

MSc and EEE PART IV: MEng and ACGI

Corrected copy

Time allowed: 3:00 hours

There are SIX questions on this paper.

Answer FOUR questions.

All questions carry equal marks

Any special instructions for invigilators and information for candidates are on page 1.

Examiners responsible

First Marker(s) :	S. Lucyszyn
Second Marker(s) :	A.S. Holmes

Special instructions for invigilators

This is a closed book examination.

Special instructions for students

None.

The Questions

1. An RF signal of 1 mW is input to a power amplifier with an output of 1 W. Design a suitable power amplifier to give the best overall performance using the following transistor stages.

$P_{OUT MAXLIN}$ [dBm]	P_{DC} [mW]	IP_3 [dBm]
25	600	40
30	2000	40
15	60	40

Table 1.1 Transistor Specifications.

(Note that all the transistors have perfect impedance matching)

[2]

- a) From the design, calculate the following at each stage and the overall values for:
- i) Power gain [1]
 - ii) Output power [2]
 - iii) Basic efficiency [2]
 - iv) PAE [2]
 - v) IP_3 [2]
 - vi) IMD_3 for two-tone power level given in (ii) [2]
 - vii) Dissipated power [2]
- b) From first principles, prove that the 3rd order intermodulation log-power gain slope is three times that of the desired output log-power slope. [2]
- c) In linear operation, if the overall input power drops by 3 dB, what happens to the following:
- i) Output power [1]
 - ii) I_3 power [1]
 - iii) IMD_3 [1]

2. a) Describe, with the aid of a diagram, a branch-line coupler having a distributed-element implementation, indicating lengths and impedances. Indicate its main characteristics. [5]
- b) Replace the distributed-element implementation in 2(a) with an equivalent lumped-element version. How does the performance compare with that in 2(a)? With a coupler having an impedance of $Z_0 = 50 \, \Omega$, calculate the components values for an operating frequency of 1.8 GHz. [5]
- c) Replace the lumped-element implementation in 2(b) with an equivalent lumped-distributed version. With a coupler having an impedance of $Z_0 = 50 \, \Omega$ and line sections of $\phi = 45^\circ$, calculate the components values for an operating frequency of 1.8 GHz. [5]
- d) Draw the topology of a balanced amplifier employing the coupler given in 2(a). [5]

3.

- a) Compare and contrast lumped-element impedance matching over the use of distributed-elements, in terms of frequency performance. How does this affect their role in DC biasing networks?
[4]
- b) With lumped-element impedance matching, what terminating impedance conditions are best suited for L-match, π -match and T-match networks.
[4]
- c) A 2 GHz narrow-band amplifier has an output impedance of $(5 - j7) \Omega$ and must be matched to a system impedance of 50Ω . Design simple matching circuits to achieve maximum power transfer:
 - i) With the use of one lumped-element component and one distributed-element component
[4]
 - ii) With the use of two lumped-element components
[4]
- d) With monolithic technology, discuss the difficulties implementing lumped-element and distributed-element components. How can micromachining technologies help to overcome some of the problems with monolithic implementations? How does this affect their role in filter networks?
[4]

4.

- a) Explain why filters having sharp frequency roll-off characteristics require large components to achieve low insertion losses. [4]
- b) Explain why impedance and admittance inverters are required for realising practical narrow bandwidth filters. In addition, with the use of simple block diagrams, explain how these inverters work. [6]
- c) Redesign the 1.8 GHz resonator topology shown in Figure 4.1, by employing all capacitor admittance inverters, so that the series tuned circuit can be replaced with a shunt parallel tuned circuit. [8]

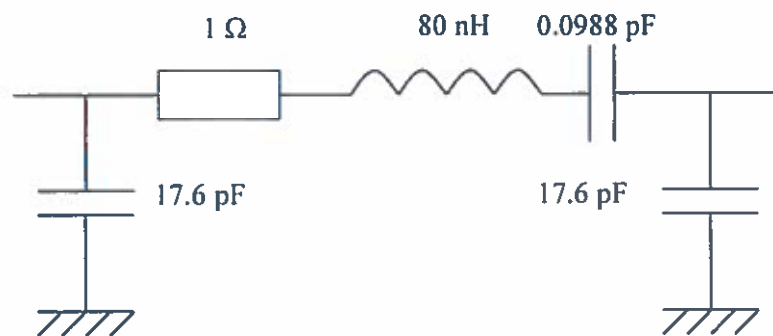


Figure 4.1: Lumped-element resonator.

