

$$SPL = 10 \log \left( \frac{\bar{P}^2}{P_{ref}^2} \right)$$

$$= 10 \log \left( \frac{4 \left( \frac{A^2}{2} \right)}{\left( \frac{A^2}{2} \right)} \right)$$

$$= 10 \log 4$$

$$\approx +6 \text{ dB}$$

2<sup>nd</sup> CASE

$$A = B, \quad \omega_1 \neq \omega_2 \quad \phi = 0$$

$$P(t) = A \sin(\omega_1 t) + A \sin(\omega_2 t)$$

$$\bar{P}^2(t) = \frac{1}{T} \int_0^T A^2 [\sin(\omega_1 t) + \sin(\omega_2 t)]^2 dt$$

$$= \frac{1}{T} \int_0^T A^2 [\sin^2(\omega_1 t) + \sin^2(\omega_2 t) + \underbrace{2 \sin(\omega_1 t) \sin(\omega_2 t)}_{\substack{\text{simplely zero} \\ \approx 0 \text{ when } \omega_1 \neq \omega_2}}] dt$$

$$\bar{P}^2(t) = \frac{1}{T} \int_0^T A^2 (\sin^2(\omega_1 t) + \sin^2(\omega_2 t)) dt \quad \left( \text{using the average value theorem} \right)$$

$$\bar{P}^2(t) = \frac{A^2}{2} + \frac{A^2}{2}$$

$$\bar{P}^2(t) = A^2$$

$$SPL = 10 \log \left( \frac{A^2}{A_{ref}^2} \right)$$

$$= 10 \log 2$$

$$SPL \approx +3 \text{ dB}$$

→ Double A signal

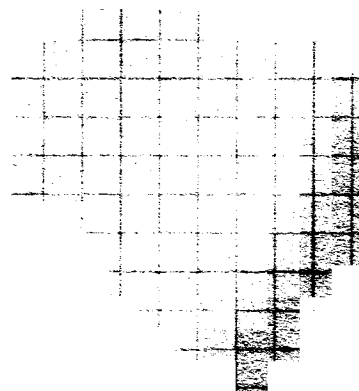
what about halved signal?

$$10 \log\left(\frac{1}{2}\right)$$

$$10 \log(2^{-1})$$

$$-10 \log 2$$

$$SPL = -3 \text{ dB}$$



MORE WORK (OPTIONAL)

$$A = B, \quad \omega_1 = \omega_2, \quad \phi = \frac{\pi}{2}$$

$$A = B, \quad \omega_1 = \omega_2, \quad \phi = \pi$$

$$A = 3B, \quad \omega_1 = \omega_2, \quad \phi = 0$$

$$A = 3B, \quad \omega_1 \neq \omega_2, \quad \phi = 0$$

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(Pass out handout)

How Does this Relate to Real World?

Tones do not exist by themselves (Fig 11.1)

TONE: single frequency

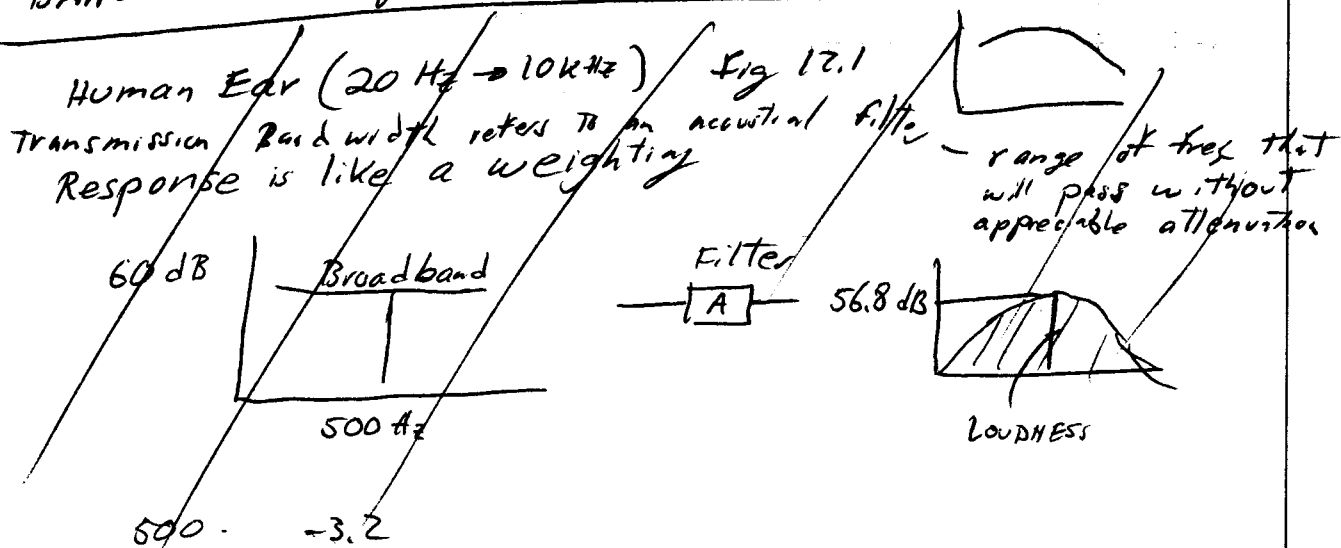
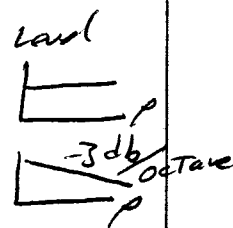
BROADBAND: multiple frequencies

