

# Dipolo in- caso con kz

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## 1 Campo magnetico

Dipolo en el interior de un cilindro de radio  $R$  recubierto con grafeno (ver ref. [Cuevas \[2017\]](#) y apunte de Depine):

$$\mathbf{A}(\rho, \theta, z) = \sum_{m=-\infty}^{m=+\infty} \int_{-\infty}^{\infty} dk_z e^{ik_z(z-z_D)} e^{im(\theta-\theta_D)} J_m(k_{t,1}\rho_{<}) H_m^{(1)}(k_{t,1}\rho_{>}) \frac{\omega}{2c} \mathbf{p}, \quad k_{t,1} = \sqrt{(\omega/c)^2 \varepsilon_1 - k_z^2} \quad (1)$$

$$\mathbf{A}(\rho, \theta, z) = \sum_{m=-\infty}^{m=+\infty} \int_{-\infty}^{\infty} dk_z e^{ik_z(z-z_D)} e^{im(\theta-\theta_D)} J_m(k_{t,1}\rho_D) H_m^{(1)}(k_{t,1}\rho) \frac{\omega}{2c} \mathbf{p} \quad \rho > \rho_D,$$

$$\mathbf{A}(\rho, \theta, z) = \sum_{m=-\infty}^{m=+\infty} \int_{-\infty}^{\infty} dk_z e^{ik_z(z-z_D)} e^{im(\theta-\theta_D)} J_m(k_{t,1}\rho) H_m^{(1)}(k_{t,1}\rho_D) \frac{\omega}{2c} \mathbf{p} \quad \rho < \rho_D.$$

Las ultimas dos ecuaciones tienen sentido dado que Hankel diverge en el cero ( $\rho < \rho_D$ ) y la de Bessel diverge en el infinito ( $\rho > \rho_D$ ). La dependencia temporal del potencial y de los campos es  $e^{-i\omega t}$ . Con el potencial  $\mathbf{A}$  se obtienen los campos (ref. [Cuevas \[2017\]](#)):

$$\mathbf{H}(\rho, \theta, z) = \vec{\nabla} \times \mathbf{A}(\rho, \theta, z) = \sum_{m=-\infty}^{m=+\infty} \int_{-\infty}^{\infty} dk_z e^{ik_z z} e^{im\theta} [h_{\rho m}(\rho) \hat{\rho} + h_{\theta m}(\rho) \hat{\theta} + h_{zm}(\rho) \hat{z}], \quad (2)$$

$$\mathbf{E}(\rho, \theta, z) = \frac{ic}{\omega \varepsilon_1} \vec{\nabla} \times \mathbf{H}(\rho, \theta, z) = \sum_{m=-\infty}^{m=+\infty} \int_{-\infty}^{\infty} dk_z e^{ik_z z} e^{im\theta} [e_{\rho m}(\rho) \hat{\rho} + e_{\theta m}(\rho) \hat{\theta} + e_{zm}(\rho) \hat{z}]. \quad (3)$$

Hallar las funciones  $h_{\rho m}(\rho)$ ,  $h_{\theta m}(\rho)$ ,  $h_{zm}(\rho)$  para obtener los campos incidentes. Las funciones  $e_{\rho m}(\rho)$ ,  $e_{\theta m}(\rho)$ ,  $e_{zm}(\rho)$  se pueden obtener a partir de las funciones  $h$ . El rotor en cilindricas es:

$$\vec{\nabla} \times \mathbf{A}(\rho, \theta, z) = \hat{\rho} \left( \frac{1}{\rho} \frac{\partial A_z}{\partial \theta} - \frac{\partial A_\theta}{\partial z} \right) + \hat{\theta} \left( \frac{\partial A_\rho}{\partial z} - \frac{\partial A_z}{\partial \rho} \right) + \hat{z} \left( \frac{1}{\rho} \frac{\partial(\rho A_\theta)}{\partial \rho} - \frac{1}{\rho} \frac{\partial A_\rho}{\partial \theta} \right).$$

Para  $\rho > \rho_D$ , al derivar respecto de la coordenada radial sólo se deriva la funcion de Bessel  $J$  y la función de Hankel se evalúa en  $\rho_D$ . Para  $\rho < \rho_D$  se realiza lo inverso. Lo importante es que nunca se derivan las dos funciones simultaneamente

(no quedan dos terminos al derivar respecto de  $\rho$ ). Tener en cuenta (ver seccion A):

$$p_x = p_\rho \cos(\theta) - p_\theta \sin(\theta), p_y = p_\rho \sin(\theta) + p_\theta \cos(\theta) \quad (4)$$

$$p_\rho = p_x \cos(\theta) + p_y \sin(\theta), p_\theta = -p_x \sin(\theta) + p_y \cos(\theta) \quad (5)$$

$$\rightarrow \frac{\partial p_\rho}{\partial \theta} = -p_x \sin(\theta) + p_y \cos(\theta) = p_\theta$$

$$\rightarrow \frac{\partial p_\theta}{\partial \rho} = -\frac{\partial p_x}{\partial \rho} \sin(\theta) + \frac{\partial p_y}{\partial \rho} \cos(\theta) = -\cos(\theta) \sin(\theta) + \sin(\theta) \cos(\theta) = 0$$

Se va a usar en las siguientes subsecciones:

$$\frac{\partial p_\rho}{\partial \theta} = p_\theta \quad (6)$$

$$\frac{\partial p_\theta}{\partial \rho} = 0 \quad (7)$$

Conviene definir  $p_+$ ,  $p_-$  a partir de  $p_x$ ,  $p_y$ :

$$p_+ = p_x + ip_y, p_- = p_x - ip_y, \\ p_x = \frac{p_+ + p_-}{2}, p_y = \frac{p_+ - p_-}{2i} = \frac{i(p_- - p_+)}{2}. \quad (8)$$

Se va a usar en las siguientes secciones  $p_\theta(p_+, p_-)$ ,  $p_\rho(p_+, p_-)$ :

$$p_\theta = -p_x \sin(\theta) + p_y \cos(\theta) = -\frac{(p_+ + p_-)}{2} \sin(\theta) + \frac{i(p_- - p_+)}{2} \cos(\theta) = \\ p_\theta = \frac{p_+}{2} \left\{ \underbrace{-\sin(\theta) - i \cos(\theta)}_{-ie^{-i\theta}} \right\} + \frac{p_-}{2} \left\{ \underbrace{-\sin(\theta) + i \cos(\theta)}_{ie^{i\theta}} \right\} = \\ p_\theta = -\frac{ip_+ e^{-i\theta}}{2} + \frac{ip_- e^{i\theta}}{2} = \frac{\partial p_\rho}{\partial \theta} \quad (9)$$

$$p_\rho = p_x \cos(\theta) + p_y \sin(\theta) = \frac{(p_+ + p_-)}{2} \cos(\theta) + \frac{i(p_- - p_+)}{2} \sin(\theta) = \\ p_\rho = \frac{p_+}{2} \left\{ \underbrace{\cos(\theta) - i \sin(\theta)}_{e^{-i\theta}} \right\} + \frac{p_-}{2} \left\{ \underbrace{\cos(\theta) + i \sin(\theta)}_{e^{i\theta}} \right\} = \\ p_\rho = \frac{p_+ e^{-i\theta}}{2} + \frac{p_- e^{i\theta}}{2} \quad (10)$$

## 1.1 longitudinal $h_{zm}$

La coordenada  $z$  del rotor para  $\rho < \rho_D$  es (se usa  $J_m(k_{t,1}\rho)H_m^{(1)}(k_{t,1}\rho_D)$  en la fórmula para  $\mathbf{A}$ ):

$$\begin{aligned} \mathbf{A}(\rho, \theta, z) &= \sum_{m=-\infty}^{m=+\infty} \int_{-\infty}^{\infty} dk_z e^{ik_z(z-z_D)} e^{im(\theta-\theta_D)} J_m(k_{t,1}\rho) H_m^{(1)}(k_{t,1}\rho_D) \frac{\omega}{2c} \mathbf{p} \\ (\vec{\nabla} \times \mathbf{A})_z &= \left( \frac{1}{\rho} \frac{\partial(\rho A_\theta)}{\partial \rho} - \frac{1}{\rho} \frac{\partial A_\rho}{\partial \theta} \right) = \frac{1}{\rho} \left( A_\theta + \rho \frac{\partial A_\theta}{\partial \rho} - \frac{\partial A_\rho}{\partial \theta} \right) = \\ &= \underbrace{\frac{1}{\rho} \left\{ A_\theta + \rho \frac{\omega}{2c} \sum_{m=-\infty}^{m=+\infty} \int_{-\infty}^{\infty} dk_z e^{ik_z(z-z_D)} e^{im(\theta-\theta_D)} H_m^{(1)}(k_{t,1}\rho_D) \left( J'_m(k_{t,1}\rho) k_{t,1} p_\theta + J_m(k_{t,1}\rho) \frac{\partial p_\theta}{\partial \rho} \right) \right\}}_{\partial_\rho A_\theta} + \\ &\quad - \underbrace{\frac{\omega}{2c} \sum_{m=-\infty}^{m=+\infty} \int_{-\infty}^{\infty} dk_z e^{ik_z(z-z_D)} e^{im(\theta-\theta_D)} J_m(k_{t,1}\rho) H_m^{(1)}(k_{t,1}\rho_D) \left( i m p_\rho + \frac{\partial p_\rho}{\partial \theta} \right)}_{\partial_\theta A_\rho} \underbrace{\left. \right\}}_{p_\theta} = \end{aligned}$$