- d) What effect on the insertion phase does the all capacitor admittance inverter have? [2]

5.

- (a) Given a square wave signal generator, with a clock frequency that can vary between DC and 1000 MHz, propose how this could be used to generate a sinusoidal signal at a frequency of 1800 MHz.

[4]

- (b) Design a lumped-element L - C high-pass filter to meet the following specifications:

Pass band attenuation ripple	0.1 dB
-3 dB cut-off frequency:	1500 MHz
Stop band frequency:	600 MHz
Stop band attenuation:	> 70 dB
Source impedance, Z_s :	50 Ω
Load impedance, Z_L :	50 Ω

[10]

- (c) Determine the worst-case levels of return losses within both the pass band and the stop band for the filter in 5(b). How could the stop band return loss adversely affect the implementation of 5(a) and suggest a suitable topology for overcoming this problem?

[6]

6.

- a) With the aid of a diagram, describe the S-parameter representation of a linear two-port circuit, stating the precise definitions of all parameters and the main power specifications.

[5]

- b) State which RF components best described the following S-parameter matrices and calculate any relevant power specifications:

$$(i) \quad [S] = \begin{pmatrix} 0 & e^{-j720} \\ e^{-j720} & 0 \end{pmatrix} \quad (6.1)$$

$$(ii) \quad [S] = \begin{pmatrix} 0 & 0.07e^{-j30} \\ e^{-j60} & 0 \end{pmatrix} \quad (6.2)$$

$$(iii) \quad [S] = \begin{pmatrix} 0.1e^{-j30} & 0.3e^{-j80} \\ 9.7e^{-j80} & 0.15e^{-j60} \end{pmatrix} \quad (6.2)$$

[5]

- c) Derive an algebraic expression for the overall Γ_{in} of a linear two-port network that is terminated at its output port with a one-port network represented by Γ_L .

[6]

- d) Referring to the result in 6(c), state the condition for stability for the overall one-port network, for any value of generator source impedance. If the two-port network in 6(b)(ii) is terminated with a load impedance having $\Gamma_L = 0.5$, determine if the overall one-port network is stable.

[4]

Figure 1 is a line graph showing the relationship between Attenuation (dB) on the y-axis and Frequency Ratio (f/f_0) on the x-axis. The y-axis ranges from 0 to 120 dB in increments of 12. The x-axis ranges from 1.0 to 10.0 in increments of 0.5. There are seven lines plotted, each corresponding to a different value of n (2, 3, 4, 5, 6, 7). All lines originate from the point (1.0, 0). The lines are labeled with their respective n values. The line for $n=2$ is the least steep, while the line for $n=7$ is the steepest.

Frequency Ratio (f/f_0)	$n=2$ (dB)	$n=3$ (dB)	$n=4$ (dB)	$n=5$ (dB)	$n=6$ (dB)	$n=7$ (dB)
1.0	0	0	0	0	0	0
2.0	12	20	28	36	44	52
3.0	18	30	42	54	66	78
4.0	24	40	56	72	84	96
5.0	30	50	72	90	102	114
6.0	36	60	84	108	120	-
7.0	42	70	96	120	-	-
8.0	48	80	108	-	-	-
9.0	54	90	120	-	-	-
10.0	60	100	-	-	-	-

A graph showing Attenuation (dB) on the y-axis (0 to 120) versus Frequency Ratio (f/f_0) on the x-axis (1.0 to 10). The graph contains several curves labeled 1 through 6, representing different Q values. Curve 1 is the flattest, while curve 6 is the steepest. A label $Q = 2$ is placed near curve 2.

A line graph showing the relationship between Attenuation (dB) on the y-axis and Frequency Ratio (f/f_1) on the x-axis. The y-axis is inverted, with 0 at the top and 120 at the bottom. The x-axis ranges from 1.0 to 10.0. There are seven curves labeled $n = 2, 3, 4, 5, 6, 7, 8$. All curves start at (1.0, 0) and increase in attenuation as the frequency ratio increases. The curve for $n = 2$ is the least steep, while the curve for $n = 8$ is the steepest.

