

Paper Number(s): E1.3 ✓

IMPERIAL COLLEGE OF SCIENCE, TECHNOLOGY AND MEDICINE
UNIVERSITY OF LONDON

DEPARTMENT OF ELECTRICAL AND ELECTRONIC ENGINEERING
EXAMINATIONS 2001

EEE PART I: M.Eng., B.Eng. and ACGI

DEVICES AND FIELDS

Friday, 15 June 10:00 am

There are FIVE questions on this paper.

There are two sections. Answer THREE questions including at least ONE question from each section.

Use a separate answer book for each section.

Time allowed: 2:00 hours

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Examiners: Wright, S.W., Cozens, J.R., Leaver, K.D.
and Green, T.C.

Formulae and Constants

For Silicon at 300K:

$$N_C, N_V = 2 \times 10^{25} \text{ m}^{-3}$$

$$\mu_e = 1300 \text{ cm}^2 \text{ V}^{-1} \text{ sec}^{-1}$$

$$n_i = 1.45 \times 10^{16} \text{ m}^{-3}$$

$$\mu_h = 500 \text{ cm}^2 \text{ V}^{-1} \text{ sec}^{-1}$$

For Silicon Dioxide: $\epsilon_{ox} = 4 \times \epsilon_0$

$$\epsilon_0 = 8.85 \times 10^{-12} \text{ F m}^{-1}$$

$$e = 1.6 \times 10^{-19} \text{ C} \quad k = 1.38 \times 10^{-23} \text{ JK}^{-1}$$

$$f(E) = \frac{1}{1 + \exp\left(\frac{E - E_F}{kT}\right)}$$

$$I_D = \frac{WC_{ox}\mu}{L} \left(V_{GS} - V_T - \frac{V_{DS}}{2} \right) V_{DS} \quad (V_{GS} - V_T) > V_{DS} > 0$$

$$C_{ox} = \frac{\epsilon_0 \epsilon_{ox}}{t_{ox}}$$

$$n = N_C f(E)$$

$$n \times p = n_i^2$$

$$\frac{D}{\mu} = \frac{kT}{e}$$

SECTION A

Use a separate answer book for each section

1. A silicon p-n junction diode has an acceptor doping density of 10^{24} m^{-3} and a donor doping density of 10^{22} m^{-3} .
 - i Calculate the concentrations of electrons and holes at 300K in both the p and n type regions, far away from the junction. [4]
 - ii Sketch an energy level diagram for this diode when unbiased, labelling the Fermi level and the conduction and valence bands. [3]
 - iii Give a labelled sketch of the distributions of minority carriers in the diode when it is (a) forward biased and (b) reverse biased, assuming that it behaves as a short diode. [4]
 - iv What is the significance of the word 'short' in the description of this diode? [2]
 - v From your diagram, deduce an expression for the reverse saturation current density of this diode, and evaluate it given that the n- and p- regions each have a length of $120 \mu\text{m}$. [5]
 - vi What would be the value of the reverse saturation current density if the acceptor doping density is reduced by a factor of 10^3 ? [2]

2. Figure 1 shows the dependence of drain current on gate-source voltage for a particular silicon MOSFET measured using a source-drain voltage V_{DS} of 0.1V