WHITE NOISE: equal strength at all frequencies

OCTAVE: doubling of frequency

BANDWIDTH: frequency range

Tuning Fork - single freq  
to broadband - range of freq



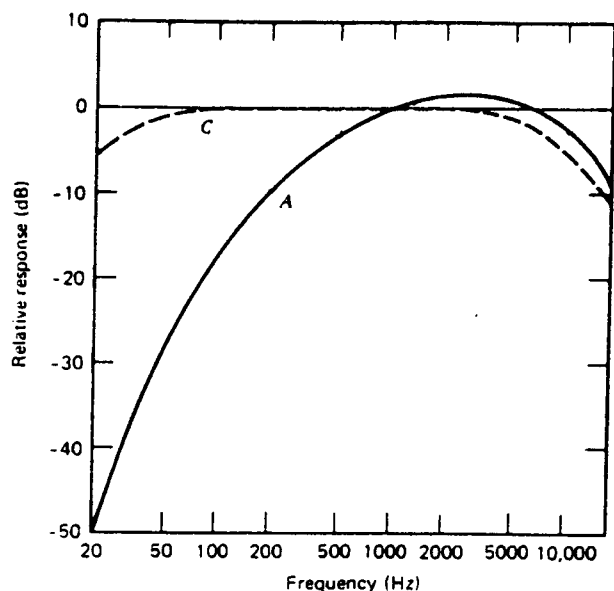


Fig. 12.1. Filter characteristics for A- and C-weighted sound levels.

Table 11.1. Preferred octave-band and 1/3-octave-band center frequencies

| Center Frequency (Hz) |            | 10 log(Bandwidth) |            |
|-----------------------|------------|-------------------|------------|
| Octave                | 1/3-Octave | Octave            | 1/3-Octave |
| 16                    | 10         | 10.5              | 3.6        |
|                       | 12.5       |                   | 4.6        |
|                       | 16         |                   | 5.7        |
|                       | 20         |                   | 6.6        |
| 31.5                  | 25         | 13.4              | 7.6        |
|                       | 31.5       |                   | 8.6        |
|                       | 40         |                   | 9.7        |
| 63                    | 50         | 16.5              | 10.6       |
|                       | 63         |                   | 11.6       |
|                       | 80         |                   | 12.7       |
| 125                   | 100        | 19.5              | 13.6       |
|                       | 125        |                   | 14.6       |
|                       | 160        |                   | 15.7       |
| 250                   | 200        | 22.5              | 16.7       |
|                       | 250        |                   | 17.6       |
|                       | 315        |                   | 18.6       |
| 500                   | 400        | 25.5              | 19.7       |
|                       | 500        |                   | 20.6       |
|                       | 630        |                   | 21.6       |
| 1000                  | 800        | 28.5              | 22.7       |
|                       | 1000       |                   | 23.6       |
|                       | 1250       |                   | 24.6       |
| 2000                  | 1600       | 31.5              | 25.7       |
|                       | 2000       |                   | 26.7       |
|                       | 2500       |                   | 27.6       |
| 4000                  | 3150       | 34.5              | 28.6       |
|                       | 4000       |                   | 29.7       |
|                       | 5000       |                   | 30.6       |
| 8000                  | 6300       | 37.5              | 31.6       |
|                       | 8000       |                   | 32.7       |