Frequency Ratio (f/f_1)	$n=2$ (dB)	$n=3$ (dB)	$n=4$ (dB)	$n=5$ (dB)	$n=6$ (dB)	$n=7$ (dB)	$n=8$ (dB)
1.0	0	0	0	0	0	0	0
2.0	12	18	24	30	36	42	48
3.0	18	27	36	45	54	63	72
4.0	24	36	48	60	72	84	96
5.0	30	45	60	75	90	105	120
6.0	36	54	72	90	108	126	-
7.0	42	63	84	105	126	-	-
8.0	48	72	96	120	-	-	-
9.0	54	81	-	-	-	-	-
10.0	60	90	-	-	-	-	-

A graph showing Attenuation (dB) on the y-axis (0 to 120, increasing downwards) versus Frequency Ratio (f/f_g) on the x-axis (1.0 to 10). Several curves are plotted for different values of n :

- $n = 2$: A nearly horizontal line at approximately 12 dB.
- $n = 3$: A line with a shallow slope, reaching about 36 dB at $f/f_g = 10$.
- $n = 4$: A line with a moderate slope, reaching about 48 dB at $f/f_g = 10$.
- $n = 5$: A line with a steeper slope, reaching about 60 dB at $f/f_g = 10$.
- $n = 6$: A line with a steep slope, reaching about 72 dB at $f/f_g = 10$.
- $n = 7$: A line with a very steep slope, reaching about 84 dB at $f/f_g = 10$.
- $n = 8$: A line with a very steep slope, reaching about 96 dB at $f/f_g = 10$.
- $n = 9$: A line with a very steep slope, reaching about 108 dB at $f/f_g = 10$.
- $n = 10$: A line with a very steep slope, reaching about 120 dB at $f/f_g = 10$.

R_g/R_L	C_1	L_2	C_2	L_1
3.000	0.572	3.133		
4.000	0.365	4.600		
8.000	0.157	9.858		
∞	1.313	1.109		
1.000	2.216	1.088	2.216	
0.500	4.431	0.817	2.216	
0.333	6.647	0.759	2.216	
0.250	8.862	0.680	2.216	
0.125	17.725	0.612	2.216	
	1.652	1.460	1.108	
3.000	0.653	4.411	0.814	2.535
4.000	0.452	7.083	0.612	2.848
8.000	0.209	17.164	0.428	3.581
∞	1.350	2.010	1.488	1.106

Table 1: Parameters for $n=5$

n	R_L/R_s	C_1	L_2	C_2	L_3	C_3	L_4	C_4
5	1.000	2.907	1.129	3.103	1.128	2.907		
	0.500	4.414	0.565	4.653	1.128	2.907		
	0.333	6.622	0.376	6.826	1.128	2.907		
	0.250	8.829	0.282	7.750	1.128	2.907		
	0.125	17.657	0.141	13.981	1.128	2.907		
	∞	1.731	1.643	2.081	1.493	1.103		

Table 2: Parameters for $n=6$

n	R_L/R_s	C_1	L_2	C_2	L_3	C_3	L_4	C_4
6	3.000	0.679	3.673	0.771	4.711	0.969	2.406	
	4.000	0.481	5.944	0.476	7.351	0.849	2.532	
	8.000	0.227	12.310	0.198	18.740	0.728	2.800	
	∞	1.378	3.097	1.690	2.074	1.494	1.102	

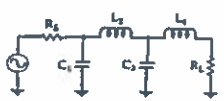
Table 3: Parameters for $n=7$

n	R_L/R_s	C_1	L_2	C_2	L_3	C_3	L_4	C_4
7	1.000	2.904	1.131	3.147	1.194	3.147	1.131	2.904
	0.500	4.406	0.566	4.653	0.965	3.147	1.131	2.904
	0.333	6.612	0.377	6.441	0.798	3.147	1.131	2.904
	0.250	8.815	0.283	7.586	0.706	3.147	1.131	2.904
	0.125	17.631	0.141	13.175	0.671	3.147	1.131	2.904
	∞	1.741	1.677	2.153	1.703	2.079	1.494	1.102

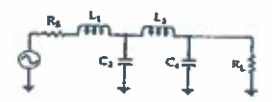
Table 4: Parameters for $n=5$ (continued)

n	R_L/R_s	L_1	C_2	L_2	C_3	L_3	C_4	L_4
5	1.000	1.129	3.103	1.128	2.907			
	0.500	0.565	4.653	1.128	2.907			
	0.333	0.376	6.826	1.128	2.907			
	0.250	0.282	7.750	1.128	2.907			
	0.125	0.141	13.981	1.128	2.907			
	∞	1.643	2.081	1.493	1.103			

