电子电路与系统基础(B2)---非线性电路

第14讲:作业选讲

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# B 课程 内容安排

第一学期:线性	序号	第二学期: 非线性
电路定律	1	器件基础
电阻电源	2	二极管
电容电感	3	MOSFET
信号分析	4	вјт
分压分流	5	反相电路
正弦稳态	6	数字门
时频特性	7	放大器
期中复习	8	期中复习
RLC二阶	9	负反馈
二阶时频	10	差分放大
受控源	11	频率特性
网络参量	12	正反馈
典型网络	13	振荡器
作业选讲	14	作业选讲
期末复习	15	期末复习

# 晶体管的两种基本应用

- 晶体管的受控非线性电阻特性可以有两种基本应用
  - 开关应用
    - 晶体管在欧姆导通区和截止区之间来回翻转,形成"导通闭合"、"截止 开路"的开关特性
      - 数字门电路
        - 利用开关通断实现0、1二值逻辑运算
      - 开关电容滤波电路
        - 用开关电容实现电荷转移来模拟电阻上的电荷转移(电流)
      - ■能量转换电路
        - 利用开关的无损性实现高效率的电能转换
  - 受控源应用
    - 晶体管在恒流导通区工作,DS受控非线性电阻具有受控电流源特性,具有 向端口外提供电能的有源功能
      - 电流源
      - 放大器
      - 振荡器

# 开关电路应用1: 数字门电路

- 开关串联与运算,开关并联或运算
- PMOS开关: 反相开关先求非
- NMOS开关: 旁路开关后求非
- 标准CMOS门电路属德摩根律的具体应用
  - Complementary: 互补
    - N串则P并
      - 与非=非或
    - N并则P串
      - 或非=非与

# 作业6.1 加法器设计

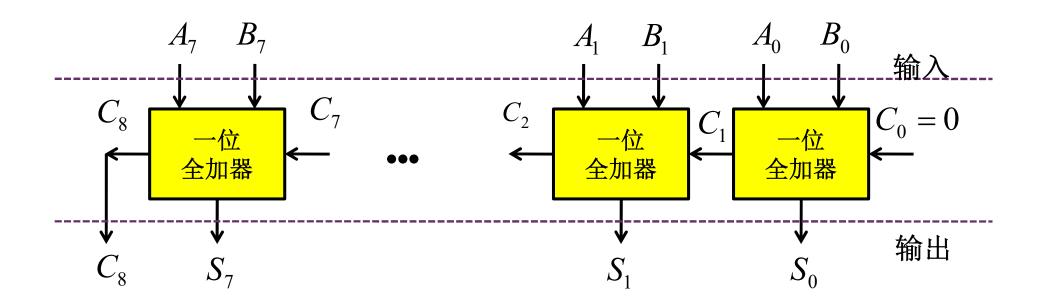
$$\begin{array}{rrr}
 & 10110100 & 180 \\
 +11101101 & +237 \\
 \hline
 & 110100001 & 417
\end{array}$$

■二进制加法运算

对每一位i,都是 $A_i+B_i+C_i$ ,产生和 $S_i$ 以及进位 $C_{i+1}$ 

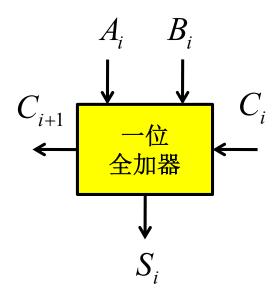
# 加法器系统框架

- 一位一位地加,同时考虑进位
  - 8个一位全加器级联,即可实现两个8位二进制数的相加功能



# 一位全加器设计

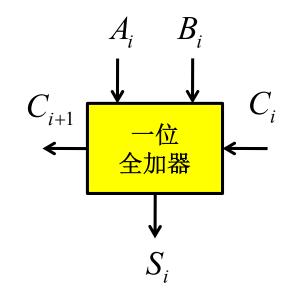
$\mathbf{A_i}$	$\mathbf{B_i}$	$\mathbf{C_i}$	$\mathbf{C}_{i+1}$	S <sub>i</sub>
0	0	0		
0	0	1		
0	1	0		
0	1	1		
1	0	0		
1	0	1		
1	1	0		
1	1	1		



- 填写真值表
- ■用卡诺图化简
- 用CMOS晶体管实现
  - 教材例题跟做一遍

## 真值表就是对功能的具体描述

$\mathbf{A_i}$	$\mathbf{B_i}$	$\mathbf{C_i}$	$\mathbf{C}_{i+1}$	S <sub>i</sub>
0	0	0	0	0
0	0	1	0	1
0	1	0	0	1
0	1	1	1	0
1	0	0	0	1
1	0	1	1	0
1	1	0	1	0
1	1	1	1	1



$$S_{i} = \overline{A_{i}} \cdot \overline{B_{i}} \cdot C_{i} + \overline{A_{i}} \cdot B_{i} \cdot \overline{C_{i}}$$
$$+ A_{i} \cdot \overline{B_{i}} \cdot \overline{C_{i}} + A_{i} \cdot B_{i} \cdot C_{i}$$

$$\begin{split} C_{i+1} &= \overline{A_i} \cdot B_i \cdot C_i + A_i \cdot \overline{B_i} \cdot C_i \\ &+ A_i \cdot B_i \cdot \overline{C_i} + A_i \cdot B_i \cdot C_i \end{split}$$

# 卡诺图化简

$$S_{i} = \overline{A_{i}} \cdot \overline{B_{i}} \cdot C_{i} + \overline{A_{i}} \cdot B_{i} \cdot \overline{C_{i}}$$
$$+ A_{i} \cdot \overline{B_{i}} \cdot \overline{C_{i}} + A_{i} \cdot B_{i} \cdot C_{i}$$

C \AB	00	01	11	10
0	0		0	
1		0	1	0

$$C_{i+1} = \overline{A_i} \cdot B_i \cdot C_i + A_i \cdot \overline{B_i} \cdot C_i$$
$$+ A_i \cdot B_i \cdot \overline{C_i} + A_i \cdot B_i \cdot C_i$$

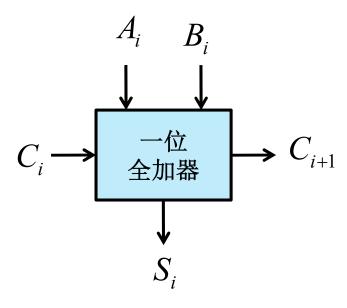
C \AB	00	01	11	10
0	0	0	1	0
1	0	$\bigcirc 1$		1)

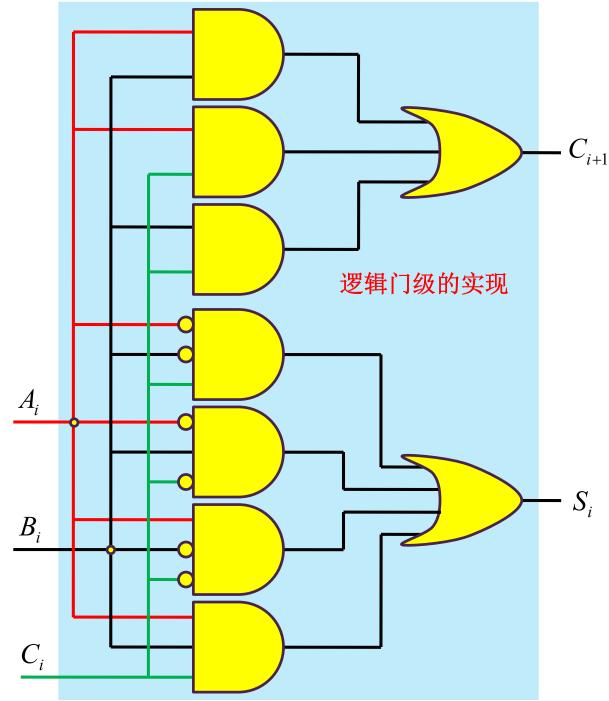
$$C_{i+1} = A_i B_i + B_i C_i + A_i C_i$$

# 逻辑级实现

$$S_{i} = \overline{A_{i}} \cdot \overline{B_{i}} \cdot C_{i} + \overline{A_{i}} \cdot B_{i} \cdot \overline{C_{i}}$$
$$+ A_{i} \cdot \overline{B_{i}} \cdot \overline{C_{i}} + A_{i} \cdot B_{i} \cdot C_{i}$$

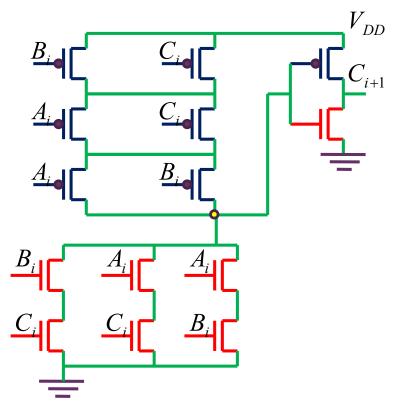
$$C_{i+1} = B_i \cdot C_i + A_i \cdot C_i + A_i \cdot B_i$$





# 进位逻辑的晶体管级实现

$$C_{i+1} = B_i \cdot C_i + A_i \cdot C_i + A_i \cdot B_i$$



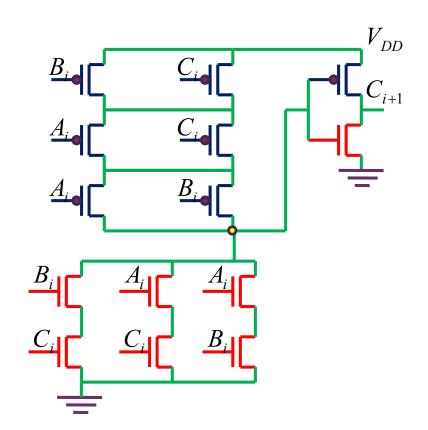
14个晶体管,5层垒叠

# 逻辑表达式整理后可降低晶体管个数

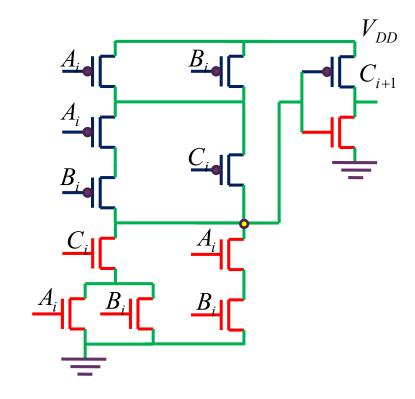
### 一个输入对应两个晶体管:减少输入个数

$$C_{i+1} = B_i \cdot C_i + A_i \cdot C_i + A_i \cdot B_i$$

$$C_{i+1} = (A_i + B_i)C_i + A_iB_i$$

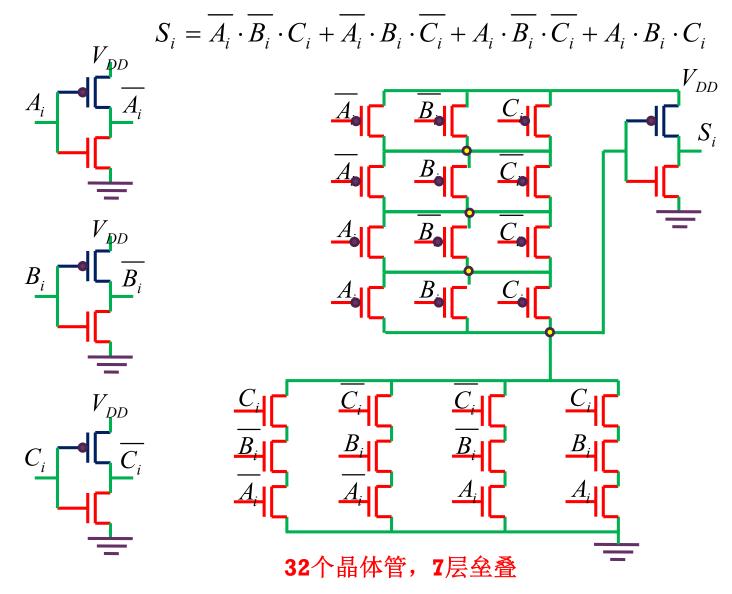


14个晶体管,5层垒叠



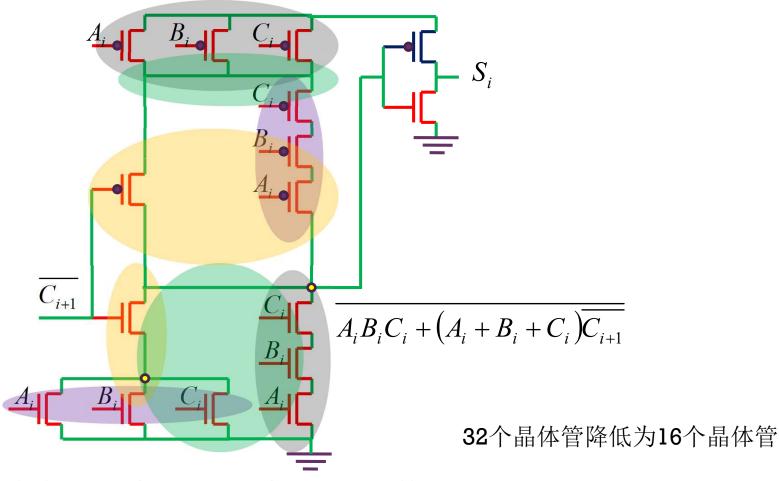
12个晶体管,5层垒叠

# 和位逻辑晶体管级实现



# 教材上给出的逻辑化简

$$S_i = \overline{A_i} \cdot \overline{B_i} \cdot C_i + \overline{A_i} \cdot B_i \cdot \overline{C_i} + A_i \cdot \overline{B_i} \cdot \overline{C_i} + A_i \cdot B_i \cdot C_i$$
  
