# FORWARD-MODE ENZYME IN DEVELOPING CONSTITUTIVE MODELS WITH RATEL

## Leila Ghaffari, William Moses, Jeremy L Thompson, Karen Stengel, Rezgar Shakeri, and Jed Brown

Department of Computer Science University of Colorado Boulder

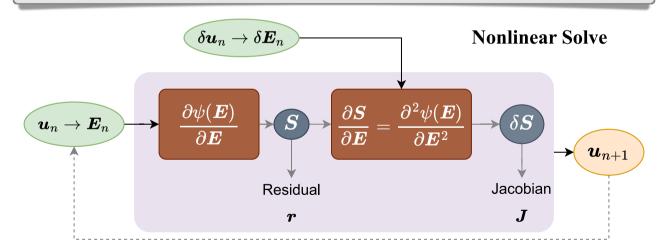
> SIAM CSE23 Feb 28, 2023

FREE ENERGY FUNCTIONAL AND PDE SOLVERS

$$\psi\left(\mathbf{E}\right) = \frac{\lambda}{4} \left(J^2 - 1 - 2\log J\right) - \mu\left(\log J + \operatorname{trace}\mathbf{E}\right), \ J = \sqrt{|\mathbf{I} + 2\mathbf{E}|}$$

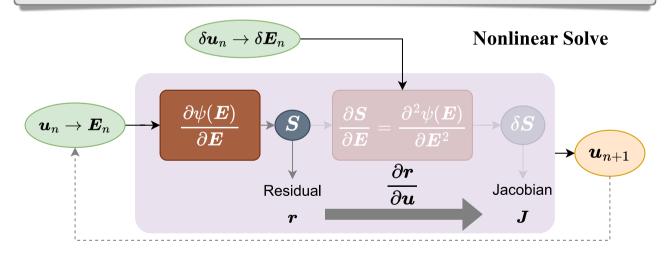
FREE ENERGY FUNCTIONAL AND PDE SOLVERS

$$\psi\left(\mathbf{\textit{E}}\right) = \frac{\lambda}{4}\left(J^2 - 1 - 2\log J\right) - \mu\left(\log J + \operatorname{trace}\mathbf{\textit{E}}\right), \ J = \sqrt{|\mathbf{\textit{I}} + 2\mathbf{\textit{E}}|}$$



FREE ENERGY FUNCTIONAL AND PDE SOLVERS

$$\psi\left(\mathbf{\textit{E}}\right) = \frac{\lambda}{4} \left(J^2 - 1 - 2\log J\right) - \mu\left(\log J + \operatorname{trace}\mathbf{\textit{E}}\right), \ J = \sqrt{|\mathbf{\textit{I}} + 2\mathbf{\textit{E}}|}$$

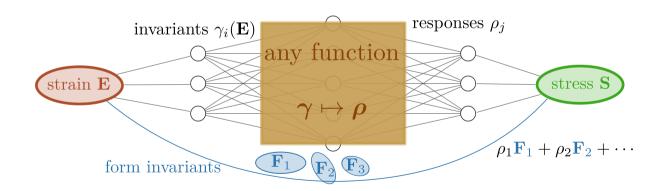


FREE ENERGY FUNCTIONAL AND INVERSE PROBLEMS

$$\psi(\mathbf{E}) = \frac{\lambda}{4} \left( J^2 - 1 - 2 \log J \right) - \mu \left( \log J + \operatorname{trace} \mathbf{E} \right), \ J = \sqrt{|\mathbf{I} + 2\mathbf{E}|}$$

FREE ENERGY FUNCTIONAL AND INVERSE PROBLEMS

$$\psi\left(\mathbf{E}\right) = \frac{\lambda}{4} \left(J^2 - 1 - 2\log J\right) - \mu\left(\log J + \operatorname{trace}\mathbf{E}\right), \ J = \sqrt{|\mathbf{I} + 2\mathbf{E}|}$$