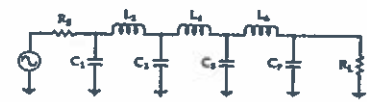
Butterworth Low-Pass
Prototype Element Values



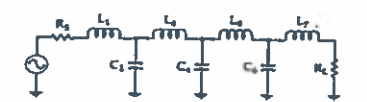
n	R_s/R_L	C_1	L_2	C_2	L_3
2	1.111	1.035	1.835		
	1.250	0.849	2.181		
	1.429	0.697	2.439		
	1.667	0.566	2.638		
	2.000	0.448	3.346		
	2.500	0.342	4.005		
	3.333	0.245	5.313		
	5.000	0.158	7.707		
	10.000	0.074	14.814		
∞		1.414	0.707		
3	0.900	0.808	1.633	1.599	
	0.800	0.844	1.384	1.928	
	0.700	0.915	1.163	2.577	
	0.600	1.023	0.905	3.702	
	0.500	1.181	0.779	5.381	
	0.400	1.425	0.604	8.664	
	0.300	1.838	0.440	15.363	
	0.200	2.690	0.284	29.101	
	0.100	5.187	0.138	55.455	
∞		1.500	1.333	0.500	
4	1.111	0.466	1.582	1.744	1.400
	1.250	0.388	1.095	1.511	1.811
	1.429	0.325	1.062	1.391	2.175
	1.667	0.280	1.103	1.082	3.813
	2.000	0.218	2.438	0.863	5.187
	2.500	0.160	2.896	0.691	8.664
	3.333	0.124	3.863	0.507	15.363
	5.000	0.080	5.884	0.331	29.101
	10.000	0.039	11.064	0.162	55.455
∞		1.531	1.577	1.082	0.583



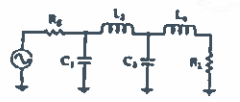
Butterworth Low-Pass Prototype Element Values



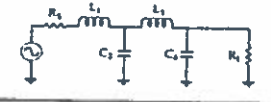
n	R_s/R_L	C_1	L_2	C_2	L_3	C_3	L_4	C_4
5	0.900	0.443	1.027	1.910	1.750	1.380		
	0.800	0.470	0.866	2.061	1.544	1.738		
	0.700	0.517	0.731	2.285	1.333	2.108		
	0.600	0.586	0.609	2.600	1.188	2.582		
	0.500	0.680	0.490	3.051	0.924	3.133		
	0.400	0.838	0.388	3.736	0.727	3.985		
	0.300	1.094	0.285	4.584	0.537	5.307		
	0.200	1.608	0.180	7.183	0.352	7.923		
	0.100	3.513	0.091	14.095	0.173	15.710		
∞		1.545	1.894	1.382	0.894	0.300		
6	1.111	0.389	1.040	1.322	2.054	1.744	1.335	
	1.250	0.345	1.116	1.126	2.339	1.580	1.688	
	1.429	0.307	1.230	0.957	2.490	1.346	2.063	
	1.667	0.273	1.407	0.801	2.858	1.143	2.500	
	2.000	0.211	1.853	0.654	3.369	0.948	3.094	
	2.500	0.141	2.028	0.514	4.141	0.745	3.931	
	3.333	0.082	2.850	0.370	5.433	0.532	5.880	
	5.000	0.054	5.917	0.248	8.020	0.363	7.922	
	10.000	0.026	7.705	0.122	15.788	0.179	15.738	
∞		1.553	1.759	1.553	1.302	0.758	0.250	
7	0.900	0.299	0.711	1.404	1.480	2.125	1.787	1.596
	0.800	0.323	0.808	1.517	1.378	2.334	1.548	1.832
	0.700	0.357	0.915	1.688	1.091	2.818	1.350	2.028
	0.600	0.406	0.438	1.928	0.917	3.005	1.150	2.477
	0.500	0.480	0.354	2.273	0.781	3.353	0.951	3.064
	0.400	0.590	0.278	2.705	0.592	4.380	0.754	3.904
	0.300	0.775	0.206	3.671	0.437	5.781	0.560	5.258
	0.200	1.145	0.135	5.427	0.287	8.529	0.380	7.908
	0.100	2.287	0.067	10.700	0.142	16.822	0.182	15.748
∞		1.558	1.709	1.650	1.307	1.053	0.658	0.223