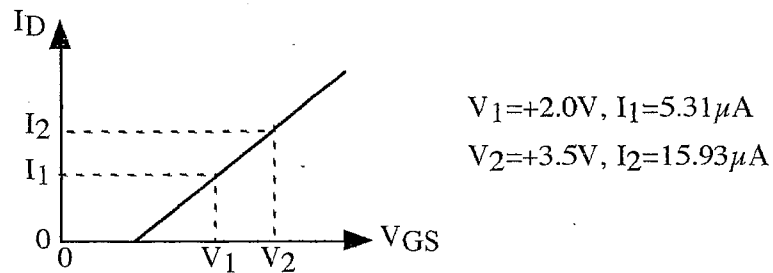


Figure 1 Drain current vs Gate-source voltage characteristic of a MOSFET

- i What type of MOSFET is this the characteristic of? [2]
 - ii What is meant by the threshold voltage? [2]
 - iii Calculate the values of the threshold voltage and transconductance for this MOSFET. [6]
 - iv If the device dimensions have the following values, calculate the mobility of the current carriers in the MOSFET - channel length= $1\mu\text{m}$, channel width= $2\mu\text{m}$, insulator thickness= 50nm . [6]
 - v Why is the value of mobility lower than that which would be measured in a sample of bulk silicon? [2]
 - vi What would be the dependence of I_D on V_{GS} in the saturation region of operation? [2]
- 3.
- i Sketch the form of the Fermi-Dirac distribution function for $T=0\text{K}$ and $T>0\text{K}$, showing the position of the Fermi energy, and the value of the function at that energy. [4]
 - ii State briefly the physical meaning of the Fermi-Dirac distribution function [2]
 - iii Calculate the differences in energy at 300K between the conduction band and Fermi level for n-type and p-type silicon, doped in each case with 10^{23}m^{-3} doping atoms. [6]
 - iv Sketch the small-signal equivalent circuit of a bipolar transistor, labelling each component in the equivalent circuit. [4]
 - v Explain briefly how the design of a bipolar transistor can be optimised to increase the current gain [4]

SECTION B

Use a separate answer book for each section

4. State Gauss' Law in electrostatics. [4]

- a) A parallel plate capacitor with plates of area A and separation d , has a block of dielectric, of relative permittivity ϵ , of cross-sectional area A , and thickness t ($t < d$), inserted between the plates.

Find the values of the electric field strength E , and the electric flux density D , in both the air and the dielectric.

[4]

Show that the capacitance of the capacitor is given by

$$C = A\epsilon\epsilon_0 / [\epsilon d - (\epsilon - 1)t] . \quad [6]$$

- b) The values of the vertical potential gradient at heights of 100 and 1000 metres above the earth's surface are 110 and 25 V/metre respectively. What is the mean electrostatic charge per cubic metre of the atmosphere between these heights? [6]
($\epsilon_0 = 8.85 \times 10^{-12}$ F/m)

5. State Ampere's Law in magnetostatics.

[4]

An electromagnet is held close to a piece of iron, of mass m , which is lying freely on a wooden surface, as shown in figure 2(a).

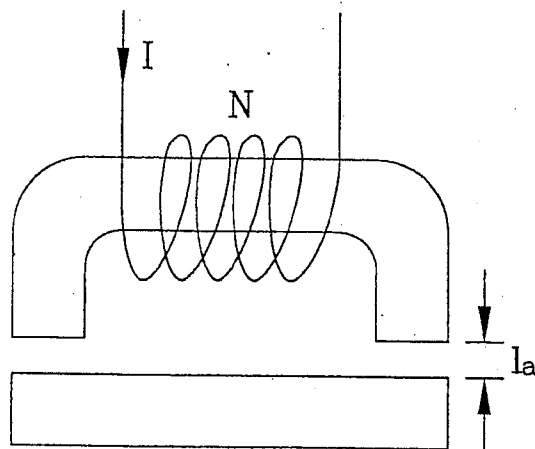


Figure 2(a)

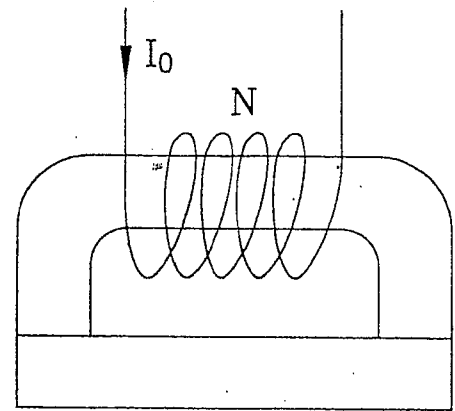


Figure 2(b)

Deduce an expression for the magnetic flux in the iron when a current of I amps flows through the coil, and also for the inductance of the coil. [4,2]

By considering the energy stored in an inductor, or otherwise, deduce an expression for the force pulling the iron piece towards the electromagnet. [4]

Given that the relevant parameters are as follows;