#### **UHYPER: USER SUBROUTINE**

#### Variables to be defined U(1) U. strain energy density function. For a compressible material, at least one derivative involving J should be nonzero. For an incompressible material, all derivatives involving J will be ignored. The strain invariants— $\bar{I}_1$ , $\bar{I}_2$ , and J—are defined in Hyperelastic behavior of rubberlike materials. U(2) $\widetilde{U}_{dev}$ , the deviatoric part of the strain energy density of the primary material response. This quantity is needed only if the current material definition also includes Mullins effect (see Mullins effect). UI1(1) $\partial U/\partial \bar{I}_1$ . UI1(2) $\partial U/\partial \bar{I}_{2}$ . UI1(3) $\partial U/\partial J$ . UI3(1) UI2(1) $\partial^2 U/\partial \bar{I}_1^2$ . $\partial^3 U/\partial {ar{I}_1}^2 \partial J.$ UI3(2) UI2(2) $\partial^3 U/\partial \bar{I}_2^2 \partial J$ . $\partial^2 U/\partial \bar{I}_2^2$ . UI2(3) UI3(3) $\partial^3 U/\partial \bar{I}_1 \partial \bar{I}_2 \partial J$ . $\partial^2 U/\partial J^2$ . UI2(4) UI3(4) $\partial^2 U/\partial \bar{I}_1 \partial \bar{I}_2$ . $\partial^3 U/\partial \bar{I}_1 \partial J^2$ . UI2(5) UI3(5) $\partial^3 U/\partial \bar{I}_2 \partial J^2$ . $\partial^2 U/\partial \bar{I}_1 \partial J$ . UI3(6) UI2(6) $\partial^3 U / \partial J^3$ . $\partial^2 U/\partial \bar{I}_2 \partial J$ .

Fully automated commercial package (Solid Mechanics, FEM)

#### **UHYPER: USER SUBROUTINE**

#### Variables to be defined

U(1)

U, strain energy density function. For a compressible material, at least one derivative involving J should be nonzero. For an incompressible material, all derivatives involving J will be ignored. The strain invariants— $\bar{I}_1$ ,  $\bar{I}_2$ , and J—are defined in Hyperelastic behavior of rubberlike materials.

U(2)

 $\hat{U}_{dev}$ , the deviatoric part of the strain energy density of the primary material response. This quantity is needed only if the current material definition also includes Mullins effect (see Mullins effect).

```
UI1(1)
     \partial U/\partial \bar{I}_1.
UI1(2)
     \partial U/\partial \bar{I}_{2}.
UI1(3)
     \partial U/\partial J.
UI2(1)
                                                                              UI3(1)
                                                                                   \partial^3 U/\partial \bar{I}_1^2 \partial J.
     \partial^2 U/\partial \bar{I}_1^2.
                                                                              UI3(2)
UI2(2)
                                                                                   \partial^3 U/\partial \bar{I}_2^2 \partial J.
     \partial^2 U/\partial I_2^2.
                                                                              UI3(3)
UI2(3)
                                                                                   \partial^3 U/\partial \bar{I}_1 \partial \bar{I}_2 \partial J.
     \partial^2 U/\partial J^2.
UI2(4)
                                                                              UI3(4)
     \partial^2 U/\partial \bar{I}_1 \partial \bar{I}_2.
                                                                                   \partial^3 U/\partial \bar{I}_1 \partial J^2.
UI2(5)
                                                                              UI3(5)
                                                                                   \partial^3 U/\partial \bar{I}_2 \partial J^2.
     \partial^2 U/\partial \bar{I}_1 \partial J.
                                                                              UI3(6)
UI2(6)
     \partial^2 U/\partial \bar{I}_2 \partial J.
                                                                                   \partial^3 U / \partial J^3.
```

- Fully automated commercial package (Solid Mechanics, FEM)
- ► Complex interface (too many inputs)

#### **UHYPER: USER SUBROUTINE**

#### Variables to be defined

U(1)

U, strain energy density function. For a compressible material, at least one derivative involving J should be nonzero. For an incompressible material, all derivatives involving J will be ignored. The strain invariants— $\bar{I}_1, \bar{I}_2$ , and J—are defined in Hyperelastic behavior of rubberlike materials.