En el tercer y cuarto renglón se usaron Eq. 6, 7. Juntando los tres términos:

$$\begin{aligned} (\vec{\nabla} \times \mathbf{A})_z &= \\ &= \frac{\omega}{2c\rho} \sum_m \int e^{-i(m\theta_D + k_z z_D)} dk_z e^{ik_z z} e^{im\theta} H_m^{(1)}(k_{t,1}\rho_D) \left[ \cancel{p_\theta J_m(k_{t,1}\rho)} - (p_\rho i m + p_\theta) J_m(k_{t,1}\rho) + p_\theta k_{t,1} \rho J'_m(k_{t,1}\rho) \right] \quad (11) \end{aligned}$$

Los términos tachados en rojo se cancelan entre si. Conviene usar una relación de recurrencia de la funcion Bessel para un modo  $n$  entero (ref. <https://www.math.usm.edu/lambers/mat415/lecture12.pdf> pag 3) para reescribir el último término de la Eq. 11 (el de la derivada  $J'$ ) en función de  $J$ :

$$J_n(x) = \pm J'_{n\pm 1}(x) + \frac{n \pm 1}{x} J_{n\pm 1}(x) \rightarrow J'_{n+1}(x) = J_n(x) - \left( \frac{n+1}{x} \right) J_{n+1}(x), \quad (12)$$

$$k_{t,1} \rho J'_m(k_{t,1}\rho) = k_{t,1} \rho \left[ J_{m-1}(k_{t,1}\rho) - \left( \frac{m}{k_{t,1}\rho} \right) J_m(k_{t,1}\rho) \right] = k_{t,1} \rho J_{m-1}(k_{t,1}\rho) - m J_m(k_{t,1}\rho) \quad (13)$$

Forma útil de sacarse la derivada de  $J$  de encima. Reescribir el integrando de la Eq. 11 usando Eq. 12:

$$p_\theta [k_{t,1} \rho J_{m-1} - m J_m] - p_\rho i m J_m$$

Usando  $p_\rho = \frac{p_+ e^{-i\theta}}{2} + \frac{p_- e^{i\theta}}{2}$ ,  $p_\theta = -\frac{i p_+ e^{-i\theta}}{2} + \frac{i p_- e^{i\theta}}{2}$  (Eqs. 10, 9) en la ecuacion anterior:

$$\begin{aligned} &\left( -\frac{i p_+ e^{-i\theta}}{2} + \frac{i p_- e^{i\theta}}{2} \right) [k_{t,1} \rho J_{m-1} - m J_m] - \left( \frac{p_+ e^{-i\theta}}{2} + \frac{p_- e^{i\theta}}{2} \right) i m J_m = \\ &= \frac{p_+}{2} \left\{ -i k_{t,1} \rho J_{m-1} e^{-i\theta} + \cancel{i m J_m e^{-i\theta}} - \cancel{i m J_m e^{-i\theta}} \right\} + \frac{p_-}{2} \left\{ i k_{t,1} \rho J_{m-1} e^{i\theta} - i m J_m e^{i\theta} - i m J_m e^{i\theta} \right\} = \\ &= \frac{i k_{t,1} \rho}{2} \left\{ -p_+ J_{m-1} e^{-i\theta} + p_- J_{m-1} e^{i\theta} \right\} - i p_- m J_m e^{i\theta} = -\frac{i p_+}{2} k_{t,1} \rho J_{m-1} e^{-i\theta} + \frac{i p_-}{2} e^{i\theta} \underbrace{\left[ k_{t,1} \rho J_{m-1} - 2 m J_m \right]}_{(*)}. \quad (14) \end{aligned}$$

Para reescribir (\*) se usa la siguiente propiedad (ref. <https://www.math.usm.edu/lambers/mat415/lecture12.pdf> pag 3)):

$$2nJ_n(x) = xJ_{n-1}(x) + xJ_{n+1}(x) \rightarrow (*) = k_{t,1}\rho J_{m-1} - 2mJ_m = -k_{t,1}\rho J_{m+1}$$

Reemplazando (\*) en Eq. 14:

$$-\frac{ip_+}{2}k_{t,1}\rho J_{m-1}e^{-i\theta} - \frac{ip_-}{2}k_{t,1}\rho J_{m+1}e^{i\theta} = -\frac{ik_{t,1}\rho}{2}\left\{p_+J_{m-1}e^{-i\theta} + p_-J_{m+1}e^{i\theta}\right\}$$

Agregar la sumatoria sobre  $m$  y los factores que dependen de  $m$  para absorber los términos  $e^{-i\theta}$ ,  $e^{+i\theta}$  con un cambio de variables:

$$\begin{aligned} & -\sum_m e^{im(\theta-\theta_D)} H_m^{(1)}(k_{t,1}\rho_D) \frac{ik_{t,1}\rho}{2} \left\{p_+J_{m-1}e^{-i\theta} + p_-J_{m+1}e^{i\theta}\right\} = \\ & = -\frac{ik_{t,1}\rho}{2} \sum_m \left\{ \underbrace{p_+e^{i(m-1)\theta} e^{-im\theta_D} H_m^{(1)} J_{m-1}}_{m'=m-1} + \underbrace{p_-e^{i(m+1)\theta} e^{-im\theta_D} H_m^{(1)} J_{m+1}}_{m''=m+1} \right\} = \\ & = -\frac{ik_{t,1}\rho}{2} \left\{ \sum_{m'} p_+e^{im'\theta} e^{-i(m'+1)\theta_D} H_{m'+1} J_{m'} + \sum_{m''} p_-e^{im''\theta} e^{-i(m''-1)\theta_D} H_{m''-1} J_{m''} \right\} = \\ & = -\frac{ik_{t,1}\rho}{2} \sum_m e^{im(\theta-\theta_D)} \left\{ p_+e^{-i\theta_D} H_{m+1} J_m + p_-e^{i\theta_D} H_{m-1} J_m \right\} = \\ & = -\frac{ik_{t,1}\rho}{2} \sum_m e^{im(\theta-\theta_D)} J_m(k_{t,1}\rho) \left\{ p_+e^{-i\theta_D} H_{m+1}(k_{t,1}\rho_D) + p_-e^{i\theta_D} H_{m-1}(k_{t,1}\rho_D) \right\} \end{aligned}$$

Reemplazando lo anterior en Eq. 11:

$$\begin{aligned} & (\vec{\nabla} \times \mathbf{A})_z = \\ & = -\frac{\omega}{2c\phi} \frac{ik_{t,1}\rho}{2} \sum_m \int dk_z e^{ik_z(z-z_D)} e^{im(\theta-\theta_D)} J_m \left\{ p_+e^{-im\theta_D} H_{m+1} + p_-e^{im\theta_D} H_{m-1} \right\} \\ & \boxed{(\vec{\nabla} \times \mathbf{A})_z = -\frac{i\omega k_{t,1}}{4c} \sum_m \int dk_z e^{ik_z(z-z_D)} e^{im(\theta-\theta_D)} J_m(k_{t,1}\rho) \left\{ p_+e^{-i\theta_D} H_{m+1}(k_{t,1}\rho_D) + p_-e^{i\theta_D} H_{m-1}(k_{t,1}\rho_D) \right\}} \quad (15)} \end{aligned}$$

De la formula anterior se obtiene  $h_{zm}(\rho)$  (Eq. 2) del campo  $\mathbf{H}_{inc}$  para  $\rho < \rho_D$ :

$$h_{zm}(\rho) = \frac{i\omega}{4c} k_{t,1} e^{-im\theta_D - ik_z z_D} J_m(k_{t,1}\rho) \left\{ -p_+e^{-i\theta_D} H_{m+1}(k_{t,1}\rho_D) - p_-e^{i\theta_D} H_{m-1}(k_{t,1}\rho_D) \right\} \quad \rho < \rho_D.$$

Dado que las propiedades de las funciones son las mismas (ver Eq. 24) se obtuvo la formula de  $h_{zm}(\rho)$  para  $\rho > \rho_D$  simplemente intercambiando las funciones y sus respectivos argumentos:

$$h_{zm}(\rho) = \frac{i\omega}{4c} k_{t,1} e^{-im\theta_D - ik_z z_D} H_m^{(1)}(k_{t,1}\rho) \left\{ -p_+e^{-i\theta_D} J_{m+1}(k_{t,1}\rho_D) - p_-e^{i\theta_D} J_{m-1}(k_{t,1}\rho_D) \right\} \quad \rho > \rho_D.$$

Mismas formulas que el apunte de Depine.

