AUTOMATIC DIFFERENTIATION IN SOLID MECHANICS INTERPRETATION AND COMPOSITION

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Department of Computer Science University of Colorado Boulder

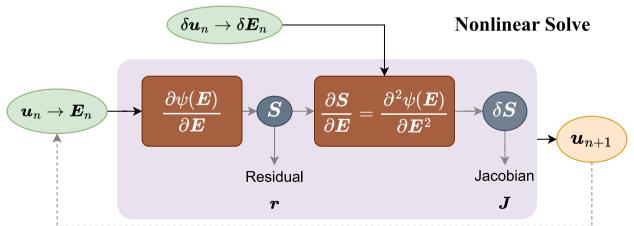
> EnzymeCon Feb 22, 2023

FREE ENERGY FUNCTIONAL AND PDE SOLVERS

$$\psi\left(\mathbf{E}\right) = \frac{\lambda}{4} \left(J^2 - 1 - 2\log J\right) - \mu\left(\log J + \operatorname{trace}\mathbf{E}\right), \ J = \sqrt{|I_3 + 2\mathbf{E}|}$$

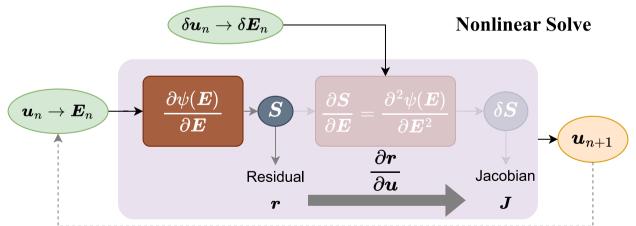
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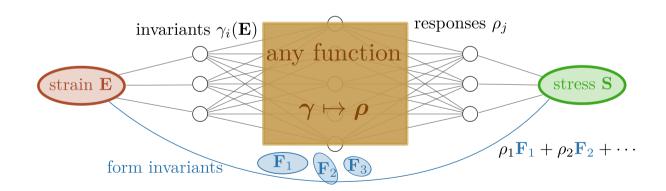


FREE ENERGY FUNCTIONAL AND INVERSE PROBLEMS

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UHYPER: USER SUBROUTINE

Variables to be defined U(1) U. strain energy density function. For a compressible material, at least one derivative involving J should be nonzero. For an incompressible material, all derivatives involving J will be ignored. The strain invariants— \bar{I}_1 , \bar{I}_2 , and J—are defined in Hyperelastic behavior of rubberlike materials. U(2) \widetilde{U}_{dev} , the deviatoric part of the strain energy density of the primary material response. This quantity is needed only if the current material definition also includes Mullins effect (see Mullins effect). UI1(1) $\partial U/\partial \bar{I}_1$. UI1(2) $\partial U/\partial \bar{I}_{2}$. UI1(3) $\partial U/\partial J$. UI3(1) UI2(1) $\partial^2 U/\partial \bar{I}_1^2$. $\partial^3 U/\partial {ar{I}_1}^2 \partial J.$ UI3(2) UI2(2) $\partial^3 U/\partial \bar{I}_2^2 \partial J$. $\partial^2 U/\partial \bar{I}_2^2$. UI2(3) UI3(3) $\partial^3 U/\partial \bar{I}_1 \partial \bar{I}_2 \partial J$. $\partial^2 U/\partial J^2$. UI2(4) UI3(4) $\partial^2 U/\partial \bar{I}_1 \partial \bar{I}_2$. $\partial^3 U/\partial \bar{I}_1 \partial J^2$. UI2(5) UI3(5) $\partial^3 U/\partial \bar{I}_2 \partial J^2$. $\partial^2 U/\partial \bar{I}_1 \partial J$. UI3(6) UI2(6) $\partial^3 U / \partial J^3$. $\partial^2 U/\partial \bar{I}_2 \partial J$.

Fully automated commercial package (Solid Mechanics, FEM)

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U(1)

U, strain energy density function. For a compressible material, at least one derivative involving J should be nonzero. For an incompressible material, all derivatives involving J will be ignored. The strain invariants— \bar{I}_1 , \bar{I}_2 , and J—are defined in Hyperelastic behavior of rubberlike materials.

