

1. a. i.

$$F(\omega) = \int_{-\infty}^{\infty} f(t) e^{-j\omega t} dt$$

$$= \int_{-b}^b a e^{-j\omega t} dt$$

$$= a \int_{-b}^b e^{-j\omega t} dt$$

$$= a \cdot \frac{1}{-j\omega} \cdot \frac{e^{-j\omega b} - e^{j\omega b}}{2}$$

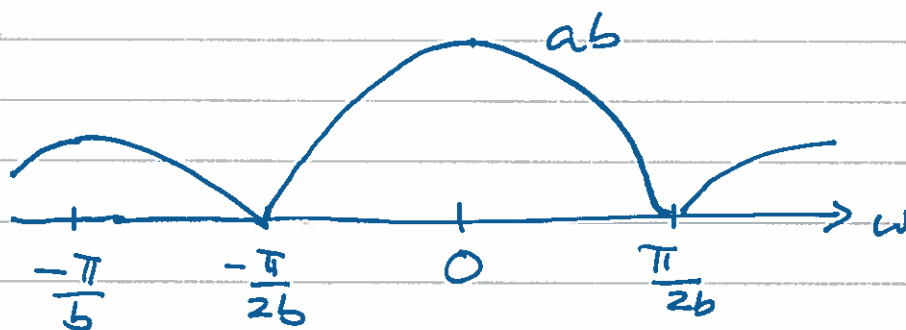
$$= a \cdot \frac{1}{-j\omega} \cdot \frac{-2j \sin(\omega b)}{2}$$

$$\Rightarrow F(\omega) = \frac{a \sin(\omega b)}{\omega}$$

$$F(\omega) = ab \cdot \text{sinc}(\omega b)$$

(4)

ii)



(3)

phase $\angle F(\omega) = 0$ because $F(\omega)$ is real

1. a. iii.

$$f(t) = \lim_{b \rightarrow 0} \begin{array}{c} \text{rectangle from } -b \text{ to } b \text{ with height } \frac{1}{2b} \end{array}$$

(2)

$$\Rightarrow f(t) = \delta(t) \quad \because \text{the area is unit and the width tends to zero}$$

In this special case

$$F(\omega) = \mathcal{F}[\delta(t)] = 1.$$

iv.

$$\mathcal{F}[f(t-t_0)]$$

$$= \int_{-\infty}^{\infty} f(t-t_0) e^{-j\omega t} dt$$

$$= \int_{-\infty}^{\infty} f(t-t_0) e^{-j\omega(t-t_0)} \cdot e^{-j\omega t_0} dt$$

$$= e^{-j\omega t_0} \int_{-\infty}^{\infty} f(t-t_0) e^{-j\omega(t-t_0)} dt$$

$$= e^{-j\omega t_0} \cdot F(\omega)$$

$$\Rightarrow \hat{F}(\omega) = e^{-j\omega t_0} F(\omega)$$

(3)

1. b. i.

$$\omega_0 = \frac{2\pi}{T_0}$$

①

ii. a_0 is the dc component of the signal $g(t)$.

①

iii. a_n reflects the degree of how $g(t)$ is similar to $\cos(n\omega_0 t)$

b_n : similarity w/ $\sin(n\omega_0 t)$

②

iv. If $g(t)$ is odd function of t ,

$$g(-t) = -g(t)$$

So,

$$g(t) = a_0 + \sum_{n=1}^{\infty} a_n \cos(n\omega_0 t) + \sum_{n=1}^{\infty} b_n \sin(-n\omega_0 t)$$

$$= a_0 + \sum_{n=1}^{\infty} a_n \cos(n\omega_0 t) - \sum_{n=1}^{\infty} b_n \sin(n\omega_0 t)$$

Since $g(-t) = -g(t)$

$$\Rightarrow a_0 + \sum_{n=1}^{\infty} a_n \cos(n\omega_0 t) - \sum_{n=1}^{\infty} b_n \sin(n\omega_0 t)$$

$$= -a_0 - \sum_{n=1}^{\infty} a_n \cos(n\omega_0 t) - \sum_{n=1}^{\infty} b_n \sin(n\omega_0 t)$$

