电子电路与系统基础Ⅱ

理论课第9讲 二阶LTI动态电路的时频分析

(二阶滤波器:低通、高通、带通、带阻、全通)

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条主干

电容器,电感器 一阶RC/RL滤波器, 开关电容积分器,整流器,张弛振荡器...

带宽,延时,移相...

四个分支

电源,电阻器 分压器, 衰减器, 电桥

理想放大器,理想变压器,理想回旋器,理想环行器...

增益,阻抗,噪声...

数字 抽象

开关,非门,与 门,或门,锁存 器,

触发器, 存储器

. .

状态, 状态转移

...

基本元件 电容, 电感 (解析法, 相图, 相量法(变换域方法).. 针对微分方程)

电路 抽象

基本元件 电源,电阻 (图解法,解析解, 线性化方法... 针对代数方程)

基本电路定律和电路定理基尔霍夫, 欧姆, 戴维南

端口抽象(场路抽象)

电压,电流,功率,有源/无源...

LC谐振腔, 负阻器件 二阶RLC滤波器。

阻抗匹配网络, 正弦波振荡器, DC-AC, DC-DC转换器...

谐振,过冲,振荡,最大功率增益,匹配,稳定性...

二极管, 晶体管

整流器,放大器, 电流镜,运放,缓冲器, 比较器,ADC/DAC...

失真,线性度,灵敏度, 负反馈/正反馈...

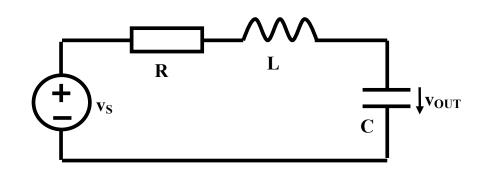
定律、定理和方法 元件或器件 功能单元电路 性能或基本电路概念

二阶LTI动态电路时频分析 大纲

以RLC串联谐振回路为考察对象,以二阶滤波器为实例,研究二阶系统的时频特性

- 二阶低通
 - 重点理解: 诸多电子测量系统都可建模为低通系统
- 二阶高通
- 二阶带通
 - 重点理解: 谐振概念,实际很多射频滤波器都是带通型的,实用的带通滤波器基本都是谐振型的
- 二阶带阻
- 二阶全通

一、二阶低通



直观理解:

低频: 电容开路, 电感短路, 信号通过高频: 电容短路, 电感开路, 信号不能通过

$$H(j\omega) = \frac{\dot{V}_C}{\dot{V}_S} = \frac{\frac{1}{j\omega C}}{R + j\omega L + \frac{1}{j\omega C}} = \frac{1}{(j\omega)^2 LC + j\omega RC + 1}$$

$$H_0 = 1$$

$$\omega_0 = \frac{1}{\sqrt{LC}}$$

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$$j\omega \to s = \frac{1}{s^2 LC + sRC + 1} = \frac{\frac{1}{LC}}{s^2 + s\frac{R}{L} + \frac{1}{LC}} = H_0 \frac{\omega_0^2}{s^2 + 2\xi\omega_0 s + \omega_0^2}$$

$$\xi = \frac{R}{2Z_0} = \frac{R}{2} \sqrt{\frac{C}{L}}$$

$$\omega_0 = \frac{1}{\sqrt{LC}}$$

$$\xi = \frac{R}{2Z_0} = \frac{R}{2} \sqrt{\frac{R}{R}}$$

幅频特性、相频特性、群延时特性

$$H(s) = \frac{\omega_0^2}{s^2 + 2\xi\omega_0 s + \omega_0^2} = \frac{\omega_0^2}{(\omega_0^2 - \omega^2) + j2\xi\omega_0 \omega} = A(\omega)e^{j\varphi(\omega)}$$

$$A(\omega) = \frac{\omega_0^2}{\sqrt{(\omega_0^2 - \omega^2)^2 + (2\xi\omega_0\omega)^2}} \qquad \varphi(\omega) = -\arctan\frac{2\xi\omega_0\omega}{\omega_0^2 - \omega^2}$$

幅频特性

相频特性

$$\tau_{g}(\omega) = -\frac{d\varphi(\omega)}{d\omega}$$

 $\tau_g(\omega) = -\frac{d\varphi(\omega)}{d\omega}$ 群延时:相频特性曲线的斜率 — 群信号通过该系统的延时大小

群延时特性

$$\tau_{g}(\omega) = \frac{2\xi\omega_{0}(\omega^{2} + \omega_{0}^{2})}{\omega^{4} + 2(2\xi^{2} - 1)\omega_{0}^{2}\omega^{2} + \omega_{0}^{4}}$$

幅频特性

$$H(s) = \frac{\omega_0^2}{s^2 + 2\xi\omega_0 s + \omega_0^2} = \frac{\omega_0^2}{(s - \lambda_1)(s - \lambda_2)}$$

$$A(\omega) = \frac{\omega_0^2}{\sqrt{(\omega_0^2 - \omega^2)^2 + (2\xi\omega_0\omega)^2}}$$

$$\lambda_{1,2} = \left(-\xi \pm \sqrt{\xi^2 - 1}\right)\omega_0$$

$$= \begin{cases} -\frac{1}{\xi + \sqrt{\xi^2 - 1}} \omega_0 = -\omega_{p1} = -\frac{1}{\tau_1} & \text{长寿命项} \\ -\left(\xi + \sqrt{\xi^2 - 1}\right) \omega_0 = -\omega_{p2} = -\frac{1}{\tau_2} & 短寿命项 \end{cases}$$

$$H(j\omega) = \frac{\omega_0^2}{(j\omega + \omega_{p1})(j\omega + \omega_{p2})}$$

$$\approx \frac{\omega < \omega_{p2}}{\omega_{p1} << \omega_{p2}(\xi >> 1)} = \frac{1}{1 + \frac{j\omega}{\omega_{p1}}}$$

 ξ =0.03, 0.1, 0.707, 0.866,1, 3, 10

阻尼系数很大时,长寿命特征根使得 系统特性在低频端(长时间观测、大 时间尺度观测)接近一阶系统

$$H(j\omega) = \frac{\omega_0^2}{(j\omega + \omega_{p1})(j\omega + \omega_{p2})}$$

$$(\xi > 1)$$

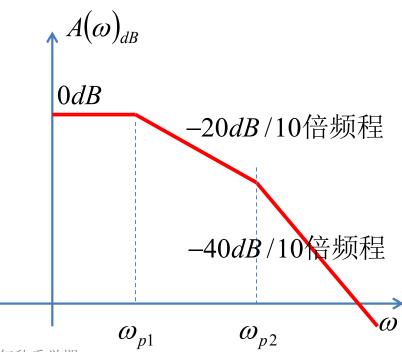
$$\omega_{p1} = \frac{1}{\xi + \sqrt{\xi^2 - 1}} \omega_0$$

$$\omega_{p2} = (\xi + \sqrt{\xi^2 - 1}) \omega_0$$

$$\omega_{p1} < \omega_{p2}$$

什
$$\approx$$

$$\begin{cases} \frac{1}{\frac{j\omega}{\omega_{p1}}} = \frac{\omega_{p1}}{j\omega} & \omega_{p1} < \omega < \omega_{p2} \\ \frac{1}{\frac{j\omega}{\omega_{p1}}} \cdot \frac{j\omega}{\omega_{p2}} = \frac{\omega_0^2}{-\omega^2} & \omega > \omega_{p2} \end{cases}$$



欠阻尼

$$(0 < \xi < 1)$$

$$\lambda_{1,2} = \left(-\xi \pm j\sqrt{1-\xi^2}\right)\omega_0$$

$$H(s) = \frac{\omega_0^2}{s^2 + 2\xi\omega_0 s + \omega_0^2} = \frac{\omega_0^2}{(s - \lambda_1)(s - \lambda_2)}$$

也可分解,但为复根分解

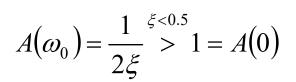
$$H(j0)=1$$
 $H(j\infty)=0$

低通特性不会改变

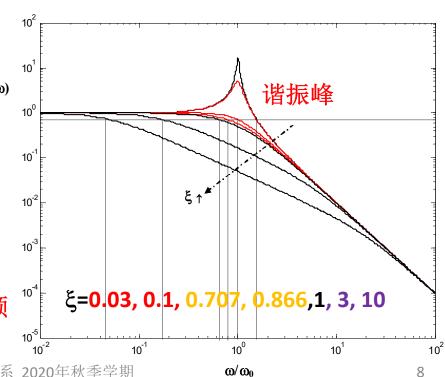
$$H(j\omega_0) = \frac{\omega_0^2}{(j\omega_0)^2 + 2\xi\omega_0(j\omega_0) + \omega_0^2}$$

$$= -j\frac{1}{2\xi} = \frac{1}{2\xi}e^{-j\frac{\pi}{2}}$$

$$= -j\frac{1}{2\xi} = \frac{1}{2\xi}e^{-j\frac{\pi}{2}}$$



自由振荡频点ω。附近幅值可以高于中心频 点(零频点),这就是谐振现象



$$\frac{dA(\omega)}{d\omega} = 0$$

$$A(\omega) = \frac{\omega_0^2}{\sqrt{(\omega_0^2 - \omega^2)^2 + (2\xi\omega_0\omega)^2}}$$

$$= -\frac{1}{2} \frac{\omega_0^2}{\left(\left(\omega_0^2 - \omega^2 \right)^2 + \left(2 \xi \omega_0 \omega \right)^2 \right)^{\frac{3}{2}}}$$

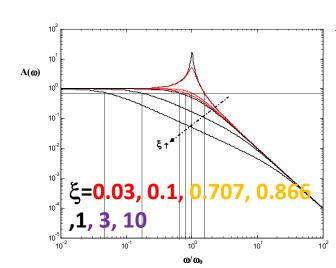
$$= -\frac{1}{2} \frac{\omega_0^2}{\left(\left(\omega_0^2 - \omega^2 \right)^2 + \left(2\xi \omega_0 \omega \right)^2 \right)^{\frac{3}{2}}} \left[2\left(\omega_0^2 - \omega^2 \right) \left(-2\omega \right) + 2\left(2\xi \omega_0 \omega \right) 2\xi \omega_0 \right]$$

极 值 点

$$= -\frac{\omega_0^2}{\left(\left(\omega_0^2 - \omega^2\right)^2 + \left(2\xi\omega_0\omega\right)^2\right)^{\frac{3}{2}}} 2\omega \left[\omega^2 + \left(2\xi^2 - 1\right)\omega_0^2\right]$$

$$\omega_e = \sqrt{1-2\xi^2}\omega_0$$
 除了零频、无穷频约 出现第三个极值点,

除了零频、无穷频外, 此为谐振峰



$$A(\omega_e) = \frac{1}{2\xi\sqrt{1-\xi^2}} > 1 = A(0)$$
 中心频点

谐振峰高度

$$\omega_e = \sqrt{1 - 2\xi^2} \omega_0^{\xi << 0.707}$$
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 $\Delta(\omega_e) = \frac{1}{2\xi\sqrt{1 - \xi^2}}$ 。 ω_0 。
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 $\omega_e = \sqrt{1 - 2\xi^2} \omega_0^{\xi << 0.70$

谐振峰频点小于自由振

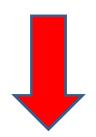
$$\frac{1}{2\mathcal{E}} = A(\omega_0)$$

幅度最大平坦

$$A(\omega) = \frac{\omega_0^2}{\sqrt{(\omega_0^2 - \omega^2)^2 + (2\xi\omega_0\omega)^2}}$$

$$\frac{dA(\omega)}{d\omega}\Big|_{\omega=0}=0$$

$$\frac{dA(\omega)}{d\omega}\Big|_{\omega=0}=0$$
Passband的中心频点最大平坦
$$\frac{d^2A(\omega)}{d\omega^2}\Big|_{\omega=0}=0$$



理想传输系统幅频特性

$$A(\omega) = A_0$$
 Passband绝对平坦

$$\frac{dA(\omega)}{d\omega}\big|_{\omega=0}=0$$

$$\frac{d^2 A(\omega)}{d\omega^2}\Big|_{\omega=0} = 0$$

$$\frac{d^n A(\omega)}{d\omega^n}\Big|_{\omega=0}=0$$

$$\xi = \frac{\sqrt{2}}{2} = 0.707$$

 $\xi = \frac{\sqrt{2}}{2} = 0.707$ 二阶低通系统的幅频特性具有最大平坦特性 此为最接近理想传输系统幅频特性的二阶低通系统: 最优

$$A_2(\omega)^{\xi=0.707} = \frac{\omega_0^2}{\sqrt{\omega_0^4 + \omega^4}}$$

$$A_2(\omega)^{\xi=0.707} = \frac{\omega_0^2}{\sqrt{\omega_0^4 + \omega^4}} \qquad A_n(\omega)^{\text{幅度最大平坦n阶滤波器}} = \frac{\omega_0^n}{\sqrt{\omega_0^{2n} + \omega^{2n}}}$$

$$A(\omega_{3dB}) = \frac{\omega_0^2}{\sqrt{(\omega_0^2 - \omega_{3dB}^2)^2 + (2\xi\omega_0\omega_{3dB})^2}} = \frac{A(0)}{\sqrt{2}} = \frac{1}{\sqrt{2}}$$