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```
UI1(1)
     \partial U/\partial \bar{I}_1.
UI1(2)
     \partial U/\partial \bar{I}_{2}.
UI1(3)
     \partial U/\partial J.
UI2(1)
                                                                              UI3(1)
                                                                                   \partial^3 U/\partial \bar{I}_1^2 \partial J.
     \partial^2 U/\partial \bar{I}_1^2.
                                                                              UI3(2)
UI2(2)
                                                                                   \partial^3 U/\partial \bar{I}_2^2 \partial J.
     \partial^2 U/\partial I_2^2.
                                                                              UI3(3)
UI2(3)
                                                                                   \partial^3 U/\partial \bar{I}_1 \partial \bar{I}_2 \partial J.
     \partial^2 U/\partial J^2.
UI2(4)
                                                                              UI3(4)
     \partial^2 U/\partial \bar{I}_1 \partial \bar{I}_2.
                                                                                   \partial^3 U/\partial \bar{I}_1 \partial J^2.
UI2(5)
                                                                              UI3(5)
                                                                                   \partial^3 U/\partial \bar{I}_2 \partial J^2.
     \partial^2 U/\partial \bar{I}_1 \partial J.
                                                                              UI3(6)
UI2(6)
     \partial^2 U/\partial \bar{I}_2 \partial J.
                                                                                   \partial^3 U / \partial J^3.
```

- Fully automated commercial package (Solid Mechanics, FEM)
- ► Complex interface (too many inputs)

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                                                                                UI3(5)
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     \partial^2 U/\partial \bar{I}_1 \partial J.
                                                                                UI3(6)
UI2(6)
     \partial^2 U/\partial \bar{I} \circ \partial J.
                                                                                     \partial^3 U / \partial J^3.
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- Fully automated commercial package (Solid Mechanics, FEM)
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- ► Unstable for small deformation due to the choice of interface design

$$F = I + \nabla_X u$$

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Not easy to change the interface

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HTTPS://GITLAB.COM/MICROMORPH/RATEL

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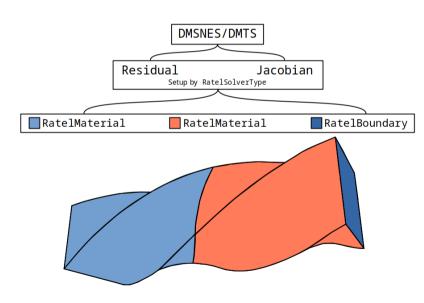
Documentation latest

coverage

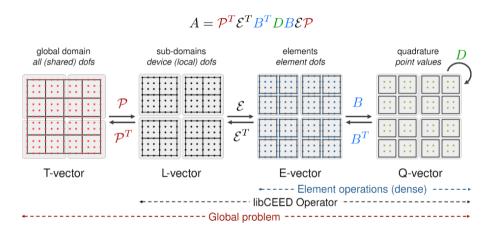
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Features:

- ► Linear elasticity
- Neo-Hookean and Mooney-Rivlin Hyperelasticity
- ► Multi-material
- ► Static, Quasistatic, Dynamic
- Initial and Current configurations



COMPOSITION AND ABSTRACTION - LIBCEED: HTTPS://LIBCEED.ORG/EN/LATEST/



- Purely algebraic high-order FEM
- ► Single source Vanilla C for physics
- ► Various CPU and GPU backends
- Backend plugins with run-time selection ./bps -ceed /gpu/cuda
- Support for Matrix-assembly and Matrix-free
- ► Operator abstraction
- User choice of data storage at quadrature point

COMPOSITION AND ABSTRACTION - PETSC AND ENZYME-AD

PETSc:

https://petsc.org/release/

- ▶ Parallel solution of PDEs
- ► CPUs (MPI)
- ► GPUs
 - CUDA
 - HIP
 - OpenCL
- ► Hybrid MPI-GPU
- ► Optimization (PETSc/Tao)

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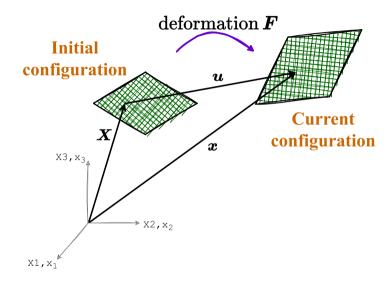
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Enzyme AD:

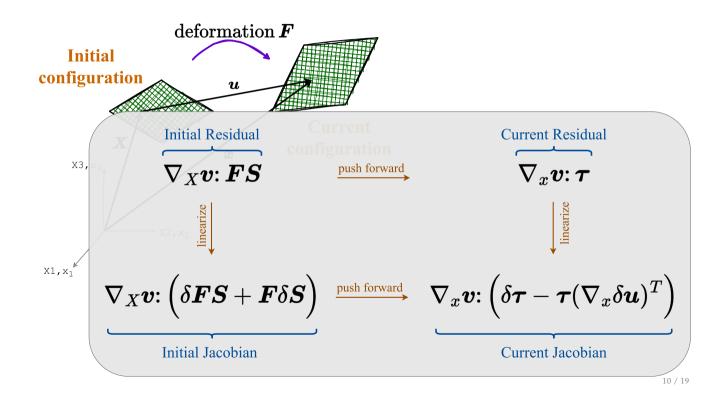
https://enzyme.mit.edu/

- ► High-Performance Automatic Differentiation
- Work at the LLVM level
- ➤ Support for variety of languages (C/C++, Julia, Rust, Fortran, etc)
- reverse and forward mode AD

INITIAL VS CURRENT CONFIGURATION



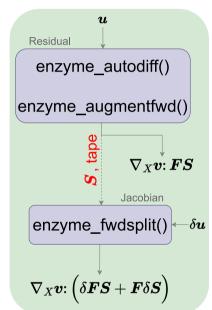
INITIAL VS CURRENT CONFIGURATION



RATEL - ENZYME AD

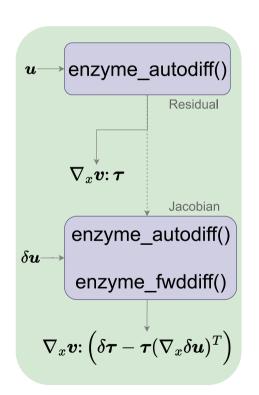
INITIAL CONFIGURATION - FORWARD SPLIT