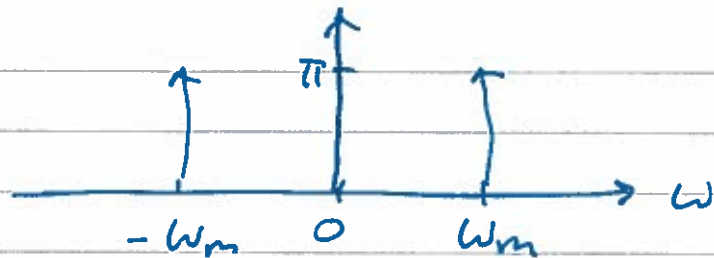
$$\Rightarrow a_0 + \sum_{n=1}^{\infty} a_n \cos(n\omega_0 t) = 0$$

③

$$\Rightarrow a_0 = 0, a_n = 0 \quad \forall \text{ all } n=1, 2, \dots, \infty$$

③

1. c. i.



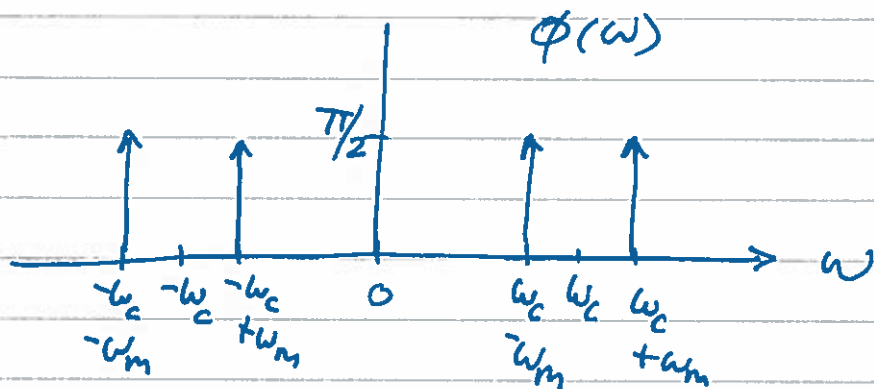
(2)

ii. $\phi(t) = m(t) \cos(\omega_c t)$

$$= \cos(\omega_m t) \cdot \cos(\omega_c t)$$

$$= \frac{1}{2} \left[\cos(\omega_c - \omega_m)t + \cos(\omega_c + \omega_m)t \right]$$

iii.



(2)

iv. The AM effectively shifts the ^{spectrum of} $m(t)$ to the frequency range surrounding the carrier frequency $\pm \omega_c$.

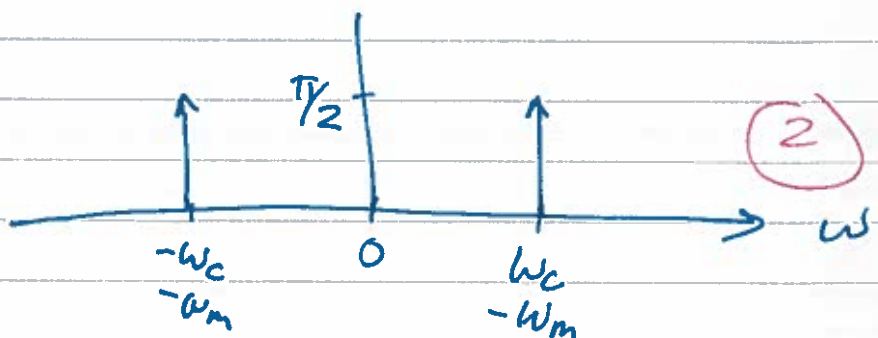
(1)

v.

$$P_{USB}(t) = \frac{1}{2} \cos(\omega_c - \omega_m)t$$

(2)

vi.



(2)

(4)

1. d. i. $\phi(t) = A \cos(\omega_c t + k_f \int m(\alpha) d\alpha)$

(2)