3dB带宽

$$\omega_{3dB}^4 + \left(4\xi^2\omega_0^2 - 2\omega_0^2\right)\omega_{3dB}^2 - \omega_0^4 = 0$$

$$\omega_{3dB}^{2} = \frac{-4\xi^{2}\omega_{0}^{2} + 2\omega_{0}^{2} + \sqrt{(4\xi^{2}\omega_{0}^{2} - 2\omega_{0}^{2})^{2} + 4\omega_{0}^{4}}}{2} = \left(-2\xi^{2} + 1 + \sqrt{(2\xi^{2} - 1)^{2} + 1}\right)\omega_{0}^{2}$$

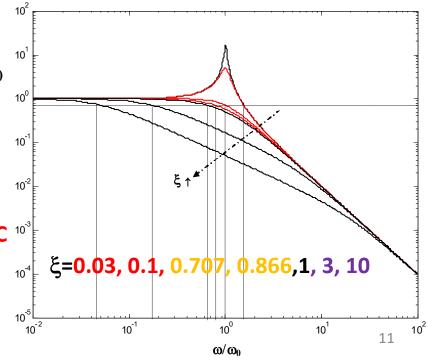
$$\omega_{3dB} = \omega_0 \sqrt{-2\xi^2 + 1 + \sqrt{(2\xi^2 - 1)^2 + 1}}$$

$$\omega_{3dB} = \omega_0$$
 $\xi = 0.707$

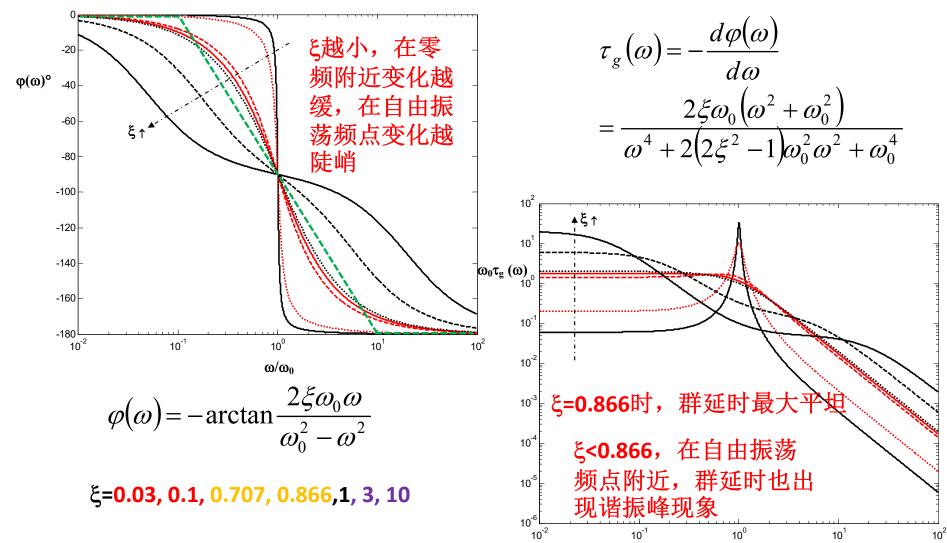
$$\omega_{3dB} = \omega_0$$

 $\omega_{3dB} \approx \frac{1}{2\xi} \omega_0$ =1/RC: RLC串联谐振回路 R很大时,行为犹如一阶RC 103

$$\omega_{3dB} \stackrel{\xi<<1}{\approx} \omega_0 \sqrt{1+\sqrt{2}} = 1.554\omega_0$$



相频特性、群延时特性



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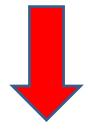
 ω/ω_0

群延时最大平坦

$$\tau_{g}(\omega) = \frac{2\xi\omega_{0}(\omega^{2} + \omega_{0}^{2})}{\omega^{4} + 2(2\xi^{2} - 1)\omega_{0}^{2}\omega^{2} + \omega_{0}^{4}}$$

$$\frac{d\tau_g(\omega)}{d\omega}\Big|_{\omega=0}=0$$

$$\frac{d^2\tau_g(\omega)}{d\omega^2}\big|_{\omega=0}=0$$



理想传输系统群延时特性

$$\tau_g(\omega) = \tau_0$$
 passband

$$\frac{d\tau_g(\omega)}{d\omega}\Big|_{\omega=0}=0$$

$$\frac{d^2\tau_g(\omega)}{d\omega^2}\big|_{\omega=0}=0$$

$$\frac{d^n \tau_g(\omega)}{d\omega^n}\Big|_{\omega=0}=0$$

$$\xi = \frac{\sqrt{3}}{2} = 0.866$$

 $\xi = \frac{\sqrt{3}}{2} = 0.866$ 二阶低通系统的群延时特性具有最大平坦特性 此为最接近理想传输系统群延时特性的二阶低通系统: 最优

最优二阶低通系统

$$\xi = \frac{\sqrt{2}}{2} = 0.707$$

 $\xi = \frac{\sqrt{2}}{2} = 0.707$ 二阶低通系统的幅频特性具有最大平坦特性(巴特沃思滤波器) 此为最接近理想传输系统幅频特性的二阶低通系统:最优

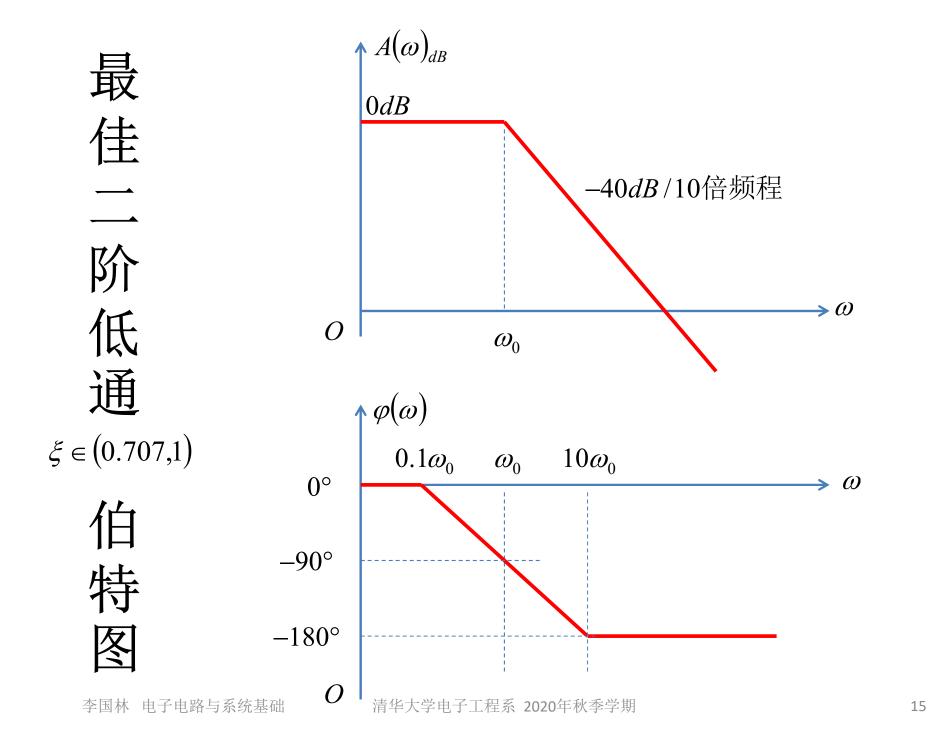
$$\xi = \frac{\sqrt{3}}{2} = 0.866$$

 $\xi = \frac{\sqrt{3}}{2} = 0.866$ 二阶低通系统的群延时特性具有最大平坦特性(贝塞尔滤波器) 此为最接近理想传输系统群延时特性的二阶低通系统,最优 此为最接近理想传输系统群延时特性的二阶低通系统: 最优

$$\xi \in (0.707,1)$$
 最优二阶低通系统:

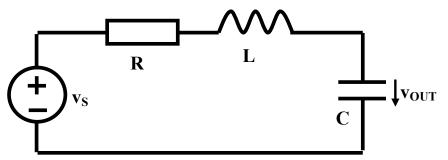
频域: 幅频特性、群延时特性相对平坦

时域:具有最快的阶跃响应(时域波形具有最小的线性失真)



时域特性: 冲激响应

$$\omega_0 = \frac{1}{\sqrt{LC}} \qquad Z_0 = \sqrt{\frac{L}{C}}$$



$$\xi = \frac{R}{2Z_0} = \frac{R}{2}\sqrt{\frac{C}{L}}$$

$$v_C(0^+) = v_C(0^-) = 0$$

$$v_S(t) = \frac{V_{S0}}{\omega_0} \cdot \delta(t)$$

$$i_L(0^-)=0$$

$$i_L(0^+) = i_L(0^-) + \frac{1}{L} \int_{0^-}^{0^+} v_L(t) dt$$

$$= \frac{1}{L} \int_{0_{-}}^{0_{+}} \frac{V_{S0}}{\omega_{0}} \delta(t) dt = \frac{V_{S0}}{\omega_{0} L} = \frac{V_{S0}}{Z_{0}}$$

$$\frac{d}{dt}v_C(0^+) = \frac{i_C(0^+)}{C} = \frac{i_L(0^+)}{C} = \frac{V_{S0}}{Z_0C} = \omega_0 V_{S0}$$

$$v_{C0}(t) = 0$$

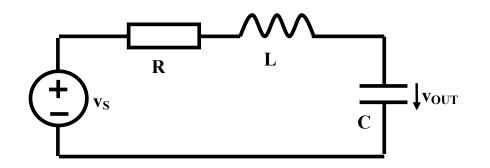
$$x(t) = x_{\infty}(t) + (X_0 - X_{\infty 0})e^{-\xi\omega_0 t} \cos\sqrt{1 - \xi^2} \omega_0 t$$

$$+ \left(\frac{\dot{X}_0 - \dot{X}_{\infty 0}}{\xi\omega_0} + X_0 - X_{\infty 0}\right) \frac{\xi}{\sqrt{1 - \xi^2}} e^{-\xi\omega_0 t} \sin\sqrt{1 - \xi^2} \omega_0 t$$

$$(t \ge 0)$$

$$v_{OUT}(t) = \frac{V_{S0}}{\sqrt{1-\xi^2}} e^{-\xi\omega_0 t} \sin\left(\sqrt{1-\xi^2}\omega_0 t\right) \cdot U(t)$$

冲激响应波形

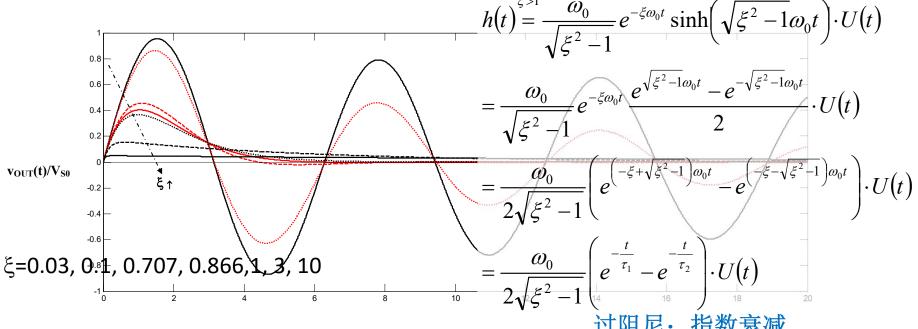


$$v_S(t) = \frac{V_{S0}}{\omega_0} \cdot \delta(t)$$

$$v_{OUT}(t) = \frac{V_{S0}}{\sqrt{1-\xi^2}} e^{-\xi\omega_0 t} \sin\left(\sqrt{1-\xi^2}\omega_0 t\right) \cdot U(t)$$

$$h(t) = \frac{\omega_0}{\sqrt{1-\xi^2}} e^{-\xi\omega_0 t} \sin\left(\sqrt{1-\xi^2}\omega_0 t\right) \cdot U(t)$$

 $h(t) = \omega_0 \sin(\omega_0 t) \cdot U(t)$ 无阻尼: 正弦振荡

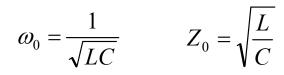


李国林 电子电路与系统基础

 $\omega_0 t$

过阻尼: 指数衰减

阶跃响应



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$$\xi = \frac{R}{2Z_0} = \frac{R}{2}\sqrt{\frac{C}{L}}$$

$$\frac{d}{dt}v_C(0^+) = \frac{i_C(0^+)}{C} = \frac{i_L(0^+)}{C} = 0$$

$$v_S(t) = V_{S0} \cdot U(t)$$

$$v_{C\infty}(t) = V_{S0}$$

$$x(t) = x_{\infty}(t) + (X_0 - X_{\infty 0})e^{-\xi\omega_0 t} \cos \sqrt{1 - \xi^2} \omega_0 t$$

$$+ \left(\frac{\dot{X}_0 - \dot{X}_{\infty 0}}{\xi\omega_0} + X_0 - X_{\infty 0}\right) \frac{\xi}{\sqrt{1 - \xi^2}} e^{-\xi\omega_0 t} \sin \sqrt{1 - \xi^2} \omega_0 t$$

$$(t > 0)$$

$$i_{L}(0^{+}) = i_{L}(0^{-}) + \frac{1}{L} \int_{0^{-}}^{0^{+}} v_{L}(t) dt$$

$$= i_{L}(0^{-}) + \frac{1}{L} \int_{0^{-}}^{0^{+}} V_{S0}U(t) dt = i_{L}(0^{-}) = 0$$

