

IMPERIAL COLLEGE LONDON

DEPARTMENT OF ELECTRICAL AND ELECTRONIC ENGINEERING
EXAMINATIONS 2015

MSc and EEE PART IV: MEng and ACGI

RADIO FREQUENCY ELECTRONICS

Wednesday, 29 April 10:00 am

Time allowed: 3:00 hours

Corrected Copy

There are SIX questions on this paper.

Answer FOUR questions.

All questions carry equal marks

Any special instructions for invigilators and information for candidates are on page 1.

Examiners responsible First Marker(s) : S. Lucyszyn
Second Marker(s) : A.S. Holmes

Special instructions for invigilators

This is a closed book examination.

Special instructions for students

Boltzmann's constant, $k = 1.3805 \times 10^{-23} \text{ [W.s / K]}$

Absolute temperature, $T[\text{K}] \approx 273 + T [^{\circ}\text{C}]$

The Questions

1. The frequency spectrum from 0.1 to 100 GHz of sky noise temperature is shown in Figure 1.1.

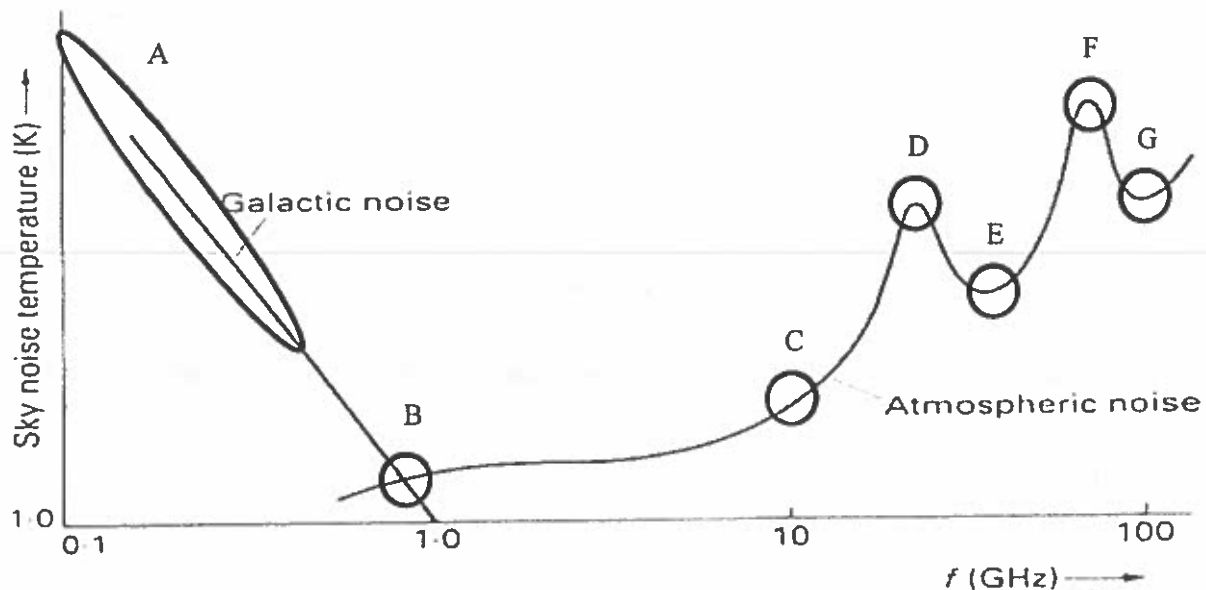


Figure 1.1: Sky noise spectrum.

- a) Qualitatively, describe what can be heard when an amplitude modulation radio receiver is not tuned to any broadcasting station and switched from UHF to VHF to HF. Justify possible reasons for what is heard, in terms of the external source and sources within the receiver. For full marks, quote any appropriate equation to support your answer. [4]
- b) State the most common domestic application at Point B on Figure 1.1, indicating its approximate frequency, and briefly explain possible implementation trade-offs at such frequencies. For full marks, quote an appropriate equation to support your answer. [4]
- c) State the most common domestic application at Point C on Figure 1.1. For this application, explain why the uplink frequency is greater than the downlink frequency. For full marks, quote an appropriate equation to support your answer. [4]
- d) Briefly explain the reason for the peak in atmospheric noise at Point D in Figure 1.1 and state the approximate frequency of this peak. [2]
- e) State the most common application at Point E on Figure 1.1, indicating its approximate frequency, and briefly explain why this application is in this band. [2]
- f) Briefly explain the reason for the broad peak in atmospheric noise at Point F in Figure 1.1 and state the approximate centre frequency of this broad peak. State the most common domestic application and why it is found in this band. [2]
- g) State the most common application at Point G on Figure 1.1, indicating its approximate frequency, and briefly explain why this application is in this band. [2]

2. An amplifier chain is illustrated in Figure 2.1. All sub-systems are assumed to be operating in their linear region and perfectly impedance matched.

