Dinámica no lineal aplicada a un láser

Mode-mode competition and unstable behavior in a homogeneously broadened ring laser, L. M. Narducci, J.R. Tredicce, L. A. Lugiato, N. B.Abraham and D. K. Bandy.

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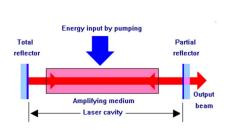
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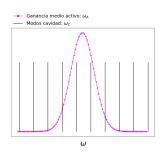
Cambio de variables $\begin{array}{l} \text{Descomposición modal} \rightarrow \text{ecuaciones para amplitudes} \\ \text{Linealizacion} + \text{Ansatz} \rightarrow \text{sistema matricial} \\ \text{Gráficos} \end{array}$

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Cavidad de un láser



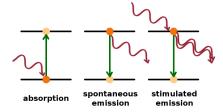
- Bombeo óptico
- Medio activo: aumentar la intensidad del láser



- ω_C : modos permitidos de la cavidad $(2\pi cn/\mathcal{L})$
- ω_A: linea atómica del medio activo → amplificación

Sistema de 2 niveles: Transiciones atómicas

- Absorción : $1 \rightarrow 2$
- ullet Emisión espontánea : 2 o 1
- Emisión estimulada : $2 \rightarrow 1$



Con la emisión de fotones se aumenta la intensidad del láser

Sistema de ecuaciones

 γ_{\parallel} tasa inversión de población

k pérdidas de fotones

g coef. de prop. asociado a emisión estimulada y absorción

$$\bullet \frac{dI}{dt} = -kI + gIN_2 - gIN_1$$

$$\bullet \frac{dN_1}{dt} = \gamma_{\parallel} N_{o1} - gIN_1 + gIN_2 - \gamma_{\parallel} N_1$$

•
$$\frac{dN_2}{dt} = \underbrace{\gamma_{\parallel} N_{o2}}_{\text{bombeo absorción}} \underbrace{+gIN_1}_{\text{emisión}} \underbrace{-gIN_2}_{\text{emisión estimulada espontánea}} \underbrace{-\gamma_{\parallel} N_2}_{\text{emisión estimulada espontánea}}$$

Simplificar ecuaciones

1. Cambio de variable: $N = N_2 - N_1$

$$\bullet \frac{dN}{dt} = \gamma_{\parallel} N_o - 2gIN - \gamma_{\parallel} N \quad \bullet \frac{dI}{dt} = -kI + gIN = I(-k + gN)$$

- 2. Adimensionalizar: $\tilde{t} = \gamma_{\parallel} t$, $\tilde{k} = k/\gamma_{\parallel}$, $\tilde{g} = gN_{o}/\gamma_{\parallel}$
- 3. Normalizar: $\tilde{N} = N/N_o, \tilde{I} = I/N_o, A = \tilde{g}/\tilde{k}$

Simplificar ecuaciones

- 1. Cambio de variable: $N = N_2 N_1$
- 2. Adimensionalizar: $\tilde{t} = \gamma_{\parallel} t$, $\tilde{k} = k/\gamma_{\parallel}$, $\tilde{g} = gN_o/\gamma_{\parallel}$

$$\bullet \frac{dN}{d\tilde{t}} = N_o - 2\frac{\tilde{g}}{N_o}IN - N \qquad \bullet \frac{dI}{d\tilde{t}} = I\left(-\tilde{k} + \frac{\tilde{g}}{N_o}N\right)$$

3. <u>Normalizar</u>: $\tilde{N} = N/N_o$, $\tilde{I} = I/N_o$, $A = \tilde{g}/\tilde{k}$

$$oxed{rac{d ilde{N}}{d ilde{t}}} = 1 - 2 ilde{g} ilde{I} ilde{N} - ilde{N} \qquad rac{d ilde{I}}{d ilde{t}} = ilde{I} ilde{g}(-1/A + ilde{N})$$