U(2)

 $\hat{U}_{dev}$ , the deviatoric part of the strain energy density of the primary material response. This quantity is needed only if the current material definition also includes Mullins effect (see Mullins effect).

```
UI1(1)
     \partial U/\partial \bar{I}_1.
UI1(2)
     \partial U/\partial \bar{I}_{2}.
UI1(3)
     \partial U/\partial J.
UI2(1)
                                                                                UI3(1)
                                                                                     \partial^3 U/\partial \bar{I}_1^2 \partial J.
     \partial^2 U/\partial \bar{I}_1^2.
                                                                                UI3(2)
UI2(2)
                                                                                     \partial^3 U/\partial \bar{I}_2^2 \partial J.
     \partial^2 U/\partial I_2^2.
UI2(3)
                                                                                     \partial^3 U/\partial \bar{I}_1 \partial \bar{I}_2 \partial J.
     \partial^2 U/\partial J^2.
UI2(4)
                                                                                UI3(4)
                                                                                     \partial^3 U/\partial \bar{I}_1 \partial J^2.
     \partial^2 U/\partial \bar{I}_1 \partial \bar{I}_2.
UI2(5)
                                                                                UI3(5)
                                                                                     \partial^3 U/\partial \bar{I}_2 \partial J^2.
     \partial^2 U/\partial \bar{I}_1 \partial J.
                                                                                UI3(6)
UI2(6)
     \partial^2 U/\partial \bar{I} \circ \partial J.
                                                                                     \partial^3 U / \partial J^3.
```

- Fully automated commercial package (Solid Mechanics, FEM)
- Complex interface (too many inputs)
- ► Unstable for small deformation due to the choice of interface design

$$F = I + \nabla_X u$$

#### **UHYPER: USER SUBROUTINE**

#### Variables to be defined

U(1)

U, strain energy density function. For a compressible material, at least one derivative involving J should be nonzero. For an incompressible material, all derivatives involving J will be ignored. The strain invariants— $\bar{I}_1, \bar{I}_2$ , and J—are defined in Hyperelastic behavior of rubberlike materials.

U(2)

 $\hat{U}_{dev}$ , the deviatoric part of the strain energy density of the primary material response. This quantity is needed only if the current material definition also includes Mullins effect (see Mullins effect).

```
UI1(1)
     \partial U/\partial \bar{I}_1.
UI1(2)
     \partial U/\partial \bar{I}_{2}.
UI1(3)
      \partial U/\partial J.
UI2(1)
                                                                                UI3(1)
                                                                                     \partial^3 U/\partial \bar{I}_1^2 \partial J.
     \partial^2 U/\partial \bar{I}_1^2.
                                                                                UI3(2)
UI2(2)
                                                                                     \partial^3 U/\partial \bar{I}_2^2 \partial J.
     \partial^2 U/\partial I_2^2.
                                                                                UI3(3)
UI2(3)
                                                                                     \partial^3 U/\partial \bar{I}_1 \partial \bar{I}_2 \partial J.
     \partial^2 U/\partial J^2.
UI2(4)
                                                                                UI3(4)
                                                                                     \partial^3 U/\partial \bar{I}_1 \partial J^2.
     \partial^2 U/\partial \bar{I}_1 \partial \bar{I}_2.
UI2(5)
                                                                                UI3(5)
                                                                                     \partial^3 U/\partial \bar{I}_2 \partial J^2.
     \partial^2 U/\partial \bar{I}_1 \partial J.
                                                                                UI3(6)
UI2(6)
     \partial^2 U/\partial \bar{I} \circ \partial J.
                                                                                     \partial^3 U / \partial J^3.
```

- Fully automated commercial package (Solid Mechanics, FEM)
- Complex interface (too many inputs)
- ► Unstable for small deformation due to the choice of interface design