## 1.2 angular $h_{\theta m}$

La coordenada  $\theta$  del rotor para  $\rho > \rho_D$  es (se usa  $J_m(k_{t,1}\rho)H_m^{(1)}(k_{t,1}\rho_D)$  en la fórmula para **A** Eq. 1):

$$\begin{aligned}
\mathbf{A}(\rho, \theta, z) &= \sum_{m=-\infty}^{m=+\infty} \int_{-\infty}^{\infty} dk_z e^{ik_z(z-z_D)} e^{im(\theta-\theta_D)} J_m(k_{t,1}\rho) H_m^{(1)}(k_{t,1}\rho_D) \frac{\omega}{2c} \mathbf{p} \\
(\vec{\nabla} \times \mathbf{A})_\theta &= \left( \frac{\partial A_\rho}{\partial z} - \frac{\partial A_z}{\partial \rho} \right) = \sum_{m=-\infty}^{m=+\infty} \int_{-\infty}^{\infty} dk_z i k_z e^{ik_z(z-z_D)} e^{im(\theta-\theta_D)} J_m(k_{t,1}\rho) H_m^{(1)}(k_{t,1}\rho_D) \frac{\omega}{2c} p_\rho + \\
&\quad - \underbrace{\sum_{m=-\infty}^{m=+\infty} \int_{-\infty}^{\infty} dk_z e^{ik_z(z-z_D)} e^{im(\theta-\theta_D)} J'_m(k_{t,1}\rho) H_m^{(1)}(k_{t,1}\rho_D) \frac{\omega k_{t,1}}{2c} p_z}_{\partial_\rho A_z} = \\
(\vec{\nabla} \times \mathbf{A})_\theta &= \frac{\omega}{2c} \sum_{m=-\infty}^{m=+\infty} \int_{-\infty}^{\infty} e^{-im\theta_D - ik_z z_D} dk_z e^{ik_z z} e^{im\theta} H_m^{(1)}(k_{t,1}\rho_D) \left[ J'_m(k_{t,1}\rho) k_{t,1} p_z + J_m(k_{t,1}\rho) i k_z p_\rho \right]. \quad (16)
\end{aligned}$$

Usar la fórmula de  $p_\rho = \frac{p_+ e^{-i\theta}}{2} + \frac{p_- e^{i\theta}}{2}$  (Eq. 10):

$$J'_m(k_{t,1}\rho) k_{t,1} p_z + J_m(k_{t,1}\rho) i k_z \left\{ \frac{p_+}{2} e^{-i\theta} + \frac{p_-}{2} e^{i\theta} \right\}$$

Reemplazando en Eq. 16:

$$\begin{aligned}
(\vec{\nabla} \times \mathbf{A})_\theta &= \frac{\omega}{2c} \sum_{m=-\infty}^{m=+\infty} \int_{-\infty}^{\infty} e^{-im\theta_D - ik_z z_D} dk_z e^{ik_z z} e^{im\theta} H_m^{(1)}(k_{t,1}\rho_D) \left[ J'_m(k_{t,1}\rho) k_{t,1} p_z + J_m(k_{t,1}\rho) i k_z \left\{ \frac{p_+}{2} e^{-i\theta} + \frac{p_-}{2} e^{i\theta} \right\} \right] = \\
&= \frac{\omega}{4c} \sum_{m=-\infty}^{m=+\infty} \int_{-\infty}^{\infty} e^{-im\theta_D - ik_z z_D} dk_z e^{ik_z z} e^{im\theta} H_m^{(1)}(k_{t,1}\rho_D) \left[ 2J'_m(k_{t,1}\rho) k_{t,1} p_z + J_m(k_{t,1}\rho) i k_z \{ p_+ e^{-i\theta} + p_- e^{i\theta} \} \right] = \\
&= \frac{\omega}{4c} \int_{-\infty}^{\infty} dk_z e^{ik_z(z-z_D)} \sum_m \left\{ 2k_{t,1} p_z e^{im\theta} e^{-im\theta_D} H_m^{(1)}(k_{t,1}\rho_D) J'_m(k_{t,1}\rho) + i k_z p_+ \underbrace{e^{i(m-1)\theta} e^{-im\theta_D} H_m^{(1)}(k_{t,1}\rho_D) J_m(k_{t,1}\rho)}_{m'=m-1} \right. \\
&\quad \left. + i k_z p_- \underbrace{e^{i(m+1)\theta} e^{-im\theta_D} H_m^{(1)}(k_{t,1}\rho_D) J_m(k_{t,1}\rho)}_{m''=m+1} \right\} = \\
&= \frac{\omega}{4c} \int_{-\infty}^{\infty} dk_z e^{ik_z(z-z_D)} \sum_m \left\{ 2k_{t,1} p_z e^{im\theta} e^{-im\theta_D} H_m^{(1)}(k_{t,1}\rho_D) J'_m(k_{t,1}\rho) + \right. \\
&\quad \left. + i k_z p_+ e^{im'\theta} e^{-i(m'+1)\theta_D} H_{m'+1}^{(1)}(k_{t,1}\rho_D) J_{m'+1}(k_{t,1}\rho) + i k_z p_- e^{im''\theta} e^{-i(m''-1)\theta_D} H_{m''-1}^{(1)}(k_{t,1}\rho_D) J_{m''-1}(k_{t,1}\rho) \right\} = \\
&= \frac{\omega}{4c} \int_{-\infty}^{\infty} dk_z e^{ik_z(z-z_D)} \sum_m \left\{ 2k_{t,1} p_z e^{im\theta} e^{-im\theta_D} H_m J'_m + \right. \\
&\quad \left. + i k_z p_+ e^{im\theta} e^{-i(m+1)\theta_D} H_{m+1} J_{m+1} + i k_z p_- e^{im\theta} e^{-i(m-1)\theta_D} H_{m-1} J_{m-1} \right\} = \\
&= \boxed{\frac{\omega}{4c} \int_{-\infty}^{\infty} dk_z e^{ik_z(z-z_D)} \sum_m e^{im(\theta-\theta_D)} \left\{ 2k_{t,1} p_z H_m J'_m + i k_z p_+ e^{-i\theta_D} H_{m+1} J_{m+1} + i k_z p_- e^{i\theta_D} H_{m-1} J_{m-1} \right\}}.
\end{aligned}$$

Recordar que Hankel esta evaluado en  $\rho = \rho_D$  (por eso la derivada que aparece es la de Bessel y no la de Hankel). De la formula anterior se obtiene la de  $h_{\theta m}(\rho)$  (Eq. 2) del campo  $\mathbf{H}_{inc}$  para  $\rho < \rho_D$ :

$$h_{\theta m}(\rho) = \frac{i\omega}{4c} e^{-im\theta_D - ik_z z_D} \left\{ -2ik_{t,1} p_z H_m J'_m + k_z p_+ e^{-i\theta_D} H_{m+1} J_{m+1} + k_z p_- e^{i\theta_D} H_{m-1} J_{m-1} \right\} \quad \rho < \rho_D,$$

con  $H_m = H_m(k_{t,1}\rho_D)$ ,  $J_m = J_m(k_{t,1}\rho)$ . Dado que las propiedades de las funciones son las mismas (ver Eq. 24) se obtuvo la formula de  $h_{\theta m}(\rho)$  para  $\rho > \rho_D$  simplemente intercambiando las funciones y sus respectivos argumentos:

$$h_{\theta m}(\rho) = \frac{i\omega}{4c} e^{-im\theta_D - ik_z z_D} \left\{ -2ik_{t,1} p_z H'_m J_m + k_z p_+ e^{-i\theta_D} H_{m+1} J_{m+1} + k_z p_- e^{i\theta_D} H_{m-1} J_{m-1} \right\} \quad \rho > \rho_D,$$

con  $H_m = H_m(k_{t,1}\rho)$ ,  $J_m = J_m(k_{t,1}\rho_D)$ . Se parece a la formula del apunte de Depine salvo por un factor  $i$  que no aparece en el primer termino con  $p_z$  y por la derivada  $H'_m$ .

### 1.3 radial $h_{\rho m}$

$$\begin{aligned} \mathbf{A}(\rho, \theta, z) &= \sum_{m=-\infty}^{m=+\infty} \int_{-\infty}^{\infty} dk_z e^{ik_z(z-z_D)} e^{im(\theta-\theta_D)} J_m(k_{t,1}\rho) H_m^{(1)}(k_{t,1}\rho_D) \frac{\omega}{2c} \mathbf{p} \\ (\vec{\nabla} \times \mathbf{A})_\rho &= \left( \frac{1}{\rho} \frac{\partial A_z}{\partial \theta} - \frac{\partial A_\theta}{\partial z} \right) = \\ &= \frac{1}{\rho} \frac{\omega}{2c} \sum_m \int_{-\infty}^{\infty} dk_z e^{ik_z(z-z_D)} e^{im(\theta-\theta_D)} J_m(k_{t,1}\rho) H_m^{(1)}(k_{t,1}\rho_D) \left\{ im p_z - \rho i k_z p_\theta \right\} \end{aligned}$$

Usar la formula  $p_\theta = -\frac{ip_+ e^{-i\theta}}{2} + \frac{ip_- e^{i\theta}}{2}$  (Eq. 9) en la ecuacion anterior: (con el factor  $i^2$  cambia de signo)

$$\begin{aligned} (\vec{\nabla} \times \mathbf{A})_\rho &= \frac{\omega}{4c\rho} \sum_m \int_{-\infty}^{\infty} dk_z e^{ik_z(z-z_D)} e^{im(\theta-\theta_D)} J_m(k_{t,1}\rho) H_m^{(1)}(k_{t,1}\rho_D) \left\{ 2im p_z - \rho k_z (p_+ e^{-i\theta} - p_- e^{i\theta}) \right\} = \\ &= \frac{\omega}{4c\rho} \int_{-\infty}^{\infty} dk_z e^{ik_z(z-z_D)} \sum_m H_m^{(1)}(k_{t,1}\rho_D) J_m(k_{t,1}\rho) \left\{ 2im p_z e^{im\theta} e^{-im\theta_D} - \rho k_z p_+ \underbrace{e^{i(m-1)\theta} e^{-im\theta_D}}_{m'=m-1} + \right. \\ &\quad \left. + \rho k_z p_- \underbrace{e^{i(m+1)\theta} e^{-im\theta_D}}_{m''=m+1} \right\} = \\ &= \frac{\omega}{4c\rho} \int_{-\infty}^{\infty} dk_z e^{ik_z(z-z_D)} \sum_m \left\{ 2im H_m J_m p_z e^{im\theta} e^{-im\theta_D} - \rho k_z p_+ H_{m+1} J_{m+1} e^{im\theta} e^{-i(m+1)\theta_D} + \right. \\ &\quad \left. + \rho k_z p_- H_{m-1} J_{m-1} e^{im\theta} e^{-i(m-1)\theta_D} \right\} = \\ &= \boxed{\frac{\omega}{4c} \int_{-\infty}^{\infty} dk_z e^{ik_z(z-z_D)} e^{im(\theta-\theta_D)} \sum_m \left\{ 2im H_m J_m \frac{p_z}{\rho} - k_z p_+ H_{m+1} J_{m+1} e^{-i\theta_D} + k_z p_- H_{m-1} J_{m-1} e^{i\theta_D} \right\}} \end{aligned}$$