=  $A_i \cdot B_i \cdot C_i + (A_i + B_i + C_i) \cdot \overline{C_{i+1}}$  把12个输入降低为7个输入



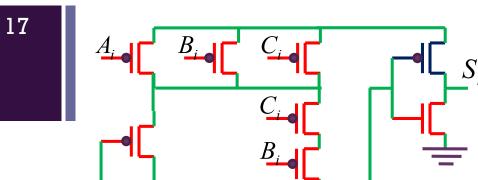
简化逻辑的证明 
$$S_i = \overline{A_i} \cdot \overline{B_i} \cdot C_i + \overline{A_i} \cdot B_i \cdot \overline{C_i} + A_i \cdot \overline{B_i} \cdot \overline{C_i} + A_i \cdot B_i \cdot C_i$$

$$= A_i \cdot B_i \cdot C_i + (A_i + B_i + C_i) \cdot \overline{C_{i+1}}$$

$A_{i}$	$B_{i}$	$C_{i}$	$C_{i+1}$	$S_{i}$	$\overline{C_{i+1}}$	$(A_i + B_i + C_i)$		$A_iB_iC_i$	
0	0	0	0	0	1	0	0	0	0
0	0	1	0	1	1	1	1	0	1
0	1	0	0	1	1	1	1	0	1
0	1	1	1	0	0	1	0	0	0
1	0	0	0	1	1	1	1	0	1
1	0	1	1	0	0	1	0	0	0
1	1	0	1	0	0	1	0	0	0
1	1	1	1	1	0	1	0	1	1
	两ク三ク	/ <b>1</b> 或 <b>1</b>	→ 一个 三个		↑ 没有1或 一个1	↑ 有 <b>1</b> 即可 -	^ - <b>^1</b>	↑ 三 <b>个1</b>	一个 <b>1</b> 或 三个 <b>1</b>

另一个简化逻辑 
$$S_{i} = \overline{A_{i}} \cdot \overline{B_{i}} \cdot C_{i} + \overline{A_{i}} \cdot B_{i} \cdot \overline{C_{i}} + A_{i} \cdot \overline{B_{i}} \cdot \overline{C_{i}} + A_{i} \cdot B_{i} \cdot C_{i}$$
$$= A_{i} \cdot B_{i} \cdot C_{i} + (A_{i} + B_{i} + C_{i}) \cdot \overline{C_{i+1}}$$
$$= (A_{i} + B_{i} + C_{i}) \cdot (A_{i} \cdot B_{i} \cdot C_{i} + \overline{C_{i+1}})$$

$A_{i}$	$B_{i}$	$C_{i}$	$C_{i+1}$	$S_{i}$	$\overline{C_{i+1}}$	$A_iB_iC_i$		$(A_i + B_i + C_i)$	
0	0	0	0	0	1	0	1	0	0
0	0	1	0	1	1	0	1	1	1
0	1	0	0	1	1	0	1	1	1
0	1	1	1	0	0	0	0	1	0
1	0	0	0	1	1	0	1	1	1
1	0	1	1	0	0	0	0	1	0
1	1	0	1	0	0	0	0	1	0
1	1	1	1	1	0	1	1	1	1
	两ク三ク	/     	→ 一个 三个		↑ 没有1頭 一个1	<b>戊</b> 三 <b>个1</b>	↑ 没有 一个		一个 <b>1</b> 或 三个 <b>1</b>
				•	, .		三个		<b>→ 1 </b>



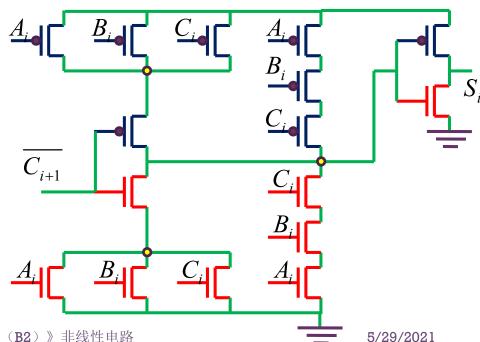
## 等同逻辑合用

 $S_{i} = \overline{A_{i}} \cdot \overline{B_{i}} \cdot C_{i} + \overline{A_{i}} \cdot B_{i} \cdot \overline{C_{i}} + A_{i} \cdot \overline{B_{i}} \cdot \overline{C_{i}} + A_{i} \cdot B_{i} \cdot C_{i}$  $= A_i \cdot B_i \cdot C_i + (A_i + B_i + C_i) \cdot \overline{C_{i+1}}$  $= \left(A_i + B_i + C_i\right) \cdot \left(A_i \cdot B_i \cdot C_i + \overline{C_{i+1}}\right)$ 

## 功能完全一样

 $\overline{C_{i+1}}$ 

但后者更对称, 更紧致

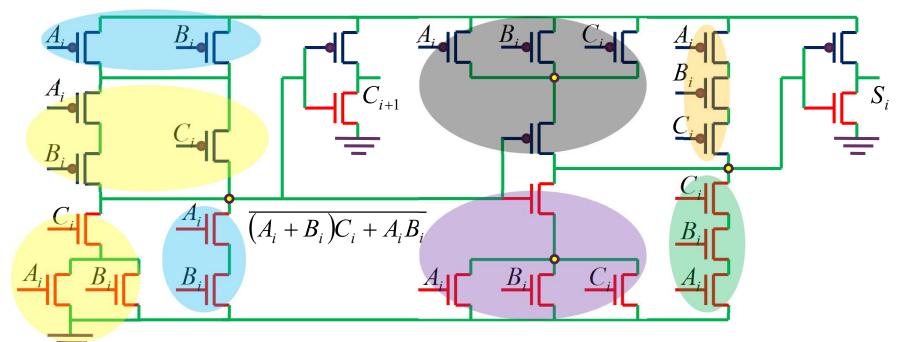


# 一位全加器的CMOS晶体管级实现

$$C_{i+1} = B_i C_i + A_i C_i + A_i B_i = (A_i + B_i) C_i + A_i B_i$$

$$S_{i} = \overline{A_{i}} \cdot \overline{B_{i}} \cdot C_{i} + \overline{A_{i}} \cdot B_{i} \cdot \overline{C_{i}} + A_{i} \cdot \overline{B_{i}} \cdot \overline{C_{i}} + A_{i} \cdot B_{i} \cdot C_{i} = A_{i} \cdot B_{i} \cdot C_{i} + (A_{i} + B_{i} + C_{i}) \cdot \overline{C_{i+1}}$$

$$= (A_{i} + B_{i} + C_{i}) \cdot (A_{i} \cdot B_{i} \cdot C_{i} + \overline{C_{i+1}})$$



- 1、用了28个晶体管实现了一位全加器;晶体管数目少
- 2、输出用反相器, 犹如缓冲器, 输出逻辑电平更稳定

# 作业6.2 卡诺图化简

- 1、化简卡诺图,写出输出Z用ABCD表述的逻辑表达式
- 2、用PMOS互补NMOS的CMOS电路形态(上P下N,形式互补) 实现这些逻辑运算,画出CMOS晶体管级电路图
- 3、如果有与门、或门、非门电路可供选用,用与、或、非门实现 上述逻辑
- 4、如果只有二输入的与非门可供选用,如何用与非门实现前述逻 辑?

AB \ CD	00	01	11	10
00	1	0	0	1
01	0	1	*	*
11	1	1	*	1
10	1	*	0	1

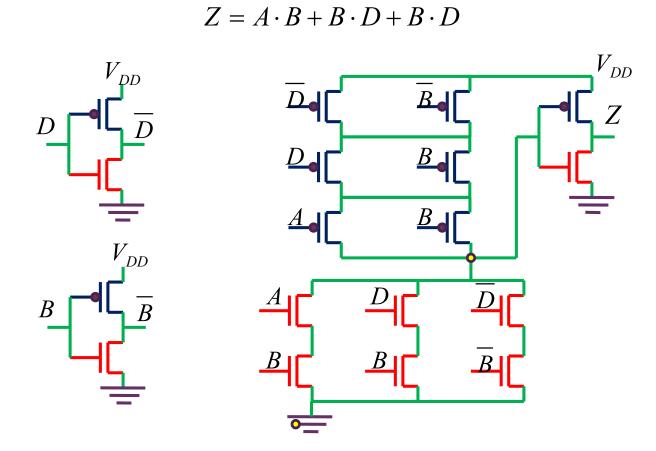
# 卡诺图化简

AB \ CD	00	01	11	10
00	1	0	0	1
01	0	1	*	*
11	1	1	*	1
10	1	*	0	1

$$Z = A \cdot B + B \cdot D + \overline{B \cdot D}$$

### 表述不唯一

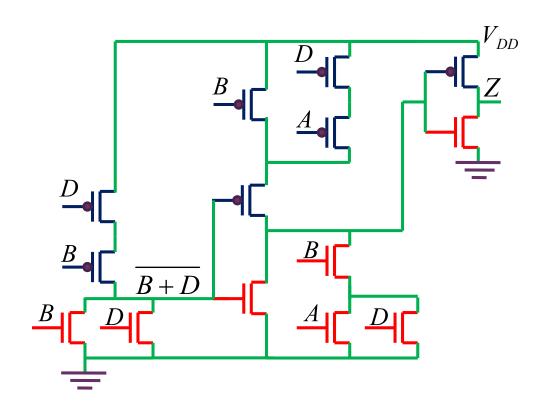
# CMOS晶体管级实现



18个晶体管,5层垒叠

# 晶体管数目减少的措施

$$Z = A \cdot B + B \cdot D + \overline{B} \cdot \overline{D} = B \cdot (A + D) + \overline{B + D}$$

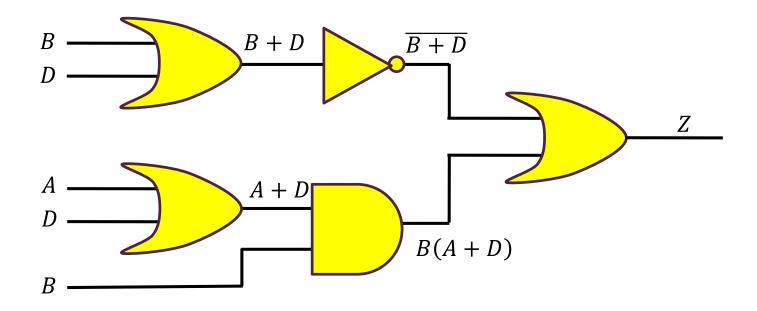


14个晶体管,5层垒叠

## 逻辑级实现

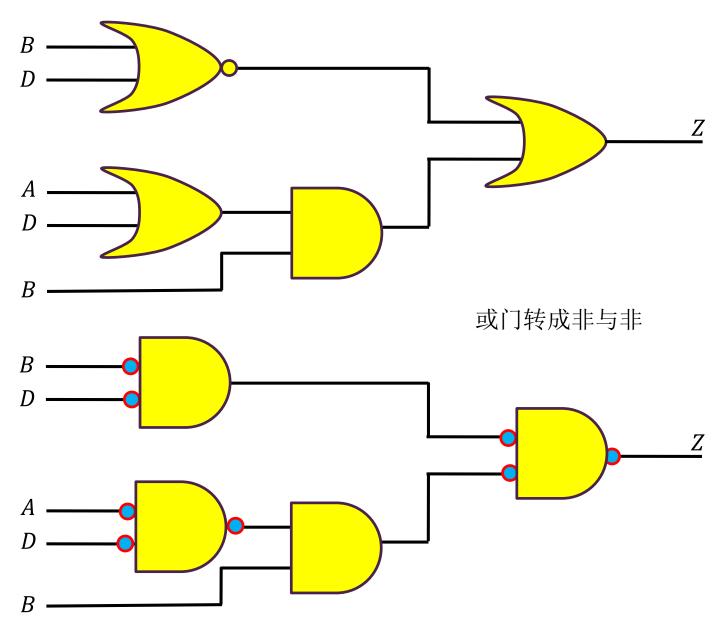
如果有与门、或门、非门电路可供选用,用与、或、非门实现上述逻辑

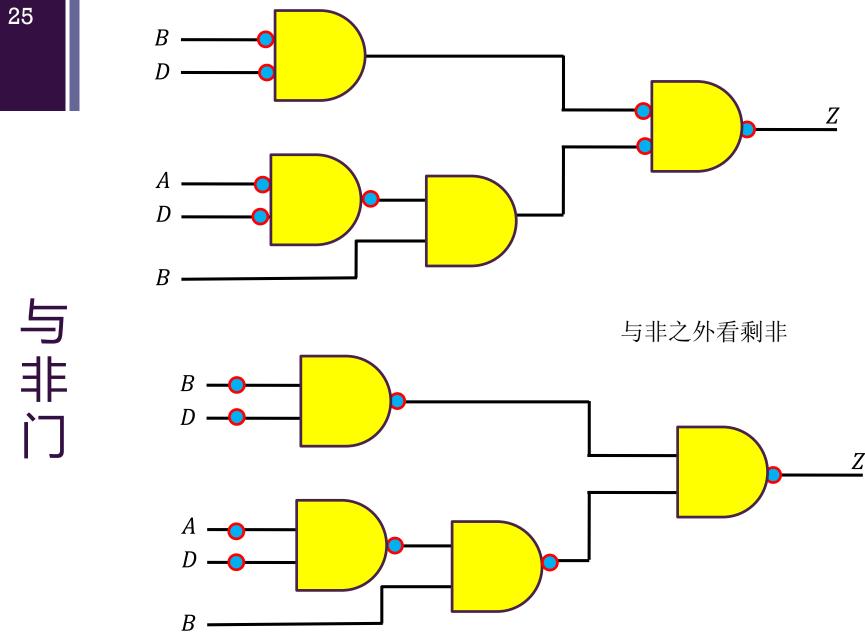
$$Z = A \cdot B + B \cdot D + \overline{B} \cdot \overline{D} = B \cdot (A + D) + \overline{B + D}$$