$$F = I + \nabla_X u$$

Not easy to change the interface

#### **UHYPER:** USER SUBROUTINE

#### Variables to be defined U(1) U. strain energy density function. For a compressible material, at least one derivative involving J should be nonzero. For an incompressible material, all derivatives involving J will be ignored. The strain invariants— $\bar{I}_1$ , $\bar{I}_2$ , and J—are defined in Hyperelastic behavior of rubberlike U(2) $\widetilde{U}_{dev}$ , the deviatoric part of the strain energy density of the primary material response. This quantity is needed only if the current material definition also includes Mullins effect (see Mullins effect). UI1(1) $\partial U/\partial \bar{I}_1$ . AD helps us to create a more generic interface UI1(2) $\partial U/\partial \bar{I}_{2}$ . UI1(3) (one input function, $\psi(E)$ ). $\partial U/\partial J$ . UI3 UI2(1) $\partial^2 U/\partial \bar{I}_1^2$ . UI3(2 UI2(2) $\partial^2 U/\partial \bar{I}_2^2$ . $\partial^3$ UI3(3) UI2(3) $\partial^3 U$ $\partial^2 U/\partial J^2$ . UI2(4) UI3(4) $\partial^3 U/\partial \bar{I}_1 \partial J^2$ . $\partial^2 U/\partial \bar{I}_1 \partial \bar{I}_2$ . UI2(5) UI3(5) $\partial^3 U/\partial \bar{I}_2 \partial J^2$ . $\partial^2 U/\partial \bar{I}_1 \partial J$ . UI3(6) UI2(6) $\partial^2 U/\partial \bar{I} \circ \partial J$ . $\partial^3 U / \partial J^3$ .

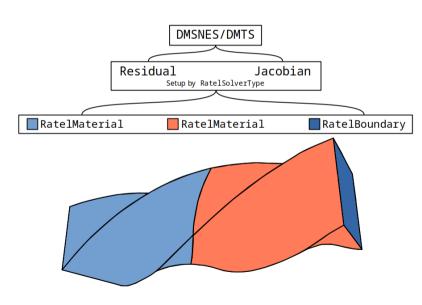
- Fully automated commercial package (Solid Mechanics, FEM)
- Complex interface many inputs) able for small mation due to the of interface design  $= I + \nabla_x u$
- Not easy to change the interface

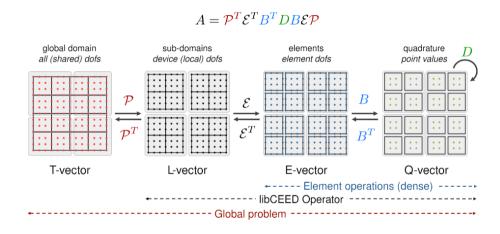
HTTPS://GITLAB.COM/MICROMORPH/RATEL

GitLab-Cl passed License BSD 2-Clause Documentation latest coverage 96.05%

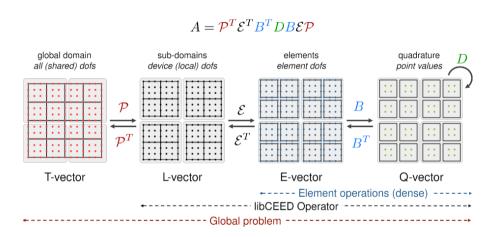
#### **Features:**

- Linear elasticity
- Neo-Hookean and Mooney-Rivlin Hyperelasticity
- ► Multi-material
- ► Static, Quasistatic, Dynamic
- Initial and Current configurations

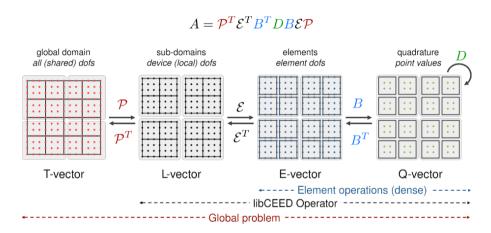




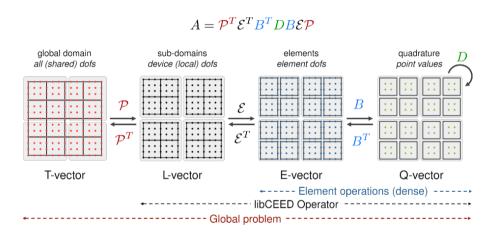
COMPOSITION AND ABSTRACTION - LIBCEED: HTTPS://LIBCEED.ORG/EN/LATEST/



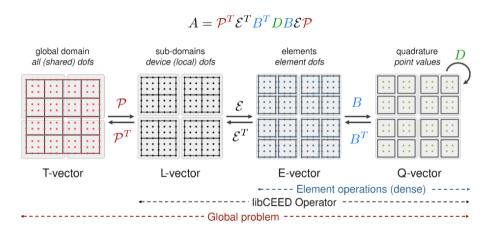
► Purely algebraic high-order FEM



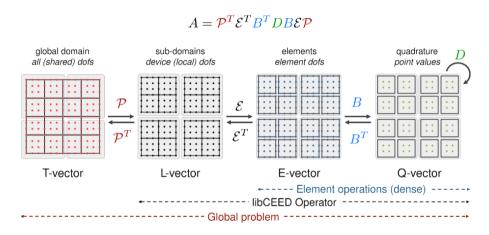
- ► Purely algebraic high-order FEM
- ► Single source Vanilla C for physics