Análisis de estabilidad lineal

Puntos fijos:

$$\tilde{N}_{pf}^{(1)} = 1$$
 $\tilde{l}_{pf}^{(1)} = 0$ $\tilde{N}_{pf}^{(2)} = 1/A$ $\tilde{l}_{pf}^{(2)} = \frac{1}{2\tilde{g}}(A-1)$

<u>Jacobiano del sistema</u>:

$$DF = \begin{bmatrix} \frac{\partial \dot{\tilde{N}}}{\partial \tilde{N}} & \frac{\partial \dot{\tilde{N}}}{\partial \tilde{I}} \\ \\ \frac{\partial \ddot{\tilde{I}}}{\partial \tilde{N}} & \frac{\partial \ddot{\tilde{I}}}{\partial \tilde{I}} \end{bmatrix} = \begin{bmatrix} -2\tilde{g}\tilde{I} - 1 & -2\tilde{g}\tilde{N} \\ \\ \tilde{g}\tilde{I} & \tilde{g}(-1/A + \tilde{N}) \end{bmatrix}$$

Análisis de estabilidad lineal: Estabilidad de puntos fijos

$$\bullet \ \lambda_1^{(1)} = -1$$

$$\implies |\vec{x}_{PF}^{(1)}|$$
 estable si $A < 1$

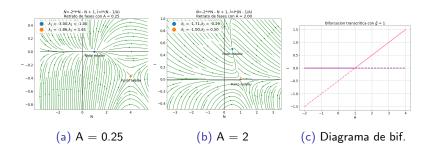
$$\bullet \ \lambda_2^{(1)} = \tilde{g}(1 - 1/A)$$

$$\mathrm{o}\ \lambda_1^{(2)} = -rac{\mathcal{A}}{2} + \sqrt{\left(rac{\mathcal{A}}{2}
ight)^2 - ilde{g}(1-1/\mathcal{A})}$$

$$\Rightarrow \vec{x}_{PF}^{(2)}$$
 estable si $A > 1$

$$\mathrm{o}\ \lambda_2^{(2)} = -rac{A}{2} - \sqrt{\left(rac{A}{2}
ight)^2 - ilde{g}(1-1/A)}$$

Bifurcación transcrítica + diagramas de flujos



Transcrítica:

Cambio en la estabilidad de los puntos fijos al variar el parámetro

Formalismo de Maxwell-Bloch

Aproximación slowly varying complex amplitude para el campo eléctrico, se desprecian los campos transversales y $\sigma=0$

$$E(z,t) = \mathscr{E}(z,t)e^{i(kz-\omega t)} + \text{c.c}$$

$$\mathscr{F}(z,t) \equiv \mu \mathscr{E}(z,t)/[2\hbar(\gamma_{\perp}\gamma_{\parallel})^{1/2}]$$

$$\mathscr{P}(z,t) o \mathsf{Polarizaci\'{o}}$$
n compleja por átomo

$$\mathscr{D}(z,t) o \mathsf{Diferencia}$$
 de prob. entre el excitado y el fundamental

$$\gamma_{\perp}$$
 tasa de polarización

 $\gamma_{||}$ tasa de inversión de población

 ${\mathscr L}$ longitud de la cavidad

L longitud del medio activo

Formalismo de Maxwell-Bloch

Las ecuaciones de Maxwell-Bloch son:

•
$$\frac{\partial \mathscr{F}}{\partial z} + \frac{1}{c} \frac{\partial \mathscr{F}}{\partial t} = -\alpha \mathscr{P}$$
 α : ganancia/long. $\rightarrow \boxed{\alpha L}$

