

IMPERIAL COLLEGE LONDON

DEPARTMENT OF ELECTRICAL AND ELECTRONIC ENGINEERING  
EXAMINATIONS 2015

MSc and EEE/EIE PART IV: MEng and ACGI

**DISCRETE-TIME SYSTEMS AND COMPUTER CONTROL**

Tuesday, 12 May 10:00 am

Time allowed: 3:00 hours

Corrected Copy

**There are FOUR questions on this paper.**

**Answer ALL questions.**

*All questions carry equal marks*

**Any special instructions for invigilators and information for candidates are on page 1.**

Examiners responsible      First Marker(s) :      T. Parisini  
Second Marker(s) :      E.C. Kerrigan



## DISCRETE-TIME SYSTEMS AND COMPUTER CONTROL

Information for candidates:

In the following,  $\delta(k)$  denotes the discrete-time unit impulse sequence,  $u(t)$  denotes the continuous-time unit step function, and  $T$  denotes the sampling time.

- $\mathcal{Z}[\delta(k)] = 1$
- $\mathcal{Z}[u(t)] = \mathcal{Z}\left[\mathcal{L}^{-1}\left(\frac{1}{s}\right)\right] = \frac{z}{z-1} = \frac{1}{1-z^{-1}}$
- $\mathcal{Z}[e^{-at} \cdot u(t)] = \mathcal{Z}\left[\mathcal{L}^{-1}\left(\frac{1}{s+a}\right)\right] = \frac{z}{z-e^{-aT}} = \frac{1}{1-z^{-1}e^{-aT}}$
- $\mathcal{Z}[t \cdot u(t)] = \mathcal{Z}\left[\mathcal{L}^{-1}\left(\frac{1}{s^2}\right)\right] = T \frac{z}{(z-1)^2} = T \frac{z^{-1}}{(1-z^{-1})^2}$
- $\mathcal{Z}[te^{-at} \cdot u(t)] = \mathcal{Z}\left[\mathcal{L}^{-1}\left(\frac{1}{(s+a)^2}\right)\right] = Te^{-aT} \frac{z}{(z-e^{-aT})^2} = Te^{-aT} \frac{z^{-1}}{(1-e^{-aT}z^{-1})^2}$
- Transfer function of the ZOH:  $H_0(s) = \frac{1-e^{-sT}}{s}$
- Expression of a second-order polynomial with complex-conjugate roots in terms of the damping ratio  $\xi$  and the natural angular frequency  $\omega_n$ :  $s^2 + 2\xi\omega_n s + \omega_n^2$ .
- Note that, for a given signal  $r$ , or  $r(t)$ ,  $R(z)$  denotes its  $\mathcal{Z}$ -transform.

1. Consider the impulse-sampled schemes depicted in Fig. 1.1 and 1.2 below with sampling-time  $T$ :

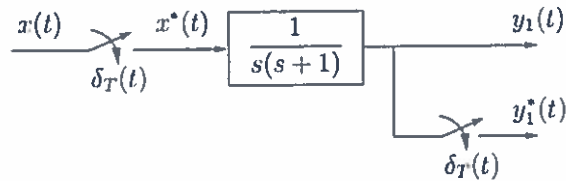


Figure 1.1

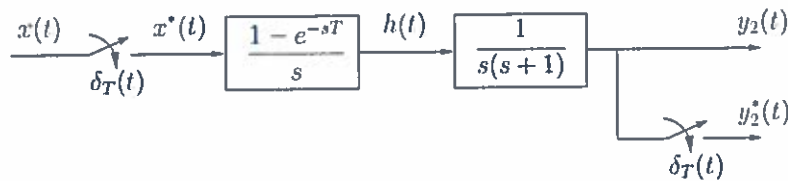


Figure 1.2

where  $x(t) = e^{-t} \cdot u(t)$ , with  $u(t)$  denoting the unit step-function, and  $\delta_T(t) = \sum_{k=0}^{\infty} \delta(t - kT)$ , where  $\delta(t)$  is the Dirac impulse function. In Fig. 1.2, the input  $h(t)$  to the block with transfer function  $G(s) = \frac{1}{s(s+1)}$  is generated by a ZOH with transfer function  $\frac{1 - e^{-sT}}{s}$ .