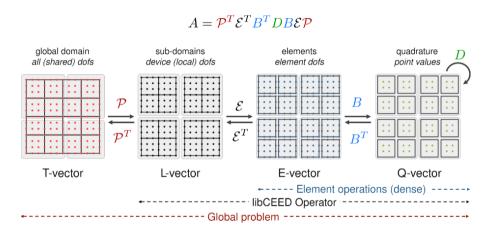
- ► Purely algebraic high-order FEM
- ► Single source Vanilla C for physics
- ► Various CPU and GPU backends



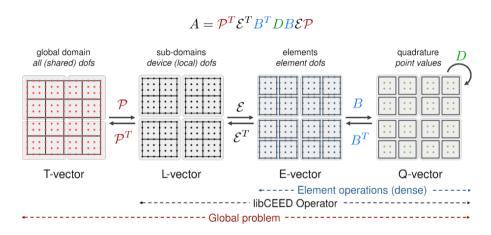
- ► Purely algebraic high-order FEM
- ► Single source Vanilla C for physics
- Various CPU and GPU backends
- Backend plugins with run-time selection ./bps -ceed /gpu/cuda



- ► Purely algebraic high-order FEM
- ► Single source Vanilla C for physics
- ▶ Various CPU and GPU backends
- ► Backend plugins with run-time selection ./bps -ceed /gpu/cuda
- Support for Matrix-assembly and Matrix-free



- Purely algebraic high-order FEM
- ► Single source Vanilla C for physics
- ► Various CPU and GPU backends
- Backend plugins with run-time selection ./bps -ceed /gpu/cuda
- Support for Matrix-assembly and Matrix-free
- Operator abstraction



- Purely algebraic high-order FEM
- ► Single source Vanilla C for physics
- ► Various CPU and GPU backends
- ► Backend plugins with run-time selection ./bps -ceed /gpu/cuda
- Support for Matrix-assembly and Matrix-free
- ► Operator abstraction
- User choice of data storage at quadrature point

COMPOSITION AND ABSTRACTION - PETSC

#### **PETSc:**

https://petsc.org/release/

► Parallel solution of PDEs

COMPOSITION AND ABSTRACTION - PETSC

#### **PETSc:**

- ► Parallel solution of PDEs
- ► CPUs (MPI)

COMPOSITION AND ABSTRACTION - PETSC

#### **PETSc:**

- ► Parallel solution of PDEs
- ► CPUs (MPI)
- ► GPUs (CUDA, HIP, and OpenCL)

COMPOSITION AND ABSTRACTION - PETSC

#### **PETSc:**

- ► Parallel solution of PDEs
- ► CPUs (MPI)
- ► GPUs (CUDA, HIP, and OpenCL)
- ► Hybrid MPI-GPU

COMPOSITION AND ABSTRACTION - PETSC

#### **PETSc:**

- ► Parallel solution of PDEs
- ► CPUs (MPI)
- ► GPUs (CUDA, HIP, and OpenCL)
- ► Hybrid MPI-GPU
- ► Optimization (PETSc/Tao)

COMPOSITION AND ABSTRACTION - ENZYME AD

# **Enzyme AD:**

https://enzyme.mit.edu/

► High-Performance Automatic Differentiation

COMPOSITION AND ABSTRACTION - ENZYME AD

# **Enzyme AD:**

https://enzyme.mit.edu/

- ► High-Performance Automatic Differentiation
- ► Work at the LLVM level

COMPOSITION AND ABSTRACTION - ENZYME AD

# **Enzyme AD:**

https://enzyme.mit.edu/

- ► High-Performance Automatic Differentiation
- ► Work at the LLVM level
- ► Support for variety of languages (C/C++, Julia, Rust, Fortran, etc)