•
$$\frac{\partial \mathscr{P}}{\partial t} = \gamma_{\perp} [\mathscr{F} \mathscr{D} - (1 + \tilde{\delta}_{AC}) \mathscr{P}]$$
 $\left[\tilde{\delta}_{AC} = (\omega_A - \omega_C) / \gamma_{\perp} \right]$

$$\bullet \frac{\partial \mathscr{D}}{\partial t} = -\gamma_{\parallel} \left[\frac{1}{2} (\mathscr{F}^* \mathscr{P} + \mathscr{F} \mathscr{P}^*) + \mathscr{D} + 1 \right]$$

$$\underline{CC}$$
: $\mathscr{F}(z=0,t) = R\mathscr{F}(z=L,t-(\mathscr{L}-L)/c)$

Solución estacionaria + coordenadas polares

$$\mathscr{F}(z,t) = \mathscr{F}(z)_{st}e^{-i\delta\omega t}$$

 $\mathscr{P}(z,t) = \mathscr{P}(z)_{st}e^{-i\delta\omega t}$
 $\mathscr{D}(z,t) = \mathscr{D}(z)_{st}$

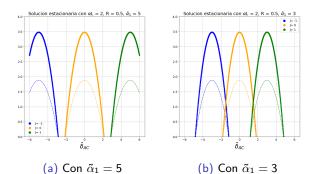
$$\mathscr{F}_{st}(z) = \rho(z)e^{i\theta(z)} \Rightarrow \frac{d\mathscr{F}_{st}}{dz} - \frac{i\delta\omega}{c}\mathscr{F}_{st} = \alpha\mathscr{F}_{st}(z)\frac{1 - i\tilde{\Delta}}{1 + \tilde{\Delta}^2 + |\mathscr{F}_{st}(z)|^2}$$
 CC de $\theta \Rightarrow 2\pi i$

$$\tilde{\Delta}_{j} = \tilde{\delta}_{AC} - \delta\omega_{j}/\gamma_{\perp} \quad \frac{\delta\omega_{j}}{\gamma_{\perp}} = \frac{\tilde{k}\tilde{\delta}_{AC} + j\tilde{\alpha}_{1}}{1 + \tilde{k}} \quad \boxed{\tilde{\alpha}_{1} = \frac{2\pi c}{\mathscr{L}\gamma_{\perp}}} \quad \tilde{k} = \frac{c|\ln R|}{\mathscr{L}\gamma_{\perp}}$$

Estados estacionarios

$$\rho_j^2(L) = \frac{2}{1 - R^2} [\alpha L - (1 + \tilde{\Delta}_j^2) |\ln(R)|]$$

$$|\mathscr{F}_{st}^{(j)}|^2 \xrightarrow[\substack{R \to 1^- \\ \alpha L \to 0}]{} \left[2C - (1 + \tilde{\Delta}_j^2) \right] \quad 2C \equiv \frac{\alpha L}{|\ln R|} < \infty$$



Cambio de variables: simplificar la condición de contorno

$$z' = z$$

$$t' = t + \frac{\mathcal{L} - L}{c} \frac{z}{L}$$

$$\Longrightarrow \underline{CC} : F(z = 0, t') = F(z = L, t')$$

Nuevos campos: F(z',t'), P(z',t'), D(z',t') con sus nuevas ecuaciones

$$k_n = \frac{2\pi n}{I}$$
 $\tilde{\alpha}_n = n\tilde{\alpha}_1$ $\delta\Omega = \delta\omega_j - j\alpha_1$

Descomposición modal de los nuevos campos

$$F(z',t') = e^{-i\delta\Omega t'} \sum_{n=-\infty}^{\infty} e^{ik_n z'} e^{-i\alpha_n t'} f_n(t')$$

$$P(z',t') = e^{-i\delta\Omega t'} \sum_{n=-\infty}^{\infty} e^{ik_n z'} e^{-i\alpha_n t'} p_n(t')$$

$$D(z',t') = \sum_{n=-\infty}^{\infty} e^{ik_n z'} e^{-i\alpha_n t'} d_n(t')$$

$$F^*(z',t') = e^{i\delta\Omega t'} \sum_{n=-\infty}^{\infty} e^{-ik_n z'} e^{i\alpha_n t'} f_n^*(t')$$

$$P^*(z',t') = e^{i\delta\Omega t'} \sum_{n=-\infty}^{\infty} e^{-ik_n z'} e^{i\alpha_n t'} p_n^*(t')$$