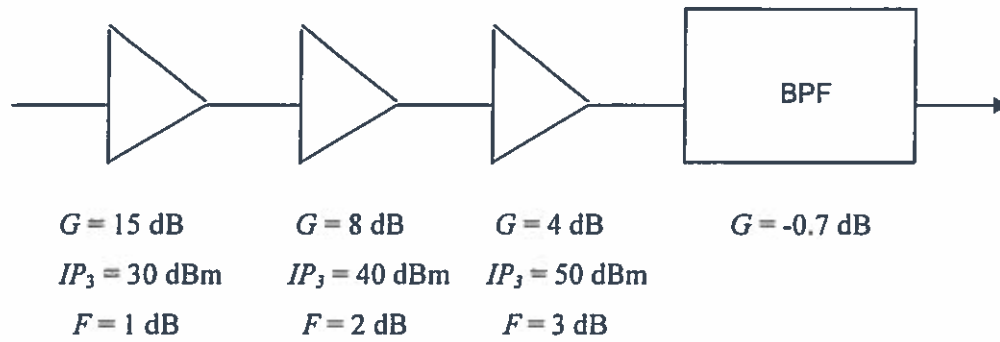


Figure 2.1: Amplifier chain.

For an overall input power of 3 dBm, calculate the following at the output of each subsystem:

- a) C [2]
- b) IP_3 [6]
- c) IMD_3 [3]
- d) I_3 [3]
- e) Overall F [6]

All variables have their usual meaning.

3.

- a) Draw the circuit diagram for a series *RLC* tuned circuit, identifying all the elements, and write down the expression for its total impedance. Assume that the element values are all frequency invariant.

[3]

- b) From the total impedance in 3(a), and given the general mathematical identity in equation (3.1), derive an expression for the associated differential-phase group delay for all frequencies.

$$\frac{\partial}{\partial x} \{ \tan^{-1}(u) \} = \frac{1}{1+u^2} \frac{\partial u}{\partial x} \quad (3.1)$$

[5]

- c) For the element values in 3(a), write down the well-known expressions for:

- i) Ideal lossless resonance frequency, ω_r .

[1]

- ii) Unloaded quality factor at ω_r .

[1]

- d) Using the results in 3(b) and 3(c), prove that the unloaded quality factor at ω_r is directly proportional to the ratio of differential-phase group delay and the time period of the cycle.

[4]

- e) Given an n^{th} -stage BPF, constructed using lossless *LC* tuned circuits, the maximum theoretical insertion phase variation is $n\pi$ (as frequency increases from dc to infinity).

- i) Derive a qualitative expression for the differential-phase group delay, in terms of the order of the filter and -3 dB bandwidth.

[2]

- ii) Using the rough approximation in 3(e)(i), show how the loaded quality factor at centre frequency ω_o is directly proportional to the ratio of differential-phase group delay and the time period of the cycle.

[2]

- iii) Comment on the similarity of the expression in 3(e)(ii) for quality factor and that derived in 3(d).

[2]

4.

- a) Compare and contrast lumped-element impedance matching over the use of distributed-elements, in terms of frequency performance. How does this affect their role in dc biasing networks?
[4]
- b) With lumped-element impedance matching, what terminating impedance conditions are best suited for L-match, π -match and T-match networks?
[4]
- c) A 2 GHz narrow-band amplifier has an output impedance of $(5 - j7) \Omega$ and must be matched to a system impedance of 50Ω . Design simple matching circuits to achieve maximum power transfer:
 - i) With the use of one lumped-element component and one distributed-element component.
[4]
 - ii) With the use of two lumped-element components.
[4]
- d) With MMIC technology, discuss the difficulties implementing lumped-element and distributed-element components. How can micromachining technologies help to overcome some of the problems with monolithic implementations? How does this affect their role in filter networks?
[4]

5.

- a) Using S-parameters, what are the levels of insertion loss and return loss at the -3 dB cut-off frequency for a lossless filter? You are asked to design a filter with a maximum pass band return loss level of -6.868 dB. What will be the worst-case pass band insertion loss ripple for a lossless band-pass filter?

