# CONTROL ENGINEERING - MODEL ANSWERS

1. a) The reachability matrix is

$$\mathcal{R} = \left[ \begin{array}{ccc} 0 & 1 & 0 \\ 1 & 0 & -1 \\ 0 & 0 & 0 \end{array} \right].$$

This has rank equal to two, hence the system is not reachable. To check controllability, note that

$$A^3 \in \operatorname{Im} \mathscr{R}$$
,

hence the system is controllable. Similarly, one could observe that the unreachable mode is  $\lambda=0$ , hence controllability. [4 marks]

b) The set of states  $\mathcal{R}_2$  that can be reached from x(0) = 0 in two steps is given by

$$x(2) = ABu(0) + Bu(1) = \begin{bmatrix} u(0) \\ u(1) \\ 0 \end{bmatrix}.$$

 $\mathcal{R}_2$  is a two dimensional subspace.

[4 marks]

The set of states  $\mathscr{C}_2$  that can be controlled to zero in two steps is given by the states which satisfy the condition

$$0 = x(2) = A(Ax(0) + Bu(0)) + Bu(1) = \begin{bmatrix} x_3(0) - x_1(0) + u(0) \\ -x_2(0) + u(1) \\ 0 \end{bmatrix},$$

for some selection of u(0) and u(1). This shows that all states can be controlled to zero in two steps:  $\mathscr{C}_2$  is a three dimensional subspace, that is spans the whole state space. The set  $\mathscr{C}_2$  is larger than the set  $\mathscr{R}_2$  because the system is controllable, but not reachable. [6 marks]

d) Note that  $(K = [k_1 \ k_2 \ k_3])$ 

$$A + BK = \left[ \begin{array}{ccc} 0 & 1 & 0 \\ k_1 - 1 & k_2 & k_3 + 1 \\ 0 & 0 & 0 \end{array} \right].$$

The characteristic polynomial of A + BK is

$$p(\lambda) = \lambda^3 - k_2 \lambda^2 + (1 - k_1) \lambda.$$

Selecting  $k_2 = 0$  and  $k_1 = 1$  yields  $p(\lambda) = \lambda^3$ , as requested. Note that, since the unreachable mode is at  $\lambda = 0$  there problem of assigning the eigenvalues is feasible, and has infinitely many solutions, namely

$$K = \begin{bmatrix} 1 & 0 & k_3 \end{bmatrix}$$
.

Note that  $KK' = 1 + k_3^2$ , hence the *optimal K* is

$$K = \begin{bmatrix} 1 & 0 & 0 \end{bmatrix}$$
.

[6 marks]

- 2. a) For this part h = 1, that is T(t+1) = u(t).
  - i) Note that

$$T(t+1) = u(t) = u(t-1) - \alpha(T(t) - T_0)$$

and that

$$T(t) = u(t-1).$$

As a result

$$T(t+1) = T(t) - \alpha(T(t) - T_0) = (1-\alpha)T(t) + \alpha T_0.$$

[2 marks]

ii) The system in part a.i) is stable if and only if

$$-1 < 1 - \alpha < 1$$
.

or, equivalently,

$$\alpha \in (0,2)$$
.

Since  $\alpha \in (1,2)$  then the closed-loop system is asymptotically stable and for any initial condition the temperature converges to the desired value  $T_0$ . [2 marks]

- b) For this part h = 2, that is T(t+2) = u(t).
  - i) Note that

$$T(t+2) = u(t) = u(t-1) - \alpha(T(t) - T_0)$$

and that

$$T(t+1) = u(t-1)$$

As a result

$$T(t+2) = T(t+1) - \alpha(T(t) - T_0).$$

[4 marks]

ii) Let 
$$y(t) = x_1(t) = T(t)$$
,  $x_2(t) = T(t+1)$  and  $u(t) = T_0$ . Then  $x_1^+ = x_2$ ,  $x_2^+ = x_2 - \alpha(x_1 - u)$ .

As a result

$$A = \begin{bmatrix} 0 & 1 \\ -\alpha & 1 \end{bmatrix}, \qquad B = \begin{bmatrix} 0 \\ \alpha \end{bmatrix}, \qquad C = \begin{bmatrix} 1 & 0 \end{bmatrix}.$$

[6 marks]

iii) The charcateristic polynomial of the matrix A is

$$p(z) = \det(zI - A) = z^2 - z + \alpha.$$

Using the transformation

$$z = \frac{1+s}{1-s}$$

one obtains a rational function the numerator of which is

$$\bar{p}(s) = (2+\alpha)s^2 + 2(1-\alpha)s + \alpha.$$

Note that for  $\alpha \in (1,2)$  the coefficient of "s" is negative, whereas the coefficients of "s<sup>2</sup>" and "s<sup>0</sup>" are positive. The closed-loop system is therefore unstable. [4 marks]

c) A fast boiler let you control the temperature to the desired value, a slow one will not! [2 marks]

#### 3. a) The three equations are

$$\dot{x}_1 - x_2 + x_3 = 0$$
  $\dot{x}_2 + x_1 - x_2 + u = 0$ ,  $x_1 - x_3 + u = 0$ .