→ ecuaciones para las amplitudes modales

Linealizacion alrededor de estado estacionario + Ansatz

$$\chi_n = \chi_n^{(j)} \delta_{n,j} + \delta \chi_n$$
$$d_n = d_n^{(j)} \delta_{n,0} + \delta d_n$$

$$\begin{bmatrix} \delta f_{j+n}(t') \\ \delta f_{j-n}^*(t') \\ \delta p_{j+n}(t') \\ \delta p_{j+n}^*(t') \\ \delta d_n(t') \end{bmatrix} = e^{\lambda t'} \begin{bmatrix} \delta f_{j+n}(0) \\ \delta f_{j-n}^*(0) \\ \delta p_{j+n}(0) \\ \delta d_n(0) \end{bmatrix} \rightarrow \begin{bmatrix} \dot{\delta} f_{j+n} \\ \dot{\delta} f_{j-n}^* \\ \dot{\delta} p_{j+n} \\ \dot{\delta} p_{j-n}^* \\ \dot{\delta} d_n \end{bmatrix} = \lambda e^{\lambda t} \begin{bmatrix} \delta f_{j+n}(0) \\ \delta f_{j-n}^*(0) \\ \delta p_{j+n}(0) \\ \delta p_{j-n}^*(0) \\ \delta d_n(0) \end{bmatrix} =$$

$$= \begin{bmatrix} \delta f_{j+n}(t') \\ \delta f_{j-n}^*(t') \\ \delta p_{j+n}(t') \\ \delta p_{j+n}^*(t') \\ \delta d_n(t') \end{bmatrix} = A \begin{bmatrix} \delta f_{j+n}(t') \\ \delta f_{j-n}^*(t') \\ \delta p_{j+n}(t') \\ \delta p_{j-n}^*(t') \\ \delta d_n(t') \end{bmatrix}$$

Sistema matricial adimensionalizado

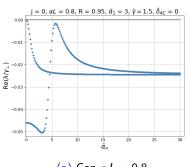
$$\tilde{A} = \frac{1}{\gamma_{\perp}} \begin{bmatrix} i\delta\Omega_{j} - \kappa & 0 & -\kappa2C & 0 & 0 \\ 0 & -i\delta\Omega_{j} - \kappa & 0 & -\kappa2C & 0 \\ \gamma_{\perp}d_{0}^{(j)} & 0 & -\gamma_{\perp}\tilde{\Delta}_{j,n}^{+} & 0 & \gamma_{\perp}f_{j}^{(j)} \\ 0 & \gamma_{\perp}d_{0}^{(j)} & 0 & -\gamma_{\perp}\tilde{\Delta}_{j,n}^{-} & \gamma_{\perp}(f_{j}^{(j)})^{*} \\ -\frac{\gamma_{\parallel}}{2}(\rho_{j}^{(j)})^{*} & -\frac{\gamma_{\parallel}}{2}\rho_{j}^{(j)} & -\frac{\gamma_{\parallel}}{2}(f_{j}^{(j)})^{*} & -\frac{\gamma_{\parallel}}{2}f_{j}^{(j)} & i\tilde{\alpha}_{n} - \gamma_{\parallel} \end{bmatrix}$$

$$\tilde{\Delta}_{j,n}^{+} = [1 + i(\tilde{\Delta}_{j} - \tilde{\alpha}_{n})]$$
$$\tilde{\Delta}_{j,n}^{-} = [1 - i(\tilde{\Delta}_{j} + \tilde{\alpha}_{n})]$$