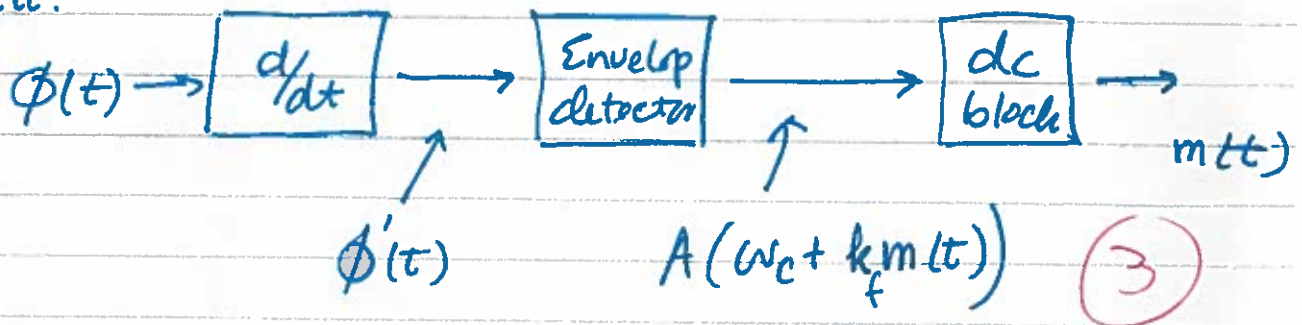
ii. $\phi'(t) = d\phi(t)/dt$

$= A [\omega_c + k_f m(t)]$

(2)

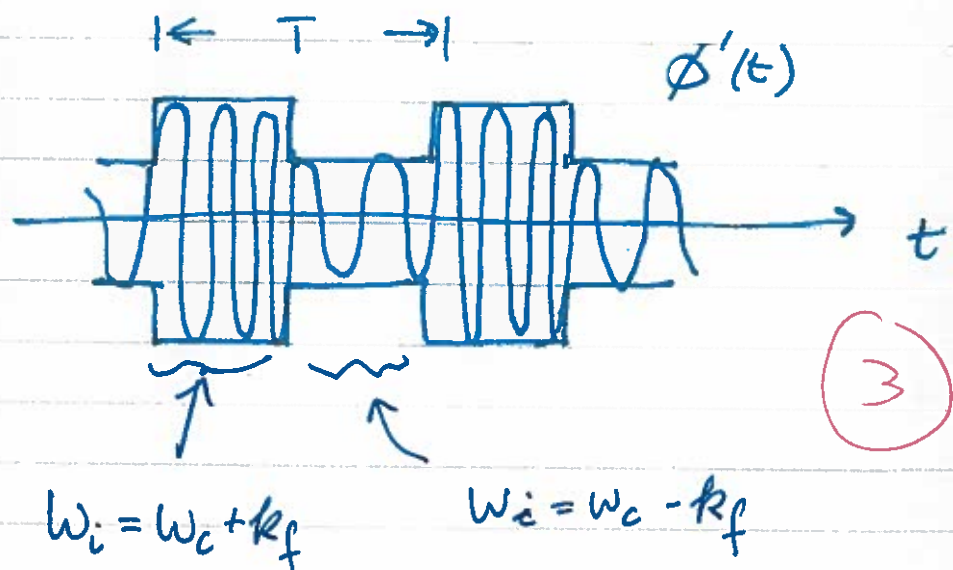
$\sin[\omega_c t + k_f \int m(\alpha) d\alpha]$

iii.



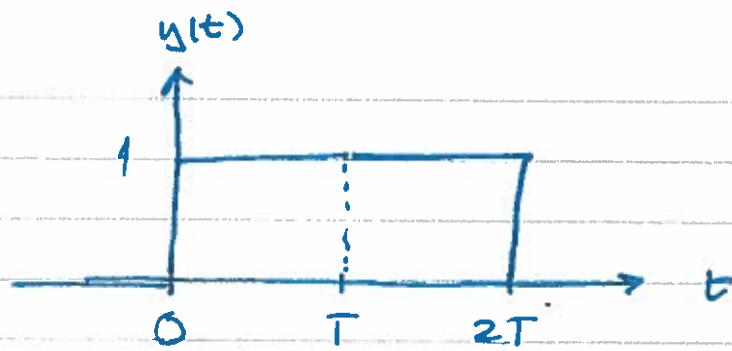
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iv.



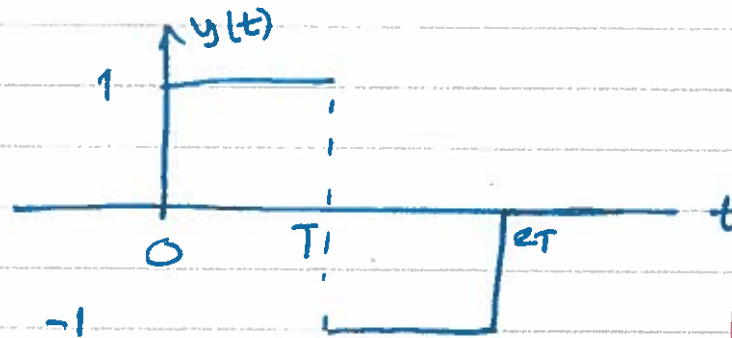
(3)

2. a i.