De la formula anterior se obtiene la de  $h_{\rho m}(\rho)$  (Eq. 2) del campo  $\mathbf{H}_{inc}$ :

$$h_{\rho m}(\rho) = \frac{i\omega}{4c} e^{-im\theta_D - ik_z z_D} \left\{ 2m \frac{p_z}{\rho} H_m J_m + ik_z p_+ e^{-i\theta_D} H_{m+1} J_{m+1} - ik_z p_- e^{i\theta_D} H_{m-1} J_{m-1} \right\}.$$

Con  $H_m = H_m(k_{t,1}\rho_D)$ ,  $J_m = J_m(k_{t,1}\rho)$  para  $\rho < \rho_D$  y con  $H_m = H_m(k_{t,1}\rho)$ ,  $J_m = J_m(k_{t,1}\rho_D)$  para  $\rho > \rho_D$ .

## 2 Campo eléctrico

Las formulas del campo electrico deberian coincidir con las del apunte de Depine salvo por un factor  $-$  porque ellos usaron la convencion  $e^{+i\omega t}$ . Ellos usaron  $\mathbf{E} = -\frac{ic}{\omega\epsilon_1}\vec{\nabla} \times \mathbf{H}$  mientras que aca usamos  $\mathbf{E} = +\frac{ic}{\omega\epsilon_1}\vec{\nabla} \times \mathbf{H}$ .

Las funciones  $e_{\rho m}(\rho)$ ,  $e_{\theta m}(\rho)$ ,  $e_{zm}(\rho)$  se pueden obtener a partir de las funciones  $h$ .

$$\begin{aligned} \frac{ic}{\omega\epsilon_1}\vec{\nabla} \times \mathbf{H}_{inc}(\rho, \theta, z) &= \frac{ic}{\omega\epsilon_1}\hat{\rho}\left(\frac{1}{\rho}\frac{\partial H_z}{\partial\theta} - \frac{\partial H_\theta}{\partial z}\right) + \frac{ic}{\omega\epsilon_1}\hat{\theta}\left(\frac{\partial H_\rho}{\partial z} - \frac{\partial H_z}{\partial\rho}\right) + \frac{ic}{\omega\epsilon_1}\hat{z}\left(\frac{1}{\rho}\frac{\partial(\rho H_\theta)}{\partial\rho} - \frac{1}{\rho}\frac{\partial H_\rho}{\partial\theta}\right) = \\ &= \frac{ic\hat{\rho}}{\omega\epsilon_1}\left(\frac{1}{\rho}{}^{\prime\prime}imH_z - {}^{\prime\prime}ik_zH_\theta\right) + \frac{ic\hat{\theta}}{\omega\epsilon_1}\left({}^{\prime\prime}ik_zH_\rho - \frac{\partial h_{zm}(\rho)}{\partial\rho}\right) + \frac{ic\hat{z}}{\omega\epsilon_1}\left(\frac{H_\theta}{\rho} + \frac{\partial H_\theta}{\partial\rho} - \frac{1}{\rho}\frac{\partial H_\rho}{\partial\theta}\right) \end{aligned}$$

Parte radial:

$$e_{\rho m}(\rho) = \frac{ic}{\omega\epsilon_1}\left[\frac{imh_{zm}(\rho)}{\rho} - ik_zh_{\theta m}(\rho)\right]. \quad (17)$$

Parte angular:

$$e_{\theta m}(\rho) = \frac{ic}{\omega\epsilon_1}\left[ik_zh_{\rho m}(\rho) - \frac{\partial h_{zm}(\rho)}{\partial\rho}\right]. \quad (18)$$

Parte longitudinal:

$$e_{zm}(\rho) = \frac{ic}{\omega\epsilon_1}\left[\frac{h_{\theta m}(\rho)}{\rho} + \frac{\partial h_{\theta m}(\rho)}{\partial\rho} - \frac{im}{\rho}h_{\rho m}(\rho)\right]. \quad (19)$$

### 2.1 longitudinal $e_{zm}$

Recordar que  $H_m = H_m(k_{t,1}\rho_D)$ ,  $J_m = J_m(k_{t,1}\rho)$  (se deriva  $J$  nada mas):

$$e_{zm}(\rho) = \frac{ic}{\omega\epsilon_1}\left[\frac{h_{\theta m}(\rho)}{\rho} + \frac{\partial h_{\theta m}(\rho)}{\partial\rho} - \frac{im}{\rho}h_{\rho m}(\rho)\right],$$

$$\bullet h_{\theta m}(\rho) = \frac{i\omega}{4c}e^{-im\theta_D - ik_z z_D}\left\{-2ik_{t,1}p_z H_m J'_m + k_z p_+ e^{-i\theta_D} H_{m+1} J_{m+1} + k_z p_- e^{i\theta_D} H_{m-1} J_{m-1}\right\},$$

$$\bullet h_{\rho m}(\rho) = \frac{i\omega}{4c}e^{-im\theta_D - ik_z z_D}\left\{2m\frac{p_z}{\rho} H_m J_m + ik_z p_+ e^{-i\theta_D} H_{m+1} J_{m+1} - ik_z p_- e^{i\theta_D} H_{m-1} J_{m-1}\right\}$$

$$\begin{aligned} e_{zm}(\rho) &= \frac{ic}{\omega\epsilon_1}\frac{i\omega}{4c}\left[-2ik_{t,1}p_z H_m\left(\frac{J'_m}{\rho} + k_{t,1}J''_m\right) + k_z p_+ e^{-i\theta_D} H_{m+1}\left(\frac{J_{m+1}}{\rho} + k_{t,1}J'_{m+1}\right) + k_z p_- e^{i\theta_D} H_{m-1}\left(\frac{J_{m-1}}{\rho} + k_{t,1}J'_{m-1}\right) + \right. \\ &\quad \left. - \frac{2im^2 p_z}{\rho^2} H_m J_m - i^2 m \frac{k_z}{\rho} p_+ e^{-i\theta_D} H_{m+1} J_{m+1} + i^2 m \frac{k_z}{\rho} p_- e^{i\theta_D} H_{m-1} J_{m-1}\right] e^{-im\theta_D - ik_z z_D} \end{aligned}$$

Juntar los terminos con  $p_z, p_+, p_-$ :

$$e_{zm}(\rho) = \frac{ic}{\omega\varepsilon_1} \frac{i\omega}{4c} \left[ -2ip_z H_m \underbrace{\left( \frac{J'_m k_{t,1}}{\rho} + k_{t,1}^2 J''_m + \frac{m^2 J_m}{\rho^2} \right)}_{(1)} + k_z p_+ e^{-i\theta_D} H_{m+1} \underbrace{\left( \frac{J_{m+1}}{\rho} + k_{t,1} J'_{m+1} + \frac{m J_{m+1}}{\rho} \right)}_{(2)} + \right. \\ \left. + k_z p_- e^{i\theta_D} H_{m-1} \underbrace{\left( \frac{J_{m-1}}{\rho} + k_{t,1} J'_{m-1} - \frac{m J_{m-1}}{\rho} \right)}_{(3)} \right] e^{-im\theta_D - ik_z z_D}$$

Simplificar el (2) y (3):

$$(2) = \frac{J_{m+1}}{\rho} + k_{t,1} J'_{m+1} + \frac{m J_{m+1}}{\rho} = \frac{1}{\rho} [J_{m+1} + k_{t,1} \rho J'_{m+1} + m J_{m+1}] = \frac{1}{\rho} \left[ \cancel{J_{m+1}} + \underbrace{k_{t,1} \rho \cancel{J_{m+1}} + \cancel{m J_{m+1}}}_{k_{t,1} \rho J'_{m+1}} \right] = k_{t,1} J_m$$

$$(3) = \frac{J_{m-1}}{\rho} + k_{t,1} J'_{m-1} - \frac{m J_{m-1}}{\rho} = \frac{1}{\rho} [J_{m-1} + k_{t,1} \rho J'_{m-1} - m J_{m-1}] = \frac{1}{\rho} \left[ \cancel{J_{m-1}} - \underbrace{k_{t,1} \rho \cancel{J_{m-1}} + \cancel{m J_{m-1}}}_{k_{t,1} \rho J'_{m-1}} \right] = -k_{t,1} J_m$$

Para simplificar (1) primero hay que reescribir  $J''_m$  y  $J'_m$  en terminos de  $J_{m+1}$ ,  $J_m$ :

$$J''_m(z) = [J'_m(z)]' = \left[ -J_{m+1}(z) + \frac{m}{z} J_m(z) \right]' = -J'_{m+1}(z) - \frac{m}{z^2} J_m(z) + \frac{m}{z} J'_m(z) = \\ = - \left[ J_m(z) - \left( \frac{m+1}{z} \right) J_{m+1}(z) \right] - \frac{m}{z^2} J_m(z) + \frac{m}{z} \left[ -J_{m+1}(z) + \frac{m}{z} J_m(z) \right] = \\ = J_m(z) \left\{ -1 - \cancel{\frac{m}{z^2}} + \cancel{\frac{m^2}{z^2}} \right\} + J_{m+1}(z) \left\{ \frac{m+1}{z} - \frac{m}{z} \right\} = -J_m(z) + \frac{1}{z} J_{m+1}(z)$$