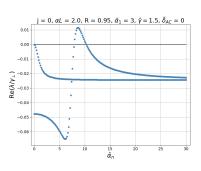
Análisis de estabilidad lineal con $\tilde{\delta}_{AC}=0$

Estable sii $Re(\lambda_i) < 0 \ \forall i, n$

Inestabilidad dada por λ amplitud





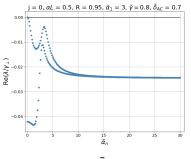


(b) Con $\alpha L = 2$

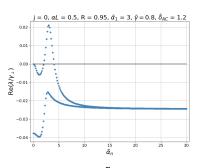
Análisis de estabilidad lineal con $\tilde{\delta}_{AC} \neq 0$

Si aumento $\tilde{\delta}_{AC}$ requiero menor ganancia para inestabilidad

Inestabilidad dada por λ fase

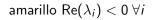


(a) Con $\tilde{\delta}_{AC}=0.7$

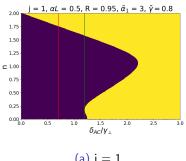


(b) Con $\tilde{\delta}_{AC}=1.2$

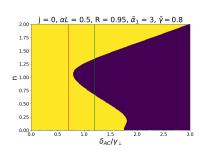
Análisis de estabilidad lineal



violeta
$$Re(\lambda_i) > 0$$



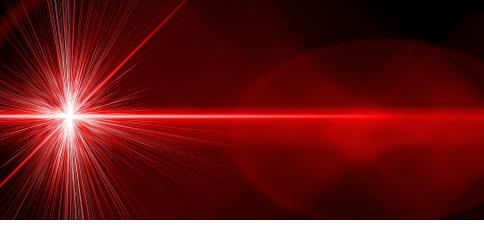
(a)
$$j = 1$$



(b)
$$j = 0$$

Conclusiones

- Se pudo modelar la física de un láser como un balance de poblaciones y con el formalismo de Maxwell-Bloch
- Se calculó la matriz adimensional A de 5×5 y sus autovalores
- Se lograron reproducir los gráficos de la segunda y tercera secciones del paper
- Se observó el comportamiento esperado de $\tilde{\delta}_{AC}$ y $\tilde{\alpha}_1$
- Se graficaron mapas de color mostrando las zonas de estabilidad y de inestabilidad



Muchas gracias!!!

Sistema de ecuaciones

$$\bullet \frac{dI}{dt} = -kI + gIN_2 - gIN_1$$

$$\bullet \frac{dN_1}{dt} = -gIN_1 + gIN_2 + \gamma_{\parallel}N_2 + R_1$$

$$\bullet \frac{dN_2}{dt} = gIN_1 - gIN_2 - \gamma_{\parallel}N_2 + R_2$$

$$R_2 \equiv \gamma_{\parallel}N_{o2} \text{ y } R_1 \equiv \gamma_{\parallel}(N_{o1} - N_T) \text{ con } N_T \equiv N_1 + N_2.$$

$$\bullet \frac{dN_2}{dt} = gIN_1 - gIN_2 - \gamma_{\parallel}N_2 + \gamma_{\parallel}N_{o2}$$

$$\bullet \frac{dN_1}{dt} = -gIN_1 + gIN_2 - \gamma_{\parallel}N_1 + \gamma_{\parallel}N_{o1}$$

Sistema de ecuaciones

Sea
$$N_T \equiv N_1 + N_2$$
 y $N_{oT} \equiv N_{o1} + N_{o2}$:

$$\frac{dN_T}{dt} = \gamma_{\parallel} (N_{oT} - N_T)$$

$$\implies N_T(t) = N_{oT} (1 - Ae^{-\gamma_{\parallel} t})$$

Me queda que N_T =cte si y sólo si A=0, o equivalentemente si $N_T(t=0) = N_{oT} = N_{o1} + N_{o2}$, o equivalentemente $R_1 + R_2 = 0 \iff R_2 = -R_1$.