- With reference to Fig. 1.1, determine the closed-form expression of the discrete-time sequence  $y_1(kT)$ ,  $k = 0, 1, \dots$ .  
[ 8 marks ]
- With reference to Fig. 1.2, determine the closed-form expression of the discrete-time sequence  $y_2(kT)$ ,  $k = 0, 1, \dots$ .  
[ 8 marks ]
- Set  $T = 1$  sec and plot the first 5 samples of  $y_1(kT)$  and  $y_2(kT)$ , that is,  $y_1(kT)$ ,  $k = 0, 1, \dots, 4$  and  $y_2(kT)$ ,  $k = 0, 1, \dots, 4$ . Compare the two discrete-time sequences and comment on your findings.  
[ 4 marks ]

2. Consider the discrete-time dynamic system described by the block scheme depicted in Fig. 2.1:

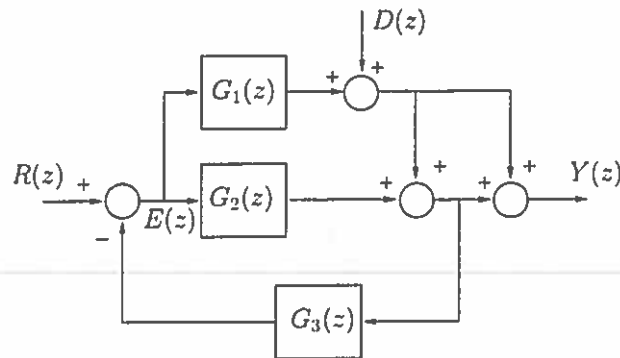


Figure 2.1 Block scheme of a discrete-time system.

where the discrete-time transfer functions  $G_1(z)$ ,  $G_2(z)$ ,  $G_3(z)$  are given by

$$G_1(z) = \frac{z-1}{3z+2}; \quad G_2(z) = \frac{K}{z}, \text{ with } K \in \mathfrak{R}; \quad G_3(z) = \frac{z}{z-1},$$

and where  $R(z)$ ,  $E(z)$ ,  $D(z)$ ,  $Y(z)$  denote the  $\mathcal{Z}$  transforms of the discrete-time variables  $r(k)$ ,  $e(k)$ ,  $d(k)$ ,  $y(k)$ , respectively.

- a) Determine the transfer function  $H_{ry}(z)$  from the input  $r(k)$  to the output  $y(k)$ , that is,  $H_{ry}(z) = \frac{Y(z)}{R(z)}$ .

[ 5 marks ]

- b) Determine the transfer function  $H_{dy}(z)$  from the input  $d(k)$  to the output  $y(k)$ , that is,  $H_{dy}(z) = \frac{Y(z)}{D(z)}$ .

[ 5 marks ]

- c) Determine all values of  $K \in \mathfrak{R}$  (if any) such that the overall discrete-time dynamic system shown in Fig. 2.1 is asymptotically stable.

[ 5 marks ]

- d) Letting  $K = 1$ ,  $r(k) = 0, \forall k \geq 0$ , and  $d(k) = \delta(k)$  (where  $\delta(k)$  is the discrete-time unit impulse function), determine the closed-form expression of the output sequence  $y(k)$ ,  $\forall k \geq 0$ .

[ 5 marks ]

3. Consider the digital system shown in Figure 3.1:

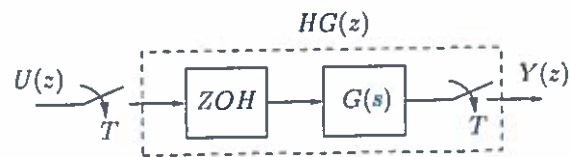


Figure 3.1

where  $T$  is the sampling time, “ZOH” stands for “zero-order hold”, and  $HG(z)$  denotes the equivalent discrete-time model for the plant  $G(s) = \frac{1/2}{(s^2 + 1/4)(s^2 + 9/4)}$  connected to the ZOH and the sampler, where  $H(s) = \frac{1 - e^{-sT}}{s}$  denotes the transfer function of the ZOH.