Reemplazando en (1):

$$(1) = \frac{J'_m k_{t,1}}{\rho} + k_{t,1}^2 J''_m + \frac{m^2 J_m}{\rho^2} = \frac{k_{t,1}}{\rho} \left[ \underbrace{\cancel{J_{m+1}} + \frac{m}{k_{t,1} \rho} J_m}_{J'_m} \right] + k_{t,1}^2 \left[ \underbrace{-J_m + \frac{1}{k_{t,1} \rho} J_{m+1}}_{J''_m} \right] + \frac{m^2 J_m}{\rho^2} = J_m \left\{ \frac{m(m+1)}{\rho^2} - k_{t,1}^2 \right\}$$

Reemplazando en  $e_{zm}(\rho)$  y sacando factor comun  $J_m$ :

$$e_{zm}(\rho) = \frac{ic}{\omega\varepsilon_1} \frac{i\omega}{4c} J_m \left[ -2ip_z H_m \left\{ \frac{m(m+1)}{\rho^2} - k_{t,1}^2 \right\} + k_z k_{t,1} p_+ e^{-i\theta_D} H_{m+1} - k_z k_{t,1} p_- e^{i\theta_D} H_{m-1} \right] e^{-im\theta_D - ik_z z_D}$$

$$e_{zm}(\rho) = -\frac{1}{4\varepsilon_1} J_m \left[ -2ip_z H_m \left\{ \frac{m(m+1)}{\rho^2} - k_{t,1}^2 \right\} + k_z k_{t,1} p_+ e^{-i\theta_D} H_{m+1} - k_z k_{t,1} p_- e^{i\theta_D} H_{m-1} \right] e^{-im\theta_D - ik_z z_D}$$

$$e_{zm}(\rho) = \frac{k_{t,1}}{4\varepsilon_1} e^{-im\theta_D - ik_z z_D} J_m(k_{t,1}\rho) \left[ 2ip_z H_m(k_{t,1}\rho) \left\{ \frac{m(m+1)}{\rho^2 k_{t,1}} - k_{t,1} \right\} - k_z p_+ e^{-i\theta_D} H_{m+1}(k_{t,1}\rho) + k_z p_- e^{i\theta_D} H_{m-1}(k_{t,1}\rho) \right]$$

$$e_{zm}(\rho) = \frac{k_{t,1}}{4\varepsilon_1} e^{-im\theta_D - ik_z z_D} H_m(k_{t,1}\rho) \left[ 2ip_z J_m(k_{t,1}\rho) \left\{ \frac{m(m+1)}{\rho^2 k_{t,1}} - k_{t,1} \right\} - k_z p_+ e^{-i\theta_D} J_{m+1}(k_{t,1}\rho) + k_z p_- e^{i\theta_D} J_{m-1}(k_{t,1}\rho) \right]$$



para  $\rho < \rho_D$  y  $\rho > \rho_D$ , respectivamente. **Diferencia con la formula del apunte de Depine:** aca sobra el  $\frac{m(m+1)}{\rho^2}$ . Recordar que tiene que haber un signo  $-$  de diferencia con la formula de Depine.

## 2.2 angular $e_{\theta m}$

Recordar que  $H_m = H_m(k_{t,1}\rho_D)$ ,  $J_m = J_m(k_{t,1}\rho)$  (se deriva  $J$  nada mas):

$$e_{\theta m}(\rho) = \frac{ic}{\omega\varepsilon_1} \left[ ik_z h_{\rho m}(\rho) - \frac{\partial h_{zm}(\rho)}{\partial \rho} \right],$$

$$\bullet h_{\rho m}(\rho) = \frac{i\omega}{4c} e^{-im\theta_D - ik_z z_D} \left\{ 2m \frac{p_z}{\rho} H_m J_m + ik_z p_+ e^{-i\theta_D} H_{m+1} J_{m+1} - ik_z p_- e^{i\theta_D} H_{m-1} J_{m-1} \right\},$$

$$\bullet h_{zm}(\rho) = \frac{i\omega}{4c} e^{-im\theta_D - ik_z z_D} J_m \left\{ -p_+ e^{-i\theta_D} H_{m+1} - p_- e^{i\theta_D} H_{m-1} \right\},$$

$$e_{\theta m}(\rho) = \frac{ic}{\omega\varepsilon_1} \frac{i\omega}{4c} e^{-im\theta_D - ik_z z_D} \left\{ 2mp_z \frac{ik_z}{\rho} H_m J_m + p_+ e^{-i\theta_D} (-k_z^2 H_{m+1} J_{m+1} + k_{t,1} J'_m H_{m+1}) + \right.$$

$$\left. + p_- e^{i\theta_D} (k_z^2 H_{m-1} J_{m-1} + k_{t,1} J'_m H_{m-1}) \right\} =$$

$$e_{\theta m}(\rho) = \frac{ic}{\omega\varepsilon_1} \frac{i\omega}{4c} e^{-im\theta_D - ik_z z_D} \left\{ 2mp_z \frac{ik_z}{\rho} H_m J_m + p_+ e^{-i\theta_D} H_{m+1} (-k_z^2 J_{m+1} + k_{t,1} J'_m) + p_- e^{i\theta_D} H_{m-1} (k_z^2 J_{m-1} + k_{t,1} J'_m) \right\}$$

no se parece a la formula del apunte de Depine

## 3 Campos totales

Se agregan los campos del dipolo en los campos longitudinales del medio 1 (principio de superposicion) porque  $\rho_D < R$  (el dipolo está en el interior del cilindro):

$$E_z^{(1)}(\rho, \phi, z, t) = \sum_{n=-\infty}^{\infty} [A_n^{(1)} J_n(k_{t,1}\rho) + e_{zm}(\rho)] e^{in\phi} e^{i(k_z z - \omega t)} \quad \rho < R$$

$$E_z^{(2)}(\rho, \phi, z, t) = \sum_{n=-\infty}^{\infty} [B_o i^n J_n(k_{t,2}\rho) + B_n^{(2)} H_n^{(1)}(k_{t,2}\rho)] e^{in\phi} e^{i(k_z z - \omega t)} \quad \rho > R$$

$$H_z^{(1)}(\rho, \phi, z, t) = \sum_{n=-\infty}^{\infty} [C_n^{(1)} J_n(k_{t,1}\rho) + h_{zm}(\rho)] e^{in\phi} e^{i(k_z z - \omega t)} \quad \rho < R$$

$$H_z^{(2)}(\rho, \phi, z, t) = \sum_{n=-\infty}^{\infty} [A_o i^n J_n(k_{t,2}\rho) + D_n^{(2)} H_n^{(1)}(k_{t,2}\rho)] e^{in\phi} e^{i(k_z z - \omega t)} \quad \rho > R$$

Se deduce de lo anterior que las unidades de los campos del dipolo son las mismas unidades que la de los coeficientes. Los campos del dipolo  $e_{zm}(\rho)$  y  $h_{zm}(\rho)$  son diferentes para  $\rho > \rho_D$  y  $\rho < \rho_D$  (siendo  $\rho_D$  la posicion del dipolo). Se utilizan las siguientes formulas para obtener los campos transversales:

$$E_\rho = \frac{1}{k_t^2} \left[ \frac{i\omega\mu}{c\rho} \frac{\partial H_z}{\partial \phi} + ik_z \frac{\partial E_z}{\partial \rho} \right] \quad E_\phi = \frac{1}{k_t^2} \left[ \frac{ik_z}{\rho} \frac{\partial E_z}{\partial \phi} - \frac{i\omega\mu}{c} \frac{\partial H_z}{\partial \rho} \right]$$

$$H_\rho = \frac{1}{k_t^2} \left[ -\frac{i\omega\varepsilon}{c} \frac{1}{\rho} \frac{\partial E_z}{\partial \phi} + ik_z \frac{\partial H_z}{\partial \rho} \right] \quad H_\phi = \frac{1}{k_t^2} \left[ \frac{ik_z}{\rho} \frac{\partial H_z}{\partial \phi} + \frac{i\omega\varepsilon}{c} \frac{\partial E_z}{\partial \rho} \right]$$