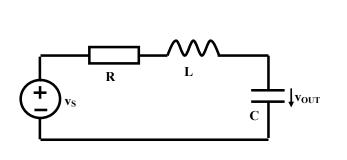
$$v_{OUT}(t) = V_{S0} \left(1 - e^{-\xi \omega_0 t} \left(\cos \sqrt{1 - \xi^2} \omega_0 t + \frac{\xi}{\sqrt{1 - \xi^2}} \sin \sqrt{1 - \xi^2} \omega_0 t \right) \right) \cdot U(t)$$
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李国林 电子电路与系统基础

 $i_I(0^-)=0$

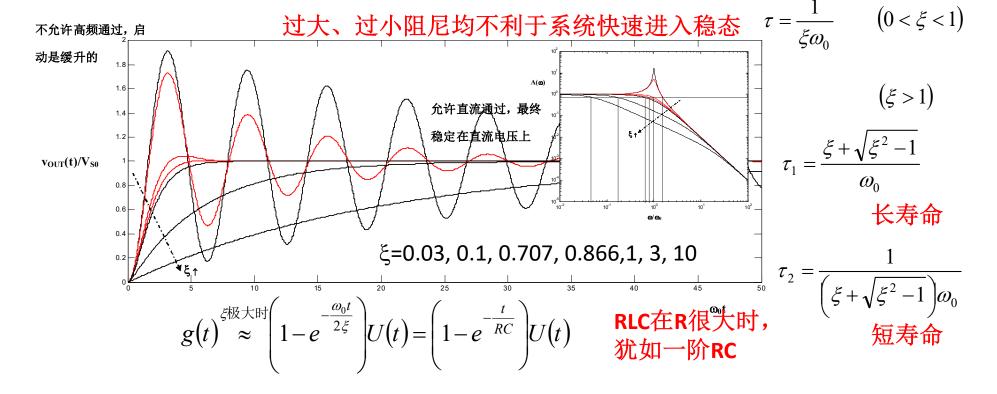
阶跃响应波形

$$v_S(t) = V_{S0} \cdot U(t)$$

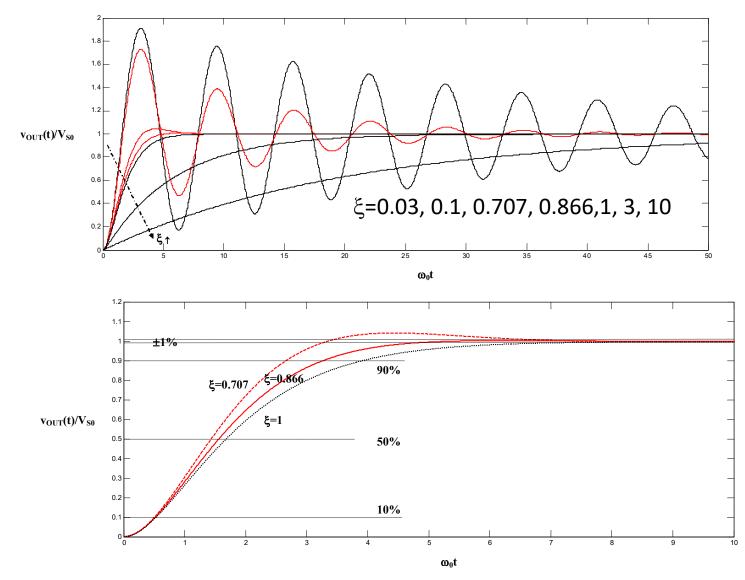


$$v_{OUT}(t) = V_{S0} \left(1 - e^{-\xi \omega_0 t} \left(\cos \sqrt{1 - \xi^2} \omega_0 t + \frac{\xi}{\sqrt{1 - \xi^2}} \sin \sqrt{1 - \xi^2} \omega_0 t \right) \right) \cdot U(t)$$

$$g(t) = \left(1 - e^{-\xi\omega_0 t} \left(\cos\sqrt{1 - \xi^2}\omega_0 t + \frac{\xi}{\sqrt{1 - \xi^2}}\sin\sqrt{1 - \xi^2}\omega_0 t\right)\right) \cdot U(t)$$



通系统



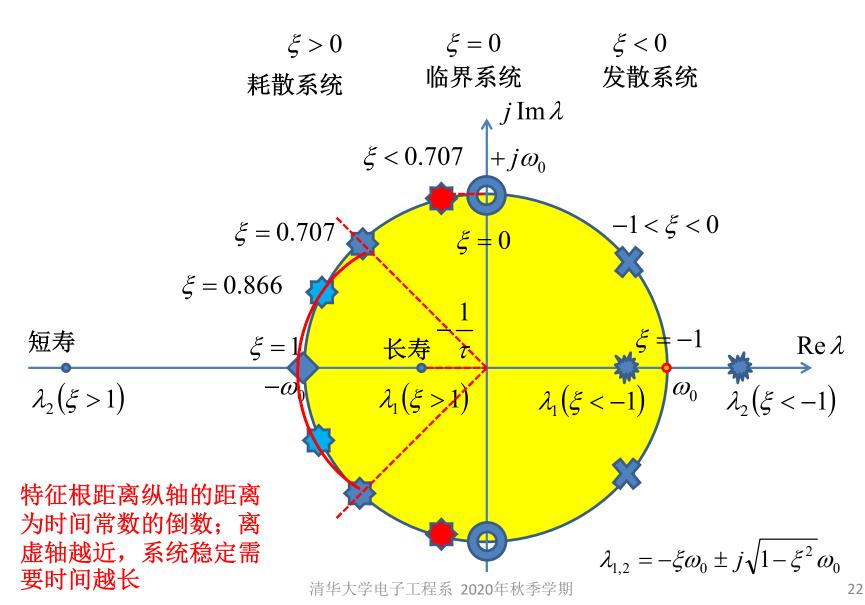
 $\xi \in (0.707,1)$

阻尼系数在0.707-1之间时,系统进入稳态需要的时间最短:最优二阶低通系统

低 通系统

		•	1	1	1	
		ξ=0.707	ξ=0.866	ξ=1	一阶	备注
上升沿时间和带宽	t _{0.1} :v _{out} (t)=0.1V _{S0}	0.507/ω ₀	0.520/ω ₀	0.533/ω ₀	0.105τ	
	t _{0.9} :v _{out} (t)=0.9V _{s0}	2.654/ω ₀	3.254/ω ₀	3.891/ω ₀	2.303τ	
	T _{rise} =t _{0.9} -t _{0.1}	2.147/ω ₀	2.734/ω ₀	3.358/ω ₀	2.198τ	
	3dB带宽2πBW _{3dB}	ω_0	0.7862ω ₀	0.6436 ω ₀	1/τ	
	T _{rise} *BW _{3dB}	0.342	0.342	0.344	0.35	0.35
响应速度	t _{delay} :v _{out} (t)=0.5V _{s0}	1.343/ω ₀	1.560/ω ₀	1.679/ ω_0	0.693τ	
与过冲	过冲	4.3%	0.43%	0	0	
		•				
进入稳态 稳定时间	t _{<1%} : v _{out} (t)/V _{s0} -1 <1%	6.587/ω ₀	4.662/ω ₀	6.640/ω ₀		
		4.657/ξω ₀	4.037/ξω ₀	6.640/ξω ₀	4.605τ	5τ
	t _{<0.1%} : v _{out} (t)/V _{s0} -1 <0.1%	10.24/ω ₀	8.757/ω ₀	9.236/ω ₀		
		7.240/ ξω ₀	7.584/ ξω ₀	9.236/ξω ₀	6.908τ	7 τ, 8τ
	•	•				
频域特性		幅度	群延时	两个一阶		
		最大平坦	最大平坦	系统级联		
时域特性		延时小	最快进入	没有过冲		
		略有过冲	稳态			

从特征根位置看二阶最优低通系统



二、二阶高通



$$H(j\omega) = \frac{\dot{V}_L}{\dot{V}_S} = \frac{j\omega L}{R + j\omega L + \frac{1}{j\omega C}} = \frac{(j\omega)^2 LC}{(j\omega)^2 LC + j\omega RC + 1} \qquad H_0 = 1$$

$$\omega_0 = \frac{1}{\sqrt{LC}}$$

$$\int_{-\infty}^{j\omega \to s} \frac{s^2 LC}{s^2 LC + sRC + 1} = \frac{s^2}{s^2 + s\frac{R}{L} + \frac{1}{LC}} = H_0 \frac{s^2}{s^2 + 2\xi\omega_0 s + \omega_0^2} \qquad \xi = \frac{R}{2Z_0} = \frac{R}{2} \sqrt{\frac{C}{L}}$$

二阶高通传函典型形式

$$H_0 = 1$$

$$\omega_0 = \frac{1}{\sqrt{LC}}$$

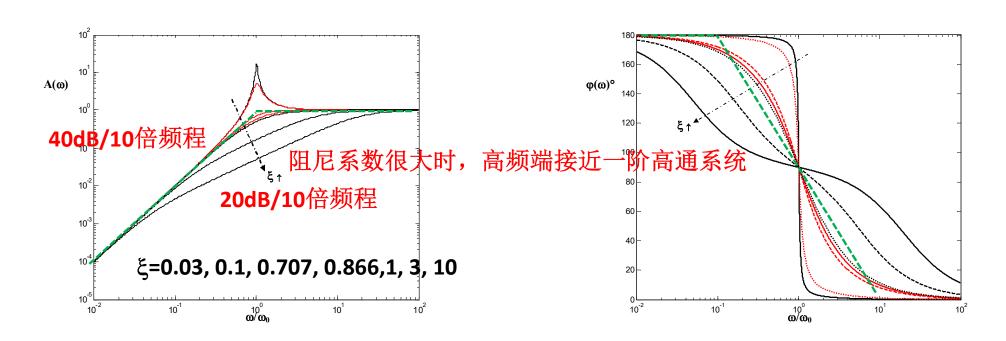
$$\xi = \frac{R}{2Z_0} = \frac{R}{2} \sqrt{\frac{C}{L}}$$

幅频特性、相频特性

$$H(s) = \frac{s^2}{s^2 + 2\xi\omega_0 s + \omega_0^2} = \frac{-\omega^2}{\omega_0^2 - \omega^2 + j2\xi\omega_0 \omega} = A(\omega)e^{j\varphi(\omega)}$$

$$A(\omega) = \frac{\omega^2}{\sqrt{(\omega_0^2 - \omega^2)^2 + (2\xi\omega_0\omega)^2}} \qquad \varphi(\omega) = \pi - \arctan\frac{2\xi\omega_0\omega}{\omega_0^2 - \omega^2}$$

$$\varphi(\omega) = \pi - \arctan \frac{2\xi\omega_0\omega}{\omega_0^2 - \omega^2}$$



$$A(\omega) = \frac{\omega^2}{\sqrt{(\omega_0^2 - \omega^2)^2 + (2\xi\omega_0\omega)^2}}$$

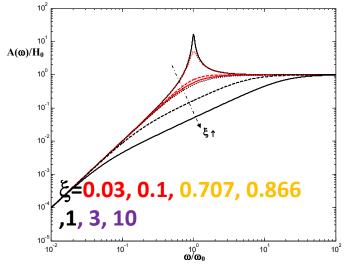
$$= \frac{2\omega\omega_0^2}{\left(\left(\omega_0^2 - \omega^2\right)^2 + \left(2\xi\omega_0\omega\right)^2\right)^{\frac{3}{2}}} \left[\omega_0^2 + \left(2\xi^2 - 1\right)\omega^2\right]$$

谐 振 峰

$$\omega_e = \frac{\omega_0}{\sqrt{1 - 2\xi^2}} \qquad (\xi < 0.707) \qquad \begin{array}{c} \text{除了零频、无穷频外} \\ \text{出现第三个极值点,} \\ \text{此为谐振峰} \end{array}$$

除了零频、无穷频外,

$$A(\omega_e) = \frac{1}{2\xi\sqrt{1-\xi^2}} > 1 = A(\infty)$$
 谐振峰高度 中心频点



$$\omega_e = \frac{\omega_0}{\sqrt{1 - 2\xi^2}} \approx \omega_0$$

为谐振峰所

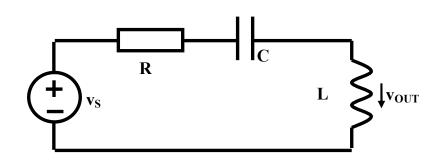
$$A(\omega_e) = \frac{1}{2\xi\sqrt{1-\xi^2}} \approx \frac{1}{2\xi} = A(\omega_0)$$