# — 输 入与非 门实现

$$Z = A \cdot B + B \cdot D + \overline{B} \cdot \overline{D} = B \cdot (A + D) + \overline{B + D}$$



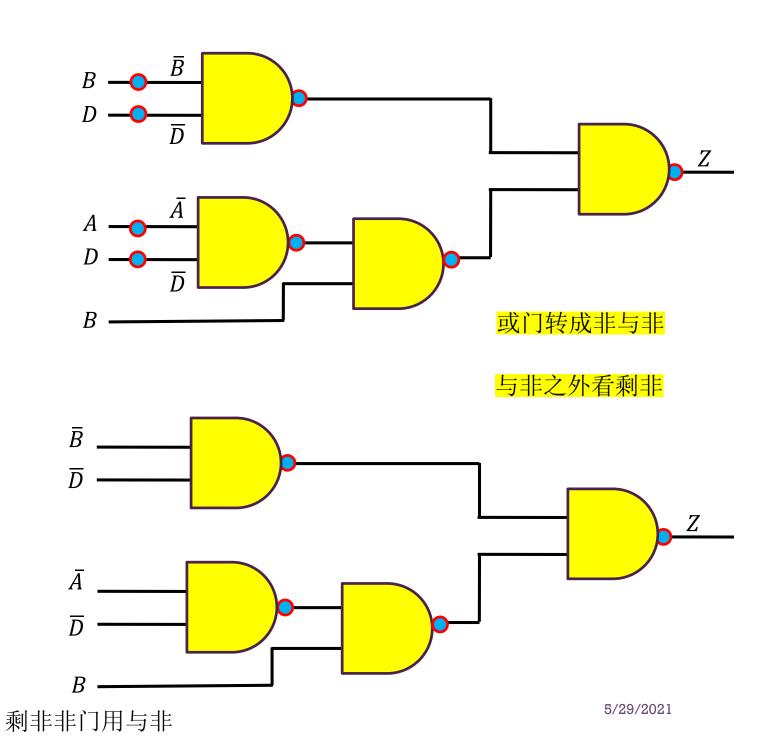


# 非门实现

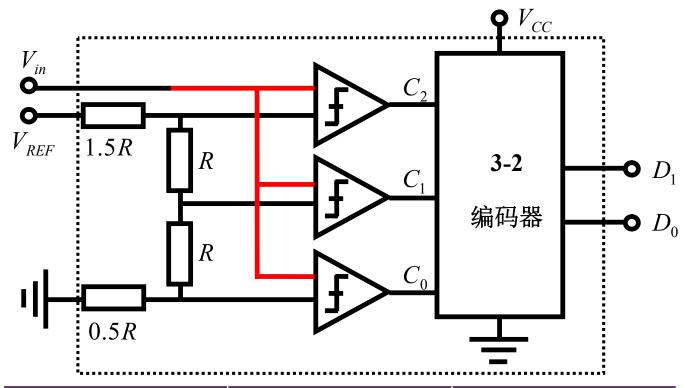
D

 $\overline{B}$ 

 $\overline{D}$ 



# 作业6.3 Flash ADC 编码器设计



模拟输入电压	$\mathbf{C}_2\mathbf{C}_1\mathbf{C}_0$	数字输出码 $\mathbf{D_1}\mathbf{D_0}$
~1/8V <sub>REF</sub>	000	00
$1/8V_{REF}$ ~ $3/8V_{REF}$	001	01
$3/8V_{REF}\sim5/8V_{REF}$	011	10
5/8V <sub>REF</sub> ~	111	11

## 编码器设计

- 已知flash-ADC的码表如 左图
- 给出逻辑表达式,用与非 门实现上述逻辑表达式
- 画出编码器的CMOS实现 方案

$\mathbf{C}_2\mathbf{C}_1\mathbf{C}_0$	数字输出码 $\mathbf{D_1D_0}$
000	00
001	01
011	10
111	11

三个输入变量,共8种情况,这里仅 有4种情况

剩下4种情况真值表中都是\*(是0是1 不在乎),因为在实际电路中,这4种 情况不会也不应该出现

# 从码表到卡诺图

$\mathbf{C_2C_1C_0}$	数字输出码 $\mathbf{D_1}\mathbf{D_0}$
000	00
001	01
011	10
111	11

 $\mathbf{D}_1$ 

$\mathbf{C}_2 \setminus \mathbf{C}_1 \mathbf{C}_0$	00	01	11	10
0	0	0	1	*
1	*	*	1	*

$$D_1 = C_1$$

 $\mathbf{D}_{0}$ 

$\mathbf{C}_2 \backslash \mathbf{C}_1 \mathbf{C}_0$	00	01	11	10
0	0	1	0	*
1	*	*	1	*

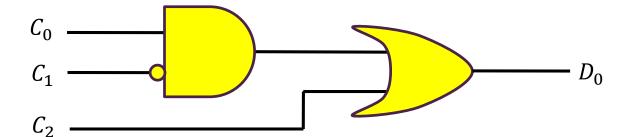
$$D_0 = C_2 + \overline{C_1} \cdot C_0$$

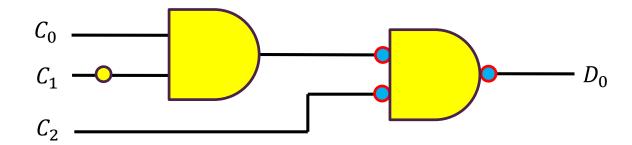
## 与非门实现

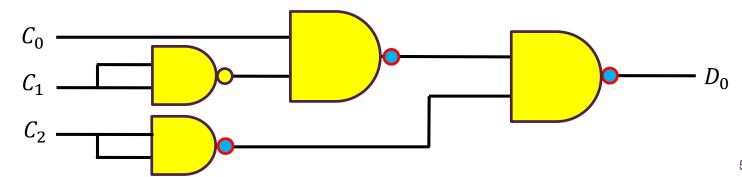
$$D_1 = C_1$$

$$C_1$$
 —  $D_1$ 

$$D_0 = C_2 + \overline{C_1} \cdot C_0$$





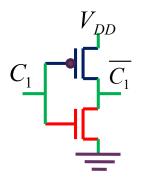


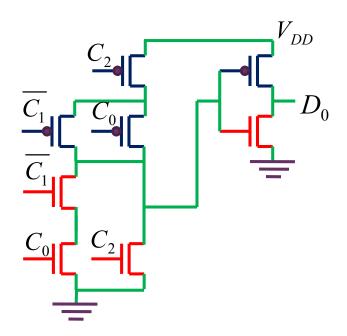
# CMOS晶体管级实现

$$D_1 = C_1$$

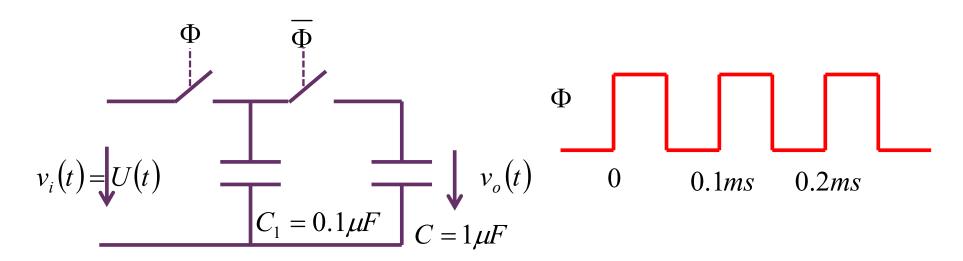
$$C_1 - D$$

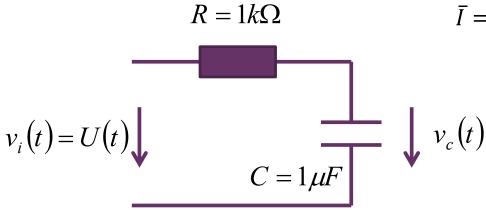
$$D_0 = C_2 + \overline{C_1} \cdot C_0$$





# 开关应用2: 开关电容滤波器



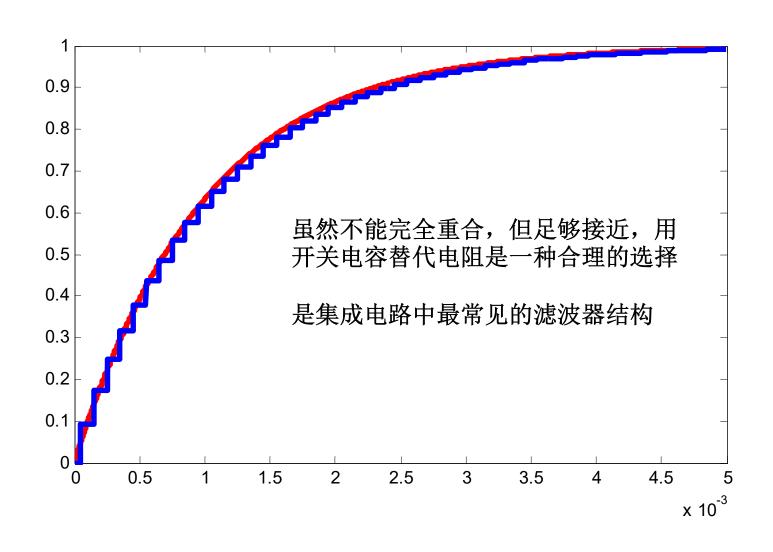


$$\bar{I} = \frac{\Delta Q}{T} = \frac{CV_1 - CV_2}{T} = C\frac{\Delta V}{T} = \frac{\Delta V}{T/C} = \frac{\Delta V}{R_{eff}}$$

开关电容实现的电荷转移被用来拟合电阻上的电流

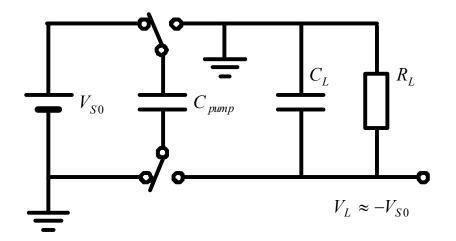
$$R_{eff} = \frac{T}{C}$$

# 阶跃响应的一致性说明滤波特性的一致性



# 开关应用3:能量转换电路 作业6.4 开关电容做DC-DC转换电路

■ 习题9.9 开关电容实现反压 两个开关在占空比为50%的时钟控制下,在前50%方波周期内使得泵电容C<sub>pupm</sub>接到直流电压源V<sub>so</sub>上,从 V<sub>so</sub>上获取电荷(电能),后50%方波周期内再接到负载电路上,泵 电容将部分电荷转移到滤波电容C<sub>L</sub>上,在泵电容接电源的50%周期内,滤波电容为负载提供电能。分析当电路进入稳态后,输出反相直流电压的纹波电压为多少?分析提高能量转换效率的措施?



