#### Finite Element Method for Heat Transfer

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#### Outline

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- Method of Manufactured Solutions (MMS)
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- Future Work

#### Heat Equation

- Predicts the temperature of the body (domain) subjected to the heat source
- Derived from Fourier's law and the conservation of energy
- Of fundamental importance in diverse scientific fields

Fourier's Law  $\rightarrow \boldsymbol{q} = -\mathsf{k} \; \nabla u$ 

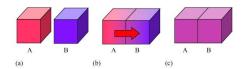


Figure: Heat conduction

#### Heat Equation

$$\frac{\partial u}{\partial t} = \alpha \nabla^2 u = \alpha \left( \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2} \right),\tag{1}$$

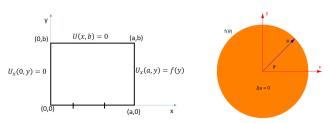
$$u(x,y,z,t) = \text{Temperature}$$

$$\alpha = \frac{k}{c_p \rho} = \text{Thermal Diffusivity} \quad c_p = \text{Specific Heat Capacity}$$

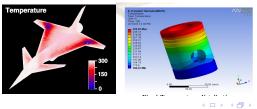
$$k = \text{Thermal conductivity} \quad \rho = \text{Mass density}$$

#### Heat Equation

We can solve (1) analytically in **simple geometries** like rectangular (cubic in 3D) or circular by the **Separation of Variables** method.



But how about the complex region? Like aircraft, blade of the turbine?!



## Finite Element Method (FEM)

- Divide the domain to small pieces called Element
- Implement the weak form of Heat Equation for each element
- Expand the unknown variable (here temperature) using shape functions at each element
- Assemble the general form of the equation and find the solution

$$\frac{\partial^2 u}{\partial x^2} = f(x) \Longrightarrow \int_0^L w(x) \left[ \frac{\partial^2 u}{\partial x^2} - f(x) \right] dx = 0$$

$$\left( w \frac{\partial u}{\partial x} \right)_0^L - \int_0^L \frac{\partial w}{\partial x} \frac{\partial u}{\partial x} dx - \int_0^L w(x) f(x) dx = 0$$
(2)

Above equation is correct for each piece of the domain (element)

#### Finite Element Method (FEM)

$$\begin{aligned} u^{h^e}(x) &= \sum_{a=1}^{n_{\rm en}} N_a^e(x) d_a^e &= N_1^e(x) d_1^e + N_2^e(x) d_2^e \\ &= \left[ \begin{array}{cc} N_1^e & N_2^e \end{array} \right] \left[ \begin{array}{c} d_1^e \\ d_2^e \end{array} \right] \\ &= N^e(x) \cdot \boldsymbol{d}^e \end{aligned}$$

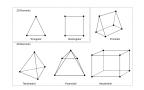




Figure: Different types of element and example of the Piston mesh

Let's say we are interested in finding a numerical solution, v, of the following initial-boundary-value-problem

$$\frac{\partial u^{2}}{\partial t^{2}} = \frac{\partial u^{2}}{\partial x^{2}} + f, \quad 0 \le x \le 1, \ t \ge 0, 
u(0, t) = g_{1}(t), \quad u(1, t) = g_{2}(t) \quad t \ge 0, 
u(x, 0) = u_{\circ}(x), \quad u_{t}(x, 0) = v_{\circ}(x), \quad 0 \le x \le 1,$$
(3)

by implementing FEM.

How can we convince ourselves (or our advisor/instructor) that the code we implemented is correct?

Simple answer: We compute the error and check if you get the expected convergence rate,  $O(h^r)$ .

$$\varepsilon(t) = \sqrt{\sum_{n=1}^{N} (u(x_n, t) - v_n)^2},$$
 (4)

**Example:** Consider  $f(x) = x^2$ , let's find the error of the first derivative using the Forward Euler method at  $x_n = 1$  using different mesh size h.

h	f'=2x	$\frac{f(x_{n+1})-f(x_n)}{h}$	$\varepsilon \approxeq O(h)$
1	2.0	$\frac{f(2)-f(1)}{h}=3.0$	1.00
0.5	2.0	$\frac{f(1.5)^n - f(1)}{h} = 2.5$	0.50
0.25	2.0	$\frac{f(1.25)^n - f(1)}{h} = 2.25$	0.25

Computing the error,  $\varepsilon$ , requires the knowledge of exact solution, which we never know!

This is where the Method of Manufactured Solutions comes in. Lets start with a simple example.

$$Ax = b \Longrightarrow x = A^{-1}b$$

how can we check the algorithm that we wrote for  $A^{-1}$  is correct?

$$A*1=b_{\circ}$$

then

$$Ax = b_{\circ} \Longrightarrow x = A^{-1}b_{\circ}$$

now you can easily compute the error  $\varepsilon = \|x-1\|$ 



To do MMS for equation (3) we start with this solution,

$$u(x,t) = \sin(\omega t - kx), \tag{5}$$

How should we adjust (3) so that (5) holds? We just need to choose the forcing, initial and boundary values we get by plugging (5) in (3). For example here,

$$f = \frac{\partial u^2}{\partial t^2} - \frac{\partial u^2}{\partial x^2} = (k^2 - \omega^2) \sin(\omega t - kx)$$

$$u(0, t) = \sin(\omega t), \quad u(1, t) = \sin(\omega t - k)$$

$$u(x, 0) = \sin(-kx), \quad u_t(x, 0) = \omega \cos(-kx),$$
(6)

Now, if we rewrite (3) with the above forcing and initial and boundary conditions, we will have

$$\frac{\partial u^2}{\partial t^2} = \frac{\partial u^2}{\partial x^2} + (k^2 - \omega^2) \sin(\omega t - kx), \quad 0 \le x \le 1, \ t \ge 0, 
u(0, t) = \sin(\omega t), \quad u(1, t) = \sin(\omega t - k), \quad t \ge 0, 
u(x, 0) = \sin(-kx), \quad u_t(x, 0) = \omega \cos(-kx), \quad 0 \le x \le 1,$$
(7)

We definitely know the exact solution is  $u(x,t) = \sin(\omega t - kx)$  and simply computed the error,  $\varepsilon$ , and see whether the code is correctly implemented or not.

#### **Primary Results**

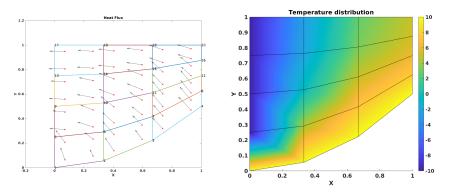


Figure: Heat flux and temperature distribution, bottom and left edges are subjected to the 10 and -10 boundary conditions. Right and top edges are insulated.

first we found temperature by solving  $\frac{\partial^2 u}{\partial x^2}+\frac{\partial^2 u}{\partial y^2}=0$  then we computed flux  ${m q}=$  -k  $\nabla u$ 

#### **Future Work**

- Transfer existing MATLAB code to Python
- Implement MMS
- Add unit and functional tests

# Question