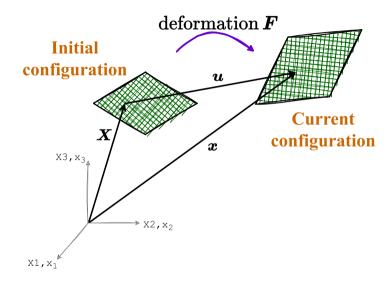
COMPOSITION AND ABSTRACTION - ENZYME AD

# **Enzyme AD:**

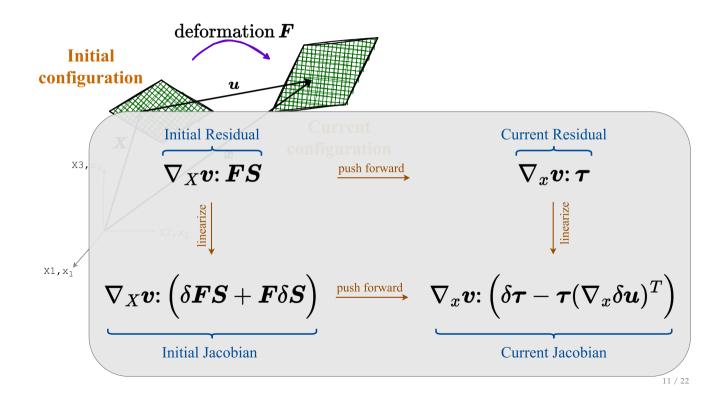
https://enzyme.mit.edu/

- ► High-Performance Automatic Differentiation
- ► Work at the LLVM level
- ► Support for variety of languages (C/C++, Julia, Rust, Fortran, etc)
- ► reverse and forward mode AD

# INITIAL VS CURRENT CONFIGURATION



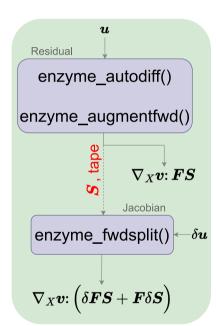
#### INITIAL VS CURRENT CONFIGURATION



#### RATEL - ENZYME AD

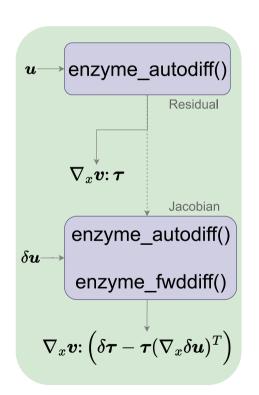
INITIAL CONFIGURATION - REVERSE AND FORWARD SPLIT

```
//S = d(psi) / d(E) [Reverse mode]
void SecondPiolaKirchhoffStress NeoHookean AD(...) {
 __enzyme_autodiff((void *)StrainEnergy, ...);
// Call forward S and return tape
__enzyme_augmentfwd(
(void *) SecondPiolaKirchhoffStress NeoHookean AD,
enzyme allocated, tape bytes, enzyme tape, tape,
enzyme nofree, ...);
// Compute dS using the stored tape [Forward-split]
enzyme fwdsplit(
(void *) SecondPiolaKirchhoffStress NeoHookean AD,
enzyme allocated, tape bytes, enzyme tape, tape, ...);
```



#### RATEL - ENZYME AD

#### CURRENT CONFIGURATION - REVERSE AND FORWARD

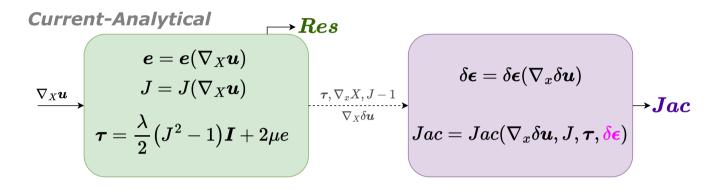


```
// Compute tau = (dPsi / de) * (2 e + I) [Reverse]
void Kirchhofftau Voigt NeoHookean AD(...) {
 enzyme autodiff((void *)StrainEnergy, ...);
  for (int j = 0; j < 6; j++)
   b Voigt[j] = 2 * e Voigt[j] + (j < 3);
 RatelMatMatMult(1., dPsi, b, tau);
// Compute dtau [Forward]
CEED OFUNCTION HELPER void dtau fwd(...) {
 __enzyme_fwddiff(
  (void *) Kirchhofftau Voigt NeoHookean AD, ...);
```

