 \; \frac{\varOmega}{\pmb{km}} \quad L_{c33kV} \coloneqq 35 \; \pmb{km}$$

$$R_{c33kV} := R_{33kV} \cdot L_{c33kV} = 3.574 \ \Omega$$
 $X_{c33kV} := X_{33kV} \cdot L_{c33kV} = 5.058 \ \Omega$

$$Z_{c33kV}\!\coloneqq\!R_{c33kV}\!+\!X_{c33kV}\!\cdot\!1\mathrm{i}\!=\!\left(6.193\! \angle 54.756^\circ\right) \mathbf{\Omega}$$

Distribution cable 10kV

$$R_{10kV}\!\coloneqq\!0.1571\;\frac{\varOmega}{\pmb{km}} \quad X_{10kV}\!\coloneqq\!0.31\;\frac{\varOmega}{\pmb{km}} \qquad L_{c10kV}\!\coloneqq\!10\;\pmb{km}$$

$$R_{c10kV}\!\coloneqq\!R_{10kV}\!\cdot\!L_{c10kV}\!=\!1.571\;\mathbf{\Omega} \qquad \qquad X_{c10kV}\!\coloneqq\!X_{10kV}\!\cdot\!L_{c10kV}\!=\!3.1\;\mathbf{\Omega}$$

$$Z_{c10kV} := R_{c10kV} + X_{c10kV} \cdot 1i = (3.475 \angle 63.125^{\circ}) \Omega$$

Byer

$$P_{by}\!\coloneqq\!0.5\;\textit{MW} \quad Q_{by}\!\coloneqq\!0.242\;\textit{MW} \quad S_{by}\!\coloneqq\!\sqrt{{P_{by}}^2+{Q_{by}}^2}=0.555\;\textit{MW} \qquad V_{by}\!\coloneqq\!0.333\;\textit{kV}$$

$$Z_{by}\!\coloneqq\!\frac{{V_{by}}^2}{S_{by}}\!=\!0.2\;\mathbf{\Omega}$$

$$R_{by} := Z_{by} \cdot \frac{P_{by}}{S_{by}} = 0.18 \ \Omega$$
 $X_{by} := \sqrt{Z_{by}^2 - R_{by}^2} = 0.087 \ \Omega$

$$Z_{by} := R_{by} + X_{by} \cdot 1i = (0.2 \angle 25.827^{\circ}) \Omega$$

Equivalent circuit

Source impedance

$$a_1 \coloneqq \frac{V_{T1LV}}{V_{T1HV}} = 0.22 \qquad a_2 \coloneqq \frac{V_{T2LV}}{V_{T2HV}} = 0.4 \qquad a_3 \coloneqq \frac{V_{T3LV}}{V_{T3HV}} = 0.167 \qquad a_4 \coloneqq \frac{V_{T4LV}}{V_{T4HV}} = 0.167 \qquad a_5 \coloneqq \frac{V_{T4LV}}{V_{T4HV}} = 0.167 \qquad a_7 \coloneqq \frac{V_{T4LV}}{V_{T4HV}} = 0.1$$

$$Z_{pp'} := Z_{pp} \cdot \left(\frac{1}{a_1}\right)^2 \cdot a_2^2 \cdot a_3^2 = (0.373 + 3.727i) \Omega$$

$$Z_{T1'} = Z_{T1} \cdot a_2^2 \cdot a_3^2 = (0.022 + 0.534i) \Omega$$

$$Z_{c150kV} := Z_{c150kV} \cdot a_2^2 \cdot a_3^2 = (0.043 + 0.089i) \Omega$$

$$Z_{T2'} := Z_{T2} \cdot a_2^2 \cdot a_3^2 = (0.022 + 0.534i) \Omega$$

$$Z_{c60kV} := Z_{c60kV} \cdot a_3^2 = (0.463 + 0.239i) \Omega$$

$$Z_{T3} := Z_{T3} \cdot a_3^2 = (0.022 + 0.534i) \Omega$$

$$Z_{source} := Z_{T1'} + Z_{c150kV'} + Z_{T2'} + Z_{c60kV'} + Z_{T3'} = (2.014 \angle 73.461^{\circ}) \Omega$$