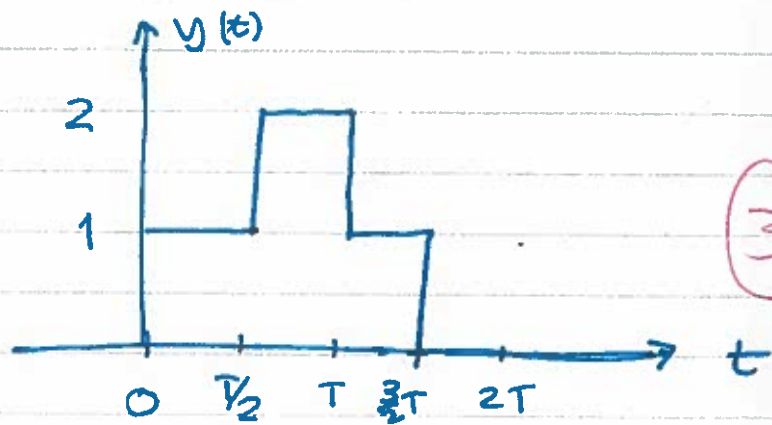
(3)

ii.



(3)

iii.



(3)

iv. maximum signal rate :

$$f = 1/T$$

(6)

It is so because each impulse (signal) has a response time (duration) of T time units (sec). To avoid use of complicated technique for receiving, keep the signal rate of $1/T$ samples per sec will be supported by the channel.

2. b. i. $f(t) * g(t)$

$$= \int_{u=-\infty}^{\infty} f(u) g(t-u) du$$

(3)

ii. $\mathcal{F}[f(t) * g(t)]$

$$= \int_{t=-\infty}^{\infty} \int_{u=-\infty}^{\infty} f(u) g(t-u) e^{-j\omega t} du dt$$

$$= \int_{u=-\infty}^{\infty} \int_{t=-\infty}^{\infty} f(u) g(t-u) e^{-j\omega t} dt du$$

$$= \int_{u=-\infty}^{\infty} \int_{t=-\infty}^{\infty} f(u) g(t-u) e^{-j\omega(t-u)} \cdot e^{-j\omega u} dt du$$

$$= \int_{u=-\infty}^{\infty} f(u) e^{-j\omega u} \int_{t=-\infty}^{\infty} g(t-u) e^{-j\omega(t-u)} dt du$$

$$= \int_{u=-\infty}^{\infty} f(u) e^{-j\omega u} \cdot \int_{t'=-\infty}^{\infty} g(t') e^{-j\omega t'} dt' du$$

where $t' = t - u$

$$= \int_{u=-\infty}^{\infty} f(u) e^{-j\omega u} G(\omega) du$$

$$= G(\omega) \cdot F(\omega)$$

(5)

2. b. iii. $F(\omega) * G(\omega)$

$$= \int_{u=-\infty}^{\infty} F(u) G(\omega - u) du$$

(2)

iv. $\mathcal{F}[f(t)g(t)]$

$$= \int_{t=-\infty}^{\infty} f(t) g(t) e^{-j\omega t} dt$$

$$= \int_{t=-\infty}^{\infty} \frac{1}{2\pi} \int_{u=-\infty}^{\infty} F(u) e^{jut} du g(t) e^{-j\omega t} dt$$

$$= \frac{1}{2\pi} \int_{t=-\infty}^{\infty} \int_{u=-\infty}^{\infty} F(u) g(t) e^{-j(\omega - u)t} du dt$$

$$= \frac{1}{2\pi} \int_{u=-\infty}^{\infty} F(u) \int_{t=-\infty}^{\infty} g(t) e^{-j(\omega - u)t} dt du$$