和前一个**RC**滤波电路的相同点: 中间有一个泵电容做电荷**中转站** 

### 和前一个RC滤波电路的区别:

- 1、双掷开关使得两个电路不共地(完全隔离)
- 2、有负载电阻一直在耗能: DC-DC转换电路

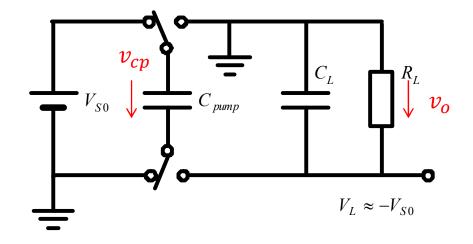
# 只考虑稳态响应

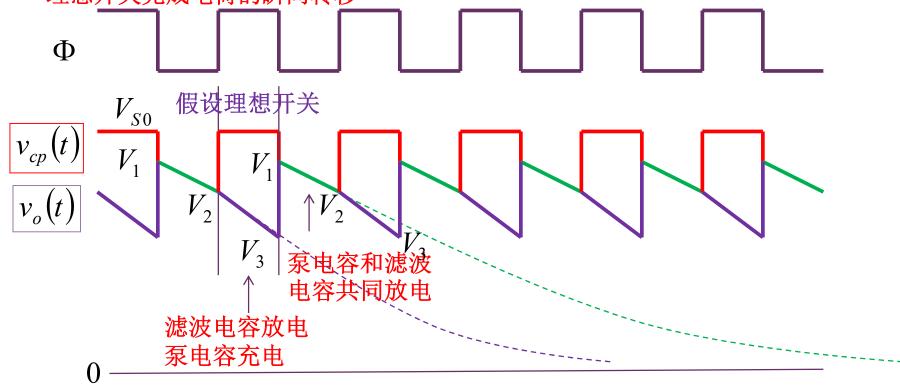
如果不假设理想开关

1、二极管、晶体管开关是非 线性电阻,电容通过非线性电 阻充放电分析过于复杂

**2**、二阶非线性分析过于复杂 真实开关实现电荷转移**需要时间** 

理想开关完成电荷的瞬间转移

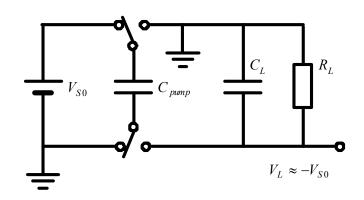


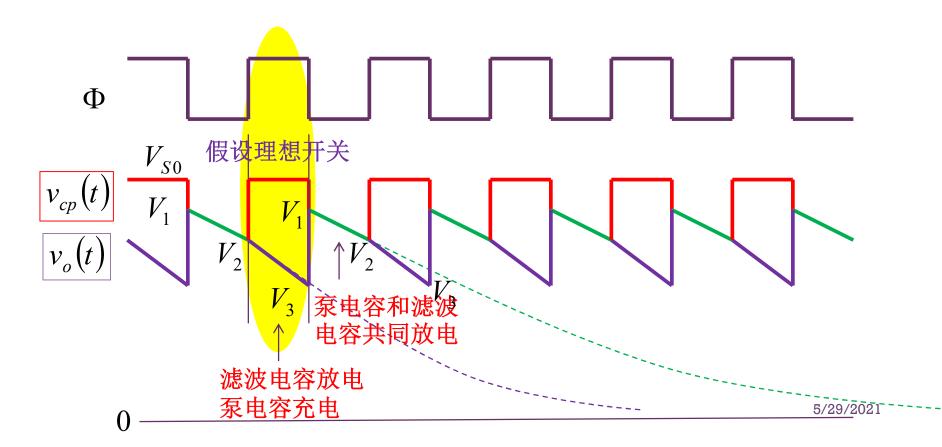


# 开关左拨半周期

$$v_o(t) = V_2 e^{-\frac{t}{R_L C_L}} \approx V_2 \left(1 - \frac{t}{R_L C_L}\right)$$

$$V_3 \approx V_2 \left( 1 - \frac{0.5T}{R_L C_L} \right)$$





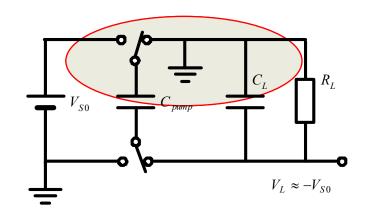
#### 开关右拨瞬间

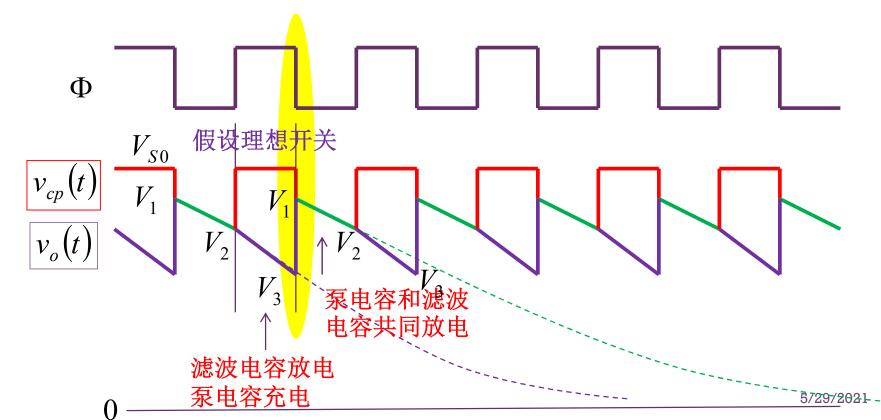
$$v_{cp}(0^-) = V_{S0}$$

$$v_o(0^-) = V_3$$

$$C_L v_o(0^-) + C_p v_{cp}(0^-) = (C_L + C_p) v_o(0^+)$$

$$v_o(0^+) = \frac{C_L}{C_L + C_p} V_3 + \frac{C_p}{C_L + C_p} V_{S0} = V_1$$





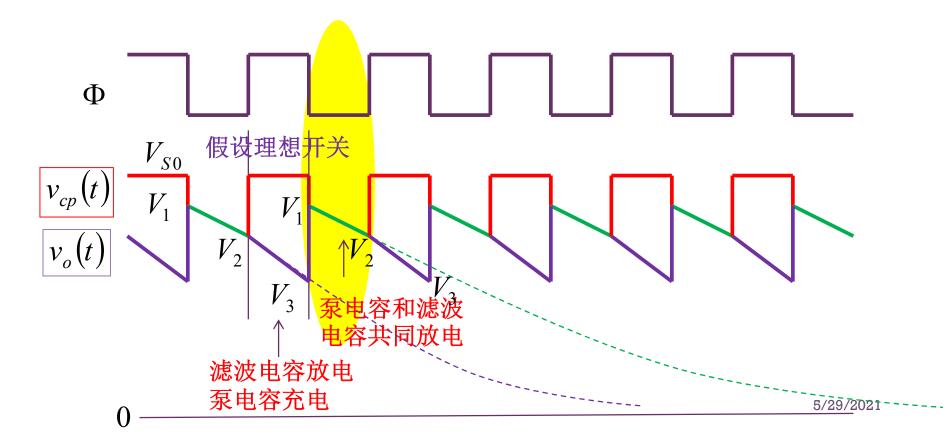
### 开关右拨半周期

$$v_o(t) = V_1 e^{-\frac{t}{R_L(C_L + C_p)}} \approx V_1 \left( 1 - \frac{t}{R_L(C_L + C_p)} \right)$$

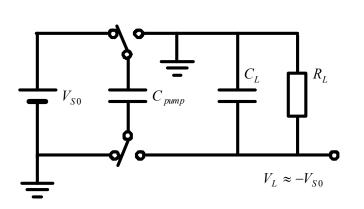
$$V_{S0} = C_{pump}$$

$$V_{L} \approx -V_{S0}$$

$$V_2 \approx V_1 \left( 1 - \frac{0.5T}{R_L(C_L + C_p)} \right)$$



# 电容电 能 释 放过程 描 述

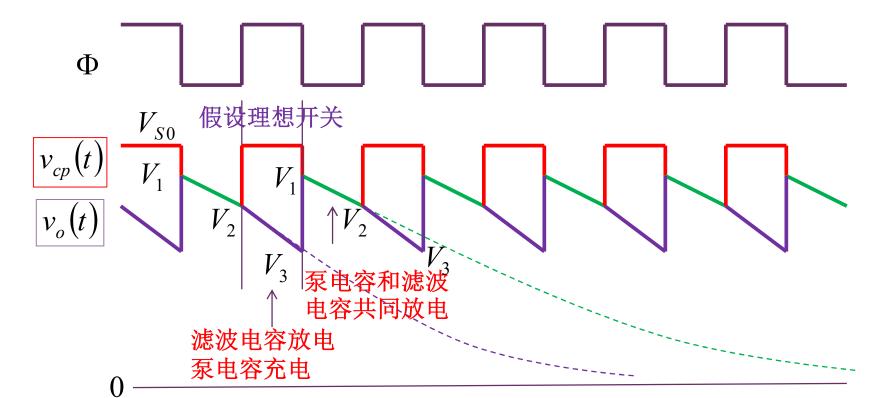


$$V_3 \approx V_2 \left( 1 - \frac{0.5T}{R_L C_L} \right)$$
 开关左拨半周期

$$V_1 = \frac{C_L}{C_L + C_p} V_3 + \frac{C_p}{C_L + C_p} V_{S0}$$
  
开关右拨瞬间

$$V_2 \approx V_1 \left( 1 - \frac{0.5T}{R_L(C_L + C_p)} \right)$$

开关右拨半周期



# 波纹大小

$$V_2 \approx V_1 \left( 1 - \frac{0.5T}{R_L(C_L + C_p)} \right)$$

$$V_{3} \approx V_{2} \left( 1 - \frac{0.5T}{R_{L}C_{L}} \right)$$

$$\approx V_{1} \left( 1 - \frac{0.5T}{R_{L}(C_{L} + C_{p})} \right) \left( 1 - \frac{0.5T}{R_{L}C_{L}} \right)$$

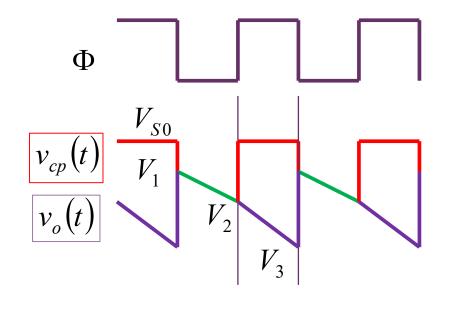
$$\approx V_{1} \left( 1 - \frac{0.5T}{R_{L}(C_{L} + C_{p})} - \frac{0.5T}{R_{L}C_{L}} \right)$$

$$\approx V_{1} \left( 1 - \frac{0.5T}{R_{L}(C_{L} + C_{p})} - \frac{0.5T}{R_{L}C_{L}} \right)$$

$$V_{1} = \frac{C_{L}}{C_{L} + C_{p}} V_{3} + \frac{C_{p}}{C_{L} + C_{p}} V_{S0}$$

$$\approx \frac{C_{L}}{C_{L} + C_{p}} V_{1} \left( 1 - \frac{0.5T}{R_{L} \left( (C_{L} + C_{p}) \oplus C_{L} \right)} \right) + \frac{C_{p}}{C_{L} + C_{p}} V_{S0}$$

$$\approx \frac{R_{L} \left( (C_{L} + C_{p}) \oplus C_{L} \right)}{R_{L} \left( (C_{L} + C_{p}) \oplus C_{L} \right)} \times \frac{R_{L} \left( (C_{L} + C_{p}) \oplus C_{L} \right)}{R_{L} \left( (C_{L} + C_{p}) \oplus C_{L} \right)} \times \frac{R_{L} \left( (C_{L} + C_{p}) \oplus C_{L} \right)}{R_{L} \left( (C_{L} + C_{p}) \oplus C_{L} \right)}$$



$$V_{1} \approx \frac{C_{p}}{C_{p} + C_{L} \frac{0.5T}{R_{L} \left( \left( C_{L} + C_{p} \right) \oplus C_{L} \right)}} V_{S0}$$

$$\Delta V = V_1 - V_3$$

$$\approx \frac{0.5T}{R_L \left( \left( C_L + C_p \right) \oplus C_L \right)} V_1$$

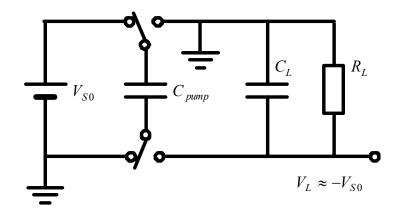
$$\approx \frac{C_p}{R_L \left( \left( C_L + C_p \right) \oplus C_L \right)} V_{S0}$$

$$\frac{R_L \left( \left( C_L + C_p \right) \oplus C_L \right)}{0.5T} C_p + C_L$$

# 输出纹波越小 越接i斤理想直流

$$\Delta V \approx \frac{C_p}{R_L \left( \left( C_L + C_p \right) \oplus C_L \right)} V_{S0}$$

$$\frac{1}{0.5T} C_p + C_L$$



$$C_L >> C_p$$
  $\Delta V pprox rac{R_{pe}}{R_L + R_{pe}} rac{C_p}{C_L} V_{S0}$   $R_{pe} = rac{T}{C_p}$   $C_p >> rac{T}{R_L}$   $R_{pe} \ll R_L$   $\Delta V o 0$ 

$$C_p >> \frac{T}{R_L}$$
  $R_{pe} \ll R_L$   $\Delta V \to 0$ 

$$\Phi$$
 $V_{S0}$ 
 $V_{cp}(t)$ 
 $V_1$ 
 $V_0(t)$ 
 $V_2$ 
 $V_3$ 

$$V_{1} \approx \frac{C_{p}}{C_{p} + C_{L}} \frac{C_{p}}{R_{L}} \left( \left( C_{L} + C_{p} \right) \oplus C_{L} \right)$$