Total path length in iron	=	1m
Each air gap	=	5 mm.
Cross Sectional area	=	25 cm^2
Number of turns	=	100
Mass of iron piece	=	2 kg
Relative permeability of iron	=	10^4
μ_0	=	$4\pi 10^{-7} \text{ F/m}$
g	=	9.81 m/s^2

calculate a value for the minimum current, I_0 , required to lift the iron from the surface. [4]

If the iron is brought into contact with the electromagnet, as shown in figure 2(b), and the current I_0 is maintained, what is the minimum force required to separate the iron from the magnet? [2]

Q1

(i)

n side

$$n = N_D = 10^{22} \text{ m}^{-3}$$

$$P_n = \frac{n_c^2}{n_n} = \frac{(1.45 \times 10^{16})^2}{10^{22}} = 2.025 \times 10^{10} \text{ m}^{-3}$$

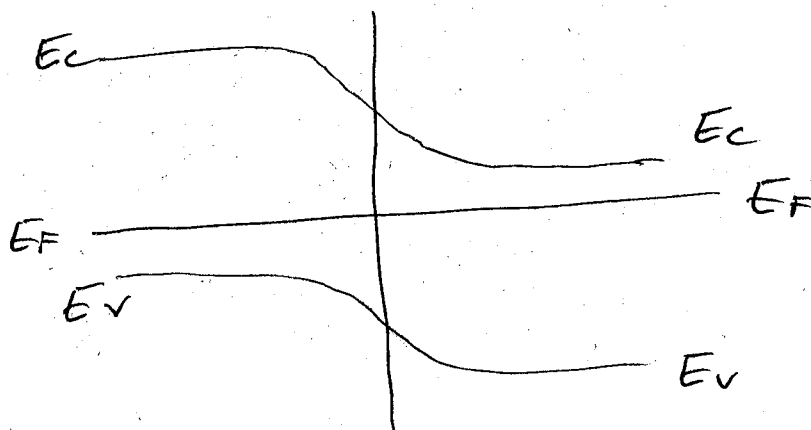
[4]

p side

$$P_p = N_A = 10^{24} \text{ m}^{-3}$$

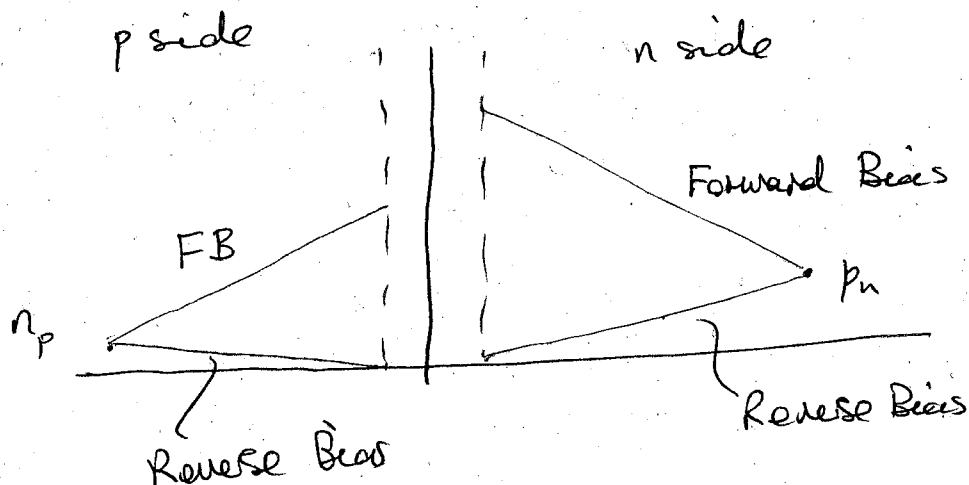
$$n_p = \frac{n_c^2}{P_p} = \frac{(1.45 \times 10^{16})^2}{10^{24}} = 2.025 \times 10^8 \text{ m}^{-3}$$

(ii)



[3]

(iii)



[4]

- (iv) A "short" diode - ~~no recombination~~
recombination of minority carriers can
be neglected [2]