Análisis de estabilidad lineal: Primer punto fijo

$$DF = \begin{bmatrix} \frac{\partial \dot{\tilde{N}}}{\partial \tilde{N}} & \frac{\partial \dot{\tilde{N}}}{\partial \tilde{I}} \\ \\ \frac{\partial \dot{\tilde{I}}}{\partial \tilde{N}} & \frac{\partial \dot{\tilde{I}}}{\partial \tilde{I}} \end{bmatrix} = \begin{bmatrix} -2\tilde{g}\tilde{I} - 1 & -2\tilde{g}\tilde{N} \\ \\ \tilde{g}\tilde{I} & \tilde{g}(-1/A + \tilde{N}) \end{bmatrix}$$

$$DF\Big|_{N_{pf}^{(1)},I_{pf}^{(1)}} = DF\Big|_{1,0} = \begin{bmatrix} -1 & -2\tilde{g} \\ 0 & -\tilde{g}/A + \tilde{g} \end{bmatrix}$$

$$\lambda_1^{(1)} = -1$$
 $\lambda_2^{(1)} = \tilde{g}(1 - 1/A)$

Análisis de estabilidad lineal: Segundo punto fijo

$$DF\Big|_{N_{pf}^{(2)},I_{pf}^{(2)}} = DF\Big|_{\frac{1}{A},\frac{A-1}{2\tilde{g}}} = \begin{bmatrix} -A & -\frac{2\tilde{g}}{A} \\ \frac{A-1}{2} & 0 \end{bmatrix}$$

$$\lambda_1^{(2)} = -rac{A}{2} + \sqrt{\left(rac{A}{2}
ight)^2 - ilde{g}(1 - 1/A)}$$
 $\lambda_2^{(2)} = -rac{A}{2} - \sqrt{\left(rac{A}{2}
ight)^2 - ilde{g}(1 - 1/A)}$

Solución estacionaria

$$\mathscr{F}(z,t) = \mathscr{F}(z)_{st}e^{-i\delta\omega t} \to \tilde{\Delta} = \tilde{\delta}_{AC} - \delta\omega/\gamma_{\perp}$$

 $\mathscr{P}(z,t) = \mathscr{P}(z)_{st}e^{-i\delta\omega t}$
 $\mathscr{D}(z,t) = \mathscr{D}(z)_{st}$

$$egin{aligned} \mathscr{P}_{st}(z) &= -\mathscr{F}_{st}(z) rac{1 - i ilde{\Delta}}{1 + ilde{\Delta}^2 + |\mathscr{F}_{st}(z)|^2} \ \mathscr{D}_{st}(z) &= -\mathscr{F}_{st}(z) rac{1 + ilde{\Delta}}{1 + ilde{\Delta}^2 + |\mathscr{F}_{st}(z)|^2} \end{aligned}$$

$$\underline{\mathsf{CC}}:\mathscr{F}_{\mathsf{st}}(z=0)=R\mathscr{F}_{\mathsf{st}}(z=L)e^{i\delta\omega(\mathscr{L}-L)/c}$$

Coordenadas polares

$$\mathscr{F}_{st}(z) = \rho(z)e^{i\theta(z)} \rightarrow \frac{d\mathscr{F}_{st}}{dz} - \frac{i\delta\omega}{c}\mathscr{F}_{st} = \alpha\mathscr{F}_{st}(z)\frac{1 - i\tilde{\Delta}}{1 + \tilde{\Delta}^2 + |\mathscr{F}_{st}(z)|^2}$$

$$\rho'(z) = \frac{\alpha \rho(z)}{1 + \tilde{\Delta}^2 + |\rho(z)|^2}$$

$$\theta'(z) = -\frac{\alpha \tilde{\Delta}}{1 + \tilde{\Delta}^2 + |\rho(z)|^2} + \frac{\delta \omega}{c}$$

$$\underline{CC}: \qquad \rho(z=0) = R\rho(z=L)
\theta_j(z=L) - \theta(z=0) = -\delta\omega(\mathcal{L}-L)/c + 2\pi j$$

