IMPERIAL COLLEGE LONDON

DEPARTMENT OF ELECTRICAL AND ELECTRONIC ENGINEERING **EXAMINATIONS 2016**

EEE PART II: MEng, BEng and ACGI

POWER ENGINEERING

Corrected Copy

Wednesday, 1 June 2:00 pm

Time allowed: 2:00 hours

There are THREE questions on this paper.

Answer ALL questions.

Q1 carries 40% of the marks. Questions 2 and 3 carry equal marks (30% each).

Any special instructions for invigilators and information for candidates are on page 1.

Examiners responsible

First Marker(s):

T.C. Green

Second Marker(s): B. Chaudhuri

Information for Candidates

Switch-Mode Power Supplies

Voltage ratio equations for buck SMPS

$$\frac{V_o}{V_i} = \delta \qquad \text{or} \qquad \frac{V_o}{V_t} = \frac{1}{1 + \frac{2fLI_o}{V_t \delta^2}}$$

$$\frac{V_o}{V_i} = \frac{1}{1 - \delta} \quad \text{or} \quad \frac{\frac{V_o}{V_i}}{V_i} = \frac{1}{1 - \frac{V_i \delta^2}{2fLI_i}}$$

Voltage ratio equations for boost SMPS

Three-Phase Systems

Line Voltages and Current

$$V_L = \sqrt{3} \, V_P \quad I_L = I_P$$

Delta
$$V_L = V_P$$
 $I_L = \sqrt{3} I_P$

$$P_{3\Phi} = 3 V_P I_P \cos(\phi)$$
Power
$$= \sqrt{3} V_L I_L \cos(\phi)$$

Induction Machines

$$\omega_{S} = \frac{\omega_{E}}{P} \quad S = \frac{\omega_{S} - \omega_{R}}{\omega_{S}} \qquad T_{cm} = \frac{3 I_{R}^{'2} R_{R}^{'}}{\omega_{R}} \left(\frac{1 - s}{s}\right)$$

Photovoltaic Systems

$$I_{PV} = I_{Ph} - I_{AK} - I_{Sh}$$
 $I_{AK} = I_0 \left[e^{\frac{V_{PV} + I_{PV}R_S}{K_I v_T}} - 1 \right]$

Power Flow in Lines and Cables

Cable Parameters

$$R'_{IF} = \frac{1}{\sigma_c \pi r_c^2} + \frac{1}{\sigma_c 2\pi r_o t_o} L' = \frac{\mu_o}{2\pi} \ln \begin{pmatrix} r_o \\ r_c \end{pmatrix} \qquad C' = \frac{2\pi \varepsilon_o \varepsilon_{RI}}{\ln \begin{pmatrix} r_o \\ r_c \end{pmatrix}} \quad G' = \frac{2\pi \sigma_I}{\ln \begin{pmatrix} r_o \\ r_c \end{pmatrix}}$$

OHL Parameters (approximate form)

$$R^{\prime}_{LF} = \frac{2}{\sigma_{c}\pi r_{c}^{2}} \quad L^{\prime} = \frac{\mu_{0}}{\pi} \ln\left(\frac{d}{r_{c}}\right) \quad C^{\prime} = \frac{\pi \varepsilon_{0} \varepsilon_{RI}}{\ln\left(\frac{d}{r_{c}}\right)} \quad G^{\prime} = \frac{\pi \sigma_{t}}{\ln\left(\frac{d}{r_{c}}\right)}$$

Power Flow (full form)

$$P_{S} = \frac{V_{S}^{2}}{Z_{SD}} \cos(\theta) - \frac{V_{S} V_{R}}{Z_{SD}} \cos(\theta + \delta)$$

$$Q_S = \frac{V_S^2}{Z_{SR}} \sin(\theta) - \frac{V_S V_R}{Z_{SR}} \sin(\theta + \delta)$$

Voltage Drop (approximate form)

$$\Delta V = |V_S| - |V_R| \approx \frac{RP_S + XQ_S}{|V_S|}$$

- 1. This question covers several topics and all parts should be attempted.
- a) Consider a national-scale electricity system based on AC.
 - i) Describe the principal difference between the transmission and distribution networks and explain why transmission networks use higher voltages than distribution networks.

[6]

ii) Most countries of the world operate their electricity networks at a nominal frequency of 50 or 60 Hz, however, in practice the frequency is not strictly constant. Explain why the frequency varies a little around its nominal value.