[5]

- b) Using the worst-case level of ripple calculated in 5(a), but this time for the stop band return loss, design a lumped-element *LC* band stop filter to meet the following specifications:

Lower pass band -3 dB cut-off frequency:	540 MHz
Upper pass band -3 dB cut-off frequency:	660 MHz
Stop band bandwidth:	60 MHz
Band stop attenuation:	> 45 dB
Source impedance, Z_s :	50 Ω
Load impedance, Z_L :	100 Ω

[10]

- c) Using S-parameters, define differential-phase group delay and explain the general relationship between its frequency response and that of sharp cut-off insertion loss characteristics.

[5]

6. The photograph in Figure 6.1 is of a 38 GHz receiver MMIC.

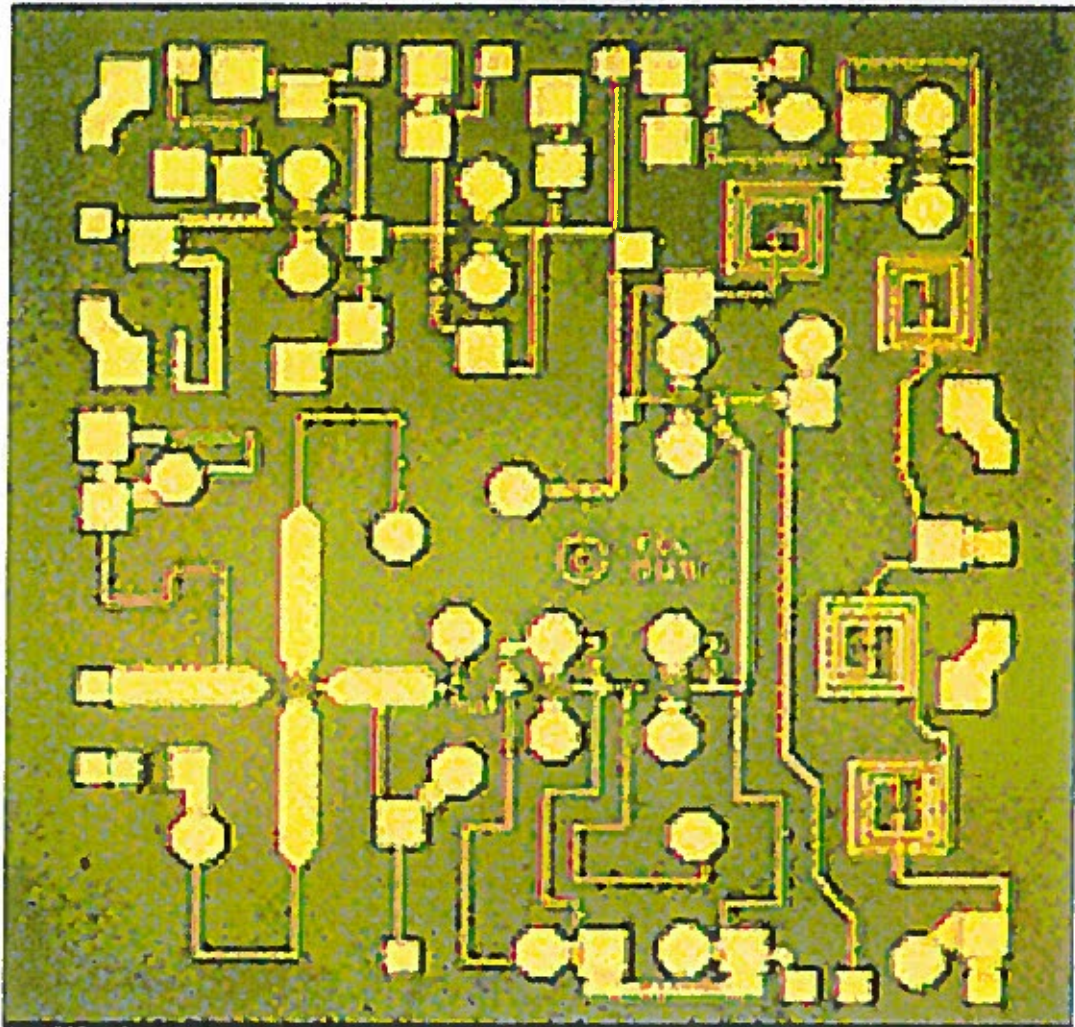
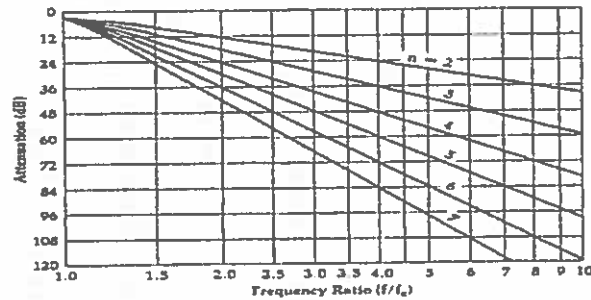