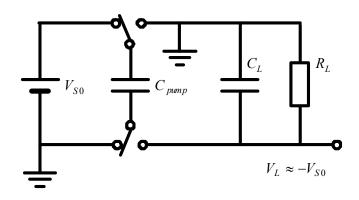
$$C_{L} >> C_{p} >> \frac{T}{R_{L}}$$

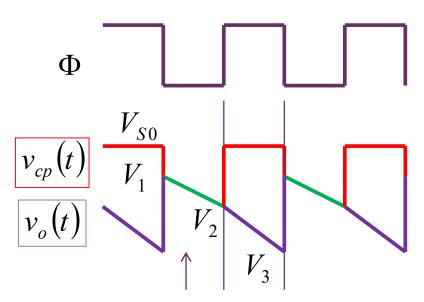
$$V_{1} \approx \frac{C_{p}}{C_{p} + \frac{T}{R_{L}}} V_{S0} = \frac{R_{L}}{\frac{T}{C_{p}} + R_{L}} V_{S0}$$

$$= \frac{R_{L}}{R_{ne} + R_{L}} V_{S0} \approx V_{S0}$$

清华大学电子工程系

#### 非负载耗能





电容电荷重分配时,电流流过开关(晶体管、二极管),非线性电阻耗能。这里为了简化分析,把晶体管抽象为理想开关,电容电荷重分配在开关拨动瞬间完成,以冲激电流(电磁辐射)形态表现。事实上,这部分能量基本上是被晶体管消耗掉的,但计算时,只能以理想开关电磁辐射能量估计。

开关左拨,恒压源对 $C_p$ 瞬间充电,冲激电流耗能

$$\Delta E_1 = \frac{1}{2} C_p (V_{S0} - V_2)^2$$

开关左拨,冲激电流瞬间完成 $\mathbf{C}_{\mathbf{p}}$ 和 $\mathbf{C}_{\mathbf{L}}$ 的电荷重分配,冲激电流耗能

$$\Delta E_2 = \frac{1}{2} C_p V_{S0}^2 + \frac{1}{2} C_L V_3^2 - \frac{1}{2} (C_p + C_L) V_1^2$$

$$= \frac{1}{2} \frac{C_L C_p}{C_L + C_p} (V_{S0} - V_3)^2$$

# 非负载耗能越小 DC-DC转换效率越高

$$\Delta E_1 = \frac{1}{2} C_p (V_{S0} - V_2)^2$$

$$\Delta E_2 = \frac{1}{2} \frac{C_L C_p}{C_L + C_p} (V_{S0} - V_3)^2$$

$$R_{pe} = \frac{T}{C_p}$$

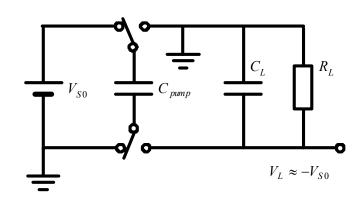
$$V_{S0} - V_2 \approx V_{S0} \left( \frac{R_{pe}}{R_L + R_{pe} \frac{C_L + 0.5C_p}{C_L + C_p}} \right) \stackrel{C_L >> C_p}{\approx} V_{S0} \frac{R_{pe}}{R_L + R_{pe}}$$

$$V_{S0} - V_3 \approx V_{S0} \frac{R_{pe}}{R_L \frac{C_L}{C_L + 0.5C_p} + R_{pe} \frac{C_L}{C_L + C_p}} \stackrel{c_L >> c_p}{\approx} V_{S0} \frac{R_{pe}}{R_L + R_{pe}}$$

$$\Delta E = \Delta E_1 + \Delta E_2 \overset{C_L >> C_p}{\approx} C_p V_{S0}^2 \left( \frac{R_{pe}}{R_{pe} + R_L} \right)^2 \overset{R_{pe} << R_L}{\approx} C_p V_{S0}^2 \left( \frac{R_{pe}}{R_L} \right)^2 = \frac{V_{S0}^2}{R_L^2} \frac{T^2}{C_p}$$

$$P_D = \frac{\Delta E}{T} \approx \frac{V_{S0}^2}{R_L^2} \frac{T}{C_p} \approx I_L^2 R_{pe}$$

 $P_D = \frac{\Delta E}{T} \approx \frac{V_{S0}^2}{R_L^2} \frac{T}{C_p} \approx I_L^2 R_{pe}$  非负载耗能恰好就是开关电容等效电阻耗能显然,开关等效电阻越小,**DC-DC**转换效率越高



$$C_L >>> C_p$$
  $R_{pe} = \frac{T}{C_p}$ 

$$\Delta V \overset{C_L >> C_p}{\approx} \frac{R_{pe}}{R_L + R_{pe}} \frac{C_p}{C_L} V_{S0}$$

$$\stackrel{R_{pe} << R_L}{\approx} \frac{T}{R_L C_L} V_{S0} = \frac{I_L}{f C_L}$$

$$V_{L} \approx V_{1} \approx \frac{C_{p}}{C_{p} + C_{L}} \frac{C_{p}}{R_{L} \left( \left( C_{L} + C_{p} \right) \oplus C_{L} \right)} V_{S0}$$

$$C_{L} \gtrsim C_{p} \frac{R_{L}}{R_{L} + R_{pe}} V_{S0} \stackrel{R_{pe} < < R_{L}}{\approx} V_{S0}$$

$$P_D \overset{R_{pe} << R_L}{\approx} I_L^2 R_{pe}$$

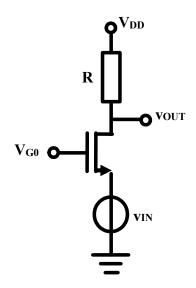
在满足 $C_L >> C_p >> \frac{T}{R_I}$ 条件下,电容越大,**DC-DC**转换效果越好

#### 晶体管做放大器用

- 晶体管具有将直流电能转换为交流电能的能力,从而可以实现有源功能,即向端口外提供电能量的能力,从而可以实现放大器和振荡器电路
- 放大器有两种类型
  - 小信号放大器
    - 在直流工作点附近的小区域内视为线性---局部线性化处理
      - 先做直流分析找到直流工作点,再做交流小信号微分元件线性分析
      - 小信号线性放大: 关注线性放大器的增益、输入/输出阻抗
  - 大信号放大器
    - 正弦信号可能占满恒流区,或者超出恒流区进入截止区或欧姆区---<mark>往</mark> 往做分段折线处理
      - A类线性放大,B类、AB类非线性放大
      - 大信号放大: 关注效率---多少百分比的直流电能被转换为交流电能?

## 作业8.2 共栅组态解析分析

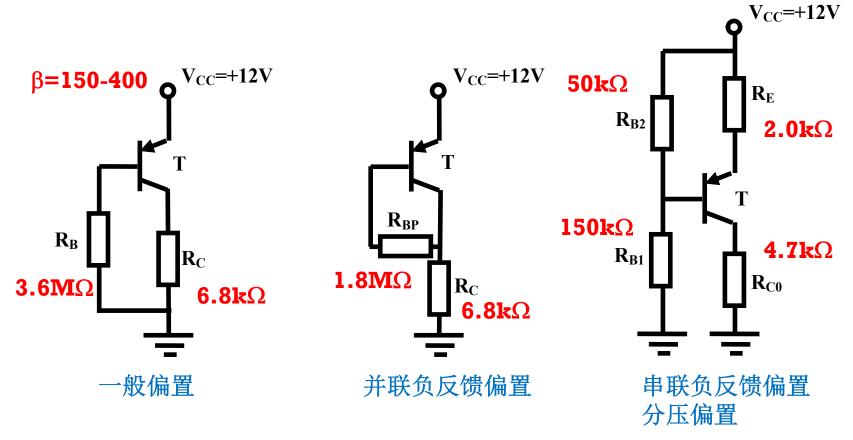
- 如图所示晶体管栅极接固定电压V<sub>GO</sub>,在源极加激励电压V<sub>IN</sub>,请分析漏极电压V<sub>OUT</sub>随源极电压V<sub>IN</sub>的变化规律
  - 确认当晶体管工作在恒流导通区时,输入输出转移特性曲线的微分斜率 恰好是共栅组态晶体管的电压增益g<sub>m</sub>R
    - 并分析此时的功率增益---电阻R上获得的交流功率与信源V<sub>IN</sub>=V<sub>INO</sub>+V<sub>in</sub> 提供的交流功率的比值,并以此说明共栅组态晶体管的电流缓冲器特性



本题意图告知: 只有工作在恒流区,输入输出转移特性曲线具有最大的斜率,也就是说具有最大的增益,因而做放大器使用时,应将晶体管偏置在恒流导通区

#### 作业4.2 分立PNP-BJT的直流偏置

本题意图告知:如何直流偏置,使得晶体管工作于恒流导通区,其中分压偏置电路是最常见的工作点稳定的直流偏置电路



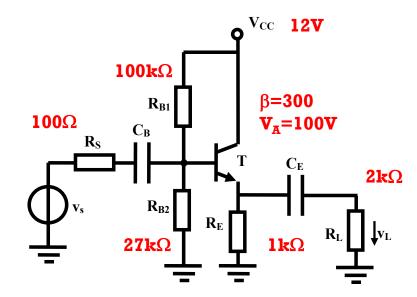
分析上述三个电路的BJT的直流工作点:  $I_c=?V_{EC}=?$ 说明负反馈可以稳定直流工作点

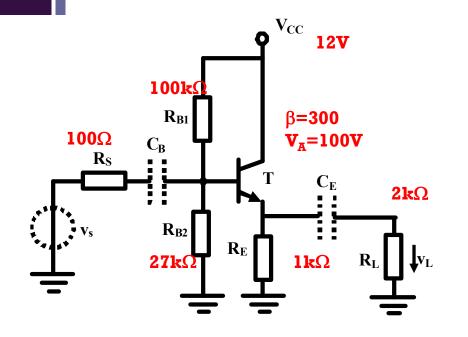
### 作业7.2 CC组态晶体管放大器

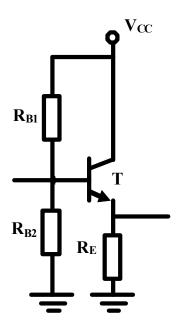
- (1) 直流分析
- (2) 交流分析

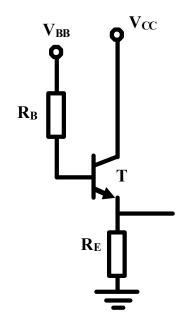
$$A_{v} = \frac{v_{L}}{v_{S}} = ?$$

#### 小信号放大器分析







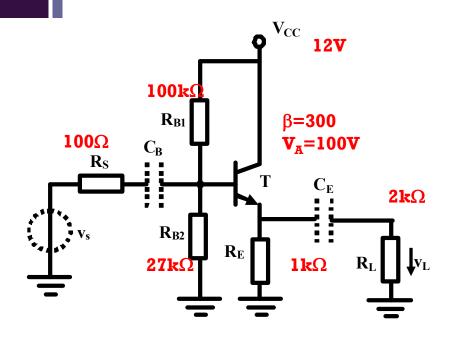


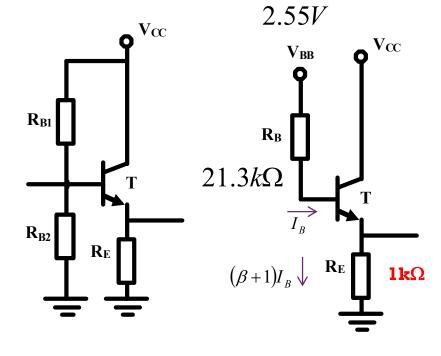
$$V_{BB} = \frac{R_{B2}}{R_{B1} + R_{B2}} V_{CC} = \frac{27k}{100k + 27k} \times 12 = 2.55V$$

戴维南等效

$$R_B = R_{B1} || R_{B2} = \frac{R_{B1}R_{B2}}{R_{B1} + R_{B2}} = \frac{100k \times 27k}{100k + 27k} = 21.3k\Omega$$

#### 直流工作点





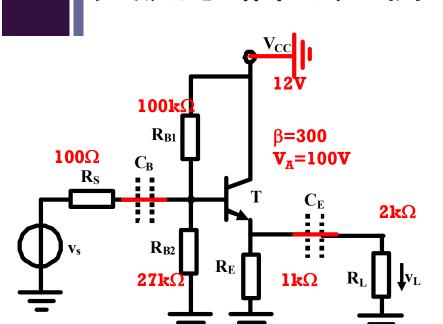
$$I_{B}R_{B} + V_{BE} + (\beta + 1)I_{B}R_{E} = V_{BB}$$