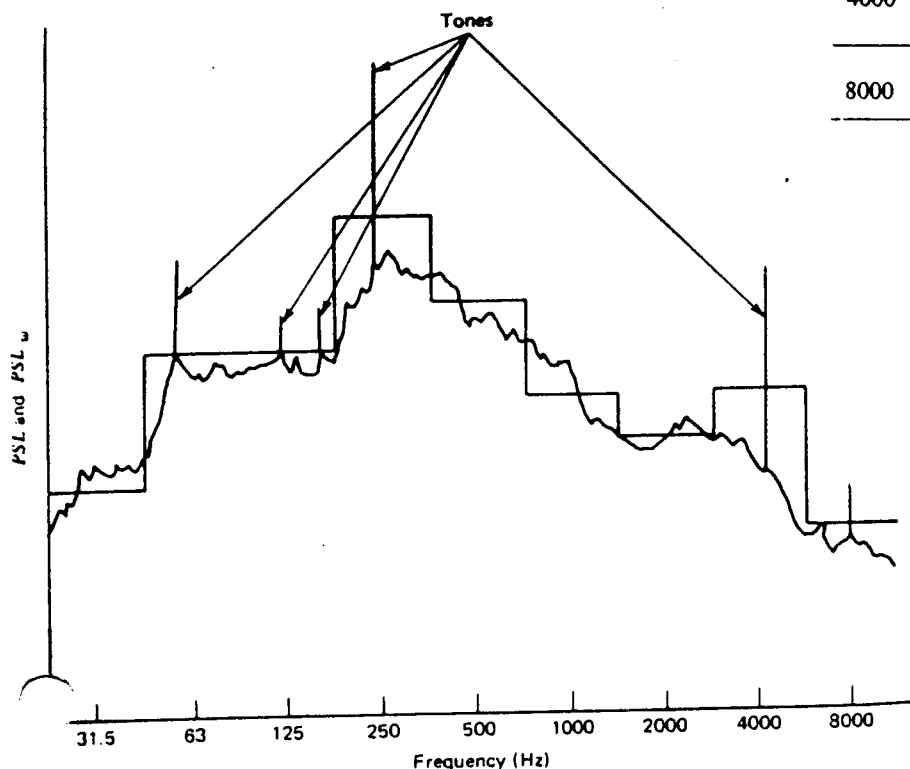


Fig. 11.1. Representative spectrum for noise with the PSL determined over octave bands.

Table 12.1. Correction to be added to octave-band levels to convert them to A-weighted band levels

| Center Frequency (Hz) | Correction (dB) |
|-----------------------|-----------------|
| 31.5                  | -39.4           |
| 63                    | -26.2           |
| 125                   | -16.1           |
| 250                   | -8.6            |
| 500                   | -3.2            |
| 1000                  | 0               |
| 2000                  | +1.2            |
| 4000                  | +1.0            |
| 8000                  | -1.1            |

of rating procedures that use the statistical behavior of the A-weighted sound level are the *day-night averaged sound level* ( $L_{A\text{dn}}$ ), the *50-percentile exceeded sound level* ( $L_{A50}$ ), and the *community noise equivalent level* (CNEL).

One exception to the use of A-weighted sound levels is the calculation of the impact of airport noise, where the *effective perceived noise level* ( $L_{EPN}$ ), calculated from the instantaneous spectra, is used to make a *noise exposure forecast* (NEF).

Excellent general and comprehensive treatments of environmental noise and its control are contained in the books edited by Harris<sup>1</sup> and Beranek.<sup>2</sup>

**12.2 WEIGHTED SOUND LEVELS.** The simplest and probably most widely used measure of environmental noise is the *A-weighted sound level* ( $L_A$ ), expressed in dBA or dB(A). (The reference pressure is 20  $\mu\text{Pa}$  as discussed in Sect. 5.12 and will be left implicit.) A-weighting assigns to each frequency a "weight" that is related to the sensitivity of the ear at that frequency. For example, in a sound level meter the received signal is passed through a filter network with the dBA frequency characteristic, as shown in Fig. 12.1, and the level of the filtered signal is then determined and displayed. The dBA frequency characteristic was originally designed to mirror the 40-phon equal-loudness-level contour of the 1933 Fletcher-Munson data. It is also a