Para el medio 1, se reemplazan por las formulas  $E_z^{(1)}, H_z^{(1)}$  en las formulas anteriores para obtener las formulas de los campos transversales. Para las derivadas respecto de  $\phi : \partial_\phi \rightarrow in$ . En los términos con  $\partial_\phi$  ya hay un factor  $i$  entonces se simplifica  $i^2 = -1$ , es decir que el signo cambia. En las derivadas respecto de la coordenada radial  $\partial_\rho$  aparece el factor  $k_{t,1}$  ( $k_{t,1} = \sqrt{k_1^2 - k_z^2}$ ):

$$\begin{aligned} E_\rho^{(1)} &= \frac{1}{k_{t,1}^2} \sum_n \left[ -\frac{\omega\mu_1 n}{c\rho} \left[ C_n^{(1)} J_n(k_{t,1}\rho) + h_{zn}(\rho) \right] + ik_z \left[ k_{t,1} A_n^{(1)} J'_n(k_{t,1}\rho) + e'_{zn}(\rho) \right] \right] e^{in\phi} e^{i(k_z z - \omega t)} \\ E_\phi^{(1)} &= \frac{1}{k_{t,1}^2} \sum_n \left[ -\frac{k_z n}{\rho} \left[ A_n^{(1)} J_n(k_{t,1}\rho) + e_{zn}(\rho) \right] - \frac{i\omega\mu_1}{c} \left[ k_{t,1} C_n^{(1)} J'_n(k_{t,1}\rho) + h'_{zn}(\rho) \right] \right] e^{in\phi} e^{i(k_z z - \omega t)} \\ H_\rho^{(1)} &= \frac{1}{k_{t,1}^2} \sum_n \left[ \frac{\omega\varepsilon_1 n}{c\rho} \left[ A_n^{(1)} J_n(k_{t,1}\rho) + e_{zn}(\rho) \right] + ik_z \left[ k_{t,1} C_n^{(1)} J'_n(k_{t,1}\rho) + h'_{zn}(\rho) \right] \right] e^{in\phi} e^{i(k_z z - \omega t)} \\ H_\phi^{(1)} &= \frac{1}{k_{t,1}^2} \sum_n \left[ -\frac{k_z n}{\rho} \left[ C_n^{(1)} J_n(k_{t,1}\rho) + h_{zn}(\rho) \right] + \frac{i\omega\varepsilon_1}{c} \left[ k_{t,1} A_n^{(1)} J'_n(k_{t,1}\rho) + e'_{zn}(\rho) \right] \right] e^{in\phi} e^{i(k_z z - \omega t)} \end{aligned}$$

Para el medio 2, se reemplazan por las formulas  $E_z^{(2)}, H_z^{(2)}$  y el razonamiento sobre las derivadas que se menciono en el medio 1 se repiten:

$$\begin{aligned} E_\rho^{(2)} &= \frac{1}{k_{t,2}} \sum_n \left[ -\frac{\omega\mu_2 n}{c\rho k_{t,2}} (A_o i^n J_n(k_{t,2}\rho) + D_n^{(2)} H_n^{(1)}(k_{t,2}\rho)) + ik_z (B_o i^n J'_n(k_{t,2}\rho) + B_n^{(2)} H_n'^{(1)}(k_{t,2}\rho)) \right] e^{in\phi} e^{i(k_z z - \omega t)} \\ E_\phi^{(2)} &= \frac{1}{k_{t,2}} \sum_n \left[ -\frac{k_z n}{\rho k_{t,2}} (B_o i^n J_n(k_{t,2}\rho) + B_n^{(2)} H_n^{(1)}(k_{t,2}\rho)) - \frac{i\omega\mu_2}{c} (A_o i^n J'_n(k_{t,2}\rho) + D_n^{(2)} H_n'^{(1)}(k_{t,2}\rho)) \right] e^{in\phi} e^{i(k_z z - \omega t)} \\ H_\rho^{(2)} &= \frac{1}{k_{t,2}} \sum_n \left[ \frac{\omega\varepsilon_2 n}{c\rho k_{t,2}} (B_o i^n J_n(k_{t,2}\rho) + B_n^{(2)} H_n^{(1)}(k_{t,2}\rho)) + ik_z (A_o i^n J'_n(k_{t,2}\rho) + D_n^{(2)} H_n'^{(1)}(k_{t,2}\rho)) \right] e^{in\phi} e^{i(k_z z - \omega t)} \\ H_\phi^{(2)} &= \frac{1}{k_{t,2}} \sum_n \left[ -\frac{k_z n}{\rho k_{t,2}} (A_o i^n J_n(k_{t,2}\rho) + D_n^{(2)} H_n^{(1)}(k_{t,2}\rho)) + \frac{i\omega\varepsilon_2}{c} (B_o i^n J'_n(k_{t,2}\rho) + B_n^{(2)} H_n'^{(1)}(k_{t,2}\rho)) \right] e^{in\phi} e^{i(k_z z - \omega t)} \end{aligned}$$

Las formulas del medio 2 no cambiaron porque el dipolo esta en el interior del cilindro.

## 4 Condiciones de contorno

Las condiciones de borde ( $\rho = R$ ) para los campos son:

$$E_z^{(1)}(\rho = R, \phi, z) = E_z^{(2)}(\rho = R, \phi, z), \quad (20)$$

$$E_\phi^{(1)}(\rho = R, \phi, z) = E_\phi^{(2)}(\rho = R, \phi, z), \quad (21)$$

$$H_z^{(1)}(\rho = R, \phi, z) - \frac{4\pi}{c} \sigma(\omega) E_\phi(\rho = R, \phi, z) = H_z^{(2)}(\rho = R, \phi, z), \quad (22)$$

$$H_\phi^{(1)}(\rho = R, \phi, z) + \frac{4\pi}{c} \sigma(\omega) E_z(\rho = R, \phi, z) = H_\phi^{(2)}(\rho = R, \phi, z). \quad (23)$$

Observemos que los campos  $E_z$  y  $E_\phi$  son continuos en  $\rho = R$ , por lo tanto podemos elegir el campo  $E_\phi^{(1)}$  o el campo  $E_\phi^{(2)}$  en la tercera ecuación. Lo mismo para la cuarta ecuación: podemos elegir el campo  $E_z^{(1)}$  o el campo  $E_z^{(2)}$ . De la Eq. 20:

$$E_z^{(1)}(\rho = R, \phi, z) = E_z^{(2)}(\rho = R, \phi, z) \rightarrow A_n^{(1)} J_n(k_{t,1}R) + e_{zn}(R) = B_o i^n J_n(k_{t,2}R) + B_n^{(2)} H_n^{(1)}(k_{t,2}R)$$

La ultima condición de borde Eq. 23: (vamos a ordenar las condiciones segun cómo se arme la matriz)

$$H_\phi^{(1)}(\rho = R, \phi, z) + \frac{4\pi}{c} \sigma(\omega) E_z^{(1)}(\rho = R, \phi, z) = H_\phi^{(2)}(\rho = R, \phi, z)$$

$$\frac{1}{k_{t,1}^2} \left[ -\frac{k_z n}{R} \left[ C_n^{(1)} J_n(k_{t,1} R) + h_{zn}(R) \right] + \frac{i\omega \varepsilon_1}{c} \left[ k_{t,1} A_n^{(1)} J'_n(k_{t,1} R) + e'_{zn}(R) \right] \right] + \frac{4\pi\sigma}{c} \left[ A_n^{(1)} J_n(k_{t,1} R) + e_{zn}(R) \right] =$$

$$\frac{1}{k_{t,2}} \left[ -\frac{k_z n}{R k_{t,2}} (A_o i^n J_n(k_{t,2} R) + D_n^{(2)} H_n^{(1)}(k_{t,2} R)) + \frac{i\omega \varepsilon_2}{c} (B_o i^n J'_n(k_{t,2} R) + B_n^{(2)} H_n'^{(1)}(k_{t,2} R)) \right]$$

$$A_n^{(1)} \left( \frac{4\pi\sigma}{c} J_{1n} + \frac{i\omega \varepsilon_1}{c k_{t,1}} J'_{1n} \right) - \frac{i\omega \varepsilon_2}{c k_{t,2}} B_n^{(2)} H'_{2n} - C_n^{(1)} \frac{k_z n}{R k_{t,1}^2} J_{1n} + \frac{k_z n}{R k_{t,2}^2} D_n^{(2)} H_{2n} =$$

$$= -\frac{k_z n}{R k_{t,2}^2} A_o i^n J_{2n} + \frac{i\omega \varepsilon_2}{c k_{t,2}} B_o i^n J'_{2n} - \frac{4\pi\sigma}{c} e_{zn}(R) + \frac{k_z n}{R k_{t,1}^2} h_{zn}(R) - \frac{i\omega \varepsilon_1}{c k_{t,1}^2} e'_{zn}(R)$$

$$\boxed{A_n^{(1)} \left( \frac{4\pi\sigma}{c} J_{1n} + \frac{i\omega \varepsilon_1}{c k_{t,1}} J'_{1n} \right) - \frac{i\omega \varepsilon_2}{c k_{t,2}} B_n^{(2)} H'_{2n} - C_n^{(1)} \frac{k_z n}{R k_{t,1}^2} J_{1n} + \frac{k_z n}{R k_{t,2}^2} D_n^{(2)} H_{2n} =}$$

$$= \frac{k_z n}{R} \left[ \frac{h_{zn}(R)}{k_{t,1}^2} - \frac{A_o i^n}{k_{t,2}^2} J_2 \right] + \frac{i\omega}{c} \left[ \frac{\varepsilon_2 B_o i^n}{k_{t,2}} J'_2 - \frac{\varepsilon_1}{k_{t,1}^2} e'_{zn}(R) \right] - \frac{4\pi\sigma}{c} e_{zn}(R)$$