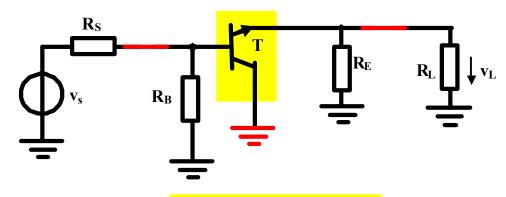
戴维南等效

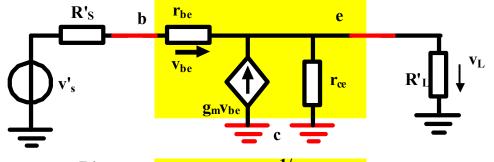
$$I_B = \frac{V_{BB} - V_{BE}}{R_B + (\beta + 1)R_E} = \frac{2.55 - 0.7}{21.3k + 301 \times 1} = 5.74 \,\mu A \qquad I_C = \beta I_B = 1.72 \,m A$$

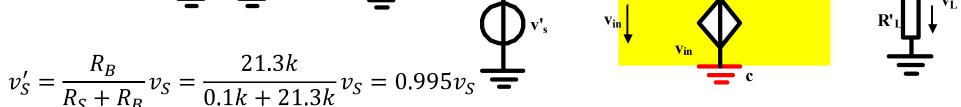
$$V_{CE} = V_{CC} - R_E I_E = 12 - 301 \times 5.74 \mu \times 1k = 10.27 V > 0.2 = V_{CE,sat}$$
 确认在恒流区

#### 交流小信号分析









$$R_S' = R_S ||R_B| = \frac{R_S R_B}{R_S + R_B} = 99.5\Omega \ll r_{be}$$

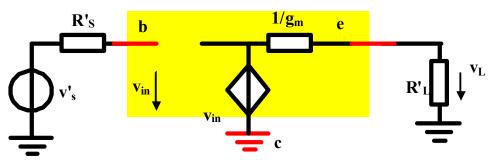
$$R_L' = R_L ||R_E = 1k\Omega||2k\Omega = 667\Omega$$

$$g_m = \frac{I_C}{v_T} = 66.2mS$$

$$r_{ce} = \frac{V_A}{I_C} = 58.1k\Omega$$

$$r_{be} = \beta \frac{1}{g_m} = 4.53k\Omega$$

$$99.5\Omega = R_S' << r_{be} = 4.53k$$

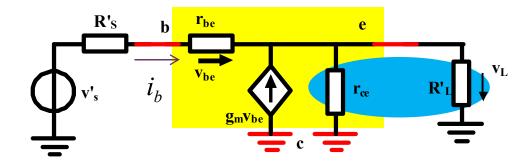


$$v_{in} = v_S' = 0.995 v_S$$

$$v_{L} = \frac{R'_{L}}{R'_{L} + \frac{1}{g_{m}}} v'_{S} = \frac{g_{m}}{1 + g_{m}R'_{L}} R'_{L} v'_{S} = g_{mf}R'_{L}v'_{S}$$

$$= \frac{66.2m \times 0.667k}{1 + 66.2m \times 0.667k} \times 0.995v_S = \frac{44.1}{45.1} \times 0.995v_S = 0.973v_S$$

$$A_v = \frac{v_L}{v_S} = 0.973$$



$$v'_{S} = i_{b}(R'_{S} + r_{be}) + (i_{b} + g_{m}r_{be}i_{b})R''_{L}$$

$$v_L = (i_b + g_m r_{be} i_b) R_L''$$

$$R''_{L} = R'_{L} || r_{ce}$$
  
= 667||58.1 $k$   
= 659 $\Omega$ 

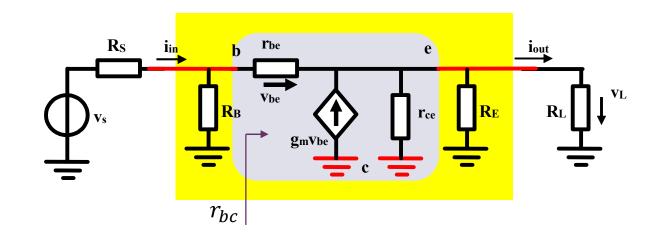
$$A_{v} = \frac{v_{L}}{v_{S}} = \frac{(i_{b} + g_{m}r_{be}i_{b})R_{L}''}{i_{b}(R_{S}' + r_{be}) + (i_{b} + g_{m}r_{be}i_{b})R_{L}''} \frac{v_{S}'}{v_{S}}$$

$$= \frac{(1 + g_{m}r_{be})R_{L}''}{R_{S}' + r_{be} + R_{L}'' + g_{m}r_{be}R_{L}''} \frac{v_{S}'}{v_{S}}$$

$$= \frac{(1 + 66.2m \times 4.53k) \times 0.659}{0.0995 + 4.53 + (1 + 66.2m \times 4.53k) \times 0.659} \times 0.995$$

$$= 0.977 \times 0.995 = 0.972$$

### 电压增益小于1还是放大器吗?

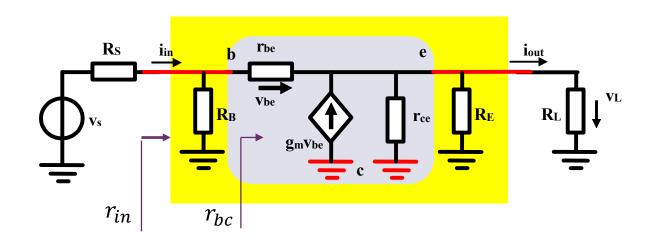


$$A_{i} = \frac{i_{out}}{i_{in}} = \frac{i_{out}R_{L}}{i_{in}(R_{S} + R_{B}||r_{bc})} \frac{(R_{S} + R_{B}||r_{bc})}{R_{L}} = \frac{v_{L}}{v_{S}} \frac{(R_{S} + R_{B}||r_{bc})}{R_{L}}$$

$$= A_v \frac{\left(R_S + R_B || \left(r_{be} + (r_{ce} || R_E || R_L) + g_m r_{be} (r_{ce} || R_E || R_L)\right)\right)}{R_L}$$

$$= 0.972 \times \frac{\left(100 + 21.3k||(4.53k + (58.1k||1k||2k) + 66.2m \times 4.53k \times 659)\right)}{2k}$$
  
=  $0.972 \times \frac{(100 + 21.3k||203k)}{2k} = 0.972 \times \frac{19.28k}{2k} = 9.417$ 

#### 功率增益大于1的可能性就是放大器



$$G_p = \frac{P_L}{P_{in}} = \frac{v_L i_{out}}{v_{in} i_{in}} = \frac{v_L}{v_S} \frac{v_S}{v_{in}} \frac{i_{out}}{i_{in}} = 0.972 \times \frac{r_{in} + R_S}{r_{in}} \times 9.417$$
$$= 0.972 \times \frac{19.28k + 0.1k}{19.28k} \times 9.417 = 9.2 = 9.6dB$$

两个端口未做匹配的情况下功率增益已经大于1了,肯定是有源的。

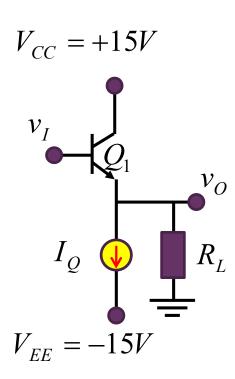
如果两个端口同时匹配,将得到最大功率增益,只要最大功率增 益大于1,就是有源的,就是放大器

#### 作业10.3 输出级

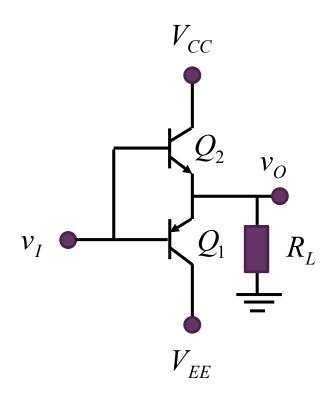
■ 这里有三个转移特性曲线,试分析这三条 转移特性曲线分别对应哪种输出级,说明 为什么会形成这样的转移特性曲线,并将 正确的表达式列写于图上问号位置

#### ■ A类射极跟随器

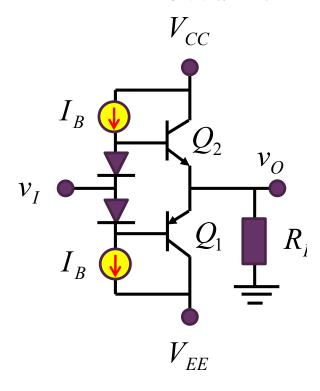
- B类推挽结构
- AB类推挽结构



A类射极跟随器

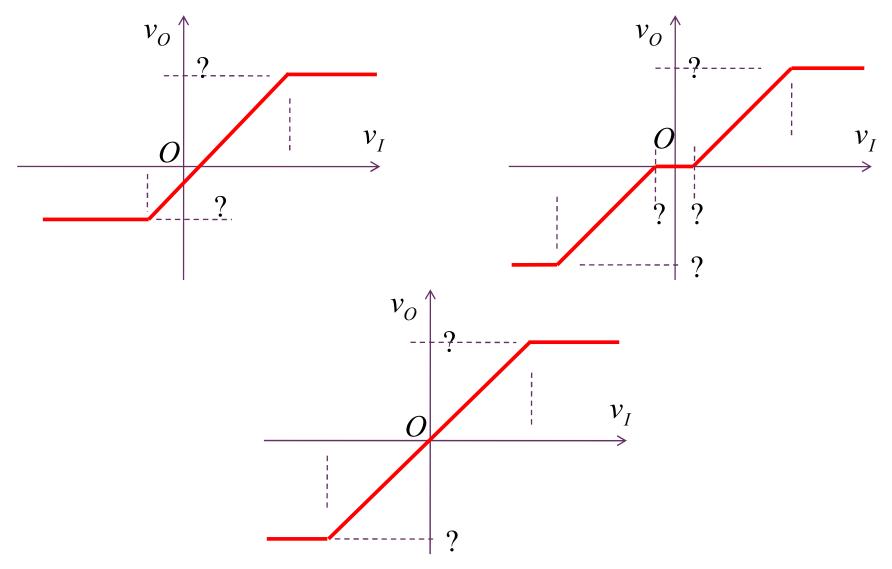


B类推挽



AB类推挽

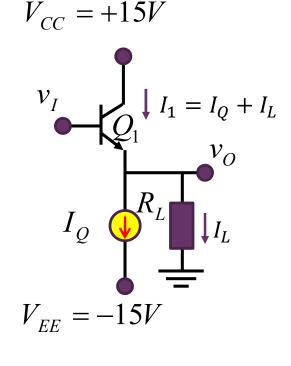
#### 转移特性曲线



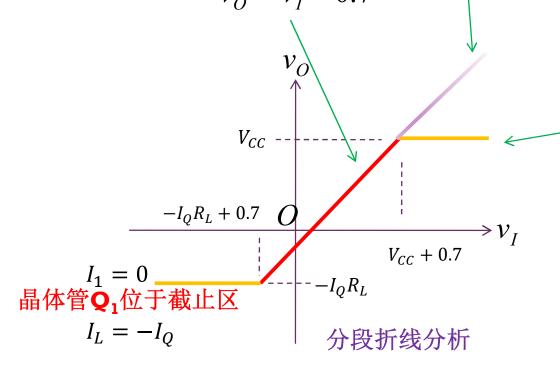
#### A类缓冲器

晶体管 $Q_1$ 位于有源区:  $V_{cc}$ 提供 直流能量, $Q_1$ 将其转化为交流能 量输出: 此为正常工作区,电压 缓冲,具有电流增益  $v_O = v_I - 0.7$ 

理想恒压源V<sub>I</sub> 提供能量,晶 体管Q<sub>I</sub>变成双 二极管,不具 期望的能量转 化作用

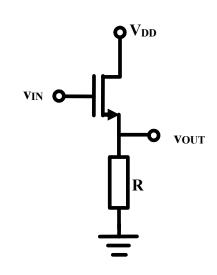


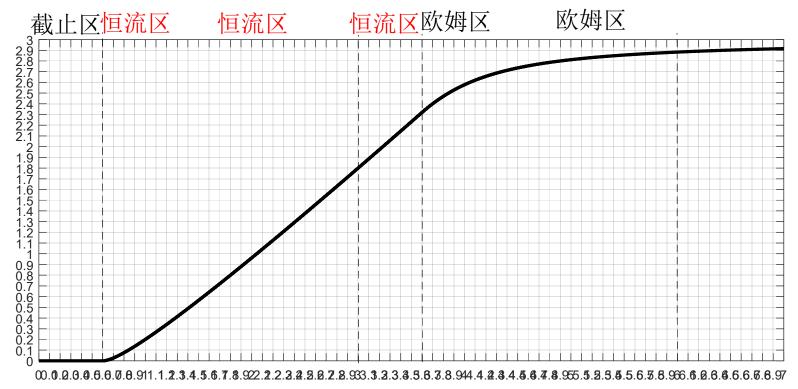
前级电路等效戴维南电压源内阻的限流作用,V<sub>I</sub>电压被限制在V<sub>CC</sub>+0.7V以内,此处电压最高V<sub>CC</sub>,晶体管位于饱和区;对于MOSFET,即使是理想恒压源V<sub>I</sub>驱动,此处电压最高也是V<sub>DD</sub>,此时晶体管位于欧姆导通区