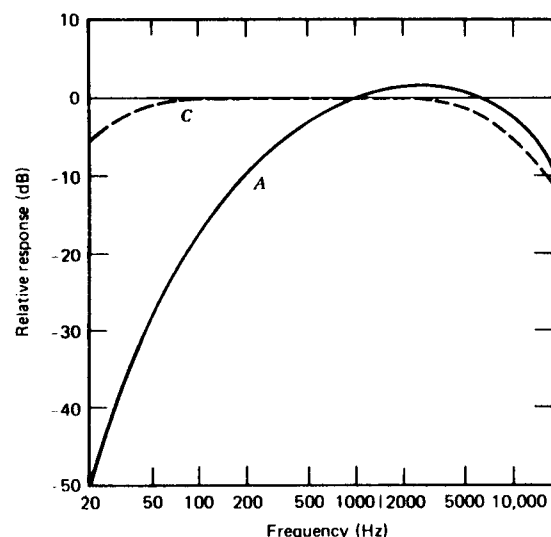


Fig. 12.1. Filter characteristics for A- and C-weighted sound levels.

good approximation of the 10-phon contour of the more recent Robinson-Dadson data, which is reproduced in Fig. 11.9. Accurate A-weighted levels can be obtained from octave-band levels by applying the corrections shown in Table 12.1 to each band level and then combining the corrected band levels with the nomograph of Fig. 11.2. Table 12.2 displays A-weighted sound levels for some commonly encountered noises.

Table 12.1. Correction to be added to octave-band levels to convert them to A-weighted band levels

| Center Frequency (Hz) | Correction (dB) |
|-----------------------|-----------------|
| 31.5                  | -39.4           |
| 63                    | -26.2           |
| 125                   | -16.1           |
| 250                   | -8.6            |
| 500                   | -3.2            |
| 1000                  | 0               |
| 2000                  | +1.2            |
| 4000                  | +1.0            |
| 8000                  | -1.1            |

Other weightings have been proposed but few have gained widespread acceptance. Most sound level meters will allow selection of either A-weighting,  $L_A$ , or C-weighting,  $L_C$ . The frequency characteristic for C-weighting (also shown in Fig. 12.1) is nearly flat, rolling off slightly at high and low frequencies. Although no single overall sound level can give information about the spectrum of a noise, measurement of both  $L_A$  and  $L_C$  will yield some information about the prominence of noise for frequencies below about 200 Hz. If there is significant energy in these lower frequencies, the  $L_C$  will be appreciably greater than the  $L_A$ .

The  $L_A$  is in widespread use mainly because it is inexpensive to obtain and easier for laypersons to appreciate than are any of the other more accurate, but more complicated, noise rating procedures. In addition, for most environmental noises  $L_A$  does correlate fairly well with the other rating procedures. While the A-weighted sound level  $L_A$  cannot completely replace more precise rating procedures, it has been shown<sup>3</sup> that for a wide variety of environmental noises measurements of  $L_A$  and  $L_C$  can be used to predict accurately the results of more complicated procedures. When a loudness level (for example, calculated by the method of Stevens, as mentioned in the previous chapter) is plotted against the A-weighted sound level for the same noise, the data for a given  $L_C - L_A$  difference fall nearly on a line (Fig. 12.2).

<sup>1</sup> Harris (editor), *Handbook of Noise Control*, 2nd ed., McGraw-Hill (1979).

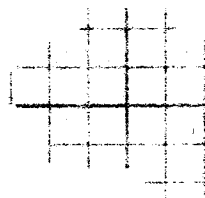
<sup>2</sup> Beranek (editor), *Noise and Vibration Control*, McGraw-Hill (1971).

<sup>3</sup> Botsford, *Sound and Vibration*, 3, 16 (Oct. 1969).

Transmission Bandwidth refers to an acoustical filter - range of frequencies that will pass without appreciable attenuation

The bandwidth of filters can be

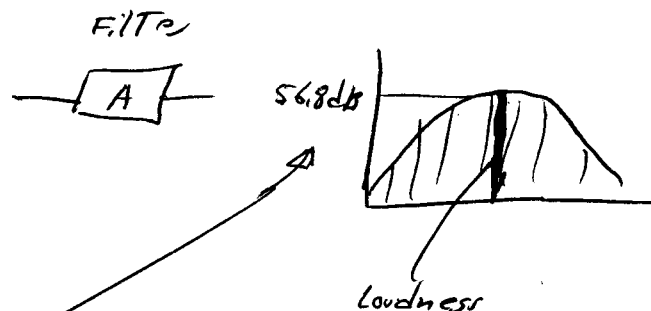
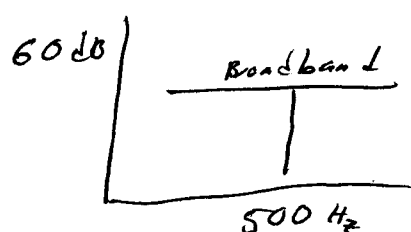
- single freq
- narrow band
- octave band
- "weighted" to simulate the freq response of the ear.