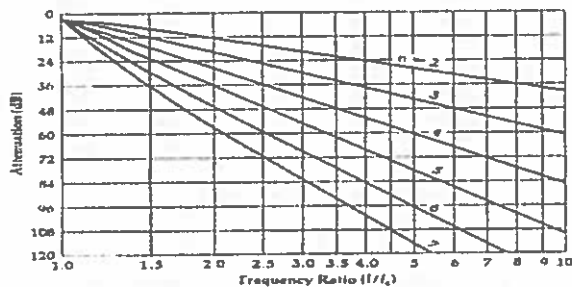
Figure 6.1: Photograph of a 38 GHz receiver MMIC (Nam *et al.*, IEE Coll., 1999).

- a) Draw the high level subsystems block diagram from what can be deduced from Figure 6.1. An active transistor should be represented as a discrete amplifier stage. [4]
- b) State the type of receiver that Figure 6.1 represents and list its general characteristics. [4]
- c) What type of mixer is used and how is it configured to operate? Briefly explain what this design is attractive for an MMIC. [4]
- d) If the LO needs the use of a dielectric resonator, where would this resonator be located in practical applications and what is the reasoning for this? [2]
- e) In general, what is the rule-of-thumb power level needed for an LO signal at the input of a general mixer used in a receiver and justify the reason for this level? [2]
- f) For a more complete receiver, what subsystem block is missing from the front end? Explain why this is needed and list three possible solutions to alleviate the problem. [4]

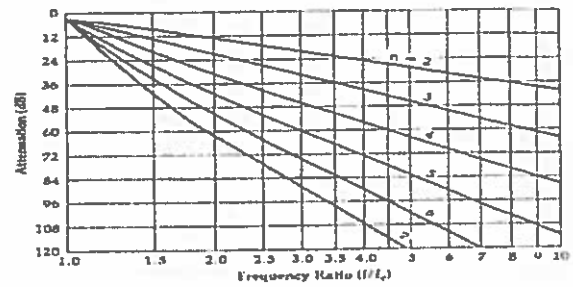
Standard Filter Curves and Tables



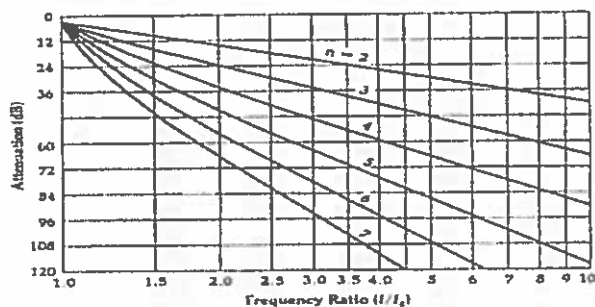
Attenuation characteristics for Butterworth filters.



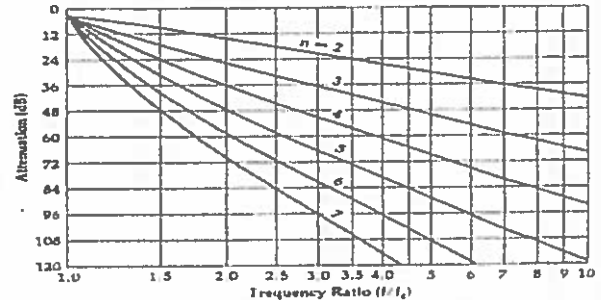
Attenuation characteristics for a Chebyshev filter with 0.01-dB ripple.



Attenuation characteristics for a Chebyshev filter with 0.1-dB ripple.

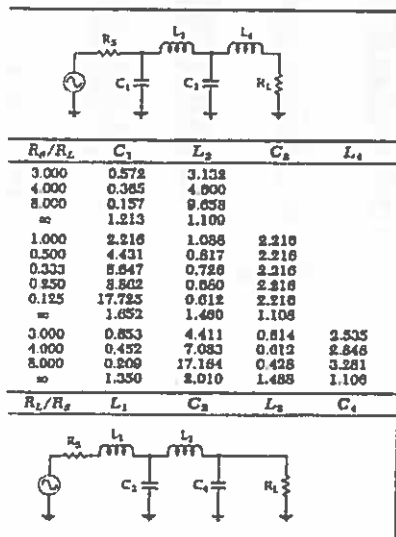


Attenuation characteristics for a Chebyshev filter with 0.5-dB ripple.