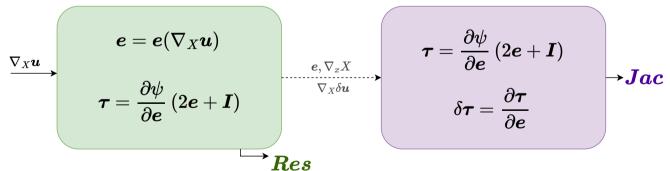
# RATEL - ENZYME AD

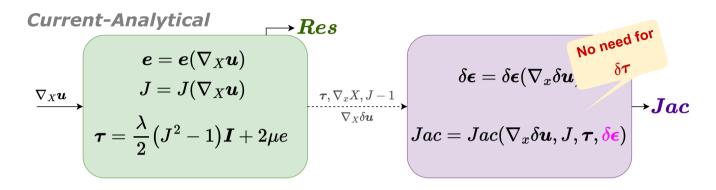
#### PERFORMANCE FOR DIFFERENT JACOBIAN REPRESENTATIONS

Problem	Storage	Scalars	Time (s)
current	$W; \nabla_x \boldsymbol{\xi}, \boldsymbol{ au}, J-1$	17	36.2
initial	$W, \nabla_X \boldsymbol{\xi}; \nabla_X \boldsymbol{u}$	19	48.4
initial-AD	$W,  abla_X oldsymbol{\xi};  abla_X oldsymbol{u}, S,  exttt{tape}$	31	53.9
current-AD	$W; \nabla_x \boldsymbol{\xi}, \boldsymbol{e}$	16	55.8