Human Ear, (20 Hz  $\rightarrow$  10 kHz)

Table  
Fig 12.1

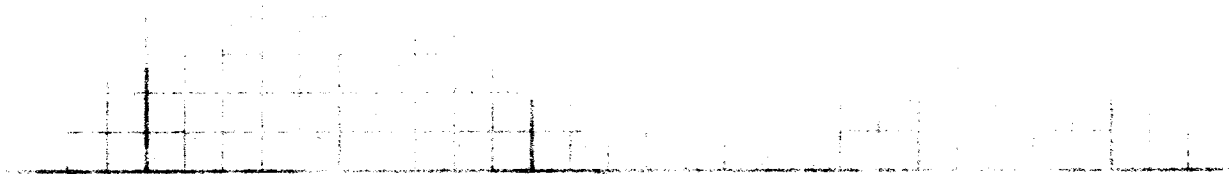
Response is like a weighting

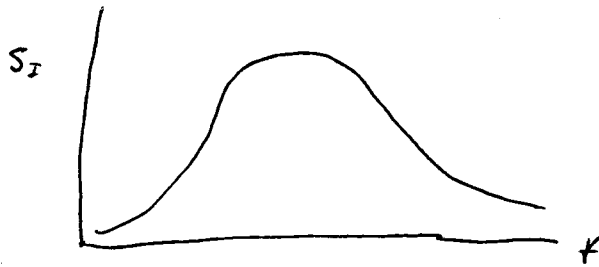


from Table 12.1  
freq correction  
500 - 3.2

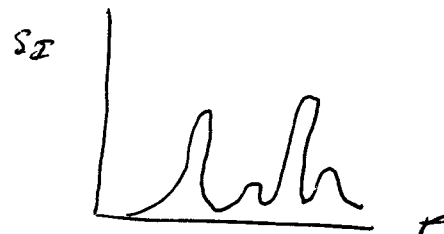
A-weighting assigns to each frequency a "weight" that is related to the sensitivity of the ear at that frequency

~~weighting~~  
~~weighting~~  
~~weighting~~





Broad band



Narrow band

$S_I$  = Spectral ~~Intensity~~ (Intensity) or spectrum level

$$BL \text{ (Band level)} = 10 \log \frac{I_w}{I_{ref}}$$

$$I_w = \Delta I$$

$$BL = SPL + 10 \log W$$

$$W = \Delta f \text{ (frequency band)}$$

| dB(A)        | Location                  | $P_0$                           |
|--------------|---------------------------|---------------------------------|
| 20 - 30 dB   | Wilderness                | $3.5 \times 10^{-4} \text{ Pa}$ |
| 30 - 50 dB   | Quiet Residential (night) | $45 \times 10^{-4} \text{ Pa}$  |
| 40 - 50 dB   | " (day)                   | $1.2 \times 10^{-3} \text{ Pa}$ |
| 60 - 70 dB   | Vacuum cleaner            | $8 \times 10^{-3} \text{ Pa}$   |
| 100 - 110 dB | Jet @ 300 m               | 0.32 Pa                         |
| 110 - 120 dB | Night Club                | 0.79 Pa                         |
| 140          | Threshold of Pain         |                                 |

### Homework

- 1) The power output from a loudspeaker is raised from 5 to 50 watts. What is the change in sound power level?
- 2) Show that the ratio of the acoustic powers of two sounds in decibels is equal to the difference of their power levels.
- 3) Determine the acoustic intensity level at a distance of 10 m from a source which radiates 1 watt of acoustic power. Use reference intensities of a) 100 b) 1 c)  $10^{-12}$  d)  $10^{-13} \frac{\text{watts}}{\text{m}^2}$
- 4) An air-conditioning unit operates with a sound intensity level of 73 dB. If it is operated in a room with an ambient sound intensity level of 68 dB, what will be the resultant intensity level?

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- ⑤ Calculate the sound pressure level for a sound wave having an effective pressure of  $3.5 \frac{\text{N}}{\text{m}^2}$ . (3.5)  
 Use reference pressures of a) 10 b) 1 c)  $10^{-4}$  d)  $2(10)^{-4}$  microbar  
 $1 \text{ microbar} = 0.1 \frac{\text{N}}{\text{m}^2}$
- ⑥ If sound pressure is doubled, find the increase in sound pressure level.
- ⑦ Two sound sources  $S_1$  and  $S_2$  are radiating sound waves of different frequencies. If their sound pressure levels recorded at position  $S$  as shown in the figure are 75 and 80 dB respectively, find the total sound pressure level at  $S$  due to the two sources together.