```
//S = d(psi) / d(E) [Reverse mode]
void SecondPiolaKirchhoffStress NeoHookean AD(...) {
 __enzyme_autodiff((void *)StrainEnergy, ...);
// Call forward S and return tape
__enzyme_augmentfwd(
(void *) SecondPiolaKirchhoffStress NeoHookean AD,
enzyme_allocated, tape_bytes, enzyme_tape, tape,
enzyme nofree, ...);
// Compute dS using the stored tape [Forward-split]
enzyme fwdsplit(
(void *) SecondPiolaKirchhoffStress NeoHookean AD,
enzyme allocated, tape bytes, enzyme tape, tape, ...);
```



RATEL - ENZYME AD

CURRENT CONFIGURATION - REVERSE AND FORWARD

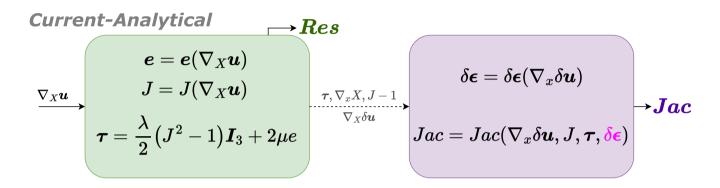


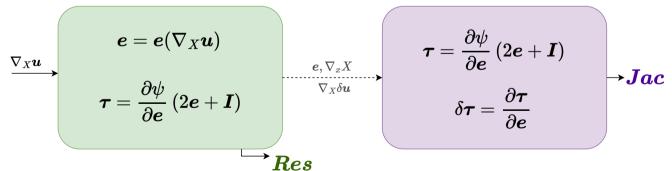
```
// Compute tau = (dPsi / de) * (2 e + I) [Reverse]
void Kirchhofftau Voigt NeoHookean AD(...) {
 enzyme autodiff((void *)StrainEnergy, ...);
  for (int j = 0; j < 6; j++)
   b Voigt[j] = 2 * e Voigt[j] + (j < 3);
 RatelMatMatMult(1., dPsi, b, tau);
// Compute dtau [Forward]
CEED OFUNCTION HELPER void dtau fwd(...) {
 __enzyme_fwddiff(
  (void *) Kirchhofftau Voigt NeoHookean AD, ...);
```

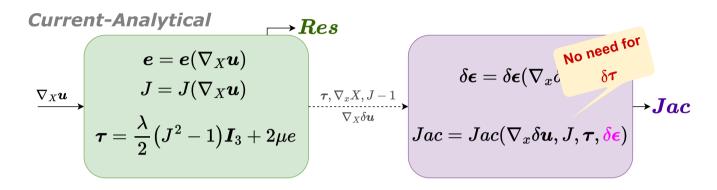
RATEL - ENZYME AD

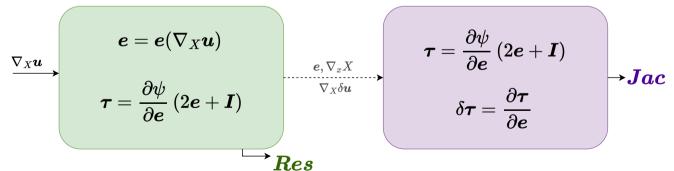
PERFORMANCE FOR DIFFERENT JACOBIAN REPRESENTATIONS

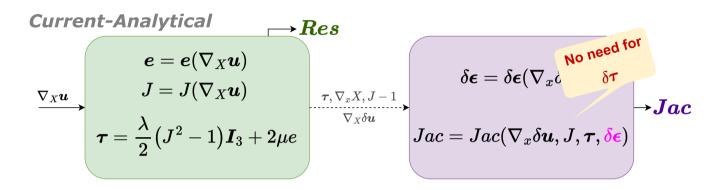
| Problem | Storage | Scalars | Time (s) |
|------------|--|---------|----------|
| current | $W; \nabla_x \boldsymbol{\xi}, \boldsymbol{	au}, J-1$ | 17 | 36.2 |
| initial | $W, \nabla_X \boldsymbol{\xi}; \nabla_X \boldsymbol{u}$ | 19 | 48.4 |
| initial-AD | $W, abla_X oldsymbol{\xi}; abla_X oldsymbol{u}, S, 	exttt{tape}$ | 31 | 53.9 |