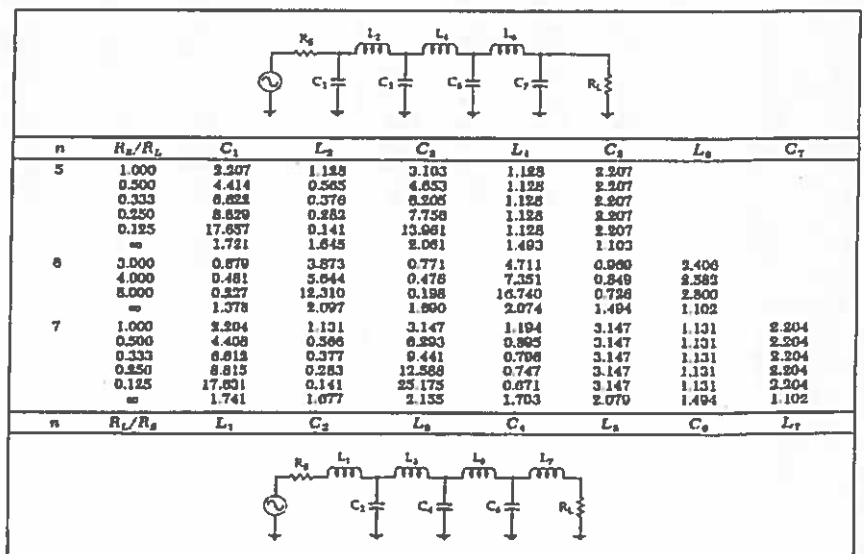


Attenuation characteristics for a Chebyshev filter with 1-dB ripple.

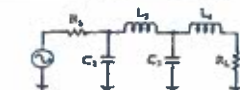
Chebyshev Low-Pass Prototype Element Values for 1.0-dB Ripple



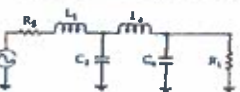
Chebyshev Low-Pass Prototype Element Values for 1.0-dB Ripple



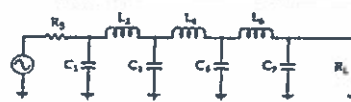
Butterworth Low-Pass
Prototype Element Values



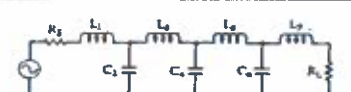
n	R_1/R_L	C_1	L_2	C_2	L_3
2	1.111	1.035	1.835		
	1.835	0.849	2.121		
	1.429	0.687	2.439		
	1.267	0.566	2.928		
	2.000	0.448	3.346		
	2.500	0.342	4.005		
	3.333	0.243	5.313		
	5.000	0.159	7.707		
	10.000	0.074	14.814		
∞	1.414		0.707		
3	0.800	0.908	1.633	1.599	
	0.800	0.841	1.584	1.525	
	0.700	0.815	1.163	3.577	
	0.600	0.823	0.603	2.708	
	0.500	1.181	0.779	3.801	
	0.400	1.423	0.604	4.064	
	0.300	1.838	0.440	5.363	
	0.200	2.808	0.284	7.910	
	0.100	5.187	0.135	15.455	
∞	1.500		1.333	0.500	
4	1.111	0.498	1.592	1.744	1.499
	1.835	0.388	1.095	1.511	1.811
	1.429	0.325	1.803	1.381	3.173
	1.267	0.260	2.103	1.082	3.613
	2.000	0.318	2.453	0.883	3.187
	2.500	0.180	3.859	0.661	4.009
	3.333	0.124	5.881	0.507	5.338
	5.000	0.060	8.684	0.351	7.940
	10.000	0.030	11.094	0.162	15.042
∞	1.531		1.577	1.082	0.583



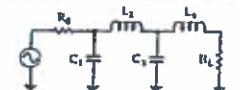
Butterworth Low-Pass Prototype Element Values