La tercera condicion de contorno Eq. 22 es:

$$H_z^{(1)}(\rho = R, \phi, z) - \frac{4\pi}{c} \sigma(\omega) E_\phi^{(1)}(\rho = R, \phi, z) = H_z^{(2)}(\rho = R, \phi, z) :$$

$$C_n^{(1)} J_n(k_{t,1} R) + h_{zn}(R) - \frac{4\pi\sigma}{c} \cdot \frac{1}{k_{t,1}^2} \left\{ -\frac{k_z n}{R} \left[ A_n^{(1)} J_n(k_{t,1} R) + e_{zn}(R) \right] - \frac{i\omega \mu_1}{c} \left[ k_{t,1} C_n^{(1)} J'_n(k_{t,1} R) + h'_{zn}(R) \right] \right\} =$$

$$[A_o i^n J_n(k_{t,2} R) + D_n^{(2)} H_n^{(1)}(k_{t,2} R)]$$

$$\frac{4\pi\sigma}{c} \frac{k_z n}{R k_{t,1}^2} A_n^{(1)} J_{1n} + C_n^{(1)} \left( J_{1n} + \frac{4\pi\sigma}{c} \frac{i\omega \mu_1}{c k_{t,1}} J'_{1n} \right) - D_n^{(2)} H_{2n} =$$

$$= A_o i^n J_{2n} - h_{zn}(R) - \frac{4\pi\sigma}{c} \frac{k_z n}{R k_{t,1}^2} e_{zn}(R) - \frac{4\pi\sigma}{c} \frac{i\omega \mu_1}{c k_{t,1}^2} h'_{zn}(R)$$

$$\frac{4\pi\sigma}{c} \frac{k_z n}{R k_{t,1}^2} A_n^{(1)} J_{1n} + C_n^{(1)} \left( J_{1n} + \frac{4\pi\sigma}{c} \frac{i\omega \mu_1}{c k_{t,1}} J'_{1n} \right) - D_n^{(2)} H_{2n} = A_o i^n J_{2n} - h_{zn}(R) - \frac{4\pi\sigma}{c} \left[ \frac{k_z n}{R k_{t,1}^2} e_{zn}(R) + \frac{i\omega \mu_1}{c k_{t,1}^2} h'_{zn}(R) \right]$$

Se repite lo mismo para la segunda condición de borde (Eq. 21):

$$E_\phi^{(1)}(\rho = R, \phi, z) = E_\phi^{(2)}(\rho = R, \phi, z) :$$

$$\frac{1}{k_{t,1}^2} \left[ -\frac{k_z n}{R} \left[ A_n^{(1)} J_n(k_{t,1} R) + e_{zn}(R) \right] - \frac{i\omega \mu_1}{c} \left[ k_{t,1} C_n^{(1)} J'_n(k_{t,1} R) + h'_{zn}(R) \right] \right] =$$

$$\frac{1}{k_{t,2}} \left[ -\frac{k_z n}{R k_{t,2}} [B_o i^n J_n(k_{t,2} R) + B_n^{(2)} H_n^{(1)}(k_{t,2} R)] - \frac{i\omega \mu_2}{c} [A_o i^n J'_n(k_{t,2} R) + D_n^{(2)} H_n'^{(1)}(k_{t,2} R)] \right]$$

$$- \frac{k_z n}{R k_{t,1}^2} A_n^{(1)} J_{1n} - \frac{i\omega \mu_1}{c k_{t,1}} C_n^{(1)} J'_{1n} + \frac{k_z n}{R k_{t,2}^2} B_n^{(2)} H_{2n} + \frac{i\omega \mu_2}{c k_{t,2}} D_n^{(2)} H'_{2n} =$$

$$= -\frac{i\omega \mu_2}{c k_{t,2}} A_o i^n J'_{2n} - \frac{k_z n}{R k_{t,2}^2} B_o i^n J_{2n} + \frac{k_z n}{R k_{t,1}^2} e_{zn}(R) + \frac{i\omega \mu_1}{c k_{t,1}^2} h'_{zn}(R) =$$

Con  $J_{1n} \equiv J_n(k_{t,1}R)$ ,  $H_{2n}^{(1)} \equiv H_n(k_{t,2}R)$  y los terminos que van con  $A_o$ ,  $B_o$  tienen  $J_{2n} \equiv J_n(k_{t,2}R)$ . La segunda condicion de contorno es:

$$-\frac{k_z n}{R k_{t,1}^2} A_n^{(1)} J_{1n} - \frac{i\omega\mu_1}{c k_{t,1}} C_n^{(1)} J'_{1n} + \frac{k_z n}{R k_{t,2}^2} B_n^{(2)} H_{2n} + \frac{i\omega\mu_2}{c k_{t,2}} D_n^{(2)} H'_{2n} = \frac{i\omega}{c} \left[ \frac{\mu_1}{k_{t,1}^2} h'_{zn}(R) - \frac{\mu_2}{k_{t,2}} A_o i^n J'_{2n} \right] + \frac{k_z n}{R} \left[ \frac{e_{zn}(R)}{k_{t,1}^2} - \frac{B_o i^n}{k_{t,2}^2} J_{2n} \right]$$

Se simplifica la notación de la siguiente manera:  $J_i = J_n(k_{t,i}R)$ ,  $H_2 = H_n^{(1)}(k_{t,2}R)$  sobreentendiendo el modo n-esimo. Con las 4 ecuaciones recuadradas, se construye la matriz de 4x4 del caso inhomogeneo:

$$\begin{pmatrix} J_1 & -H_2 & 0 & 0 \\ \frac{4\pi\sigma}{c} J_1 + \frac{i\omega\varepsilon_1}{c k_{t,1}} J'_1 & -\frac{i\omega\varepsilon_2}{k_{t,2}c} H'_2 & -\frac{k_z\nu}{k_{t,1}^2 R} J_1 & \frac{k_z\nu}{k_{t,2}^2 R} H_2 \\ \frac{4\pi\sigma k_z\nu}{c R k_{t,1}^2} J_1 & 0 & J_1 + \frac{4\pi i\sigma\omega\mu_1}{c^2 k_{t,1}} J'_1 & -H_2 \\ -\frac{k_z\nu}{R k_{t,1}^2} J_1 & \frac{k_z\nu}{R k_{t,2}^2} H_2 & -\frac{i\omega\mu_1}{c k_{t,1}} J'_1 & \frac{i\omega\mu_2}{c k_{t,2}} H'_2 \end{pmatrix} \begin{bmatrix} A_\nu^{(1)} \\ B_\nu^{(2)} \\ C_\nu^{(1)} \\ D_\nu^{(2)} \end{bmatrix} =$$

$$= \begin{bmatrix} B_o i^\nu J_2 - e_{z\nu}(R) \\ \frac{k_z\nu}{R} \left[ \frac{h_{z\nu}(R)}{k_{t,1}^2} - \frac{A_o i^\nu}{k_{t,2}^2} J_2 \right] + \frac{i\omega}{c} \left[ \frac{\varepsilon_2 B_o i^\nu}{k_{t,2}} J'_2 - \frac{\varepsilon_1}{k_{t,1}^2} e'_{z\nu}(R) \right] - \frac{4\pi\sigma}{c} e_{z\nu}(R) \\ A_o i^\nu J_{2\nu} - h_{z\nu}(R) - \frac{4\pi\sigma}{c} \left[ \frac{k_z\nu}{R k_{t,1}^2} e_{z\nu}(R) + \frac{i\omega\mu_1}{c k_{t,1}^2} h'_{z\nu}(R) \right] \\ \frac{i\omega}{c} \left[ \frac{\mu_1}{k_{t,1}^2} h'_{z\nu}(R) - \frac{\mu_2}{k_{t,2}} A_o i^\nu J'_2 \right] + \frac{k_z\nu}{R} \left[ \frac{e_{z\nu}(R)}{k_{t,1}^2} - \frac{B_o i^\nu}{k_{t,2}^2} J_2 \right] \end{bmatrix}$$

Observar que la matriz y los campos quedaron escritos en funcion de  $h_{zm}(R)$ ,  $e_{zm}(R)$ , con lo cual sólo hay que hallar dichas funciones para  $\rho < \rho_D$  y  $\rho > \rho_D$ .

$$h_{zm}(\rho) = \frac{i\omega}{4c} k_{t,1} e^{-im\theta_D - ik_z z_D} J_m(k_{t,1}\rho) \left\{ -p_+ e^{-i\theta_D} H_{m+1}(k_{t,1}\rho_D) - p_- e^{i\theta_D} H_{m-1}(k_{t,1}\rho_D) \right\} \quad \rho < \rho_D,$$

$$h_{zm}(\rho) = \frac{i\omega}{4c} k_{t,1} e^{-im\theta_D - ik_z z_D} H_m^{(1)}(k_{t,1}\rho) \left\{ -p_+ e^{-i\theta_D} J_{m+1}(k_{t,1}\rho_D) - p_- e^{i\theta_D} J_{m-1}(k_{t,1}\rho_D) \right\} \quad \rho > \rho_D$$

Derivando respecto de  $\rho$ :

$$h'_{zm}(\rho) = \frac{\partial h_{zm}(\rho)}{\partial(k_{t,1}\rho)} \frac{\partial(k_{t,1}\rho)}{\partial\rho} = k_{t,1} \frac{\partial h_{zm}(\rho)}{\partial(k_{t,1}\rho)} =$$

$$h'_{zm}(\rho) = \frac{i\omega}{4c} k_{t,1}^2 e^{-im\theta_D - ik_z z_D} J'_m(k_{t,1}\rho) \left\{ -p_+ e^{-i\theta_D} H_{m+1}(k_{t,1}\rho_D) - p_- e^{i\theta_D} H_{m-1}(k_{t,1}\rho_D) \right\} \quad \rho < \rho_D,$$

$$h'_{zm}(\rho) = \frac{i\omega}{4c} k_{t,1}^2 e^{-im\theta_D - ik_z z_D} H'_m(k_{t,1}\rho) \left\{ -p_+ e^{-i\theta_D} J_{m+1}(k_{t,1}\rho_D) - p_- e^{i\theta_D} J_{m-1}(k_{t,1}\rho_D) \right\} \quad \rho > \rho_D$$