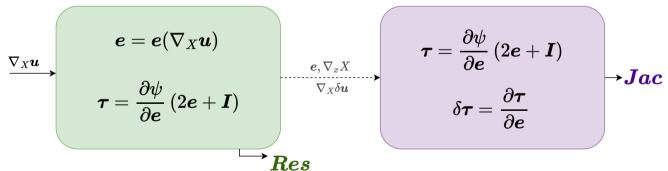


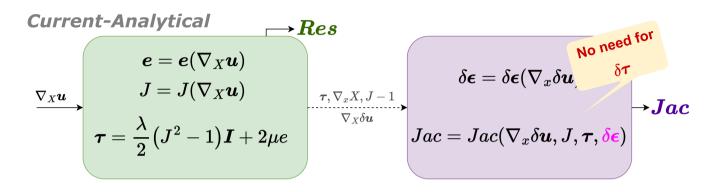
## Current-AD



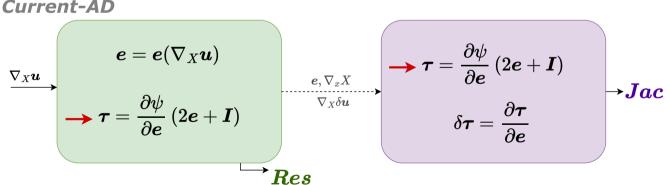


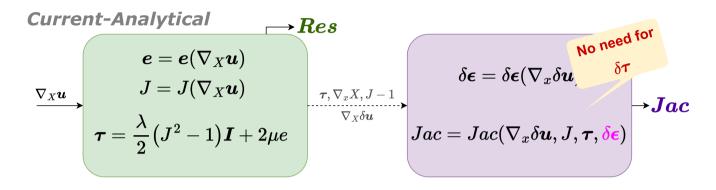
## Current-AD



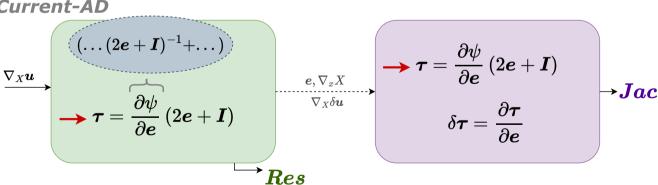


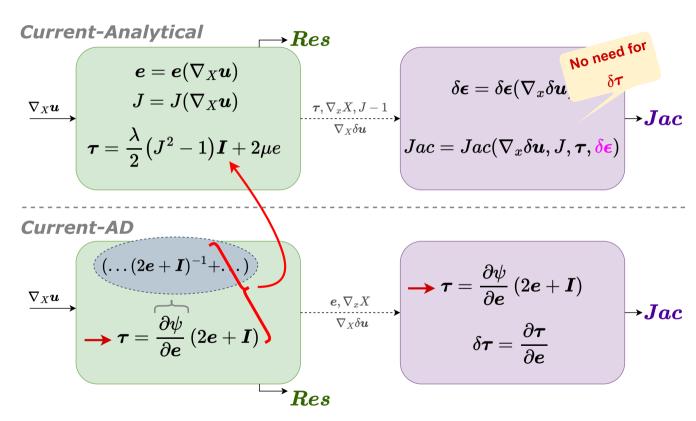
## Current-AD

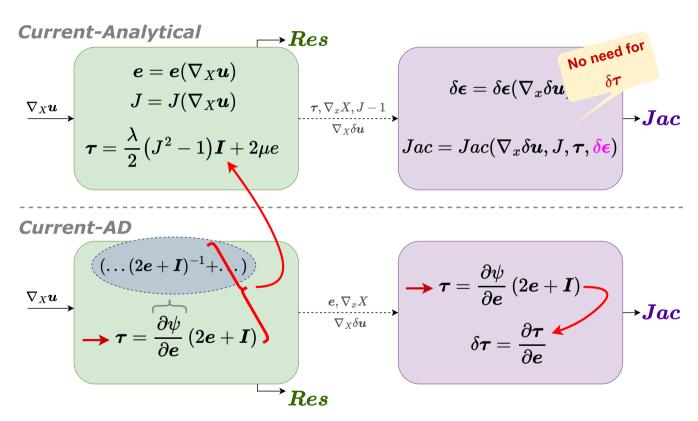


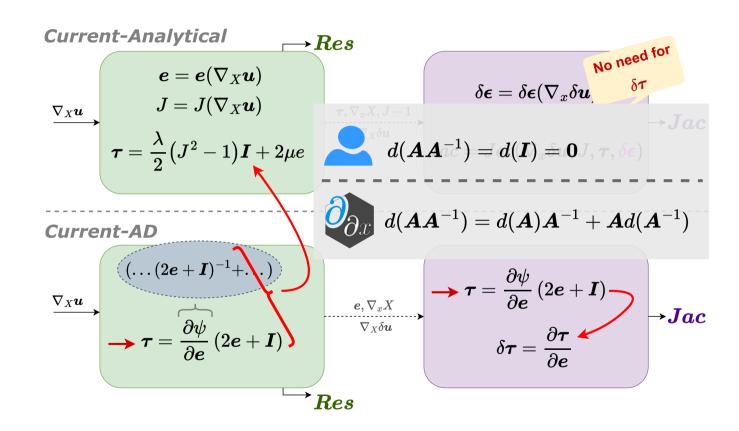


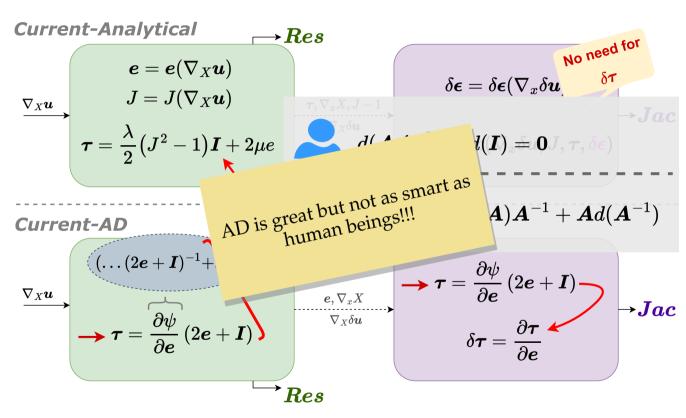












# OUTLOOK

#### TOWARDS PLASTICITY

Input Scalar Functions = 
$$\begin{cases} \psi(E; \mathbb{I}) & \leftarrow \text{ free energy} \\ \phi(S; \mathbb{I}) & \leftarrow \text{ dissipation potential} \\ f(S; \mathbb{I}) & \leftarrow \text{ yield surface} \end{cases}$$

This material is based upon work supported by the U.S. Department of Energy, Office of Science, Office of Advanced Scientific Computing Research under Award Number DE-SC0016140.

Registration and travel support for this presentation was provided by the Society for Industrial and Applied Mathematics.