Load impedance

$$Z_{by'}\!\coloneqq\!Z_{by}\!\cdot\!\left(\!\frac{1}{a_4}\!\right)^2 =\!\left(124.766\angle 25.827^\circ\right)\,\mathbf{\Omega}$$

$$Z_{load} \coloneqq Z_{c10kV} + \frac{1}{\left(Z_{c10kV} + \frac{1}{\left(Z_{c10kV} + Z_{T4} + Z_{by'}\right)^{-1} + \left(Z_{T4} + Z_{by'}\right)^{-1}}\right)^{-1} + \left(Z_{T4} + Z_{by'}\right)^{-1} + \left(Z_{c10kV} + \frac{1}{\left(Z_{c10kV} + Z_{T4} + Z_{by'}\right)^{-1}}\right)^{-1} + \left(Z_{T4} + Z_{by'}\right)^{-1} + \left(Z_{C10kV} + Z_{C10kV} + Z_{C10kV} + Z_{C10kV}\right)^{-1}}$$

$$Z_{load} = (24.724 + 15.665i) \Omega$$

Spændingsfald

Beregning

$$\boldsymbol{V}_{10kVact} \!\coloneqq\! \boldsymbol{V}_{T4HV} \! \cdot\! \frac{\boldsymbol{Z}_{load}}{\boldsymbol{Z}_{load} \!+\! \boldsymbol{Z}_{source}} \!=\! \left(9.498 \angle \!-\! 2.462^\circ\right) \boldsymbol{kV}$$

Simulering

$$V_{10kVsim} = (9.452 \angle -2.465 \ deg) \ kV$$

$$V_{10kVpu} = 0.945$$

SC calculation

Synkron gennerator kortslutningsimpedans

$$S_{pp} \coloneqq 6.01 \cdot 10^3 \ \textbf{kV} \cdot \textbf{A} \qquad V_{pp} \coloneqq 33 \ \textbf{kV} \qquad \chi''_{dpp} \coloneqq 0.12 \qquad pf_{pp} \coloneqq 0.8$$

$$V_{nn} = 33 \ kV$$

$$\chi''_{dpp} := 0.12$$

$$pf_{nn} = 0.8$$

$$S_{ppSC} \coloneqq \frac{S_{pp}}{\chi''_{dpp}} = 50.083 \; \boldsymbol{MW}$$

$$\phi_{pp} \coloneqq \operatorname{acos}\left(pf_{pp}\right) = 0.644$$

$$Kg_{pp} \coloneqq 1 \cdot \frac{c}{1 + \chi''_{dpp} \cdot \sin\left(\phi_{pp}\right)} = 1.026$$

$$X''_{dpp} \coloneqq \chi''_{dpp} \cdot Kg_{pp} \cdot \frac{{V_{pp}}^2}{S_{pp}} = 22.312 \; \boldsymbol{\Omega} \qquad \qquad R_{pp} \coloneqq \frac{X''_{dpp}}{X''Rratio} = 2.231 \; \boldsymbol{\Omega}$$

$$R_{pp} \coloneqq \frac{X''_{dpp}}{X''Bratio} = 2.231 \Omega$$

$$Z_{ppSC} := R_{pp} + X''_{dpp} \cdot 1i = (2.231 + 22.312i) \Omega$$

System kortslutningsimpedans

$$Z_{ppSC'} := Z_{ppSC} \cdot \left(\frac{1}{a_1}\right)^2 \cdot a_2^2 \cdot a_3^2 = (0.205 + 2.049i) \Omega$$

$$Z_{SC} \coloneqq Z_{ppSC'} + Z_{T1'} + Z_{c150kV'} + Z_{T2'} + Z_{c60kV'} + Z_{T3'} = \left(4.055 \angle 78.936^{\circ}\right) \mathbf{\Omega}$$

Beregning

$$I_{SCact} \coloneqq \left| \frac{c \cdot V_{T3LV}}{\sqrt{3} \cdot Z_{SC}} \right| = 1.57 \ \textit{kA}$$

Simulering

$$I_{SCsim} = 1.57 \text{ kA}$$