Minority carrier distributions in (iii) above
are then linear

(v) $J_s = e \left(\frac{D_e n_p}{L_p} + \frac{D_h p_n}{L_n} \right)$ [2]

$$\begin{aligned} \frac{D}{\mu} &= \frac{kT}{e} \text{ so } J_s = kT \left(\frac{\mu_e n_p}{L_p} + \frac{\mu_h p_n}{L_n} \right) \\ &= 1.38 \times 10^{-23} \times 300 \left(\frac{0.13 \times 2.025 \times 10^8}{120 \times 10^{-6}} + \frac{0.05 \times 2.025 \times 10^{10}}{120 \times 10^{-6}} \right) \\ &= 4.14 \times 10^{-21} (2.19 \times 10^{11} + 8.44 \times 10^{12}) \\ &= \underline{3.58 \times 10^{-8} \text{ A m}^{-2}} \quad [3] \end{aligned}$$

- (vi) If N_A and hence p_p reduced by 10^3

n_p becomes $2.025 \times 10^{11} \text{ m}^{-3}$

so thus first term in above increased by $\times 10^3$ [2]

$$\begin{aligned} \text{so } J_{sc} &= 4.14 \times 10^{-21} (2.19 \times 10^{14} + 8.44 \times 10^{12}) \\ &= \underline{9.42 \times 10^{-7} \text{ A m}^{-2}} \end{aligned}$$

Q2 (i) This is an n-channel,
enhancement mode MOSFET [2]

(ii) Threshold voltage: the gate-source voltage
which is needed to cause formation of a
conducting channel between source & drain [2]

OR The gate-source voltage which inverts the
surface of the silicon

(iii) $I_D = K (V_{GS} - V_T)^2$ if $V_{DS} \ll (V_{GS} - V_T)$

so $\frac{I_{D2}}{I_{D1}} = \frac{V_{GS2} - V_T}{V_{GS1} - V_T}$ so $\frac{15.93}{5.31} = 3 = \frac{3.5 - V_T}{2 - V_T}$ [3]

so $3(2 - V_T) = (3.5 - V_T)$

$V_T = 1.25V$

$g_m = \frac{dI}{dV_{GS}} = \frac{I_2 - I_1}{V_2 - V_1} = \frac{10.62}{1.5} = \underline{7.08 \mu A/Volts}$ [3]

Q2 cont'd

$$(iv) \quad I_D = \frac{W}{L} \mu_e C_{ox} (V_{GS} - V_T) V_{DS} \quad \text{since } V_{DS} \ll (V_{GS} - V_T)$$

$$\text{Where } C_{ox} = \frac{\epsilon_0 \epsilon_{ox}}{t_{ox}} = \frac{4 \times 8.85 \times 10^{-12}}{50 \times 10^{-9}} = 7.08 \times 10^{-4} \text{ F m}^{-2}$$

$$g_m = \frac{dI}{dV_{GS}} = \frac{W}{L} C_{ox} \mu V_{DS} \quad [6]$$

$$\begin{aligned} \text{So } \mu &= \frac{g_m}{\frac{W}{L} C_{ox} V_{DS}} = \frac{7.08 \times 10^{-6}}{2 \times 7.08 \times 10^{-4} \times 0.1} \\ &= 0.05 \text{ m}^2/\text{Vsec} \end{aligned}$$

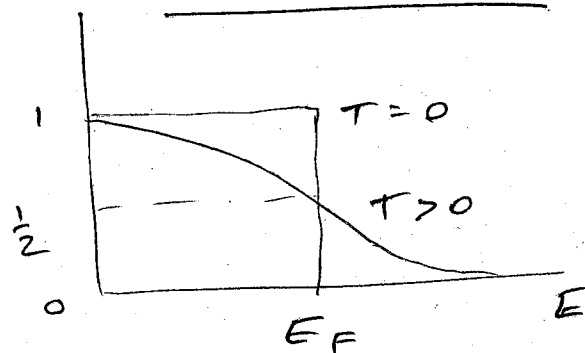
(v) This is lower than bulk mobility value because of surface scattering of electrons [2]

(vi) In the saturation region [2]

$$I_D \propto (V_{GS} - V_T)^2$$

(20)

Q3 (1)



[4]

(ii) F-D function - the value at energy E is the probability of a state at energy E being occupied by an electron. [2]