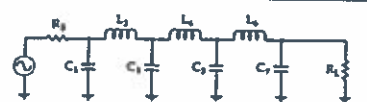
Chebyshev Low-Pass Element Values
for 0.01-dB Ripple



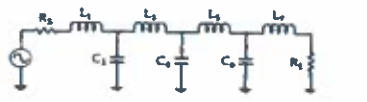
n	R_s/R_L	C_1	L_2	C_2	L_3
2	1.101	1.347	1.483		
	1.111	1.347	1.505		
	1.250	0.943	1.997		
	1.429	0.750	2.344		
	1.667	0.600	2.750		
	2.000	0.479	3.277		
	2.500	0.363	4.033		
	3.333	0.259	5.255		
	5.000	0.164	7.550		
	10.000	0.078	14.749		
∞		1.412	0.742		
3	1.000	1.181	1.821	1.181	
	0.900	1.092	1.680	1.460	
	0.800	1.007	1.443	1.806	
	0.700	1.100	1.228	2.185	
	0.600	1.274	1.024	2.508	
	0.500	1.433	0.829	3.164	
	0.400	1.734	0.645	3.974	
	0.300	2.210	0.470	5.250	
	0.200	3.193	0.305	7.834	
	0.100	8.141	0.148	15.300	
∞		1.501	1.433	0.501	
4	1.100	0.950	1.938	1.761	1.048
	1.111	0.854	1.946	1.744	1.105
	1.250	0.818	2.075	1.542	1.617
	1.429	0.495	2.279	1.334	2.008
	1.667	0.298	2.571	1.128	2.491
	2.000	0.310	2.864	0.820	3.045
	2.500	0.242	3.041	0.729	3.875
	3.333	0.174	4.727	0.538	5.209
	5.000	0.112	6.910	0.352	7.815
	10.000	0.054	13.469	0.173	15.510
∞		1.520	1.601	1.312	0.523



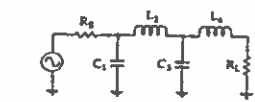
Chebyshev Low-Pass Element Values for 0.01-dB Ripple



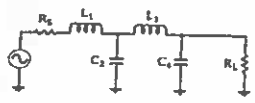
n	R_s/R_L	C_1	L_2	C_2	L_3	C_3	L_4	C_4
5	1.000	0.977	1.885	2.037	1.885	0.977		
	0.900	0.880	1.456	2.174	1.641	1.374		
	0.800	0.877	1.235	2.379	1.499	1.607		
	0.700	0.928	1.040	2.858	1.323	1.977		
	0.600	1.019	0.863	3.041	1.135	2.424		
	0.500	1.168	0.699	3.584	0.942	3.000		
	0.400	1.368	0.544	4.403	0.749	3.845		
	0.300	1.797	0.398	5.772	0.537	5.193		
	0.200	2.604	0.259	8.514	0.368	7.828		
	0.100	5.041	0.127	16.741	0.182	15.813		
∞		1.547	1.785	1.645	1.337	0.488		
6	1.101	0.851	1.706	1.841	2.027	1.831	0.937	
	1.111	0.780	1.782	1.775	2.094	1.838	1.063	
	1.250	0.545	1.864	1.489	2.403	1.507	1.504	
	1.429	0.438	2.038	1.266	2.735	1.332	1.800	
	1.667	0.351	2.298	1.061	3.167	1.145	2.357	
	2.000	0.279	2.878	0.867	3.788	0.954	2.948	
	2.500	0.214	3.281	0.682	4.867	0.761	3.790	
	3.333	0.155	4.245	0.503	6.193	0.568	5.143	
	5.000	0.100	6.223	0.330	9.151	0.378	7.785	
	10.000	0.048	12.171	0.162	18.105	0.187	15.598	
∞		1.551	1.847	1.700	1.596	1.100	0.400	
7	1.000	0.913	1.595	2.002	1.870	2.008	1.595	0.913
	0.900	0.816	1.382	2.080	1.723	2.202	1.581	1.206
	0.800	0.811	1.150	2.382	1.525	2.465	1.464	1.538
	0.700	0.857	0.987	2.516	1.323	2.802	1.307	1.910
	0.600	0.943	0.803	2.878	1.124	3.250	1.131	2.360
	0.500	1.080	0.650	3.382	0.928	3.875	0.947	2.948
	0.400	1.297	0.507	4.156	0.735	4.818	0.758	3.790
	0.300	1.869	0.372	5.454	0.546	6.370	0.568	5.148
	0.200	2.942	0.243	8.057	0.360	9.494	0.378	7.808
	0.100	4.701	0.119	15.878	0.178	18.818	0.188	15.862
∞		1.550	1.867	1.866	1.785	1.563	1.181	0.450