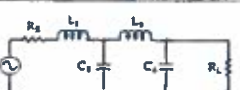
n	R_1/R_L	C_1	L_2	C_2	L_3	C_3	L_4	C_4
5	0.900	0.442	1.027	1.910	1.736	1.389		
	0.800	0.470	0.886	2.061	1.544	1.738		
	0.700	0.517	0.731	2.285	1.333	2.108		
	0.600	0.588	0.609	2.600	1.128	2.558		
	0.500	0.688	0.498	3.051	0.924	3.133		
	0.400	0.838	0.388	3.730	0.737	3.868		
	0.300	1.064	0.285	4.584	0.537	4.807		
	0.200	1.608	0.188	7.185	0.332	7.935		
	0.100	3.512	0.091	14.005	0.173	15.710		
∞	1.543		1.604	1.383	0.894	0.209		
6	1.111	0.289	1.040	1.325	2.054	1.744	1.335	
	1.835	0.245	1.116	1.128	2.230	1.550	1.688	
	1.429	0.207	1.236	0.957	2.499	1.348	2.083	
	1.267	0.173	1.407	0.801	2.858	1.143	2.509	
	2.000	0.141	1.653	0.654	3.309	0.942	3.094	
	2.500	0.111	2.028	0.514	4.141	0.745	3.831	
	3.333	0.082	2.656	0.379	5.433	0.553	5.280	
	5.000	0.054	3.917	0.246	8.020	0.363	7.922	
	10.000	0.028	7.705	0.123	15.786	0.179	15.738	
∞	1.553		1.759	1.553	1.202	0.758	0.259	
7	0.900	0.200	0.711	1.404	1.480	2.125	1.727	1.290
	0.800	0.322	0.606	1.517	1.378	2.334	1.546	1.652
	0.700	0.357	0.515	1.688	1.091	2.618	1.350	2.028
	0.600	0.406	0.432	1.928	0.917	3.006	1.150	2.477
	0.500	0.480	0.354	2.273	0.751	3.553	0.951	3.084
	0.400	0.590	0.278	2.785	0.592	4.380	0.754	3.901
	0.300	0.773	0.208	3.671	0.437	5.741	0.500	5.253
	0.200	1.145	0.135	5.437	0.287	8.326	0.309	7.900
	0.100	2.257	0.067	10.700	0.142	16.822	0.182	15.748
∞	1.558		1.799	1.650	1.397	1.055	0.650	0.223



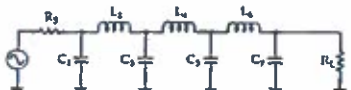
Chebyshev Low-Pass Element Values
for 0.01-dB Ripple



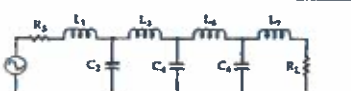
n	R_1/R_L	C_1	L_2	C_2	L_3
2	1.101	1.347	1.483		
	1.111	1.347	1.585		
	1.250	0.943	1.937		
	1.429	0.750	2.344		
	1.667	0.600	2.750		
	2.000	0.479	3.277		
	2.500	0.383	4.033		
	3.333	0.259	5.253		
	5.000	0.164	7.650		
	10.000	0.078	14.740		
∞	1.418		0.742		
3	1.000	1.181	1.821	1.181	
	0.900	1.098	1.600	1.480	
	0.800	1.087	1.443	1.800	
	0.700	1.160	1.228	2.165	
	0.600	1.374	1.034	2.588	
	0.500	1.432	0.829	3.184	
	0.400	1.734	0.645	3.974	
	0.300	2.316	0.470	5.250	
	0.200	3.193	0.305	7.834	
	0.100	6.141	0.148	15.290	
∞	1.501		1.433	0.591	
4	1.100	0.950	1.936	1.761	1.049
	1.111	0.854	1.846	1.744	1.105
	1.250	0.618	2.075	1.542	1.617
	1.429	0.485	2.379	1.234	2.008
	1.667	0.308	2.571	1.128	2.401
	2.000	0.218	2.964	0.928	3.045
	2.500	0.242	3.643	0.728	3.875
	3.333	0.174	4.737	0.538	5.209
	5.000	0.112	6.910	0.352	7.813
	10.000	0.054	13.409	0.175	15.310
∞	1.529		1.604	1.212	0.523



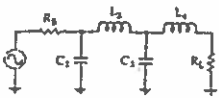
Chebyshev Low-Pass Element Values for 0.01-dB Ripple