#### MOSFET-CD组态 缓冲器作业回顾

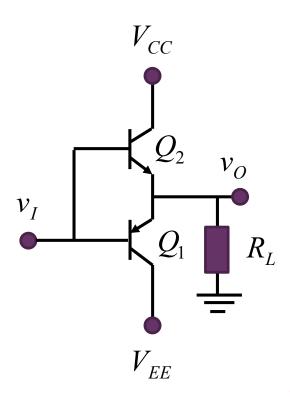
晶体管工作在恒流区,具有 将直流能量有效转化为交流 能量的换能作用,一般不应 进入到其他两个工作区

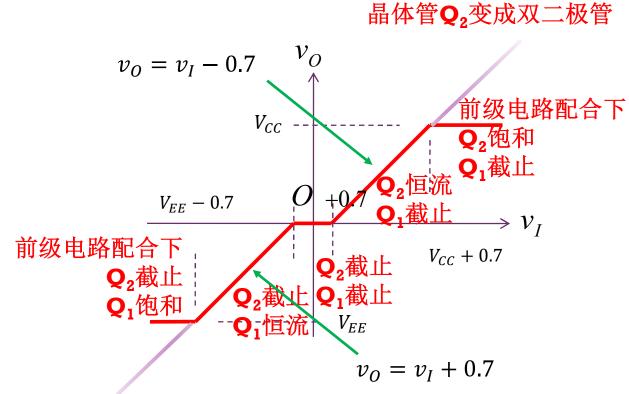




#### B类推挽结构

#### B类放大器存在交越失真:两个晶体管均截止,输入变化但输出为0

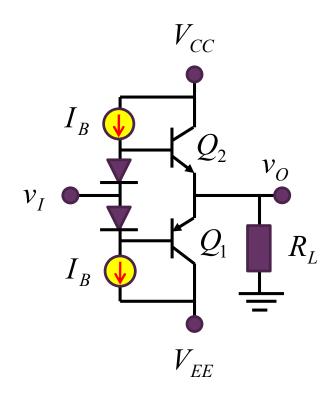


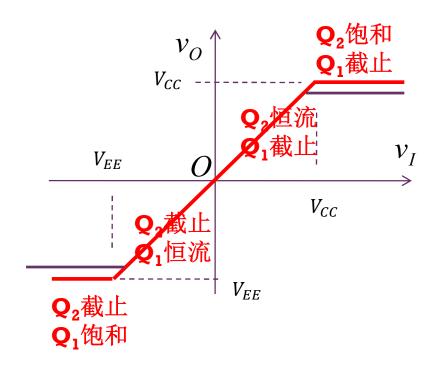


理想恒压源 $V_I$ 激励下, 晶体管 $Q_I$ 变成双二极管 理想恒压源**V**<sub>T</sub>激励下,

#### AB类推挽

#### AB类放大器近似视为线性放大器



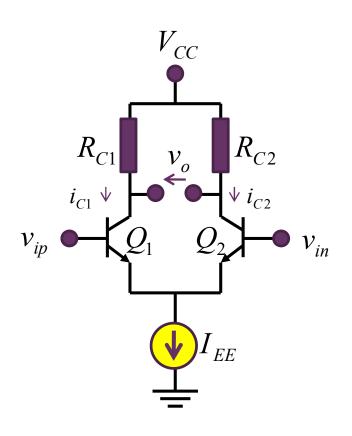


#### 差分放大

- 差分放大既可以是小信号的,也可以是大信号的
- 差分放大器的输入输出转移特性曲线是对称的
  - 当工作点位于中心位置,且交流小信号足够小时,就是小信号线性放大器
  - 当信号幅度大得进入转移特性曲线的饱和区,就是大信号放大器
    - 如果幅度极大时,差分放大器可用单刀双掷开关模型进行分析

### 作业10.3 BJT差分对特性

#### 对称结构形成的非线性转移特性曲线



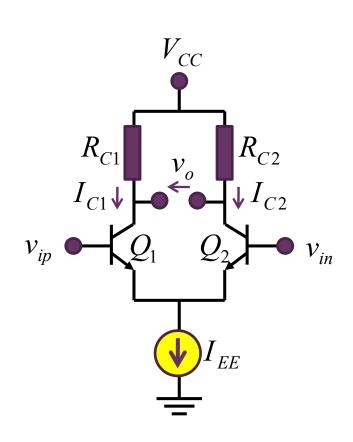
证明BJT差分对跨导控制关系:

$$i_d = i_{C1} - i_{C2} = f(v_{id}) = I_{EE} \tanh \frac{v_{id}}{2v_T}$$

#### 已知BJT跨导控制关系

$$i_b \approx 0$$
 忽略 $\beta$ 、 $\mathbf{V_A}$ 的影响  $i_c \approx I_{CS0} e^{\frac{v_{BE}}{v_T}}$   $\beta \rightarrow \infty$ ,  $\mathbf{V_A} \rightarrow \infty$ 

# 假设为理想指数律控制关系



$$igg|_{I_{C2}} I_{C1} pprox I_{CS1} e^{rac{V_{BE1}}{v_T}} = I_{CS0} e^{rac{V_{BE1}}{v_T}}$$

$$V_{in} \quad I_{C2} \approx I_{CS2} e^{\frac{V_{BE2}}{v_T}} = I_{CS0} e^{\frac{V_{BE2}}{v_T}}$$

$$\mathbf{V}_{\mathtt{A}}\!\!\to\!\!\infty$$

$$I_{EE} = I_{E1} + I_{E2} = \frac{1}{\alpha} (I_{C1} + I_{C2}) \approx I_{C1} + I_{C2}$$

电流增益β→∞

$$v_{id} = V_{BE1} - V_{BE2}$$

$$I_{C1} = I_{CS0} e^{\frac{V_{BE1}}{v_T}}$$

$$V_{BE1} = v_T \ln \frac{I_{C1}}{I_{CS0}}$$

$$I_{C2} = I_{CS0} e^{\frac{V_{BE2}}{v_T}}$$

$$I_{C2} = I_{CS0}e^{\frac{V_{BE2}}{v_T}} \qquad V_{BE2} = v_T \ln \frac{I_{C2}}{I_{CS0}} \qquad v_{ip} \bullet -$$

$$v_{id} = V_{BE1} - V_{BE2} = v_T \ln \frac{I_{C1}}{I_{C2}}$$

$$R_{C1}$$
 $V_o$ 
 $I_{C2}$ 
 $V_{ip}$ 
 $Q_1$ 
 $Q_2$ 
 $V_{in}$ 

$$\frac{I_{C1}}{I_{C2}} = e^{\frac{v_{id}}{v_T}}$$

$$I_{C1} = \frac{I_{EE}}{1 + e^{-\frac{v_{id}}{v_T}}}$$

$$I_{C2} = \frac{I_{EE}}{1 + e^{\frac{v_{id}}{v_T}}}$$

$$I_{C1} + I_{C2} = I_{EE}$$

$$I_{C1} = \frac{I_{EE}}{1 + e^{-\frac{v_{id}}{v_T}}}$$

$$i_d = I_{C1} - I_{C2} = \frac{e^{\frac{v_{id}}{v_T}} - 1}{e^{\frac{v_{id}}{v_T}} + 1} I_{EE}$$

$$= \frac{e^{\frac{v_{id}}{2v_T}} - e^{-\frac{v_{id}}{2v_T}}}{e^{\frac{v_{id}}{2v_T}} + e^{-\frac{v_{id}}{2v_T}}} I_{EE} = I_{EE} \tanh \frac{v_{id}}{2v_T}$$

差分电流 
$$I_{C1} = \frac{I_{EE}}{1 + e^{\frac{-v_{id}}{v_T}}} \qquad I_{C2} = \frac{I_{EE}}{1 + e^{\frac{-v_{id}}{v_T}}} \qquad V_{CC}$$

$$i_d = I_{C1} - I_{C2} = \frac{e^{\frac{v_{id}}{v_T}} - 1}{e^{\frac{v_{id}}{v_T}} + 1} I_{EE}$$

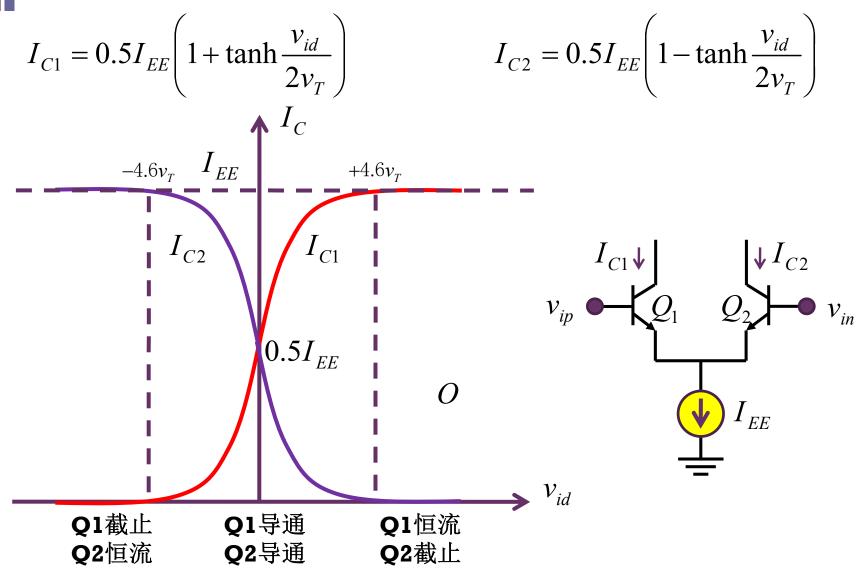
$$= \frac{e^{\frac{v_{id}}{2v_T}} - e^{-\frac{v_{id}}{2v_T}}}{e^{\frac{v_{id}}{2v_T}} + e^{-\frac{v_{id}}{2v_T}}} I_{EE} = I_{EE} \tanh \frac{v_{id}}{2v_T}$$

$$I_{C1} = 0.5I_{EE} + 0.5i_d$$

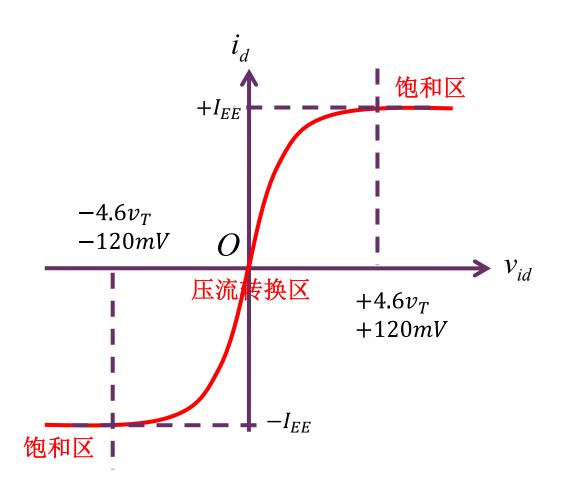
$$= 0.5I_{EE} \left( 1 + \tanh \frac{v_{id}}{2v_T} \right)$$

$$I_{C2} = 0.5I_{EE} - 0.5i_d$$
  
=  $0.5I_{EE} \left( 1 - \tanh \frac{v_{id}}{2v_T} \right)$ 

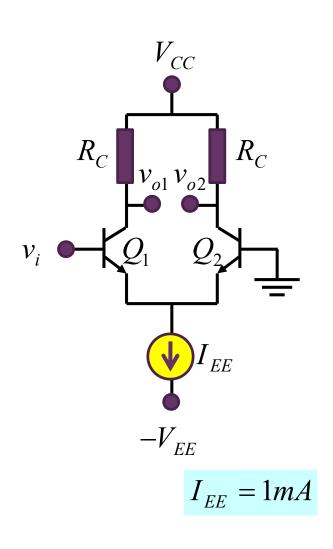
### 输入电压输出电流转移特性关系



#### 差模转移特性曲线



## 作业10.4 差分对的单端转双端



■ 电源电压为 $\pm$ 10V,差分对管参数一致, $R_C$ =3k $\Omega$ ,画出如下三种输入情况下的两个输出电压 $V_{01}$ , $V_{02}$ 的波形示意图

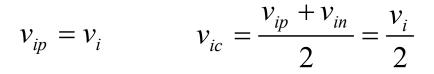
小信号激励是线性放大, 大信号激励可抽象为开关

$$v_i = 10\sin(2\pi \times 10^3 t)(mV)$$

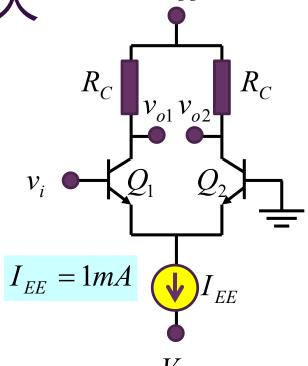
$$v_i = 0.5 \sin(2\pi \times 10^3 t)(V)$$