[2 marks]

#### b) From the third equation one obtains

$$x_3 = x_1 + u_1$$

which replaced in the  $\dot{x}_1$ ,  $\dot{x}_2$  and y equations gives

$$\dot{x}_1 = -x_1 + x_2 - u, \qquad \dot{x}_2 = -x_1 + x_2 + u, \qquad y = 2x_1 + x_2 + u.$$

[ 2 marks ]

#### c) From part b) one obtains

$$A_r = \begin{bmatrix} -1 & 1 \\ -1 & 1 \end{bmatrix}, \qquad B_r = \begin{bmatrix} -1 \\ 1 \end{bmatrix}, \qquad C_r = \begin{bmatrix} 2 & 1 \end{bmatrix}, \qquad D_r = \begin{bmatrix} 1 \end{bmatrix}.$$

[ 4 marks ]

#### d) Note that

$$\det(\lambda E - A) = \lambda^2$$
  
 $\det(\lambda I - A_r) = \lambda^2$ 

and that

$$\det(\lambda I - A_r) = \lambda^2$$

hence the descriptor system and the reduced system have the same eigenvalues.

[4 marks]

## Note that e)

$$\mathcal{O}_r = \begin{bmatrix} C_r \\ C_r A_r \end{bmatrix} = \begin{bmatrix} 2 & 1 \\ -3 & 3 \end{bmatrix}.$$

As a result,  $\det \mathcal{O}_r \neq 0$  and the reduced system is observable. Note now that

$$\begin{bmatrix} \lambda E - A \\ C \end{bmatrix} = \begin{bmatrix} \lambda & -1 & 1 \\ 1 & \lambda - 1 & 0 \\ -1 & 0 & 1 \\ 1 & 1 & 1 \end{bmatrix}$$

and this has rank equal to three for  $\lambda = 0$ , which is the only eigenvalue of the system. As a result, the descriptor system is observable.

## f) Note that

$$\mathscr{R}_r = \left[ \begin{array}{cc} B_r & A_r B_r \end{array} \right] = \left[ \begin{array}{cc} -1 & 2 \\ 1 & 2 \end{array} \right].$$

As a result,  $\det \mathcal{R}_r \neq 0$  and the reduced system is controllable. Controllability of the reduced system means that for any initial condition  $x_1(0)$  and  $x_2(0)$  there exists and interval [0,T] and an input signal, defined in this interval, such that

$$x_1(t) = 0$$
  $x_2(t) = 0$   $u(t) = 0$ 

for all  $t \ge T$ . Note now that  $x_3(t)$  is such that, by what established in part a),  $x_3(t) = x_1(t) + u(t)$ , hence  $x_3(t) = 0$ , for all  $t \ge T$ , which implies controllability of the descriptor system. [4 marks]

Consider a nonlinear, continuous-time, system described by the equations 4.

$$\dot{x} = f(x) = \begin{bmatrix} x_2^2 \\ x_3^2 \\ 0 \end{bmatrix},$$

with  $x(t) = [x_1(t), x_2(t), x_3(t)]' \in \mathbb{R}^3$ .

The equilibrium points are the solutions of the equations a)

$$x_2^2 = 0, \qquad x_3^2 = 0.$$

Hence, all points described by  $\bar{x} = (\bar{x}_1, 0, 0)$ , with  $\bar{x}_1$  any real number, are equi-[2 marks] libria of the system.

The linearization of the system around each of the equilibrium point is given by b)

$$\dot{\delta}_x = A \delta_x = \left[ \begin{array}{ccc} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{array} \right].$$

[4 marks]

- The characteristic polynomial of the matrix A is  $\det(\lambda I A) = \lambda^3$ . All eigenc) values are at zero, and have geometric multiplicity one. Hence the linearized [2 marks] system is stable (non-asymptotically).
- d) A direct integration yields

$$x_3(t) = x_3(0),$$
  $x_2(t) = x_2(0) + x_3^2(0)t$ 

ration yields 
$$x_3(t) = x_3(0), x_2(t) = x_2(0) + x_3^2(0)t,$$
 
$$x_1(t) = x_1(0) + x_2^2(0)t + x_2(0)x_3^2(0)t^2 + \frac{1}{3}x_3^4(0)t^3.$$

Note that trajectories move away from the equilibria and become unbounded, hence the equilibria are unstable. [6 marks]

Note that e)

$$y = x_1,$$
  $\dot{y} = x_2^2,$   $\ddot{y} = 2x_2x_3^2,$   $\ddot{y} = 2x_3^4,$   $\ddot{y} = 0,$ 

as claimed. Using  $x_1 = y$ ,  $x_2 = \dot{y}$ ,  $x_3 = \ddot{y}$  and  $x_4 = \ddot{y}$  as state variables yields

$$\dot{x}_1 = x_2, \qquad \dot{x}_2 = x_3, \qquad \dot{x}_3 = x_4, \qquad \dot{x}_4 = 0,$$

or, equivalently,

$$\dot{x}_e = A_e x_e = \begin{bmatrix} 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 \end{bmatrix} x_e, \qquad y_e = C_e x_e = \begin{bmatrix} 1 & 0 & 0 & 0 \end{bmatrix} x_e.$$

[6 marks]