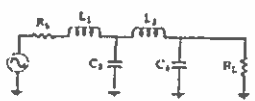
n	R_1/R_L	C_1	L_2	C_2	L_3	C_3	L_4	C_4
5	1.000	0.977	1.883	2.037	1.663	0.977		
	0.900	0.880	1.458	2.174	1.641	1.574		
	0.800	0.877	1.235	2.379	1.499	1.807		
	0.700	0.926	1.040	2.658	1.323	1.977		
	0.600	1.019	0.863	3.041	1.135	2.424		
	0.500	1.180	0.699	3.584	0.942	3.009		
	0.400	1.383	0.544	4.403	0.749	3.845		
	0.300	1.797	0.398	5.772	0.557	5.183		
	0.200	2.604	0.259	8.514	0.389	7.826		
	0.100	5.041	0.127	16.741	0.182	15.613		
∞	1.547		1.785	1.645	1.237	0.488		
6	1.101	0.851	1.796	1.841	2.027	1.631	0.937	
	1.111	0.760	1.782	1.775	2.094	1.638	1.063	
	1.250	0.545	1.864	1.489	2.403	1.507	1.504	
	1.429	0.436	2.038	1.268	2.735	1.332	1.899	
	1.667	0.351	2.298	1.091	3.187	1.145	2.357	
	2.000	0.279	2.678	0.867	3.788	0.954	2.948	
	2.500	0.214	3.261	0.682	4.667	0.761	3.790	
	3.333	0.155	4.245	0.500	6.163	0.588	5.143	
	5.000	0.100	6.223	0.330	9.151	0.378	7.785	
	10.000	0.048	12.171	0.162	18.105	0.167	15.583	
∞	1.551		1.847	1.790	1.596	1.180	0.489	
7	1.000	0.913	1.593	2.003	1.870	2.002	1.595	0.913
	0.900	0.819	1.382	2.090	1.722	2.202	1.531	1.506
	0.800	0.811	1.150	2.282	1.525	2.483	1.404	1.538
	0.700	0.837	0.967	2.510	1.323	2.802	1.307	1.910
	0.600	0.943	0.803	2.872	1.124	3.250	1.131	2.359
	0.500	1.080	0.650	3.382	0.928	3.875	0.947	2.948
	0.400	1.297	0.507	4.156	0.735	4.812	0.758	3.790
	0.300	1.869	0.378	5.454	0.546	6.370	0.508	5.148
	0.200	2.342	0.242	8.057	0.360	9.464	0.378	7.802
	0.100	4.701	0.119	15.872	0.178	18.818	0.168	15.532
∞	1.559		1.867	1.886	1.765	1.583	1.161	0.456



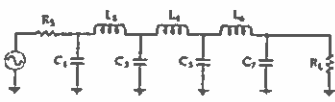
Chebyshev Low-Pass Prototype Element Values for 0.1-dB Ripple



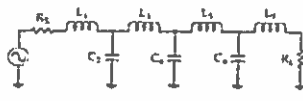
n	R_1/R_L	C_1	L_1	C_2	L_2
2	1.335	1.800	1.636		
	1.429	0.977	1.882		
	1.607	0.733	2.489		
	2.000	0.500	3.054		
	2.500	0.417	3.827		
	3.333	0.293	7.420		
	5.000	0.184	14.433		
	10.000	0.087	14.433		
∞	1.391	0.819			
3	1.000	1.433	1.564	1.433	
	0.900	1.426	1.494	1.822	
	0.800	1.451	1.356	1.871	
	0.700	1.521	1.193	2.190	
	0.600	1.648	1.017	2.803	
	0.500	1.853	0.839	3.159	
	0.400	2.189	0.660	3.968	
	0.300	2.763	0.496	5.279	
	0.200	3.942	0.317	7.850	
	0.100	7.512	0.155	15.466	
∞	1.513	1.510	0.716		
4	1.335	0.902	2.145	1.585	1.341
	1.429	0.779	2.318	1.429	1.700
	1.607	0.578	2.730	1.185	2.243
	2.000	0.440	3.227	0.907	2.858
	2.500	0.329	3.981	0.700	3.895
	3.333	0.233	5.178	0.500	5.030
	5.000	0.148	7.807	0.387	7.814
	10.000	0.079	14.857	0.180	15.230
∞	1.511	1.708	1.435	0.673	



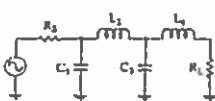
Chebyshev Low-Pass Prototype Element Values for 0.1-dB Ripple



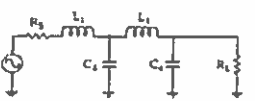
n	R_1/R_L	C_1	L_1	C_2	L_2	C_3	L_3	C_4	L_4	C_5
5	1.000	1.301	1.538	2.341	1.559	1.301				
	0.900	1.285	1.433	2.380	1.486	1.486				
	0.800	1.300	1.282	2.582	1.382	1.736				
	0.700	1.358	1.117	2.868	1.244	2.062				
	0.600	1.470	0.947	3.208	1.055	2.484				
	0.500	1.654	0.778	3.645	0.815	3.055				
	0.400	1.854	0.612	4.270	0.573	3.886				
	0.300	2.477	0.451	6.190	0.380	5.237				
	0.200	3.548	0.295	9.187	0.266	7.889				
	0.100	7.787	0.115	17.937	0.182	15.745				
∞	1.581	1.807	1.700	1.417	0.651					
6	1.335	0.942	2.080	1.050	2.247	1.534				1.377
	1.429	0.735	2.348	1.454	2.544	1.403				1.629
	1.607	0.542	2.800	1.183	3.064	1.185				2.174
	2.000	0.414	3.068	0.859	3.712	0.970				2.794
	2.500	0.310	3.785	0.749	4.651	0.778				3.645
	3.333	0.220	4.927	0.551	6.195	0.580				4.969
	5.000	0.139	7.550	0.361	9.201	0.384				7.619
	10.000	0.067	14.220	0.178	18.427	0.190				15.350
∞	1.534	1.884	1.831	1.749	1.394	0.638				
7	1.000	1.242	1.580	2.239	1.680	2.230				1.520
	0.900	1.242	1.285	2.381	1.578	2.387				1.459
	0.800	1.255	1.145	2.548	1.443	2.824				1.388
	0.700	1.310	1.083	2.810	1.253	3.442				1.233
	0.600	1.417	0.917	3.205	1.009	4.081				1.081
	0.500	1.595	0.753	3.784	0.784	4.915				0.914
	0.400	1.855	0.593	4.618	0.742	6.070				0.739
	0.300	2.392	0.437	6.054	0.550	8.569				0.557
	0.200	3.428	0.286	8.937	0.389	12.770				0.372
	0.100	8.370	0.141	17.603	0.184	19.370				0.185
∞	1.375	1.859	1.821	1.537	1.734	1.370				0.631