- a) Determine the poles of  $G(s)$  and discuss the stability of the continuous-time system described by  $G(s)$ .

[ 3 marks ]

- b) For the generic sampling time  $T$ , determine  $HG(z)$ .

[ 8 marks ]

- c) Set  $T = \pi$  sec and compute  $HG(z)$  for this specific choice of  $T$ . Moreover, the choice  $T = \pi$  sec, which is possible in theory, is not implementable in exact way in a practical digital control system. Discuss why.

[ 3 marks ]

- d) Provide a justification for the fact that the number of poles of the equivalent discrete-time model  $HG(z)$  determined in your answer to Question 3c) is lower than the number of poles of the continuous-time transfer function  $G(s)$ .

[ 6 marks ]

4. Consider the antenna tracking a satellite depicted in Fig. 4.1(a) and the block diagram of the continuous-time tracking control system shown in Fig. 4.1(b):

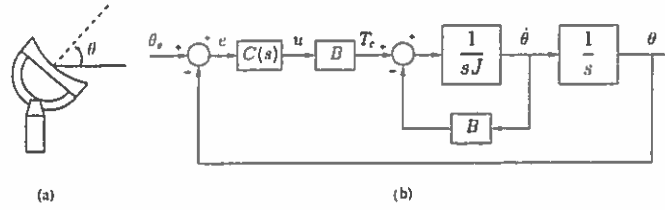


Figure 4.1

where  $\theta$  denotes the pointing angle,  $T_c$  denotes the net torque from the drive,  $J$  the inertia moment of the antenna and  $B$  the friction coefficient.

- a) Setting  $J/B = 10$ , determine the open-loop transfer function  $G(s)$  from the input  $u(t)$  to the output  $\theta(t)$ , that is,  $G(s) = \Theta(s)/U(s)$ , where  $\Theta(s)$  and  $U(s)$  denote the Laplace transforms of  $\theta(t)$  and  $u(t)$ , respectively.

[ 3 marks ]

- b) Consider a reference angle  $\theta_s(t) = 0.01 \cdot t$ ,  $t \geq 0$  to be tracked. Determine the parameters  $K \in \mathbb{R}, K > 0$  and  $a \in \mathbb{R}, a > 0$  of a tracking controller  $C(s) = K \cdot (1 + 10s)/(1 + as)$  such that the closed-loop system is asymptotically stable,  $\lim_{t \rightarrow \infty} |e(t)| \leq 1/100$ , and  $\xi \geq 0.5$  and  $\omega_n \simeq 1 \text{ rad/sec}$ , where  $\xi$  is the damping ratio and  $\omega_n$  is the natural angular frequency of the closed-loop poles.

[ 5 marks ]

- c) Consider the digital control system shown in Figure 4.2:

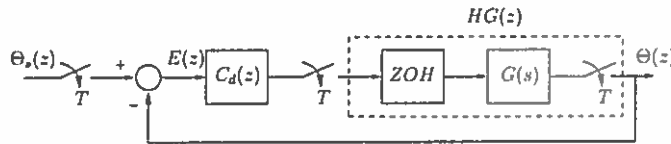


Figure 4.2

where  $G(s)$  is the transfer function obtained in your answer to Question 4a) and  $HG(z)$  denotes the equivalent discrete-time model for the plant  $G(s)$  connected to the ZOH and the sampler.  $H(s) = (1 - e^{-sT})/s$  is the transfer function of the ZOH. Setting  $T = 0.2 \text{ sec}$ , compute the "pole-zero correspondence" discrete-time approximation  $C_d(z)$  of the controller  $C(s)$  obtained in your answer to Question 4b) and compute  $HG(z)$ .

[ 6 marks ]

- d) Determine the closed-loop transfer function  $G_{cl}(z) = \Theta(z)/\Theta_s(z)$  and check whether the digital closed-loop control system is asymptotically stable. Compute the corresponding poles in the  $s$ -plane and determine the associated damping-ratio  $\xi$  and natural angular frequency  $\tilde{\omega}_n$ . Compare  $\xi$  and  $\tilde{\omega}_n$  with  $\xi$  and  $\omega_n$  determined in your answer to Question 4b). Comment on your findings.

[ 6 marks ]