| current-AD | $W; \nabla_x \boldsymbol{\xi}, \boldsymbol{e}$ | 16 | 55.8 |

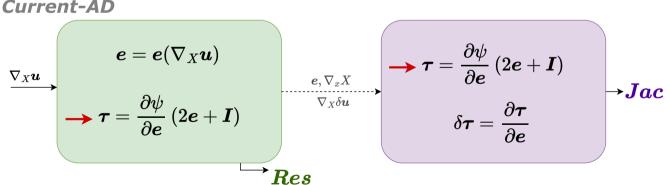


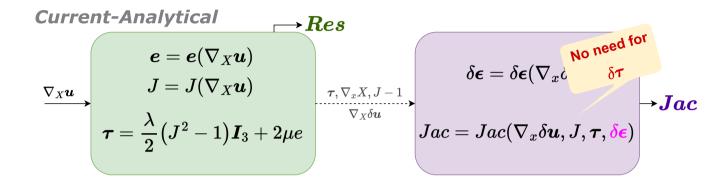


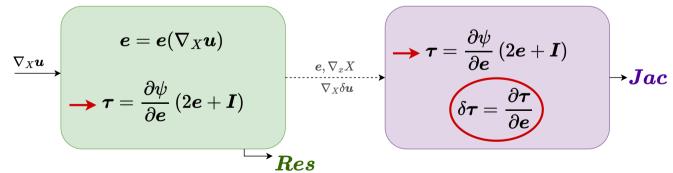


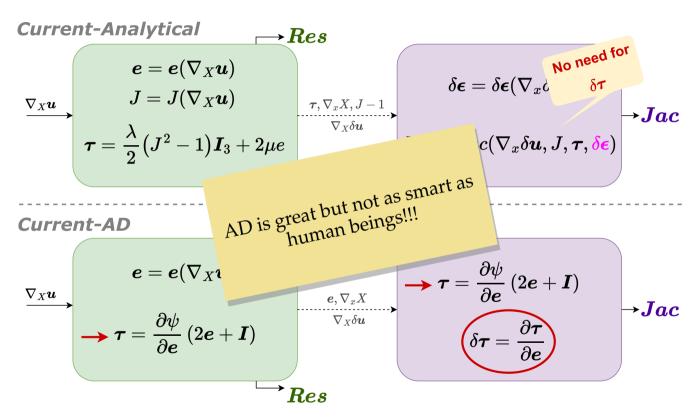












► Enzyme-aware clangd

This material is based upon work supported by the U.S. Department of Energy, Office of Science, Office of Advanced Scientific Computing Research under Award Number DE-SC0016140.

- ► Enzyme-aware clangd
- ► Compile code with -00

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- ► Enzyme-aware clangd
- ► Compile code with -00
- Calling Enzyme in a debugger

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- ► Compile code with -00
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- Internal cancellation of tensor operations

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- ► Enzyme-aware clangd
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$$d(oldsymbol{A}oldsymbol{A}^{-1})=d(oldsymbol{I})=oldsymbol{0}$$

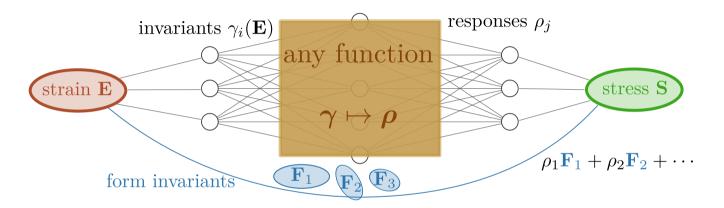


$$d(\boldsymbol{A}\boldsymbol{A}^{-1}) = d(\boldsymbol{A})\boldsymbol{A}^{-1} + \boldsymbol{A}d(\boldsymbol{A}^{-1})$$

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OUTLOOK

TOWARDS PLASTICITY



$$\begin{aligned} \text{Input Scalar Functions} &= \begin{cases} \psi(\textbf{\textit{E}}; \mathbb{I}) & \leftarrow \text{ free energy} \\ \phi(\textbf{\textit{S}}; \mathbb{I}) & \leftarrow \text{ dissipation potential} \\ f(\textbf{\textit{S}}; \mathbb{I}) & \leftarrow \text{ yield surface} \end{cases}$$