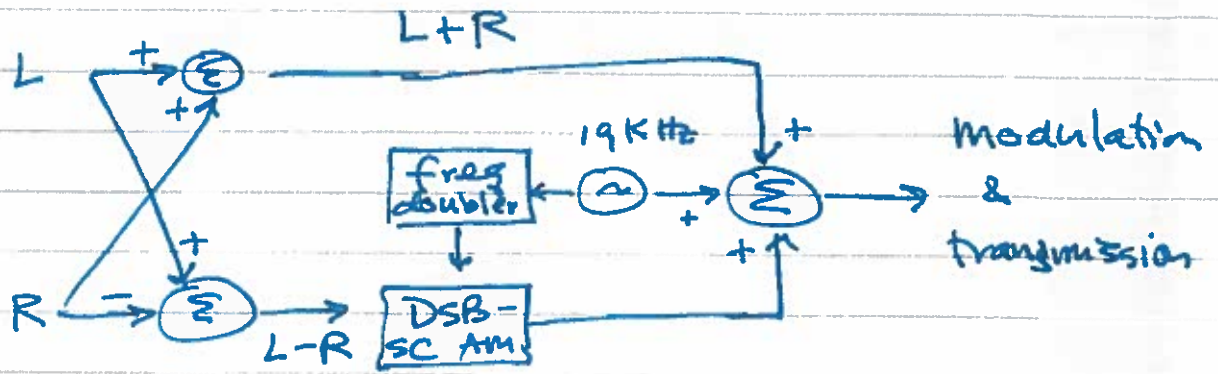
$$= \frac{1}{2\pi} \int_{u=-\infty}^{\infty} F(u) \cdot G(\omega - u) du$$

$$= \frac{1}{2\pi} F(\omega) * G(\omega) \quad \text{as result in part iii. shows}$$

(5)

(8)

3.9. i.



Form signals : $L+R$ and $L-R$.

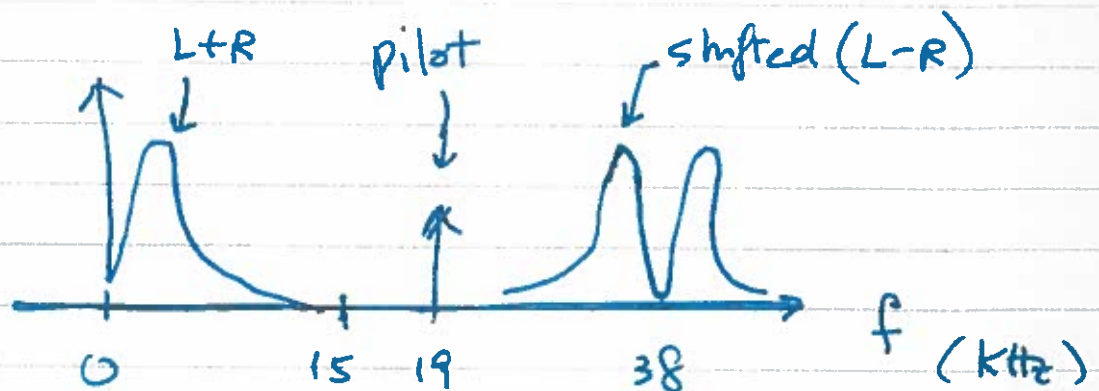
Use & double the pilot signal of 19 KHz.

Form DSB-SC signal for $L-R$ signal using the 38 KHz carrier.

Transmit the composite base band signal of

$L+R + 19 \text{ KHz} + \text{DSB-SC of } L-R \text{ signal at } 38 \text{ KHz carrier}$

ii.