 $\omega_e = \frac{\omega_0}{\sqrt{1-2\xi^2}} \stackrel{\xi<<0.707}{\approx} \omega_0$ 谐振峰大于自由振荡频率,阻尼系数很小时,以可将自由振荡频点视为谐振峰所在位置

$$\frac{1}{2\xi} = A(\omega_0)$$

时域特性:冲激响应

$$\omega_0 = \frac{1}{\sqrt{LC}} \qquad Z_0 = \sqrt{\frac{L}{C}}$$



$$v_{S}(t) = \frac{V_{S0}}{\omega_{0}} \cdot \delta(t)$$

$$i_L(0^-)=0$$

$$i_L(0^+) = i_L(0^-) + \frac{1}{L} \int_{0^-}^{0^+} v_L(t) dt$$

$$= \frac{1}{L} \int_{0^{-}}^{0^{+}} \frac{V_{S0}}{\omega_{0}} \delta(t) dt = \frac{V_{S0}}{\omega_{0} L} = \frac{V_{S0}}{Z_{0}}$$

李国林 电子电路与系统基础

$$v_C(0^+) = v_C(0^-) = 0$$
 $\xi = \frac{R}{2Z_0} = \frac{R}{2}\sqrt{\frac{C}{L}}$

 $v_L(0) = \frac{V_{S0}}{\omega_{0}} \cdot \delta(t)$ 瞬间冲激全加载到电感上

$$v_{L}(0^{+}) = v_{S}(0^{+}) - v_{R}(0^{+}) - v_{C}(0^{+})$$
$$= 0 - i_{L}(0^{+})R - 0 = -2\xi V_{S0}$$

$$\frac{d}{dt}v_{L}(0^{+}) = \frac{d}{dt}v_{S}(0^{+}) - \frac{d}{dt}v_{R}(0^{+}) - \frac{d}{dt}v_{C}(0^{+})$$

$$= 0 - R\frac{d}{dt}i_{L}(0^{+}) - \frac{i_{C}(0^{+})}{C} = -\frac{R}{L}v_{L}(0^{+}) - \frac{i_{L}(0^{+})}{C}$$

$$= -2\xi\omega_{0}(-2\xi V_{S0}) - \frac{V_{S0}}{Z_{0}C} = (4\xi^{2} - 1)\omega_{0}V_{S0}$$

$$v_{L\infty}(t) = 0$$
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$$v_L(0^+) = -2\xi V_{S0}$$

$$\frac{d}{dt}v_L(0^+) = (4\xi^2 - 1)\omega_0 V_{S0}$$

$$v_L(0) = \frac{V_{S0}}{\omega_0} \cdot \delta(t)$$

$$v_{L\infty}(t) = 0$$

$$v_{L\infty}(t) = \frac{V_{S0}}{\omega_0} \delta(t)$$

$$x(t) = x_{\infty}(t) + (X_0 - X_{\infty 0})e^{-\xi\omega_0 t}\cos\sqrt{1 - \xi^2}\omega_0 t + \left(\frac{\dot{X}_0 - \dot{X}_{\infty 0}}{\xi\omega_0} + X_0 - X_{\infty 0}\right)\frac{\xi}{\sqrt{1 - \xi^2}}e^{-\xi\omega_0 t}\sin\sqrt{1 - \xi^2}\omega_0 t$$
 (t > 0)

$$v_{OUT}(t) = \frac{V_{S0}}{\omega_0} \delta(t) + \left[-2\xi V_{S0} e^{-\xi \omega_0 t} \cos \sqrt{1 - \xi^2} \omega_0 t + \left(\frac{4\xi^2 - 1}{\xi} - 2\xi \right) V_{S0} \frac{\xi}{\sqrt{1 - \xi^2}} e^{-\xi \omega_0 t} \sin \left(\sqrt{1 - \xi^2} \omega_0 t \right) \right] \cdot U(t)$$

$$= \frac{V_{S0}}{\omega_0} \left[\delta(t) - 2\xi \omega_0 e^{-\xi \omega_0 t} \cos \sqrt{1 - \xi^2} \omega_0 t \cdot U(t) + \frac{2\xi^2 - 1}{\sqrt{1 - \xi^2}} \omega_0 e^{-\xi \omega_0 t} \sin \left(\sqrt{1 - \xi^2} \omega_0 t \right) \cdot U(t) \right]$$

$$h(t) = \delta(t) + \omega_0 e^{-\xi \omega_0 t} \left[-2\xi \cos \sqrt{1 - \xi^2} \omega_0 t + \frac{2\xi^2 - 1}{\sqrt{1 - \xi^2}} \sin \left(\sqrt{1 - \xi^2} \omega_0 t \right) \right] \cdot U(t)$$

二阶高通的冲激响应看不太出多少东西来仅作为一个五要素法应用的练习

阶跃响应

$$\omega_0 = \frac{1}{\sqrt{LC}} \qquad Z_0 = \sqrt{\frac{L}{C}}$$

$$+$$
 v_s
 R
 L

$$V_S(t) = V_{S0} \cdot U(t)$$

$$i_L(0^-)=0$$

$$i_{L}(0^{+}) = i_{L}(0^{-}) + \frac{1}{L} \int_{0^{-}}^{0^{+}} v_{L}(t) dt$$

$$= i_{L}(0^{-}) + \frac{1}{L} \int_{0^{-}}^{0^{+}} V_{S0}U(t) dt = i_{L}(0^{-}) = 0$$

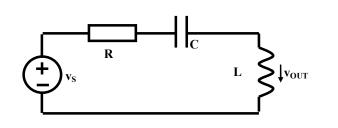
$$\zeta_L(0^+) = V_{S0} \qquad \qquad \xi = \frac{R}{2Z_0} = \frac{R}{2}\sqrt{\frac{C}{L}}$$

$$\begin{array}{c}
\downarrow_{\mathbf{V}_{L}} \mathbf{v}_{L}(0^{+}) = V_{S0} & \xi = \frac{R}{2Z_{0}} = \frac{R}{2}\sqrt{\frac{C}{L}} \\
\downarrow_{\mathbf{V}_{OUT}} & \frac{d}{dt}v_{L}(0^{+}) = \frac{d}{dt}v_{S}(0^{+}) - \frac{d}{dt}v_{R}(0^{+}) - \frac{d}{dt}v_{C}(0^{+}) \\
&= 0 - R\frac{d}{dt}i_{L}(0^{+}) - \frac{i_{C}(0^{+})}{C} = -\frac{R}{L}v_{L}(0^{+}) - \frac{i_{L}(0^{+})}{C} \\
&= -2\xi\omega_{0}V_{S0} - 0 = -2\xi\omega_{0}V_{S0} \\
v_{L\infty}(t) = 0
\end{array}$$

$$\begin{split} i_L \Big(0^+ \Big) &= i_L \Big(0^- \Big) + \frac{1}{L} \int_{0^-}^{0^+} v_L (t) dt \\ &= i_L \Big(0^- \Big) + \frac{1}{L} \int_{0^-}^{0^+} V_{S0} U(t) dt = i_L \Big(0^- \Big) = 0 \\ &= i_L \Big(0^- \Big) + \frac{1}{L} \int_{0^-}^{0^+} V_{S0} U(t) dt = i_L \Big(0^- \Big) = 0 \\ &= v_{OUT}(t) = V_{S0} e^{-\xi \omega_0 t} \left(\cos \sqrt{1 - \xi^2} \, \omega_0 t - \frac{\xi}{\sqrt{1 - \xi^2}} \sin \sqrt{1 - \xi^2} \, \omega_0 t \right) \cdot U(t) \end{split}$$

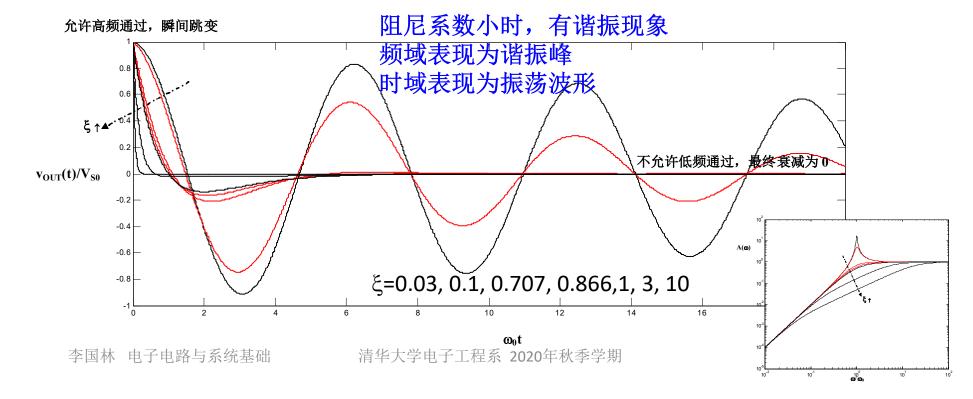
阶跃响应波形

$$v_S(t) = V_{S0} \cdot U(t)$$

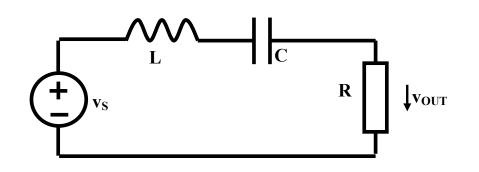


$$v_{OUT}(t) = V_{S0}e^{-\xi\omega_0 t} \left(\cos\sqrt{1-\xi^2}\omega_0 t - \frac{\xi}{\sqrt{1-\xi^2}}\sin\sqrt{1-\xi^2}\omega_0 t\right) \cdot U(t)$$

$$g(t) = e^{-\xi\omega_0 t} \left(\cos\sqrt{1-\xi^2} \omega_0 t - \frac{\xi}{\sqrt{1-\xi^2}} \sin\sqrt{1-\xi^2} \omega_0 t \right) \cdot U(t)$$



三、二阶带通



直观理解:

低频: 电容开路, 电感短路, 信号通不过高频: 电容短路, 电感开路, 信号通不过 自由振荡频点:电容电抗-jZ₀和电感电抗 +jZ₀抵消,犹如短路,信号通过

$$H(j\omega) = \frac{\dot{V}_R}{\dot{V}_S} = \frac{R}{R + j\omega L + \frac{1}{j\omega C}} = \frac{j\omega RC}{(j\omega)^2 LC + j\omega RC + 1} \qquad H_0 = 1$$

$$\omega_0 = \frac{1}{\sqrt{LC}}$$

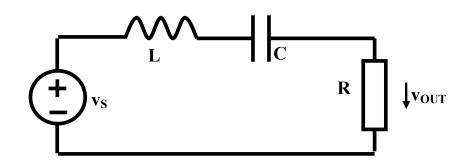
$$\psi_S = \frac{sRC}{s^2 LC + sRC + 1} = \frac{s\frac{R}{L}}{s^2 + s\frac{R}{L} + \frac{1}{LC}} = H_0 \frac{2\xi\omega_0 s}{s^2 + 2\xi\omega_0 s + \omega_0^2} \qquad \xi = \frac{R}{2Z_0} = \frac{R}{2} \sqrt{\frac{C}{L}}$$

$$H_0 = 1$$

$$\omega_0 = \frac{1}{\sqrt{LC}}$$

$$\xi = \frac{R}{2Z_0} = \frac{R}{2} \sqrt{\frac{C}{L}}$$

考察带通频域特性时习惯用参数品质因数



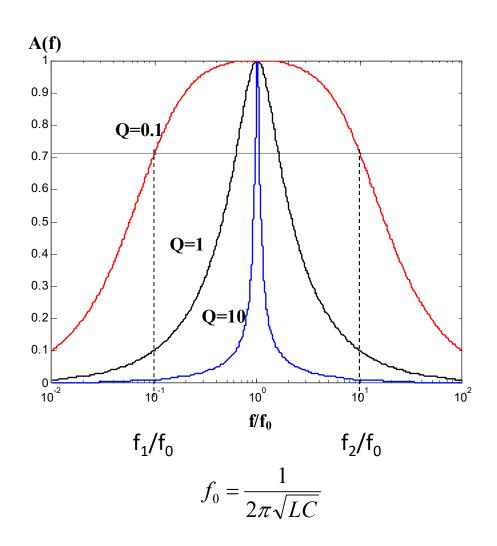
$$Q = \frac{1}{R} \sqrt{\frac{L}{C}} = \frac{Z_0}{R} = \frac{\omega_0 L}{R} = \frac{1}{2\xi}$$

品质因数:系统储能与耗能之比

$$H(j\omega) = \frac{2\xi\omega_{0}s}{s^{2} + 2\xi\omega_{0}s + \omega_{0}^{2}} = \frac{\frac{\omega_{0}}{Q}s}{s^{2} + \frac{\omega_{0}}{Q}s + \omega_{0}^{2}} = \frac{j\frac{\omega_{0}}{Q}\omega}{-\omega^{2} + j\frac{\omega_{0}}{Q}\omega + \omega_{0}^{2}}$$

$$= \frac{1}{1 + jQ\left(\frac{\omega}{\omega_{0}} - \frac{\omega_{0}}{\omega}\right)} = \frac{1}{\sqrt{1 + Q^{2}\left(\frac{\omega}{\omega_{0}} - \frac{\omega_{0}}{\omega}\right)^{2}}} e^{-j\arctan Q\left(\frac{\omega}{\omega_{0}} - \frac{\omega_{0}}{\omega}\right)} = A(\omega)e^{j\varphi(\omega)}$$