El campo electrico del dipolo:

$$e_{zm}(\rho) = \frac{k_{t,1}}{4\varepsilon_1} e^{-im\theta_D - ik_z z_D} J_m(k_{t,1}\rho) \left[ 2ip_z H_m(k_{t,1}\rho_D) \left\{ \frac{m(m+1)}{\rho^2 k_{t,1}} - k_{t,1} \right\} - k_z p_+ e^{-i\theta_D} H_{m+1}(k_{t,1}\rho_D) + \right. \\ \left. + k_z p_- e^{i\theta_D} H_{m-1}(k_{t,1}\rho_D) \right] \quad \rho < \rho_D$$

$$e_{zm}(\rho) = \frac{k_{t,1}}{4\varepsilon_1} e^{-im\theta_D - ik_z z_D} H_m(k_{t,1}\rho) \left[ 2ip_z J_m(k_{t,1}\rho_D) \left\{ \frac{m(m+1)}{\rho^2 k_{t,1}} - k_{t,1} \right\} - k_z p_+ e^{-i\theta_D} J_{m+1}(k_{t,1}\rho_D) + \right. \\ \left. + k_z p_- e^{i\theta_D} J_{m-1}(k_{t,1}\rho_D) \right] \quad \rho > \rho_D$$

Su derivada respecto de  $\rho$ :

$$e'_{zm}(\rho) = \frac{k_{t,1}^2}{4\varepsilon_1} e^{-im\theta_D - ik_z z_D} J'_m(k_{t,1}\rho) \left[ 2ip_z H_m(k_{t,1}\rho_D) \left\{ \frac{m(m+1)}{\rho^2 k_{t,1}} - k_{t,1} \right\} - k_z p_+ e^{-i\theta_D} H_{m+1}(k_{t,1}\rho_D) + \right. \\ \left. + k_z p_- e^{i\theta_D} H_{m-1}(k_{t,1}\rho_D) \right] \quad \rho < \rho_D$$

$$e'_{zm}(\rho) = \frac{k_{t,1}^2}{4\varepsilon_1} e^{-im\theta_D - ik_z z_D} H'_m(k_{t,1}\rho) \left[ 2ip_z J_m(k_{t,1}\rho_D) \left\{ \frac{m(m+1)}{\rho^2 k_{t,1}} - k_{t,1} \right\} - k_z p_+ e^{-i\theta_D} J_{m+1}(k_{t,1}\rho_D) + \right. \\ \left. + k_z p_- e^{i\theta_D} J_{m-1}(k_{t,1}\rho_D) \right] \quad \rho > \rho_D$$

El último paso es la adimensionalización de las cantidades para simplificar el trabajo numérico. Para ello, se usan las variables adimensionales:  $x_{t,j} \equiv k_{t,j}/k_0$  y  $\bar{R} \equiv Rk_0$  en el sistema matricial anterior:

$$\begin{pmatrix} J_1 & -H_2 & 0 & 0 \\ \frac{4\pi\sigma J_1}{c} + \frac{i\varepsilon_1 J'_1}{x_{t,1}} & -\frac{i\varepsilon_2 H'_2}{x_{t,2}} & -\frac{x_z \nu J_1}{x_{t,1}^2 \bar{R}} & \frac{x_z \nu H_2}{x_{t,2}^2 \bar{R}} \\ \frac{4\pi\sigma}{c} \frac{x_z \nu J_1}{\bar{R} x_{t,1}^2} & 0 & J_1 + \frac{4\pi\sigma}{c} \frac{i\mu_1 J'_1}{x_{t,1}} & -H_2 \\ -\frac{x_z \nu J_1}{\bar{R} x_{t,1}^2} & \frac{x_z \nu H_2}{\bar{R} x_{t,2}^2} & -\frac{i\mu_1 J'_1}{x_{t,1}} & \frac{i\mu_2 H'_2}{x_{t,2}} \end{pmatrix} \begin{bmatrix} A_\nu^{(1)} \\ B_\nu^{(2)} \\ C_\nu^{(1)} \\ D_\nu^{(2)} \end{bmatrix} =$$

=

$$= \left[ \begin{array}{c} B_o i^\nu J_2 - e_{z\nu}(R) \\ \frac{x_z \nu}{\bar{R}} \left[ \frac{h_{z\nu}(R)}{x_{t,1}^2} - \frac{i^\nu A_o}{x_{t,2}^2} J_2 \right] + i \left[ \frac{\varepsilon_2 i^\nu B_o}{x_{t,2}} J_2' - \frac{\varepsilon_1 (e'_{z\nu}(R)/k_0)}{x_{t,1}^2} \right] - \frac{4\pi\sigma}{c} e_{z\nu}(R) \\ A_o i^\nu J_2 - h_{z\nu}(R) - \frac{4\pi\sigma}{c} \frac{1}{x_{t,1}^2} \left[ \frac{x_z \nu}{\bar{R}} e_{z\nu}(R) + i\mu_1 (h'_{z\nu}(R)/k_0) \right] \\ i \left[ \mu_1 (h'_{z\nu}(R)/k_0) - \frac{\mu_2}{x_{t,2}} i^\nu A_o J_2' \right] + \frac{x_z \nu}{\bar{R}} \left[ \frac{e_{z\nu}(R)}{x_{t,1}^2} - \frac{i^\nu B_o}{x_{t,2}^2} J_2 \right] \end{array} \right]$$

Las unidades de los campos del dipolo son las mismas que la de los coeficientes  $A_o, B_o, A_\nu^{(1)}, B_\nu^{(2)}, C_\nu^{(1)}, D_\nu^{(2)}$  para que la formula de los campos longitudinales tenga sentido. Las unidades dan bien porque cuando aparece un  $e', h'$  siempre hay un  $k_0$  dividiendo.

## A Apendice

$$\begin{aligned}\vec{p} &= p_x \hat{x} + p_y \hat{y} \\ \vec{p} &= p_\rho \hat{\rho} + p_\theta \hat{\theta}\end{aligned}$$

Los versores se relacionan de la siguiente manera:

$$\begin{aligned}\hat{\rho} &= \cos(\theta) \hat{x} + \sin(\theta) \hat{y} \\ \hat{\theta} &= -\sin(\theta) \hat{x} + \cos(\theta) \hat{y}\end{aligned}$$

$$\begin{aligned}\hat{x} &= \cos(\theta) \hat{\rho} - \sin(\theta) \hat{\theta} \\ \hat{y} &= \sin(\theta) \hat{\rho} + \cos(\theta) \hat{\theta}\end{aligned}$$

Se reemplazan los versores y se junta todo lo que tiene  $\hat{x}$  y todo lo que tiene  $\hat{y}$  para obtener  $p_x$  y  $p_y$  en función de las coordenadas cilíndricas:

$$\begin{aligned}\vec{p} &= p_\rho \hat{\rho} + p_\theta \hat{\theta} \\ \vec{p} &= p_\rho \left( \underbrace{\cos(\theta) \hat{x} + \sin(\theta) \hat{y}}_{\hat{\rho}} \right) + p_\theta \left( \underbrace{-\sin(\theta) \hat{x} + \cos(\theta) \hat{y}}_{\hat{\theta}} \right) \\ \vec{p} &= \underbrace{(p_\rho \cos(\theta) - p_\theta \sin(\theta))}_{p_x} \hat{x} + \underbrace{(p_\rho \sin(\theta) + p_\theta \cos(\theta))}_{p_y} \hat{y} = p_x \hat{x} + p_y \hat{y}\end{aligned}$$

$$\begin{aligned}p_x &= p_\rho \cos(\theta) - p_\theta \sin(\theta) \\ p_y &= p_\rho \sin(\theta) + p_\theta \cos(\theta)\end{aligned}$$

Análogo para obtener  $p_\rho$  y  $p_\theta$  en función de las coordenadas cartesianas:

$$\begin{aligned}\vec{p} &= p_x \hat{x} + p_y \hat{y} \\ \vec{p} &= p_x \left( \underbrace{\cos(\theta) \hat{\rho} - \sin(\theta) \hat{\theta}}_{\hat{x}} \right) + p_y \left( \underbrace{\sin(\theta) \hat{\rho} + \cos(\theta) \hat{\theta}}_{\hat{y}} \right) \\ \vec{p} &= \underbrace{(p_x \cos(\theta) + p_y \sin(\theta))}_{p_\rho} \hat{\rho} + \underbrace{(-p_x \sin(\theta) + p_y \cos(\theta))}_{p_\theta} \hat{\theta} = p_\rho \hat{\rho} + p_\theta \hat{\theta}\end{aligned}$$

$$\begin{aligned}p_\rho &= p_x \cos(\theta) + p_y \sin(\theta) \\ p_\theta &= -p_x \sin(\theta) + p_y \cos(\theta)\end{aligned}$$

Propiedades de las funciones  $C = J, Y, H^{(1)}, H^{(2)}$ :

$$C_{n-1}(z) + C_{n+1}(z) = \frac{2n}{z} C_n(z), \quad (24a)$$

$$C_{n-1}(z) - C_{n+1}(z) = 2C'_n(z), \quad (24b)$$

$$C'_n(z) = C_{n-1}(z) - \frac{n}{z}C_n(z), \quad (24c)$$

$$C'_n(z) = -C_{n+1}(z) + \frac{n}{z}C_n(z). \quad (24d)$$

## References

M. Cuevas. Graphene coated subwavelength wires: a theoretical investigation of emission and radiation properties. *Journal of Quantitative Spectroscopy & Radiative Transfer*, 200:190–197, 2017.