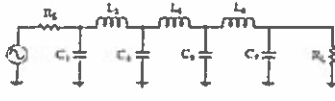
Chebyshev Low-Pass Prototype Element Values for 0.5-dB Ripple



n	R_1/R_L	C_1	L_1	C_2	L_2
2	1.984	0.983	1.950		
	2.000	0.909	2.103		
	2.500	0.504	3.185		
	3.333	0.375	4.411		
	5.000	0.228	6.700		
	10.000	0.105	13.322		
∞	1.307	0.975			
3	1.000	1.684	1.280	1.834	
	0.900	1.615	1.208	2.026	
	0.800	1.697	1.120	2.237	
	0.700	2.114	1.015	2.517	
	0.600	2.557	0.799	3.430	
	0.400	2.985	0.615	4.142	
	0.300	3.729	0.403	5.570	
	0.200	5.254	0.309	8.225	
	0.100	9.890	0.153	16.118	
∞	1.572	1.518	0.832		
4	1.984	0.920	2.586	1.304	1.828
	2.000	0.845	2.720	1.238	1.985
	2.500	0.516	3.706	0.869	3.121
	3.333	0.344	5.120	0.621	4.490
	5.000	0.210	7.708	0.400	6.897
	10.000	0.098	15.352	0.194	14.882
∞	1.436	1.880	1.521	0.913	



Chebyshev Low-Pass Prototype Element Values for 0.5-dB Ripple



n	R_1/R_L	C_1	L_1	C_2	L_2	C_3	L_3	C_4	L_4	C_5
5	1.000	1.807	1.303	2.601	1.503	1.807				
	0.900	1.854	1.222	2.849	1.338	1.970				
	0.800	1.928	1.128	3.060	1.157	2.185				
	0.700	2.035	1.015	3.353	1.038	2.470				
	0.600	2.200	0.890	3.785	0.948	2.861				
	0.500	2.457	0.754	4.387	0.810	3.414				
	0.400	2.870	0.609	5.208	0.684	4.245				
	0.300	3.593	0.459	6.871	0.506	5.625				
	0.200	5.094	0.306	10.054	0.343	8.387				
	0.100	9.558	0.153	19.647	0.173	16.574				
∞	1.630	1.740	1.522	1.514	0.903					
6	1.984	0.905	2.577	1.388	2.713	1.290				1.799
	2.000	0.850	2.704	1.291	2.872	1.237				1.956
	2.500	0.506	3.722	0.890	4.109	0.881				3.103
	3.333	0.337	5.053	0.632	5.090	0.636				4.481
	5.000	0.200	7.615	0.408	8.732	0.412				7.031
	10.000	0.098	15.186	0.197	17.681	0.202				14.433
7	1.000	1.790	1.298	2.718	1.385	2.718				1.790
	0.900	1.835	1.215	2.860	1.308	2.863				1.953
	0.800	1.905	1.113	3.076	1.215	3.107				2.188
	0.700	2.011	1.007	3.364	1.105	3.410				2.459
	0.600	2.174	0.882	3.778	0.970	3.853				2.848
	0.500	2.428	0.747	4.370	0.838	4.280				3.406
	0.400	2.835	0.604	5.295	0.685	5.470				4.243
	0.300	3.546	0.453	6.807	0.522	7.134				5.635
	0.200	5.007	0.303	10.049	0.352	10.496				8.404
	0.100	9.459	0.151	19.819	0.178	20.631				16.605
∞	1.846	1.777	2.031	1.788	1.924	1.503				0.895