幅频特性: 带通滤波特性



$$A(f) = \frac{1}{\sqrt{1 + Q^2 \left(\frac{f}{f_0} - \frac{f_0}{f}\right)^2}}$$

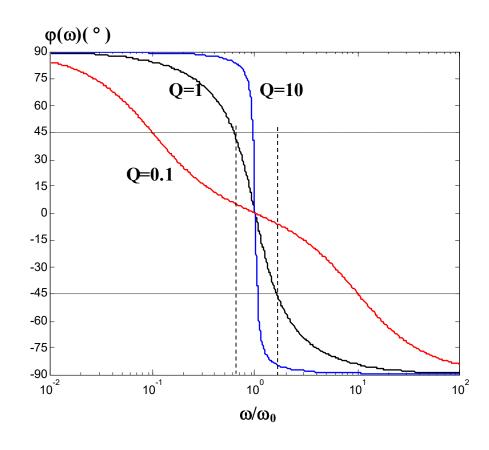
3dB通频带:
$$Q\left(\frac{f}{f_0} - \frac{f_0}{f}\right) = \pm 1$$

$$\Rightarrow f_{1,2} = \dots$$

$$\Rightarrow BW_{3dB} = f_2 - f_1 = \frac{f_0}{Q}$$

$$f_0 = \sqrt{f_1 f_2}$$

相频特性



$$BW_{3dB} \cdot \tau_{g0} = \frac{f_0}{Q} \cdot \frac{2Q}{2\pi f_0} = \frac{1}{\pi} = 0.32$$

$$\varphi(\omega) = -\arctan Q \left(\frac{\omega}{\omega_0} - \frac{\omega_0}{\omega} \right)$$

3dB通带之内,相频特性近似为直线 直线斜率代表延时

$$\tau_{g0} = -\frac{d\varphi_i}{d\omega}\Big|_{\omega=\omega_0} = \frac{2Q}{\omega_0}$$

群延时代表通带内的一群信号通过滤波器后的延时

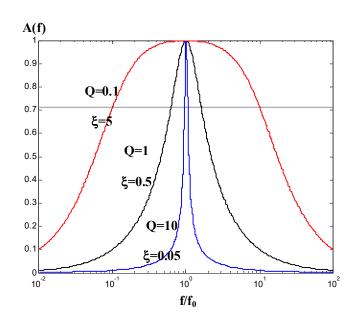
$$\varphi(\omega) \approx -Q \left(\frac{\omega}{\omega_0} - \frac{\omega_0}{\omega} \right)$$

$$= -Q \left(\frac{(\omega - \omega_0)(\omega + \omega_0)}{\omega_0 \omega} \right)$$

$$\approx -2Q \frac{(\omega - \omega_0)}{\omega_0} = -(\omega - \omega_0)\tau_{g0}$$

带宽越窄,信号延时越大

相量域分析:激励响应都是单频正弦波



$$\varphi(\mathbf{f})(^{\circ})$$
90
75
$$0$$
45
$$30$$

$$0$$

$$-15$$

$$-30$$

$$-45$$

$$-60$$

$$-75$$

$$-90$$

$$10^{-2}$$

$$10^{-1}$$

$$10^{0}$$

$$10^{1}$$

$$10^{2}$$

$$10^{1}$$

$$10^{2}$$

$$H(j\omega) = \frac{\dot{V}_R}{\dot{V}_S} = A(\omega)e^{j\varphi(\omega)}$$

$$V_{S}(t) = V_{Sm} \cos \omega t$$

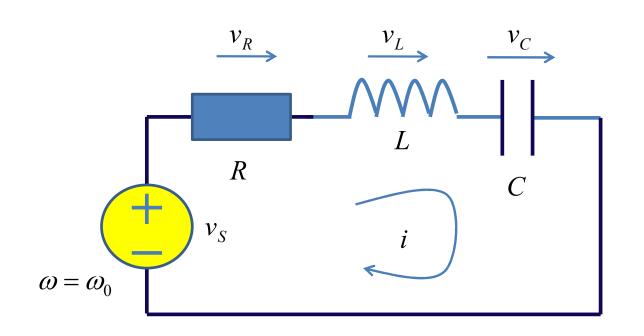
$$V_{R\infty}(t) = V_{Sm} A(\omega) \cos(\omega t + \varphi(\omega))$$

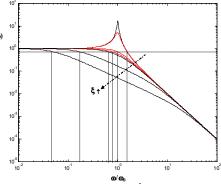
显然:在谐振频点位置,电阻获得全部输入电压??? 难道电容、电感没有分压?

$$v_S(t) = V_{Sm} \cos \omega_0 t$$
$$v_R(t) = V_{Sm} \cos \omega_0 t$$

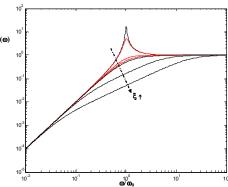
谐振: 电感电抗和电容电抗恰好抵偿

串联谐振: 电压谐振





$$A(\omega_0) = \frac{1}{2\xi} = Q$$



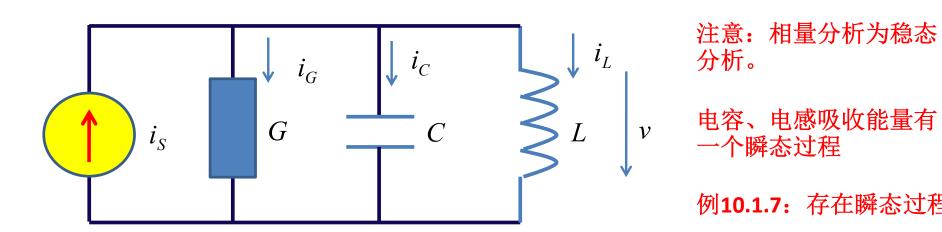
$$\dot{V}_R = \dot{V}_S$$

$$\dot{I} = \frac{\dot{V}_R}{R} = \frac{\dot{V}_S}{R}$$

$$\dot{V_L} = j\omega_0 L\dot{I} = j\frac{\omega_0 L}{R}\dot{V_S} = j\frac{Z_0}{R}\dot{V_S} = jQ\dot{V_S}$$

 $\dot{V}_C = \frac{\dot{I}}{j\omega_0 C} = -j\frac{1}{\omega_0 CR}\dot{V}_S = -j\frac{Z_0}{R}\dot{V}_S = -jQ\dot{V}_S$

谐振:外加振荡和LC自由振荡同步 并联谐振: 电流谐振

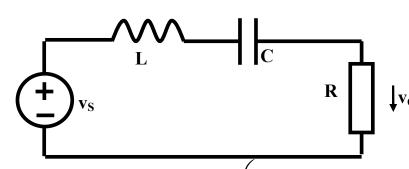


注意: 相量分析为稳态

例10.1.7: 存在瞬态过程

$$\begin{split} \dot{I}_G &= \dot{I}_S \\ \dot{V} &= \frac{\dot{I}_G}{G} = \frac{\dot{I}_S}{G} \end{split} \qquad \qquad \dot{I}_C = j\omega_0 C \dot{V} = j\frac{\omega_0 C}{G} \dot{I}_S = j\frac{Y_0}{G} \dot{I}_S = jQ\dot{I}_S \\ \dot{I}_L &= \frac{\dot{V}}{j\omega_0 L} = -j\frac{1}{\omega_0 LG} \dot{I}_S = -j\frac{Y_0}{G} \dot{I}_S = -jQ\dot{I}_S \end{split}$$

分流可以大于输入电流: 电阻电路中分流不可能大于输入电流, 分压不可能高于电源电压 电阻电路代数关系, 动态电路微分关系

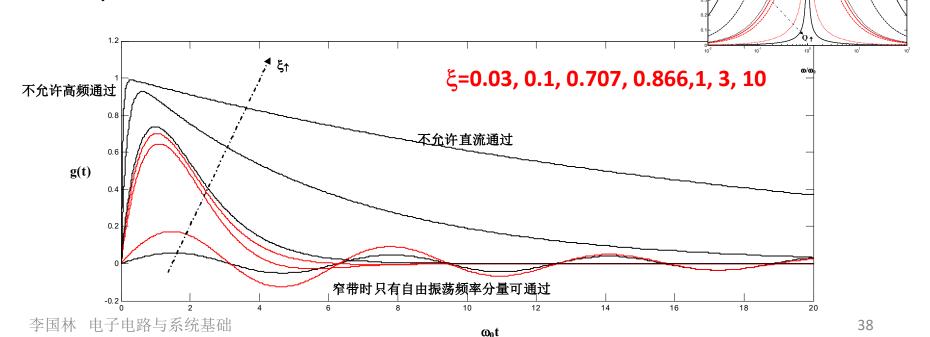


lyour 冲激响应和阶跃响应

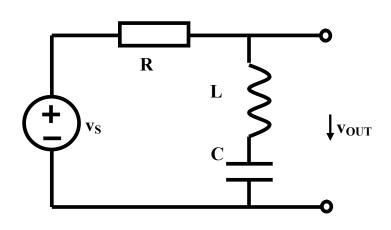
留作作业: 用五要素法证明

$$h(t) = 2\xi \omega_0 e^{-\xi \omega_0 t} \left(\cos \sqrt{1 - \xi^2} \omega_0 t - \frac{\xi}{\sqrt{1 - \xi^2}} \sin \sqrt{1 - \xi^2} \omega_0 t \right) \cdot U(t)$$

$$g(t) = \frac{2\xi}{\sqrt{1-\xi^2}} e^{-\xi\omega_0 t} \sin \sqrt{1-\xi^2} \omega_0 t \cdot U(t)$$



四、二阶带阻



直观理解:

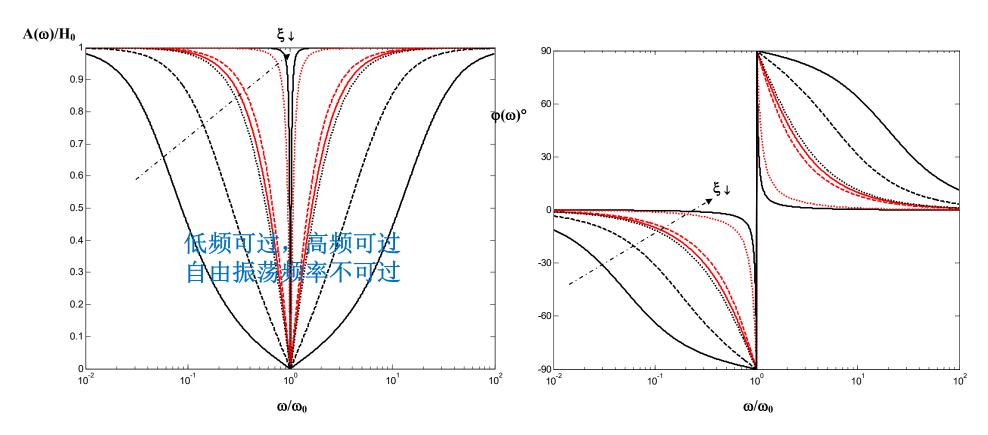
低频:电容开路,电感短路,信号全过 高频:电容短路,电感开路,信号全过 自由振荡频点:电容电抗和电感电抗抵消, 犹如短路,输出为0,信号通不过

$$H(j\omega) = \frac{\dot{V}_L + \dot{V}_C}{\dot{V}_S} = H_0 \frac{s^2 + \omega_0^2}{s^2 + 2\xi\omega_0 s + \omega_0^2} | s = j\omega$$

二阶带阻滤波器传函的一般形式

$$A(\omega) = H_0 \frac{\left|\omega_0^2 - \omega^2\right|}{\sqrt{\left(\omega_0^2 - \omega^2\right)^2 + \left(2\xi\omega_0\omega\right)^2}} \qquad \varphi(\omega) = \begin{cases} -\arctan\frac{2\xi\omega_0\omega}{\omega_0^2 - \omega^2} & \omega < \omega_0 \\ \pi - \arctan\frac{2\xi\omega_0\omega}{\omega_0^2 - \omega^2} & \omega > \omega_0 \end{cases}$$

幅频特性和相频特性



在谐振频点,信号通不过,传函为0,该位置出现相位180°跳变

只有传函为0的点允许相位出现180°跳变,其他位置相位均连续

时域特性

$$H_{BS}(s)|_{s=j\omega} = \frac{s^2 + \omega_0^2}{s^2 + 2\xi\omega_0 s + \omega_0^2} = \frac{s^2}{s^2 + 2\xi\omega_0 s + \omega_0^2} + \frac{\omega_0^2}{s^2 + 2\xi\omega_0 s + \omega_0^2} = H_{HP}(s) + H_{LP}(s)$$

$$h_{LP}(t) = \frac{\omega_0}{\sqrt{1-\xi^2}} e^{-\xi\omega_0 t} \sin\left(\sqrt{1-\xi^2}\omega_0 t\right) \cdot U(t) \quad \text{ \sharp \sharp \sharp \sharp }$$

$$h_{HP}(t) = \delta(t) + \omega_0 e^{-\xi \omega_0 t} \left[-2\xi \cos \sqrt{1 - \xi^2} \omega_0 t + \frac{2\xi^2 - 1}{\sqrt{1 - \xi^2}} \sin \left(\sqrt{1 - \xi^2} \omega_0 t \right) \right] \cdot U(t)$$

$$h_{BS}(t) = \delta(t) - 2\xi\omega_{0}e^{-\xi\omega_{0}t} \left[\cos\sqrt{1-\xi^{2}}\omega_{0}t - \frac{\xi}{\sqrt{1-\xi^{2}}}\sin(\sqrt{1-\xi^{2}}\omega_{0}t)\right] \cdot U(t) = \delta(t) - h_{BP}(t)$$

电感电压+电容电压=电源电压-电阻电压

$$H_{BS}(s)|_{s=j\omega} = \frac{s^2 + \omega_0^2}{s^2 + 2\xi\omega_0 s + \omega_0^2} = 1 - \frac{2\xi\omega_0 s}{s^2 + 2\xi\omega_0 s + \omega_0^2} = 1 - H_{BP}(s)$$

说明什么?可以直接利用时域冲激响应和频域传递函数的一一对应关系!