Cambio de variables

Nuevas campos:

$$F(z',t') = \mathscr{F}(z',t')e^{z' \ln R/L}$$

$$P(z',t') = \mathscr{P}(z',t')e^{z' \ln R/L}$$

$$D(z',t') = \mathscr{D}(z',t')$$

Nuevas ecuaciones:

$$\begin{split} &\frac{\partial F}{\partial t'} + \frac{cL}{\mathcal{L}} \frac{\partial F}{\partial z'} = -k(F + 2CP) \\ &\frac{\partial P}{\partial t'} = \gamma_{\perp} [FD - (1 + \bar{\delta}_{AC})P] \\ &\frac{\partial P}{\partial t'} = -\gamma_{\parallel} \left[\frac{1}{2} (F^*P + FP^*) + D + 1 \right] \end{split}$$

Ecuaciones para las amplitudes modales

$$\dot{f}_n = i\delta\Omega f_n - \kappa (f_n + 2Cp_n)$$

$$\dot{f}_n^* = -i\delta\Omega f_n^* - \kappa (f_n + 2Cp_n^*)$$

$$\dot{p}_{n} = \gamma_{\perp} \left[\sum_{n'} f_{n'} d_{n-n'} - p_{n} \left(1 + i \left(\tilde{\delta}_{AC} - \frac{\tilde{\Omega}}{\gamma_{\perp}} - \tilde{\alpha}_{n} \right) \right) \right]$$

$$\dot{p}_{n}^{*} = \gamma_{\perp} \left[\sum_{n'} f_{n'}^{*} d_{n-n'}^{*} - p_{n}^{*} \left(1 - i \left(\tilde{\delta}_{AC} - \frac{\tilde{\Omega}}{\gamma_{\perp}} - \tilde{\alpha}_{n} \right) \right) \right]$$

$$\dot{d}_n = i\alpha_n d_n - \gamma_{\parallel} \left[\frac{1}{2} \sum_{n'} (f_{n'}^* p_{n+n'} + f_{n'} p_{n'-n}^*) + d_n + \delta_{n,0} \right]$$

Ecuaciones de movimiento para las amplitudes modales

$$\mathscr{P}_{st}(z) = -\mathscr{F}_{st}(z) \frac{1 - i\tilde{\Delta}}{1 + \tilde{\Delta}^2 + |\mathscr{F}_{st}(z)|^2} \qquad p_n^{(j)} = -f_n^{(j)} \frac{1 - i\tilde{\Delta}_j}{1 + \tilde{\Delta}_j^2 + |f_n^{(j)}|^2}$$

$$\mathscr{D}_{st}(z) = -\mathscr{F}_{st}(z) rac{1+ ilde{\Delta}}{1+ ilde{\Delta}^2+|\mathscr{F}_{st}(z)|^2} \qquad d_n^{(j)} = -rac{1+ ilde{\Delta}_j}{1+ ilde{\Delta}_j^2+|f_n^{(j)}|^2} \delta_{n,0}$$

$$|\mathscr{F}_{st}^{(j)}|^2 \xrightarrow[R o 1^-]{} \left[2C - (1 + \tilde{\Delta}_j^2)
ight] \qquad \qquad f_n^{(j)} = [2C - (1 + \tilde{\Delta}_j^2)]^{1/2} \delta_{n,j}$$