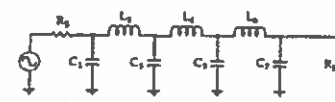
Chebyshev Low-Pass Prototype Element Values for 0.1-dB Ripple



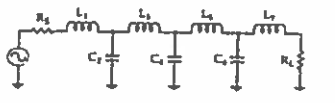
n	R_0/R_L	C_1	L_2	C_2	L_1
2	1.355	1.209	1.838		
	1.429	0.977	1.982		
	1.687	0.733	2.480		
	2.000	0.500	3.054		
	2.500	0.417	3.827		
	3.333	0.283	5.050		
	5.000	0.184	7.428		
	10.000	0.087	14.433		
∞		1.391	0.810		
3	1.000	1.433	1.594	1.433	
	0.900	1.420	1.494	1.622	
	0.800	1.451	1.358	1.871	
	0.700	1.521	1.103	2.190	
	0.600	1.648	1.017	2.603	
	0.500	1.853	0.838	3.139	
	0.400	2.186	0.680	3.968	
	0.300	2.703	0.486	5.279	
	0.200	3.942	0.317	7.850	
	0.100	7.512	0.155	15.468	
∞		1.513	1.510	0.716	
4	1.355	0.902	2.148	1.585	1.341
	1.429	0.779	2.348	1.429	1.700
	1.687	0.578	2.730	1.185	2.243
	2.000	0.440	3.227	0.987	2.850
	2.500	0.329	3.961	0.760	3.698
	3.333	0.233	5.178	0.500	5.030
	5.000	0.148	7.807	0.267	7.414
	10.000	0.070	14.587	0.180	15.230
∞		1.511	1.768	1.455	0.873



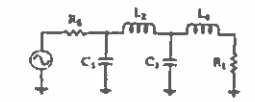
Chebyshev Low-Pass Prototype Element Values for 0.1-dB Ripple



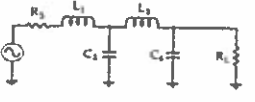
n	R_0/R_L	C_1	L_2	C_2	L_3	C_3	L_4	C_4	L_5	C_5
5	1.000	1.301	1.556	2.941	1.556	1.501				
	0.900	1.285	1.433	2.380	1.488	1.488				
	0.800	1.300	1.282	2.583	1.382	1.738				
	0.700	1.358	1.117	2.868	1.244	2.062				
	0.600	1.470	0.947	3.299	1.085	2.484				
	0.500	1.654	0.778	3.845	0.913	3.085				
	0.400	1.954	0.612	4.780	0.733	3.888				
	0.300	2.477	0.451	6.186	0.580	5.237				
	0.200	3.548	0.295	9.127	0.360	7.890				
	0.100	6.787	0.115	17.657	0.182	15.745				
∞		1.561	1.807	1.700	1.417	0.651				
6	1.355	0.948	2.080	1.659	2.247	1.534	1.277			
	1.429	0.735	2.349	1.454	2.544	1.405	1.629			
	1.687	0.543	2.800	1.183	3.064	1.185	2.174			
	2.000	0.414	3.068	0.958	3.718	0.870	2.704			
	2.500	0.310	3.785	0.749	4.651	0.778	3.645			
	3.333	0.220	4.827	0.551	6.195	0.590	4.906			
	5.000	0.130	7.850	0.301	9.281	0.384	7.618			
	10.000	0.067	14.820	0.178	18.437	0.190	15.350			
∞		1.534	1.884	1.831	1.749	1.394	0.838			
7	1.000	1.282	1.520	2.830	1.680	2.230	1.520	1.282		
	0.900	1.248	1.395	2.381	1.578	2.307	1.450	1.447		
	0.800	1.255	1.245	2.548	1.443	2.624	1.303	1.697		
	0.700	1.310	1.083	2.819	1.283	2.942	1.233	2.081		
	0.600	1.417	0.917	3.205	1.090	3.364	1.081	2.444		
	0.500	1.595	0.753	3.764	0.928	4.015	0.914	3.018		
	0.400	1.885	0.593	4.818	0.742	4.970	0.738	3.653		
	0.300	2.302	0.437	6.054	0.558	6.509	0.567	5.317		
	0.200	3.458	0.288	8.937	0.360	9.770	0.378	7.800		
	0.100	6.570	0.141	17.603	0.184	19.376	0.186	15.813		
∞		1.575	1.858	1.921	1.827	1.734	1.370	0.831		