寻找时频对应关系:一阶RC电路

一阶RC电路:低通

$$H_{LP,1}(s) = \frac{1}{1+s\tau} = \frac{\omega_0}{s+\omega_0}$$

$$h_{LP,1}(t) = \frac{1}{\tau} e^{-\frac{t}{\tau}} \cdot U(t) = \omega_0 e^{-\omega_0 t} \cdot U(t)$$

一阶RC电路:高通

$$H_{HP,1}(s) = \frac{s\tau}{1+s\tau} = \frac{s}{s+\omega_0} = 1 - \frac{\omega_0}{s+\omega_0}$$

 $h_{HP,1}(t) = \delta(t) - \frac{1}{\tau} e^{-\frac{t}{\tau}} \cdot U(t) = \delta(t) - \omega_0 e^{-\omega_0 t} \cdot U(t)$

$$\frac{\omega_0}{s + \omega_0} \Leftrightarrow \omega_0 e^{-\omega_0 t} \cdot U(t)$$

无论RC、RL,还是其他物理系统,只要是一阶低通,必有如是时频对应关系

$$\frac{1}{s+\omega_0} \Leftrightarrow e^{-\omega_0 t} \cdot U(t)$$

无需三要素,直接用时频对应关系即可可以免除考察实际电路,只需知道输入 到输出的传递函数即可

 $1 \Leftrightarrow \delta(t)$

直通电路

寻找时频对应关系: RLC串联谐振

二阶低通:

$$H_{LP,2}(s) = \frac{\omega_0^2}{s^2 + 2\xi\omega_0 s + \omega_0^2}$$

无需五要素,直接用时频对应关系即可可以免除考察实际二阶电路,只需知道输入到输出的传递函数即可,只要传递函数一样,内部电路结构并不重要

$$h_{LP,2}(t) = \frac{\omega_0}{\sqrt{1-\xi^2}} e^{-\xi\omega_0 t} \sin \sqrt{1-\xi^2} \omega_0 t \cdot U(t)$$

$$\frac{\omega_0}{s^2 + 2\xi\omega_0 s + \omega_0^2}$$

$$\updownarrow$$

$$\frac{1}{\sqrt{1 - \xi^2}} e^{-\xi\omega_0 t} \sin\sqrt{1 - \xi^2} \omega_0 t \cdot U(t)$$

寻找时频对应关系:二阶高通

$$h_{HP,2}(t) = \underbrace{\frac{\delta(t)}{\delta(t)}} - 2\xi\omega_0 e^{-\xi\omega_0 t} \cos\sqrt{1 - \xi^2} \omega_0 t \cdot U(t) - (1 - 2\xi^2)\omega_0 \underbrace{\frac{1}{\sqrt{1 - \xi^2}}} e^{-\xi\omega_0 t} \sin\sqrt{1 - \xi^2} \omega_0 t \cdot U(t)$$

$$H_{HP,2}(s) = \frac{s^2}{s^2 + 2\xi\omega_0 s + \omega_0^2} = 1 - \frac{2\xi\omega_0 s + \omega_0^2}{s^2 + 2\xi\omega_0 s + \omega_0^2}$$

$$= \frac{1}{5} - 2\xi\omega_0 \underbrace{\frac{s + \xi\omega_0}{s^2 + 2\xi\omega_0 s + \omega_0^2}}_{= \frac{s + \xi\omega_0}{s^2 + 2\xi\omega_0 s + \omega_0^2}} - (1 - 2\xi^2)\omega_0 \underbrace{\frac{\omega_0}{s^2 + 2\xi\omega_0 s + \omega_0^2}}_{= \frac{s + \xi\omega_0}{s^2 + 2\xi\omega_0 s + \omega_0^2}}$$

$$\frac{s + \xi \omega_0}{s^2 + 2\xi \omega_0 s + \omega_0^2} \Leftrightarrow e^{-\xi \omega_0 t} \cos \sqrt{1 - \xi^2} \omega_0 t \cdot U(t)$$

验证时频对应关系:二阶带通

$$H_{BP,2}(s) = \frac{2\xi\omega_0 s}{s^2 + 2\xi\omega_0 s + \omega_0^2} = 2\xi\omega_0 \frac{s + \xi\omega_0}{s^2 + 2\xi\omega_0 s + \omega_0^2} - 2\xi^2\omega_0 \frac{\omega_0}{s^2 + 2\xi\omega_0 s + \omega_0^2}$$

$$h_{BP,2}(t) = 2\xi\omega_0 e^{-\xi\omega_0 t} \cos\sqrt{1-\xi^2} \omega_0 t \cdot U(t) - 2\xi^2 \omega_0 \frac{1}{\sqrt{1-\xi^2}} e^{-\xi\omega_0 t} \sin\sqrt{1-\xi^2} \omega_0 t \cdot U(t)$$

$$\frac{s + \xi \omega_0}{s^2 + 2\xi \omega_0 s + \omega_0^2} \Leftrightarrow e^{-\xi \omega_0 t} \cos \sqrt{1 - \xi^2} \omega_0 t \cdot U(t)$$

$$\frac{\omega_0}{s^2 + 2\xi\omega_0 s + \omega_0^2} \Leftrightarrow \frac{1}{\sqrt{1 - \xi^2}} e^{-\xi\omega_0 t} \sin\sqrt{1 - \xi^2} \omega_0 t \cdot U(t)$$

时 关 系 对 应

h(t)	H(s)
$\mathcal{S}(t)$	1 直通
U(t)	
$e^{-\omega_0 t} \cdot U(t)$	$\frac{1}{s+\omega_0}$ RC低通 负实根
$t^n e^{-\omega_0 t} \cdot U(t)$	$\frac{n!}{\left(s+\omega_0^{}\right)^{n+1}}$ 负实重根
$e^{-\xi\omega_0 t}\cos\sqrt{1-\xi^2}\omega_0 t\cdot U(t)$	$\frac{s + \xi \omega_0}{s^2 + 2\xi \omega_0 s + \omega_0^2}$ 共轭复根
$\frac{1}{\sqrt{1-\xi^2}}e^{-\xi\omega_0t}\sin\sqrt{1-\xi^2}\omega_0t\cdot U(t)$	$\frac{\omega_0}{s^2 + 2\xi\omega_0 s + \omega_0^2}$

《信号与系统》拉普拉斯变换要求掌握,我们这里不做必须要求 与系统基础 我们只要求三要素法、五要素法

响

应

是

冲

·阶低通
$$h_{LP,1}(t) = \frac{1}{\tau} e^{-\frac{t}{\tau}} \cdot U(t) = \omega_0 e^{-\omega_0 t} \cdot U(t)$$

$$g_{LP,1}(t) = \int_{-\infty}^{t} h_{LP,1}(t)dt = \dots = \left(1 - e^{-\frac{t}{\tau}}\right) \cdot U(t)$$

频域积分运算为1/s,频域分解后,对应到时域

$$\frac{1}{s}H_{LP,1}(s) = \frac{1}{s} \cdot \frac{1}{1+s\tau} = \frac{1}{s} \cdot \frac{\omega_0}{s+\omega_0} = \frac{1}{s} - \frac{1}{s+\omega_0}$$

$$g_{LP,1}(t) = U(t) - e^{-\omega_0 t} \cdot U(t) = \left(1 - e^{-\frac{t}{\tau}}\right) \cdot U(t)$$

响

激

一阶高通
$$\frac{1}{s}H_{HP,1}(s) = \frac{1}{s} \cdot \frac{s\tau}{1+s\tau} = \frac{1}{s+\omega_0}$$

$$\frac{1}{s} \Leftrightarrow U(t)$$

信号时频对应关系

$$g_{HP,1}(t) = e^{-\omega_0 t} \cdot U(t) = e^{-\frac{t}{\tau}} \cdot U(t)$$

二阶低通
$$\frac{1}{s}H_{LP,2}(s) = \frac{1}{s}\frac{\omega_0^2}{s^2 + 2\xi\omega_0 s + \omega_0^2} = \frac{1}{s} - \frac{s + 2\xi\omega_0}{s^2 + 2\xi\omega_0 s + \omega_0^2}$$
$$= \frac{1}{s} - \frac{s + \xi\omega_0}{s^2 + 2\xi\omega_0 s + \omega_0^2} - \xi\frac{\omega_0}{s^2 + 2\xi\omega_0 s + \omega_0^2}$$

$$g_{LP,2}(t) = \left(1 - e^{-\xi \omega_0 t} \left(\cos \sqrt{1 - \xi^2} \omega_0 t + \frac{\xi}{\sqrt{1 - \xi^2}} \sin \sqrt{1 - \xi^2} \omega_0 t\right)\right) \cdot U(t)$$

时频对应

系

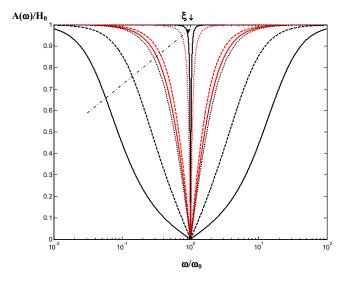
二阶带阻
$$\frac{1}{s}H_{BS,2}(s) = \frac{1}{s} \cdot \frac{s^2 + \omega_0^2}{s^2 + 2\xi\omega_0 s + \omega_0^2} = \frac{1}{s} - 2\xi \frac{\omega_0}{s^2 + 2\xi\omega_0 s + \omega_0^2}$$

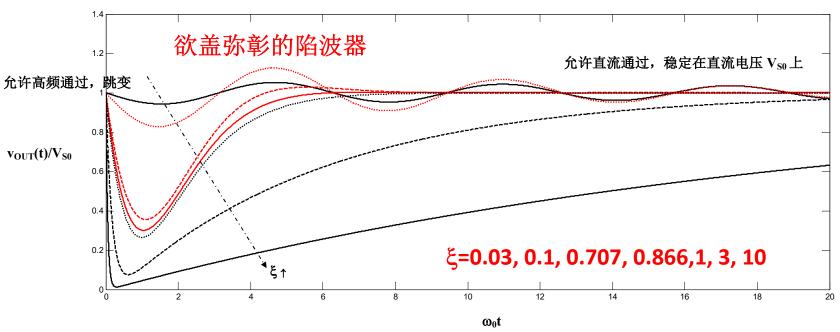
$$g_{BS,2}(t) = U(t) - \frac{2\xi}{\sqrt{1-\xi^2}} e^{-\xi\omega_0 t} \sin \sqrt{1-\xi^2} \omega_0 t \cdot U(t)$$

无需五要素法,直接根据时频对应关系给冲激响应和阶跃响应和实际系统实际构成无关,仅和端口传递特性有关端口抽象后将电路分析转化为信号的数学分析

二阶带阻的阶跃响应

$$g_{BS,2}(t) = U(t) - \frac{2\xi}{\sqrt{1-\xi^2}} e^{-\xi\omega_0 t} \sin \sqrt{1-\xi^2} \omega_0 t \cdot U(t)$$





以单频正弦波为输入, ω₀频率分量无法通过

五、二阶全通

$$H(s) = \frac{s^2 - 2\xi\omega_0 s + \omega_0^2}{s^2 + 2\xi\omega_0 s + \omega_0^2}$$

$$\stackrel{s=j\omega}{=} \frac{(\omega_0^2 - \omega^2) - j2\xi\omega_0 \omega}{(\omega_0^2 - \omega^2) + j2\xi\omega_0 \omega}$$

$$= e^{-j2\arctan\frac{2\xi\omega_0 \omega}{\omega_0^2 - \omega^2}}$$

$$= e$$

幅频特性恒为常数1 只有相位调整:可用于相位均衡

$$A(\omega) = 1$$

$$\varphi(\omega) = -2 \arctan \frac{2\xi \omega_0 \omega}{\omega_0^2 - \omega^2}$$