(iii) n-type $n = N_c f(E_c) \approx N_c e^{-\frac{(E_c - E_F)}{kT}}$

so $E_c - E_F = \frac{kT}{e} \ln\left(\frac{N_c}{n}\right)$

and $n = N_D = 10^{23} \text{ m}^{-3}$

[2]

so $E_c - E_F = \frac{kT}{e} \ln\left(\frac{N_c}{10^{23}}\right) = 0.138 \text{ eV}$

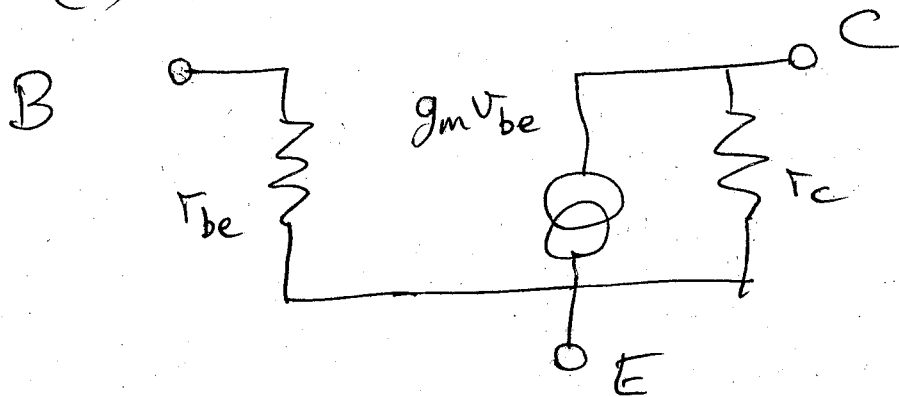
p-type $n = N_c \exp\left(-\frac{(E_c - E_F)}{kT}\right)$

and $n = \frac{n_i^2}{p} = \frac{n_i^2}{N_A} = \frac{(1.45 \times 10^{16})^2}{10^{23}}$

$= 2.025 \times 10^9 \text{ m}^{-3}$ [2]

so $E_c - E_F = \frac{kT}{e} \ln\left[\frac{2 \times 10^{25}}{(2.025 \times 10^9)}\right] = 0.957 \text{ eV}$ [2]

Q3 (iv)



[4]

(v) To improve gain of bipolar transistor

(a) Make base narrow - reduces I_B by reducing minority carrier recombination

increases I_C because steeper concentration gradient in base [4]

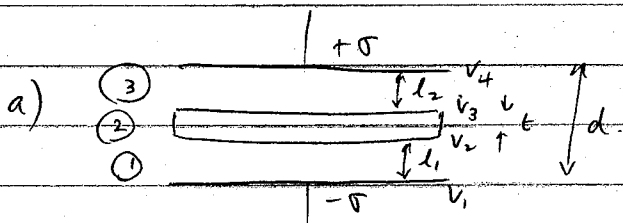
(b) Heavily doped emitter - reduce carrier injection from base to emitter.

(20)

Section BAnswers

$$4. \oint \underline{D} \cdot d\underline{s} = q \quad [4]$$

(closed surface) (net charge within closed surface)



From symmetry, lines of electric flux density are normal to the plates; and continuous between them.

∴ In all regions, $D = \sigma$ (charge/unit area).

In regions 1 & 3, $E = \frac{D}{\epsilon_0} = \frac{\sigma}{\epsilon_0}$

& in region 2, $E = \frac{D}{\epsilon_0 \epsilon} = \frac{\sigma}{\epsilon_0 \epsilon} \quad [4]$

In all regions, $E = -\frac{dV}{dx}$

∴ in ① $V_2 - V_1 = \left(\frac{\sigma}{\epsilon_0}\right) l_1$

in ② $V_3 - V_2 = \left(\frac{\sigma}{\epsilon_0 \epsilon}\right) t$

in ③ $V_4 - V_3 = \left(\frac{\sigma}{\epsilon_0}\right) l_2$

Volt drop across whole capacitor = $V_4 - V_1$
 $= \frac{\sigma}{\epsilon_0} \left[l_1 + l_2 + \frac{t}{\epsilon} \right]$