Linealizacion de las ecuaciones de amplitudes modales

$$\chi_n = \chi_n^{(j)} \delta_{n,j} + \delta \chi_n$$
$$d_n = d_n^{(j)} \delta_{n,0} + \delta d_n$$

$$\begin{split} \dot{\delta}f_{j+n} &= i\delta\Omega_{j}\delta f_{j+n} - \kappa(\delta f_{j+n} + 2C\delta p_{j+n}) \\ \dot{\delta}f_{j-n}^{*} &= -i\delta\Omega_{j}\delta f_{j-n}^{*} - \kappa(\delta f_{j-n}^{*} + 2C\delta p_{j-n}^{*}) \\ \dot{\delta}p_{j+n} &= \gamma_{\perp} \left[f_{j}^{(j)}\delta d_{n} + \delta f_{j+n}d_{0}^{(j)} - 1[1 + i(\tilde{\Delta}_{j} - \tilde{\alpha}_{n})]\delta p_{j+n} \right] \\ \dot{\delta}p_{j-n}^{*} &= \gamma_{\perp} \left[f_{j}^{(j)*}\delta d_{n} + \delta f_{j-n}d_{0}^{(j)} - 1[1 - i(\tilde{\Delta}_{j} + \tilde{\alpha}_{n})]\delta p_{j-n}^{*} \right] \\ \dot{\delta}d_{n} &= i\alpha_{n}\delta d_{n} - \gamma_{\parallel} \left[\frac{1}{2} (f_{j}^{(j)*}\delta p_{j+n} + p_{j}^{(j)}\delta f_{j-n}^{*} + f_{j}^{(j)}\delta p_{j-n}^{*} + (p_{j}^{(j)})^{*}\delta f_{j+n}) + \delta d_{n} \right] \end{split}$$

Ansatz

$$\begin{bmatrix} \delta f_{j+n}(t') \\ \delta f_{j-n}^*(t') \\ \delta p_{j+n}(t') \\ \delta p_{j+n}^*(t') \\ \delta d_n(t') \end{bmatrix} = e^{\lambda t'} \begin{bmatrix} \delta f_{j+n}(0) \\ \delta f_{j-n}^*(0) \\ \delta p_{j+n}(0) \\ \delta d_n(0) \end{bmatrix} \rightarrow \begin{bmatrix} \dot{\delta} f_{j+n} \\ \dot{\delta} f_{j-n}^* \\ \dot{\delta} p_{j+n} \\ \dot{\delta} p_{j-n}^* \\ \dot{\delta} d_n \end{bmatrix} = \lambda e^{\lambda t} \begin{bmatrix} \delta f_{j+n}(0) \\ \delta f_{j-n}^*(0) \\ \delta p_{j+n}(0) \\ \delta p_{j-n}^*(0) \\ \delta d_n(0) \end{bmatrix} =$$

$$= \lambda \begin{bmatrix} \delta f_{j+n}(t') \\ \delta f_{j-n}^*(t') \\ \delta p_{j+n}(t') \\ \delta p_{j-n}^*(t') \end{bmatrix} = A \begin{bmatrix} \delta f_{j+n}(t') \\ \delta f_{j-n}^*(t') \\ \delta p_{j+n}(t') \\ \delta p_{j-n}^*(t') \\ \delta d_n(t') \end{bmatrix}$$

Análisis de estabilidad lineal: partes imaginarias

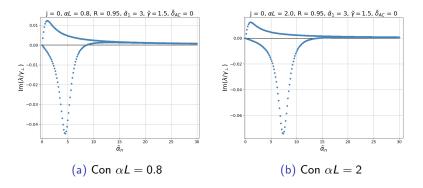


Figure: R = 0.95, $\tilde{\alpha}_1 = 3$, $\tilde{\gamma} = 1.5$, $\tilde{\delta}_{AC} = 0$

Análisis de estabilidad lineal: partes imaginarias

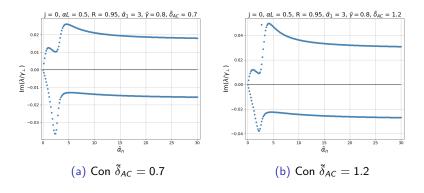


Figure: $\alpha L = 0.5$, R = 0.95, $\tilde{\alpha}_1 = 3$, $\tilde{\gamma} = 0.8$