二阶全通的时域特性目前我们不感兴趣,不再考察

关于谐振的小结

• 对于二阶线性时不变系统, 其特征方程和特征根分别为

$$\lambda^2 + 2\xi\omega_0\lambda + \omega_0^2 = 0 \qquad \lambda_{1,2} = \left(-\xi \pm \sqrt{\xi^2 - 1}\right)\omega_0$$

• 阻尼系数大于1时,两个特征根为负实根,因而二阶系统可以拆解为两个一阶系统 $\xi>1$ — 一阶系统一般不谈谐振

$$H(s) = \frac{\alpha s^{2} + \beta s + \gamma}{s^{2} + 2\xi \omega_{0} s + \omega_{0}^{2}} = \frac{\alpha s^{2} + \beta s + \gamma}{(s - \lambda_{1})(s - \lambda_{2})} = a_{0} + \frac{a_{1}}{s - \lambda_{1}} + \frac{a_{2}}{s - \lambda_{2}}$$

$$= \frac{a_{0}(s - \lambda_{1})(s - \lambda_{2}) + a_{1}(s - \lambda_{2}) + a_{2}(s - \lambda_{1})}{(s - \lambda_{1})(s - \lambda_{2})} = \frac{a_{0}s^{2} + (a_{1} + a_{2} - a_{0}(\lambda_{1} + \lambda_{2}))s + (a_{0}\lambda_{1}\lambda_{2} - a_{1}\lambda_{2} - a_{2}\lambda_{1})}{(s - \lambda_{1})(s - \lambda_{2})}$$

$$h(t) = a_0 \delta(t) + \left(a_1 e^{\lambda_1 t} + a_2 e^{\lambda_2 t}\right) \cdot U(t) = a_0 \delta(t) + \left(a_1 e^{-\frac{t}{\tau_1}} + a_2 e^{-\frac{t}{\tau_2}}\right) \cdot U(t)$$
 长寿项和短寿项

 a_0 、 a_1 、 a_2 待定系数,由传函分子项决定:由结构、响应位置共同决定 传函分母是系统结构的描述,决定响应的形态

时域波形上看谐振

 $0 < \xi < 1$

- 阻尼系数小于1时,两个特征根为共轭复根,二阶系统不 能拆解为两个一阶系统
 - 此时多以谐振概念说明系统特性

$$\lambda_{1,2} = \left(-\xi \pm \sqrt{\xi^2 - 1}\right)\omega_0 = \left(-\xi \pm j\sqrt{1 - \xi^2}\right)\omega_0 = -\xi\omega_0 \pm j\sqrt{1 - \xi^2}\omega_0 = -\frac{1}{\tau} \pm j\omega_d$$

谐振表现在时域,就是其冲激响应或阶跃响应是振荡形态的

$$H(s) = \frac{\alpha s^2 + \beta s + \gamma}{s^2 + 2\xi \omega_0 s + \omega_0^2} = a_0 + a_1 \frac{s + \xi \omega_0}{s^2 + 2\xi \omega_0 s + \omega_0^2} + a_2 \frac{\omega_0}{s^2 + 2\xi \omega_0 s + \omega_0^2}$$

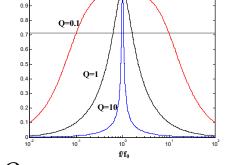
$$h(t) = a_0 \delta(t) + \left(a_1 e^{-\xi \omega_0 t} \cos \sqrt{1 - \xi^2} \omega_0 t + a_2 \frac{1}{\sqrt{1 - \xi^2}} e^{-\xi \omega_0 t} \sin \sqrt{1 - \xi^2} \omega_0 t \right) \cdot U(t)$$

$$= a_0 \delta(t) + e^{-\frac{t}{\tau}} \left(a_1 \cos \omega_d t + a_2 \frac{1}{\sqrt{1 - \xi^2}} \sin \omega_d t \right) \cdot U(t) = a_0 \delta(t) + b_0 e^{-\frac{t}{\tau}} \cos(\omega_d t + \varphi_0) \cdot U(t)$$
欠阻尼减幅正弦振荡
$$h(t) = a_0 \delta(t) + (a_1 \cos \omega_0 t + a_2 \sin \omega_0 t) \cdot U(t)$$
 无阻尼正弦振荡: 自由振荡频率

$$h(t) = a_0 \delta(t) + \left(a_1 e^{-\omega_0 t} + a_2 e^{-\omega_0 t} \omega_0 t\right) \cdot U(t)$$
 临界阻尼无振荡

带通选频特性看谐振 $Q = \begin{cases} \frac{Z_0}{R} = \frac{1}{R} \sqrt{\frac{L}{C}} & \text{串联谐振} \\ \frac{Y_0}{C} = R \sqrt{\frac{C}{L}} & \text{并联谐振} \end{cases} H_0 = \begin{cases} 1 \\ I_{S0}R \end{cases}$

电压源驱动RLC串联谐振回路,电流源驱动RLC并联 谐振回路,在电阻上都可形成带通选频电压输出特性



$$BW_{3dB} = \frac{f_0}{Q}, \tau_{g0} = \frac{2Q}{\omega_0}$$

- 在中心频点上,电抗(或电纳)相互抵偿,称之为谐振
 - ω=ω₀, 谐振
 - ω≠ω₀, 失谐

并联谐振和串联谐振

- 并联RLC是电流谐振,在谐振频点上,电感电流和电容电流是电阻电流的Q倍,但两者反相,并联LC对外总电流为0,呈现开路状态
 - 由于并联LC对外开路,并联RLC在谐振频点呈现纯阻特性,低于谐振频点,驱动电流主要从电感支路流,并联RLC整体呈现感性,高于谐振频点,驱动电流主要从电容支路流,并联RLC整体呈现容性

$$\dot{I}_G = \dot{I}_S$$
 $\dot{I}_C = jQ\dot{I}_S$ $\dot{I}_L = -jQ\dot{I}_S$ $\omega = \omega_0$

- 串联RLC是电压谐振,在谐振频点上,电感电压和电容电压是电阻电压的Q倍,但两者反相,串联LC对外总电压为0,呈现短路状态
 - 由于串联LC对外短路,串联RLC在谐振频点呈现纯阻特性,低于谐振频点,驱动电压主要加载到电容元件上,串联RLC整体呈现容性,高于谐振频点,驱动电压主要加载到电感元件上,串联RLC整体呈现感性

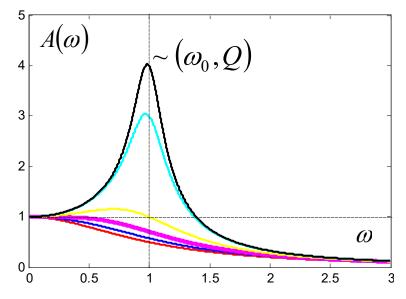
$$\dot{V}_R = \dot{V}_S$$
 $\dot{V}_L = jQ\dot{V}_S$ $\dot{V}_C = -jQ\dot{V}_S$ $\omega = \omega_0$

低通特性看谐振

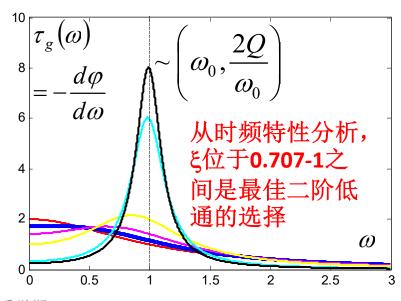
串臂电感和并臂电容可形成二阶低通传 输系统

$$H_{LP}(s) = H_0 \frac{\omega_0^2}{s^2 + 2\xi\omega_0 s + \omega_0^2} = H_0 A(\omega) e^{j\varphi(\omega)}$$

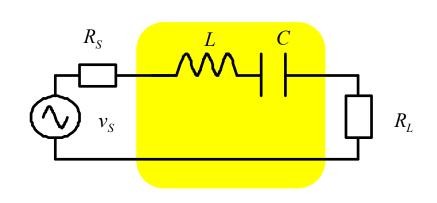
- 从幅频特性上看,当Q=0.707时,幅频特性是最平坦的(ξ=0.707)
 - 通带内信号幅度增益几乎一致: 失真小
- 当**Q>0.707**后,幅频特性在 ω_0 附近呈现谐振峰
 - ω,频率分量过去很多,时域呈现振铃现象
- 从群延时特性上看,当**Q=0.577**时,群延时特性是最平坦的(ξ**=0.866**)
 - 通带内信号几乎同时到达输出端: 失真小
- 当Q>0.577后,群延时特性在 ω_0 附近呈现 谐振峰
 - 通带内信号到达输出端时间差别大,输出波形和输入波形差别大,失真严重

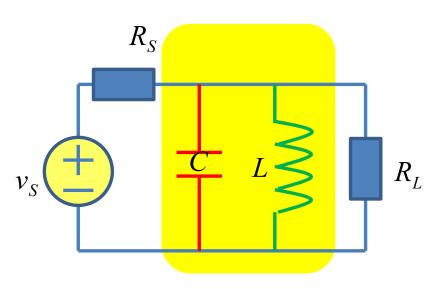


Q = 0.5/0.577/0.707/1/3/4



作业1: 带通选频特性





$$H(s) = 2\sqrt{\frac{R_S}{R_L}} \frac{v_L(s)}{v_S(s)}$$
$$= H_0 \frac{2\xi\omega_0 s}{s^2 + 2\xi\omega_0 s + \omega_0^2}$$

- 证明: LC串联谐振回路串接在信号通路上, LC并联谐振回路并接在信号通路上, LC并联谐振回路并接在信号通路上, 都具有类似的带通选频特性
 - 两个系统的传递函数形式 一致,请给出两个系统传 递函数的基本参量表述
 - 用电路元件RLC参量表述系统传递函数参量 H_0 , ξ , ω_0

1

$$H(s) = H_0 \frac{2\xi\omega_0 s}{s^2 + 2\xi\omega_0 s + \omega_0^2} \qquad H(j\omega) = H_0 \frac{1}{1 + jQ\left(\frac{\omega}{\omega_0} - \frac{\omega_0}{\omega}\right)}$$

• (1) 求它的两个3dB频点f₁,f₂表达式, 此说明

$$BW_{3dB} = f_2 - f_1 = \frac{f_0}{Q}, \qquad f_0 = \sqrt{f_1 f_2}$$

(2)以串联RLC电阻分压为例,用五要素 法和时频对应法说明二阶带通系统的冲激 响应和阶跃响应分别为

$$h(t) = 2\xi \omega_0 H_0 e^{-\xi \omega_0 t} \left(\cos \sqrt{1 - \xi^2} \omega_0 t - \frac{\xi}{\sqrt{1 - \xi^2}} \sin \sqrt{1 - \xi^2} \omega_0 t \right) \cdot U(t)$$

$$g(t) = \frac{2\xi}{\sqrt{1 - \xi^2}} H_0 e^{-\xi \omega_0 t} \sin \sqrt{1 - \xi^2} \omega_0 t \cdot U(t)$$

带 通 滤 波

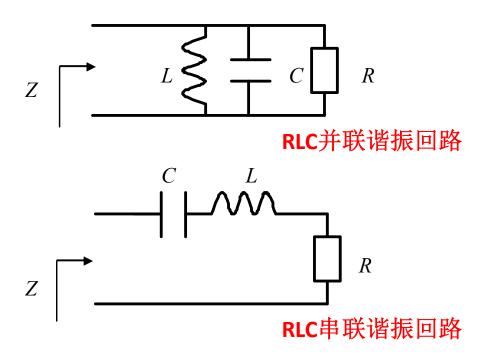
器

作业3: 串并联阻抗特性曲线

· 求RLC并联谐振回路和RLC串联谐振回路的端口输入阻抗

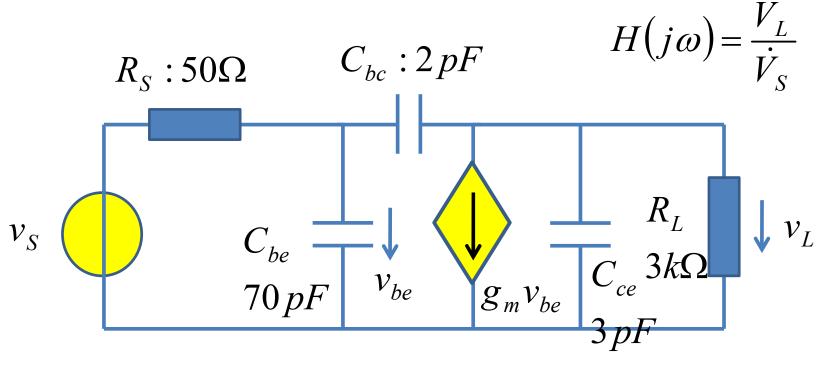
$$Z(j\omega) = R(\omega) + jX(\omega)$$
$$= |Z(\omega)|e^{j\varphi(\omega)}$$