[4]

- b) Consider power transfer in AC networks.
 - i) A single-phase cable operated at 50 Hz and 120 kV has a capacitance per unit length of 0.25 μ F/km. Calculate the capacitive charging current for a 75 km length of cable.

[2]

ii) A single-phase overhead line has a series impedance which is purely reactive with a value of 18 Ω and is operated at a voltage of 400 kV. Calculate the phase angle that would exist between sending and receiving end voltages when transferring 1,000 MW.

[4]

iii) A three-phase load is composed of impedances of $10 + j2 \Omega$ connected in star. It is connected to a supply with a line voltage of 400 V. Calculate the real and reactive power drawn.

[4]

- Compare buck and boost switch mode power supplies (SMPSs) through the following steps.
 - For a fixed input voltage, sketch the shape of the output voltage as a function of the duty-cycle of the switch (assuming continuous conduction) for each SMPS.

[3]

- ii) Sketch the shape of the currents as a function of time for the currents that flow in the inductor, diode and capacitor for each type of SMPS.
- [5]
- iii) For similar magnitudes of output current and the same choice of capacitor, compare the amplitudes of output voltage ripple.

[2]

- d) Consider a typical photovoltaic panel.
 - i) Describe the operating principle of a photovoltaic cell and the role of the band-gap energy in determining the efficiency of the cell.

[5]

ii) A PV cell was tested at 25°C. It produced a short-circuit current of 0.8 A under an irradiance of 250 W/m². The reverse saturation current of the cell was measured as $I_0 = 1 \times 10^{-10}$ A. You may assume that the cell has a very small series resistance, a very large shunt resistance and an ideality factor of 1. Boltzmann's constant is $k = 1.380 \times 10^{-23}$ J/K and the electronic charge is $q = 1.602 \times 10^{-19}$ C. Calculate the open-circuit voltage at irradiances of 250 and 1.000 W/m².

[5]

[4]

2.

A buck switch-mode power supply, SMPS, is to be designed to provide a 5 V output voltage from a 24 V input. The output current will be in the range 0.1 A to 2.0 A and it is intended that the SMPS operates in continuous conduction mode across this range. It has been decided to design for a switching frequency of 150 kHz.

A suitable MOSFET has been identified for the SMPS with the following properties:

On resistance $R_{DS(on)} = 0.25 \Omega$

Turn-on loss $E_{on} = 13 \,\mu\text{J}$ when switched on at 2.0 A

Turn-off loss $E_{off} = 7 \mu J$ when switched off at 2.0 A

The diode to be used has an on-state voltage of 1.0 V.

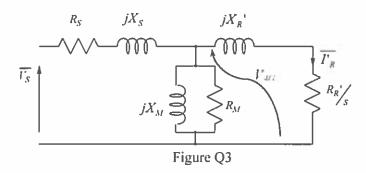
[2] Calculate the duty-cycle at which the switch will operate. i) Calculate the power losses in the semiconductors and the efficiency (ignoring other ii) [8] losses) when operating at maximum output power. Choose an inductor to ensure continuous conduction. [4] iii) Choose a capacitor to ensure that the output voltage ripple is less than 40 mV. You iv) may work on the basis that 80% of the ripple will arise from the effective series resistance of the capacitor (ESR) and 20% from the capacitance. [6] Calculate the switching frequency that would be needed to improve the efficiency to v) [6] 80%. What design changes would be needed (trends rather than numerical values are vi)

sufficient) as a consequence of the change of frequency determined in Part (v)?

3.

A 2 pole-pair, 3-phase induction machine is star-connected and supplied at 50 Hz. The equivalent circuit of the machine is shown in Figure Q3 for which the parameters, referred to the stator, are:

stator resistance	0.04 Ω,
stator leakage reactance	0.4 Ω,
referred rotor resistance	0.055 Ω,
referred rotor leakage reactance	0.4 Ω,
magnetising resistance	20 Ω,
magnetising reactance	8 Ω.



The machine is rated to develop a torque of 500 Nm at a slip of 0.03. Calculate the following for operation at rated torque:

the rotor speed in rad/s [2] i) the mechanical output power ii) [3] iii) the referred rotor current required to develop this power [5] iv) the voltage appearing across the rotor branch (denoted V_{AG} in the equivalent circuit) in the magnitude and angle form [5] the magnetising current and stator current (in any convenient form) [5] vi) the magnitude of the required stator voltage [5] vii) the efficiency at the rated torque [5]