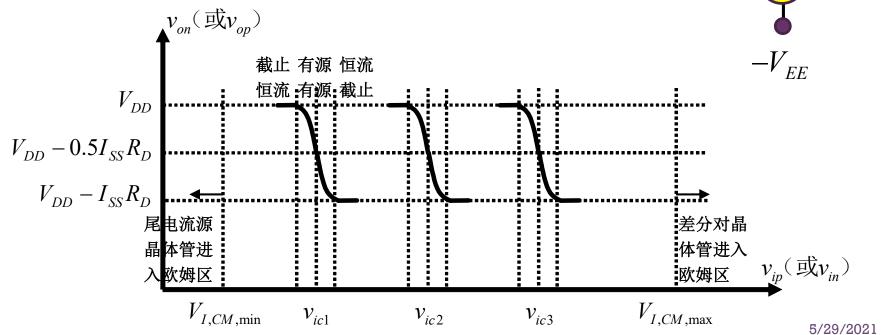
$$v_i = 50 + 100\sin(2\pi \times 10^3 t)(mV)$$

### 共模范围内不影响差模放大

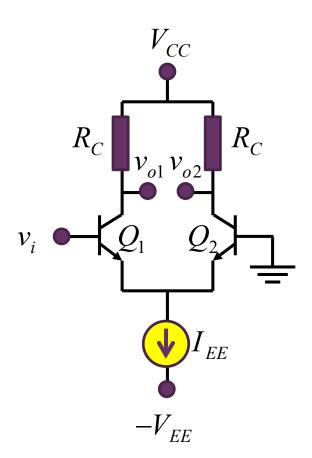


$$v_{in} = 0 \qquad v_{id} = v_{ip} - v_{in} = v_i$$





#### 两个输出电压



$$I_{FF} = 1mA$$

$$i_d = I_{EE} \tanh \frac{v_{id}}{2v_T} = I_{EE} \tanh \frac{v_i}{2v_T}$$

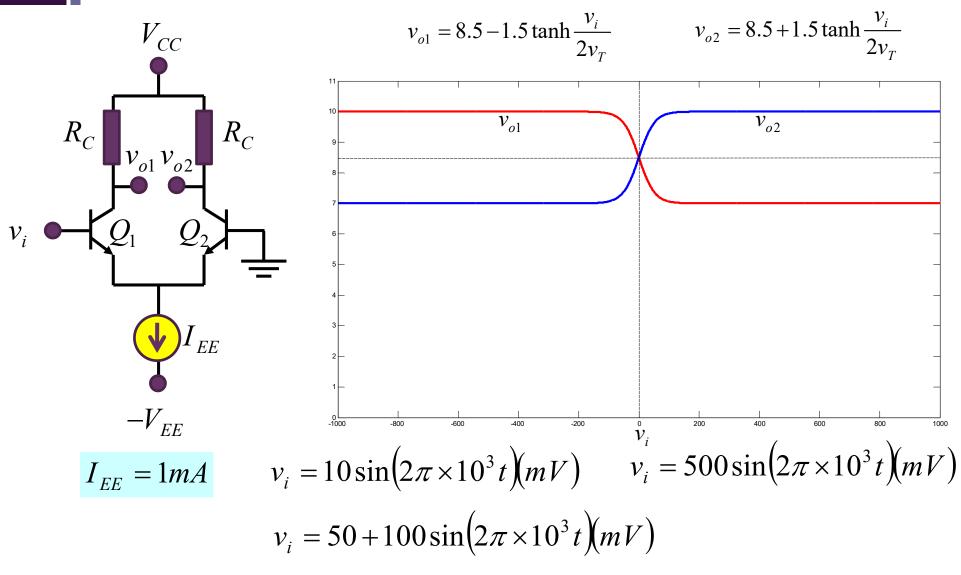
$$I_{C1} = 0.5I_{EE} \left( 1 + \tanh \frac{v_{id}}{2v_T} \right)$$
  $I_{C2} = 0.5I_{EE} \left( 1 - \tanh \frac{v_{id}}{2v_T} \right)$ 

$$v_{o1} = V_{CC} - I_{C1}R_C = V_{CC} - 0.5I_{EE}R_C - 0.5I_{EE}R_C \tanh \frac{v_i}{2v_T}$$

$$= 10 - 0.5 \times 1m \times 3k - 0.5 \times 1m \times 3k \times \tanh \frac{v_i}{2v_T} = 8.5 - 1.5 \tanh \frac{v_i}{2v_T}$$

$$v_{o2} = V_{CC} - I_{C2}R_C = 8.5 + 1.5 \tanh \frac{v_i}{2v_T}$$

## 两个输出电压与输入电压的关系曲线

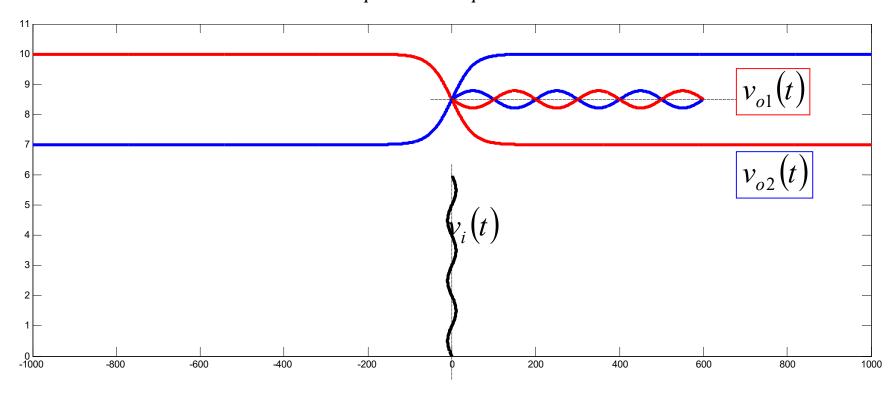


#### 线性范围内,线性放大

 $v_i = 10\sin(2\pi \times 10^3 t)(mV)$  信号幅度在线性范围内,差分对为线性跨导输出近似为正弦波

$$v_o(t) = i_d R_C = R_C I_{EE} tanh \frac{v_{id}}{2v_T}$$

$$\approx R_C I_{EE} \frac{v_{id}}{2v_T} = R_C \frac{0.5 I_{EE}}{v_T} v_{id} = g_{m0} R_C \cdot v_i(t)$$



# 大信号激励,方波输出,开关抽象

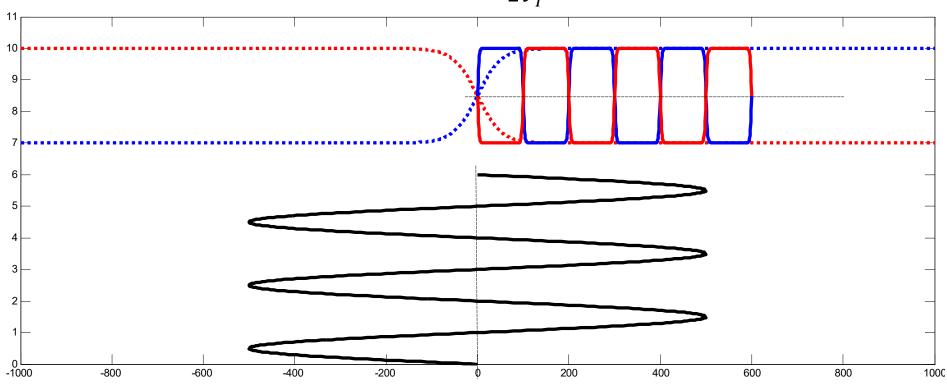
$$v_i = 500 \sin(2\pi \times 10^3 t) (mV)$$

 $S_2(\omega_0 t) = \begin{cases} +1 & \sin \omega_0 t > 0 \\ -1 & \sin \omega_0 t < 0 \end{cases}$ 

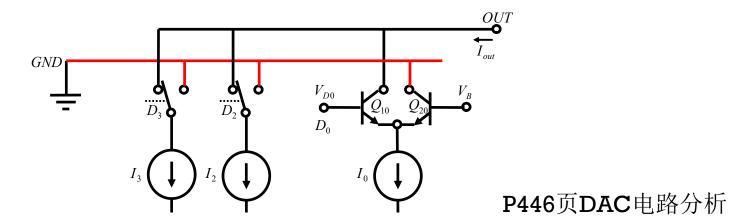
信号幅度很大,差分对为单刀双掷开关

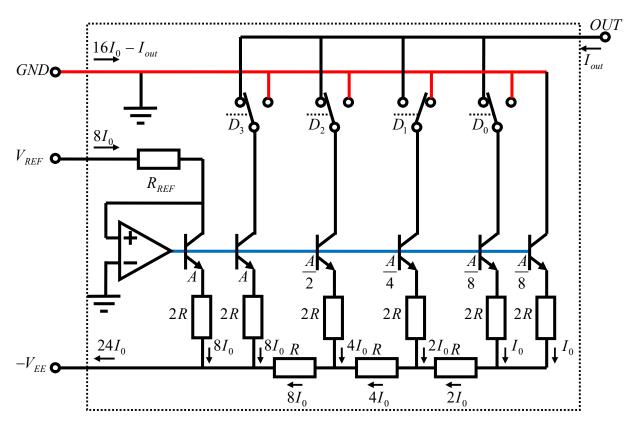
输出近似为方波

$$v_o(t) = R_C I_{EE} tanh \frac{v_{id}}{2v_T} \approx I_{EE} R_C \cdot S_2(\omega_0 t)$$



# 双 掷 开关的 应 用 例



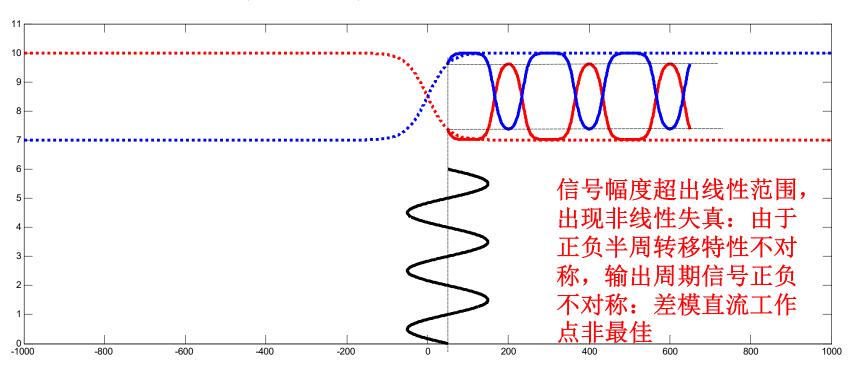


李国林 清华大学电子工程系

《电子电路与系统基础(B2)》非线性电路

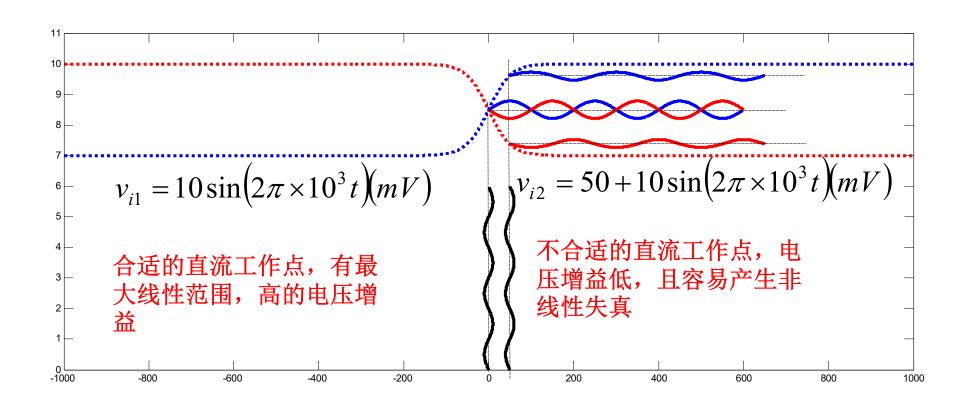
#### 工作点偏离中心的后果

 $v_i = 50 + 100 \sin(2\pi \times 10^3 t) (mV)$  差模信号并非交流信号,差模信号中也可以有直流、交流分量



$$v_{ic} = 25 + 50\sin(2\pi \times 10^{3} t)(mV)$$
$$v_{id} = 50 + 100\sin(2\pi \times 10^{3} t)(mV)$$

### 线性放大最佳工作点在中间位置



#### 考试安排

- ■考试时间:??
- ■考试地点:??
  - 不能返校只能参加线上考的留学生和我联系确认线上考事宜
    - guolinli@tsinghua.edu.cn
  - 自带计算器
  - 隔行隔列坐,严格考场纪律,不允许自带草稿纸,不允许多拿卷子
  - 手机关机装到书包中,书包放前台
  - 监考老师收卷、数卷无误后,方可离场
- 考试内容: 共108分