- 作图: 画出端口输入电阻、输入电抗、输入阻抗幅度、输入阻抗 有限 有性 曲线
 - 取Q=5,0.5,0.05三种 情况



作业4 晶体管放大器传函及其伯特图

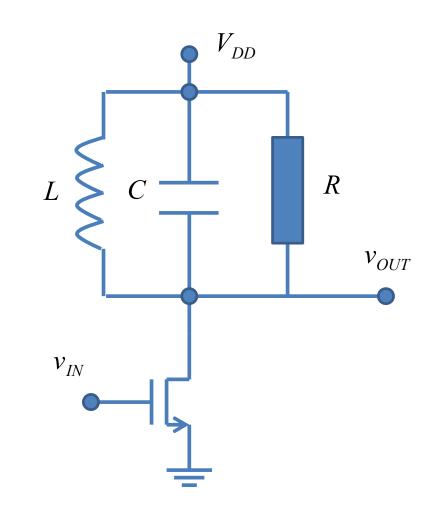
• 求如下晶体管放大器的传递函数,并画出伯特图



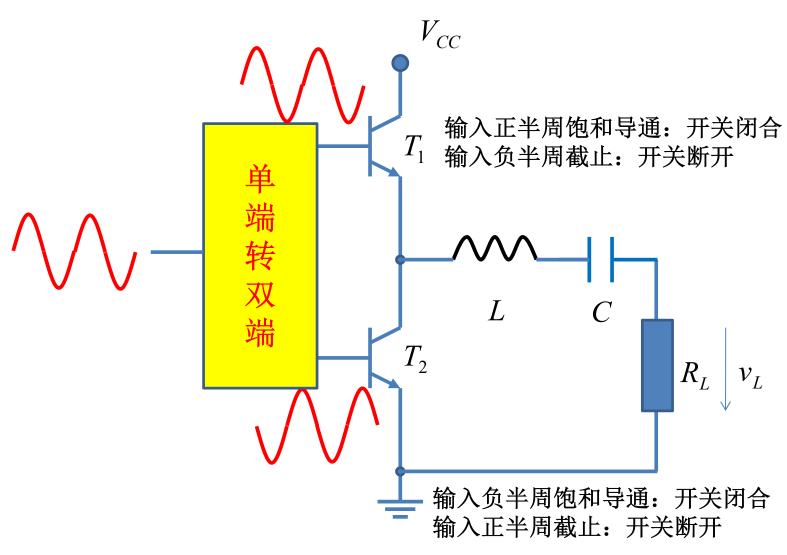
 $g_m:40mS$

- 如图所示,晶体管输入电压为 ν_{IN}= V_{GSO} +V_{sm}COSωt,其中V_{GSO}直 流电压使得晶体管偏置在有源区, 而交流小信号的幅度V_{sm}很小
- 1、假设晶体管是理想跨导器, 不考虑厄利效应,不考虑寄生电容效应,请画出交流小信号等效 电路
 - 和电阻电路的交流小信号分析一样,不同的是负载电阻R_L被负载阻抗Z_L=(R||L||C)所替代
- 2、确认对于交流小信号,输出 电压是输入电压的带通选频结果, 求出带通中心频点的放大倍数和 3dB带宽
- 3、请写出输出vour(t)的表达式。

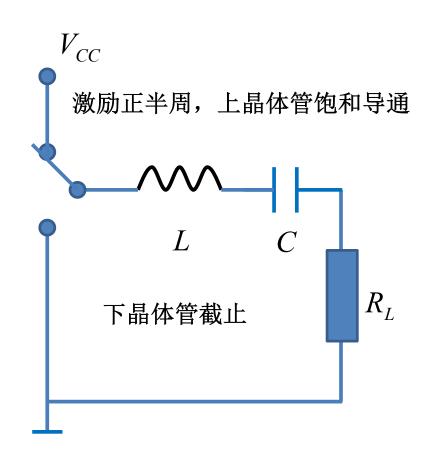
作业**5** 窄带选频放大器

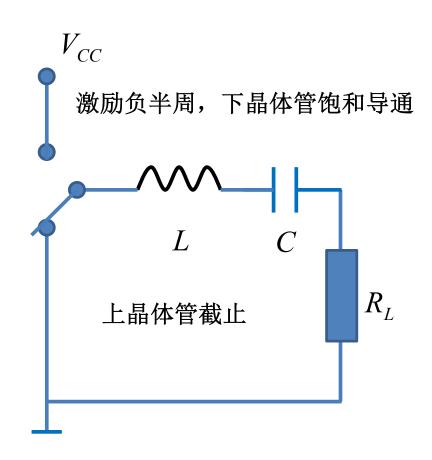


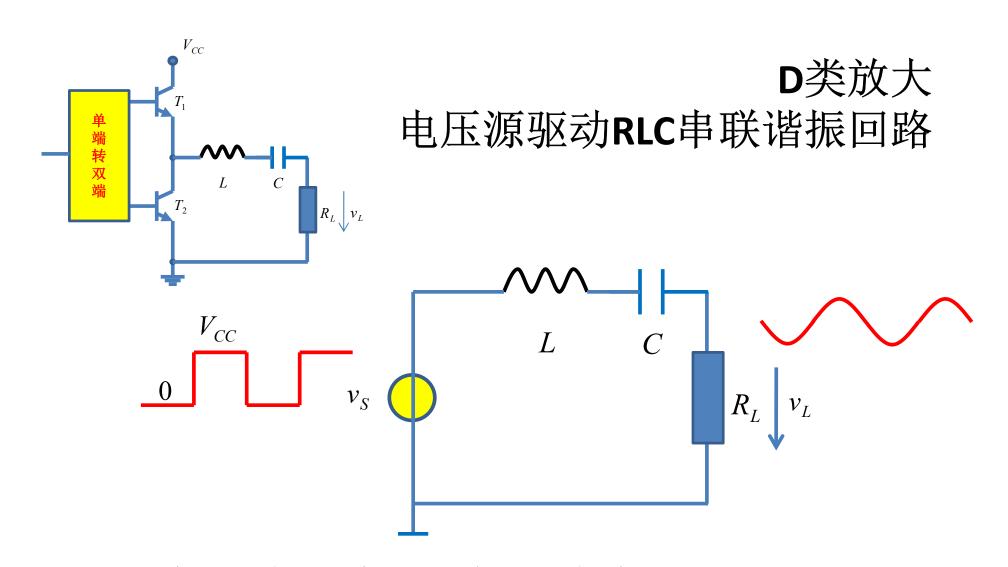
习题6 D类放大器



D类放大器等效电路





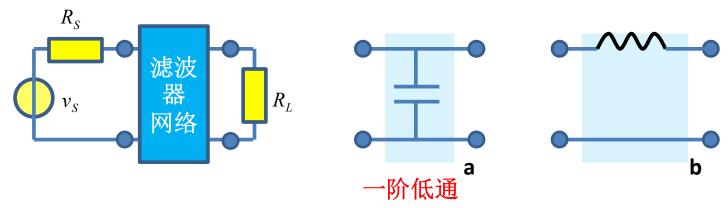


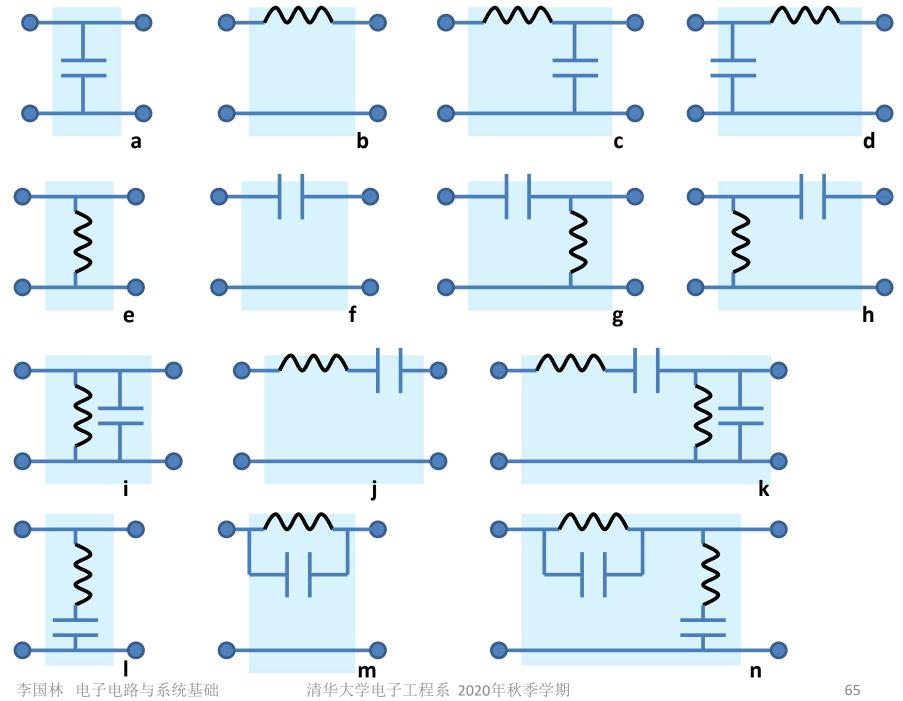
• 要想三次谐波分量低于基波分量40dB以上, 谐振回路的Q值应取多大?

作业7: 典型结构滤波器类型判断

• 电容和电感的记忆能力或者积分效应,导致时域上的延时和频域上的选频特性

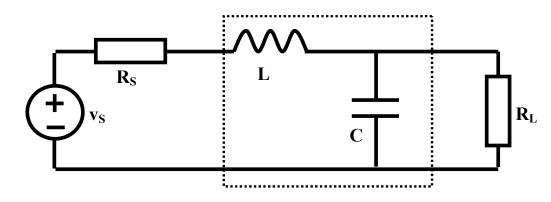
- 常见滤波器分类
 - 低通、高通、带通、带阻
 - 请给出正确的滤波器分类





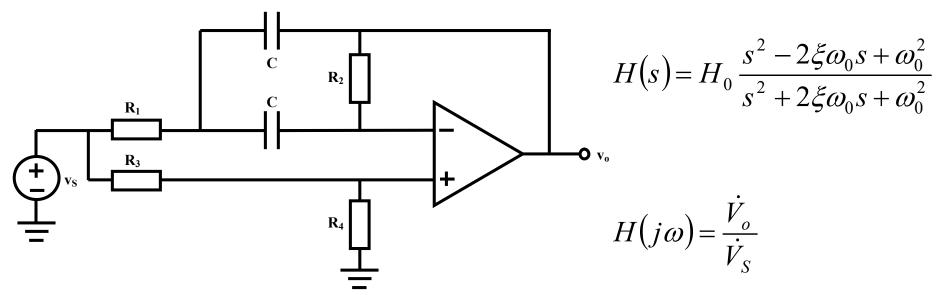
作业8: 低通滤波器设计

- 练习10.2.7 如图所示,已知信源内阻为50Ω, 负载电阻也是50Ω,请设计一个具有群延时最 大平坦特性的二阶低通LC滤波器,其3dB带宽 为1MHz,请给出虚框表示的LC低通滤波器中 电感和电容的具体数值。
 - 群延时最大平坦
 - 选作: 幅度最大平坦



作业9: 全通滤波器

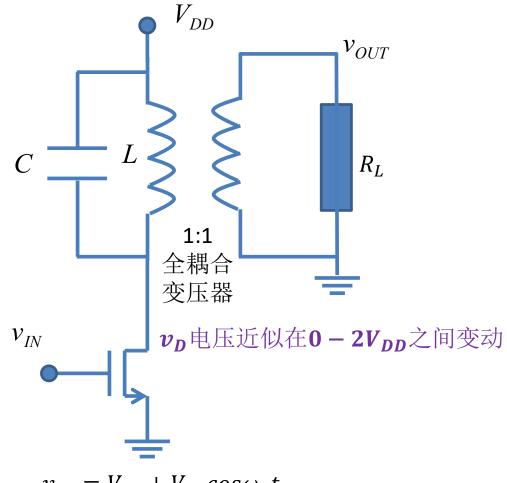
• 练习10.2.20 请分析图示电路,电阻 R_1 、 R_2 、 R_3 、 R_4 之间满足什么关系时,该电路可构成一个二阶全通滤波器。给出该全通滤波器的关键参量: H_0 , ω_0 , ξ 。



Cadence仿真

- · LC谐振在ω₀频点上, 从而只有该频点附 近频率可以通过
- 改变 V_{BO} ,使得导通角变小,同时改变 R_L ,使得 v_{OUT} 正弦波幅度接近 V_{DD}
- 研究随着导通角变小,放大器效率变化

$$\eta = \frac{P_L}{P_{DD}} = \frac{0.5 \, V_{om}^2 / R_L}{V_{DD} I_{DC}}$$



$$\eta = \frac{P_L}{P_{DD}} = \frac{0.5 V_{om}^2 / R_L}{V_{DD} I_{DC}}$$

$$= \frac{0.5 I_{om}^2 R_L}{V_{DD} I_{DC}} = \frac{0.5 I_{om} R_L I_{om}}{V_{DD} I_{DC}}$$

$$\approx \frac{0.5 I_{om}}{I_{DC}} = 0.5 \frac{I_1(\theta)}{I_0(\theta)}$$

导通角与效率