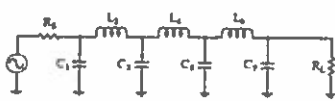
Chebyshev Low-Pass Prototype Element Values for 0.5-dB Ripple



n	R_0/R_L	C_1	L_2	C_2	L_1
2	1.984	0.983	1.930		
	2.000	0.909	2.103		
	2.500	0.504	3.185		
	3.333	0.375	4.411		
	5.000	0.228	6.700		
	10.000	0.105	13.322		
∞		1.307	0.975		
3	1.000	1.864	1.280	1.834	
	0.900	1.818	1.209	2.026	
	0.800	1.997	1.120	2.237	
	0.700	2.114	1.015	2.517	
	0.500	2.557	0.759	3.436	
	0.400	2.985	0.615	4.342	
	0.300	3.729	0.463	5.578	
	0.200	5.254	0.309	8.225	
	0.100	9.890	0.153	16.118	
∞		1.572	1.518	0.932	
4	1.984	0.920	2.588	1.304	1.828
	2.000	0.845	2.720	1.238	1.985
	2.500	0.516	3.768	0.869	3.121
	3.333	0.344	5.120	0.621	4.480
	5.000	0.210	7.708	0.400	6.987
	10.000	0.098	15.333	0.194	14.382
∞		1.436	1.888	1.521	0.913



Chebyshev Low-Pass Prototype Element Values for 0.5-dB Ripple



n	R_0/R_L	C_1	L_2	C_2	L_3	C_3	L_4	C_4	L_5	C_5
5	1.000	1.807	1.303	2.601	1.303	1.807				
	0.900	1.854	1.222	2.849	1.238	1.970				
	0.800	1.928	1.186	3.080	1.187	2.185				
	0.700	2.035	1.015	3.353	1.058	2.470				
	0.600	2.200	0.890	3.785	0.843	2.961				
	0.500	2.457	0.754	4.367	0.610	3.414				
	0.400	2.870	0.608	5.250	0.464	4.345				
	0.300	3.588	0.459	6.871	0.308	5.825				
	0.200	5.064	0.308	10.054	0.243	8.367				
	0.100	9.558	0.153	19.647	0.173	16.574				
∞		1.830	1.740	1.922	1.514	0.903				
6	1.984	0.905	2.577	1.308	2.713	1.299	1.796			
	2.000	0.830	2.704	1.291	2.872	1.237	1.956			
	2.500	0.508	3.722	0.890	4.100	0.881	3.103			
	3.333	0.337	5.055	0.632	5.969	0.635	4.481			
	5.000	0.208	7.615	0.400	8.732	0.412	7.031			
	10.000	0.098	15.186	0.197	17.681	0.202	14.433			
7	1.000	1.790	1.298	2.718	1.285	2.718	1.290	1.790		
	0.900	1.835	1.215	2.860	1.208	2.883	1.234	1.953		
	0.800	1.905	1.118	3.076	1.115	3.107	1.155	2.168		
	0.700	2.011	1.007	3.364	1.025	3.418	1.058	2.458		
	0.600	2.174	0.882	3.772	0.979	3.852	0.944	2.848		
	0.500	2.428	0.747	4.370	0.838	4.470	0.809	3.243		
	0.400	2.835	0.604	5.295	0.685	5.470	0.614	3.605		
	0.300	3.548	0.453	6.897	0.522	7.134	0.513	5.033		
	0.200	5.007	0.303	10.049	0.332	10.498	0.348	8.404		
	0.100	9.458	0.151	19.649	0.178	20.631	0.176	16.863		
∞		1.848	1.777	2.031	1.789	1.924	1.503	0.895		