4

9

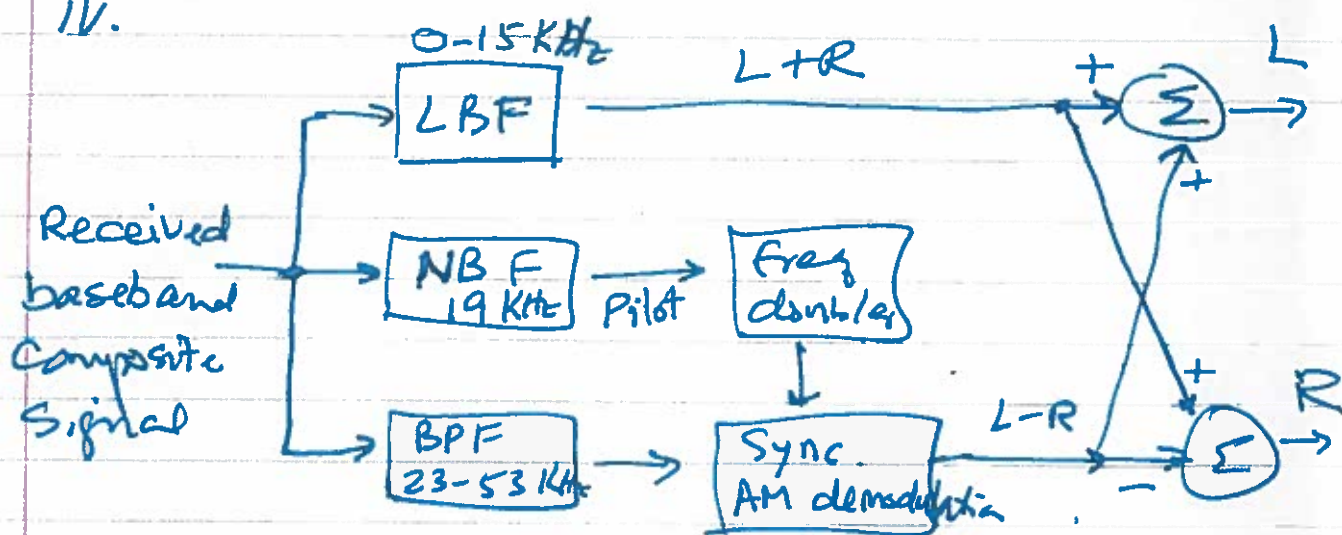
3.9. iii. The frequency of the pilot signal of 19 KHz is doubled.

Then, the 38 KHz is multiple with the L-R signal to form the DSB-SC (AM) signal at carrier frequency of 38 KHz.

The frequency multiplication is equivalent to shift the L-R signal to the carrier frequency of 38 KHz.

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iv.



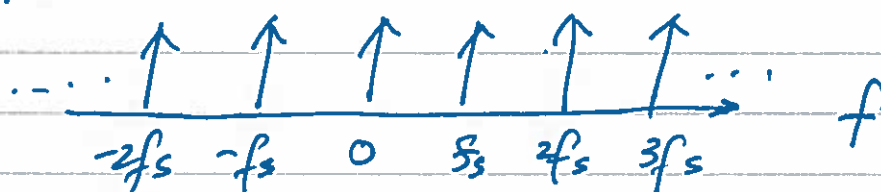
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3. b. i. Due to Nyquist Sampling Criterion:

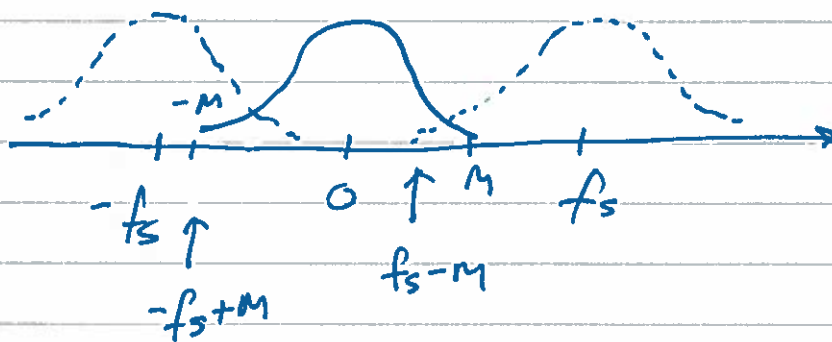
$$f_s \geq 2 \times \text{Bandwidth of } m(t)$$

$$\text{So, } M = f_s/2$$

This is so because the periodic samples are equal to multiplying a train of impulses with the signal $m(t)$. The train of impulses has a spectrum of



As a result of sampling, the samples of $m(t)$ have the following frequency spectrum:



From the above diagram, in order to recover $m(t)$, we require

$f_s - M \geq M$ to avoid overlap of replica of the original signal spectrum

$$\Rightarrow f_s \geq 2M$$

6

3. b. ii. Clearly, $C \geq M$

because the channel bandwidth must be wider than the signal bandwidth in order to avoid loss of information. (2)

iii. Since $M = f_s/2$,

we have $C \geq f_s/2$

i.e., $f_s \leq 2C$ (2)

iv.
$$R = 2C \log_2 M$$

$$= 2C \log_2 4$$

$$\Rightarrow R = 4C \text{ bits/sec} \quad (2)$$