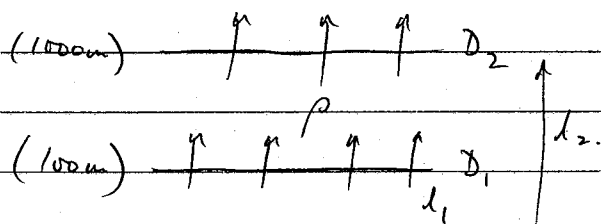
Charge on plates = $\sigma A = Q$

(PTD)

$$\therefore V = Q \cdot \frac{1}{\epsilon_0 A} \left[(d_1 + d_2) + \frac{t}{\epsilon} \right] = \frac{Q}{\epsilon_0 A} \left[(d-t) + \frac{t}{\epsilon} \right]$$

$$\therefore C = \frac{\epsilon_0 A}{\left[(d-t) + \frac{t}{\epsilon} \right]} = \frac{\epsilon_0 \epsilon A}{(\epsilon d - (\epsilon - 1)t)} \quad [6]$$

b) Since heights \ll earth's radius, earth is flat!



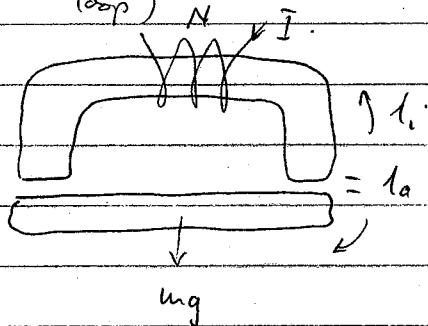
$$\text{Net flux density/unit area} = D_1 - D_2 = \rho (l_2 - l_1)$$

$$\therefore \rho = \frac{\epsilon_0 (E_1 - E_2)}{(l_2 - l_1)} = \frac{8.85 \cdot 10^{-12} (110 - 25)}{(1000 - 100)}$$

$$\rho = \underline{0.836 \text{ pCm}^{-3}} \quad [6]$$

$$5. \quad \oint H \cdot d\mathbf{l} = NI \quad [4]$$

(closed loop) (within loop).



$$\mu_r = 10^4$$

$$A = 25 \cdot 10^{-4} \text{ m}^2$$

$$m = 2 \text{ kg}$$

$$N = 10^2$$

From Ampere's Law,

$$H_i l_i + 2 H_a l_a = NI$$

$$H = \frac{B}{\mu} = \frac{\Phi}{\mu A}$$

$$\therefore \frac{\Phi}{\mu_r A} \left[\frac{l_i}{\mu_r} + 2 l_a \right] = NI$$

$$\Phi = \frac{\mu_0 A N I}{\left[\frac{l_i}{\mu_r} + 2 l_a \right]}$$

$$3.11 \times 10^{-5}$$

$$= \frac{4\pi \cdot 10^{-7} \cdot 25 \cdot 10^{-4} \cdot 10^2 I}{[10^{-4} + 10^{-2}]} = \underline{\underline{3.14 \cdot 10^{-5} I \text{ Wb}}} \quad [4]$$

$$L = \frac{N\Phi}{I} = \underline{\underline{3.14 \text{ mH}}} \quad 3.11 \text{ mH}$$

[2]

$$\text{Energy in inductor} = \frac{1}{2} LI^2$$

$$\text{and } F = - \frac{dE}{dl_a}$$

$$\therefore F = - \left\{ \frac{I_0^2}{2} \mu_0 A N^2 \right\} \left\{ \frac{-2}{\left(\frac{l_i}{\mu_r} + 2 l_a \right)^2} \right\} = mg \quad [4]$$

$$\therefore I_0^2 = \frac{mg \left(\frac{l_i}{\mu_r} + 2 l_a \right)^2}{\mu_0 A N^2} \quad \therefore \underline{\underline{I_0 = 7.9 \text{ A}}} \quad [4]$$

7.98

E1.3

When air gap is zero,

$$F = \frac{I_o^2 \mu_o AN^2}{(\frac{L_i}{\mu_r})^2} = \frac{7.9^2 \cdot 4\pi \cdot 10^{-7} \cdot 25 \cdot 10^{-4} \cdot 10^4}{10^{-8}}$$

$$F = 1.96 \cdot 10^5 N$$

[2]

$$2.00 \times 10^5 N$$