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United States Patent [19][11] **Patent Number:** **5,365,447****Dennis**[45] **Date of Patent:** **Nov. 15, 1994**[54] **GPS AND SATELLITE NAVIGATION SYSTEM**[76] **Inventor:** **Arthur R. Dennis**, 2624 Rose Hill Dr., League City, Tex. 77573[21] **Appl. No.:** **763,379**[22] **Filed:** **Sep. 20, 1991**[51] **Int. Cl.⁵** **H04B 7/185**[52] **U.S. Cl.** **364/449; 342/357; 342/356; 342/352**[58] **Field of Search** **342/352, 356, 357, 451, 342/457; 364/443, 449, 459; 73/178 R**[56] **References Cited****U.S. PATENT DOCUMENTS**

4,445,118	4/1984	Taylor et al.	342/356
4,613,864	9/1986	Hofgen	342/357
4,652,884	3/1987	Starker	342/357
4,751,512	6/1988	Longaker	342/357
4,812,991	3/1989	Hatch	364/458
4,876,550	10/1989	Kelly	342/451
4,879,713	11/1989	Ichiyoshi	370/75
4,894,662	1/1990	Counselman	342/357
4,918,609	4/1990	Yamawaki	364/449
5,017,926	5/1991	Ames et al.	342/357
5,036,330	7/1991	Imae et al.	342/357
5,041,833	8/1991	Weinberg	342/357

FOREIGN PATENT DOCUMENTS

2180426 9/1989 United Kingdom

OTHER PUBLICATIONS

Paul Massatt and Karl Rudnick, "Geometric Formulas for Dilution of Precision Calculations", *Journal of The Institute of Navigation*, vol. 37, No. 4, pp. 379-391, published in Los Angeles, California, Dec. 1989.

A. R. Dennis, "Special Methods for Using GPS in the Offshore Industry", 12 pages, paper presented at ION GPS-89, Colorado Springs, Colorado, Sep. 27-29, 1989.

Offshore Navigation, Inc., Report on IDGPS Demon-

stration, 17 pages, published in Houston, Texas, Oct. 1990.

A. R. Dennis, "STARFIX—A New High-Precision Satellite Positioning System", 9 pages, presented at International Symposium on Marine Positioning: INS-MAP 86 in Reston, Virginia on Oct. 14-17, 1986.

A. R. Dennis, "New Satellite Positioning System in Operation for Civilian Marine Use", 3 pages, published in *Sea Technology* in Houston, Texas in Sep. 1986.

Rudy Lambert, "Integrating Differential GPS for Higher 3-D Seismic Survey Accuracy", pp. 35-36, 38, Mar. 1992 issue of *Sea Technology*.

Kim Cassis, "STARS—The Second Part of Houston", pp. 24-26, 31-32 in Feb. 1992 issue of DBA.

Interavia, *Space Directory* 1990-1991, pp. 179-181, 395, 405-407, 410-412, published in 1990.

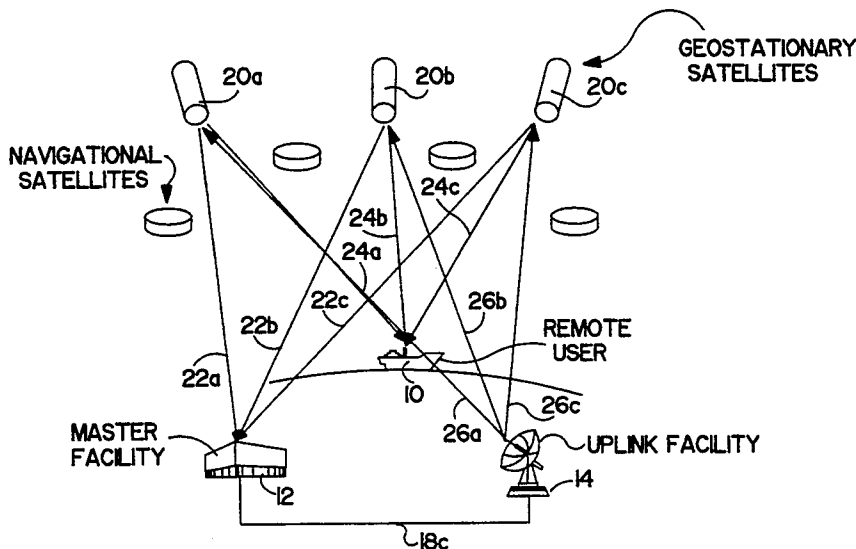
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[57] **ABSTRACT**

A satellite-based navigation system providing improved accuracy and reliability over wide geographical areas, including remote regions, is disclosed. Ranging-type signals transmitted through two or more commercial geostationary telecommunication satellites are received at known reference locations where navigation and correction information is generated and transmitted back to remote users. At the same time, the reference stations receive signals from the Global Positioning System (GPS), generate corrections for the GPS measurements, then transmit these corrections to the remote user. The remote user receives all of this information plus direct measurements from both the GPS and the geostationary satellites and, using conditional error processing techniques, provides a position solution whose accuracy and reliability exceeds that of GPS alone.

5 Claims, 4 Drawing Sheets

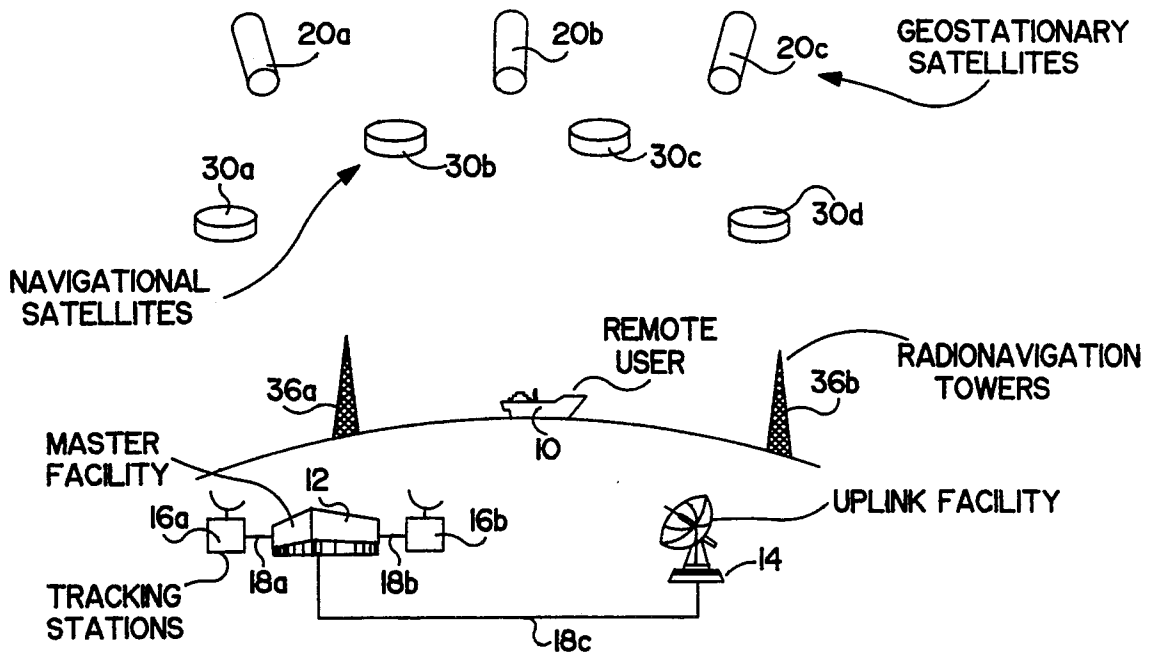


FIG. 1

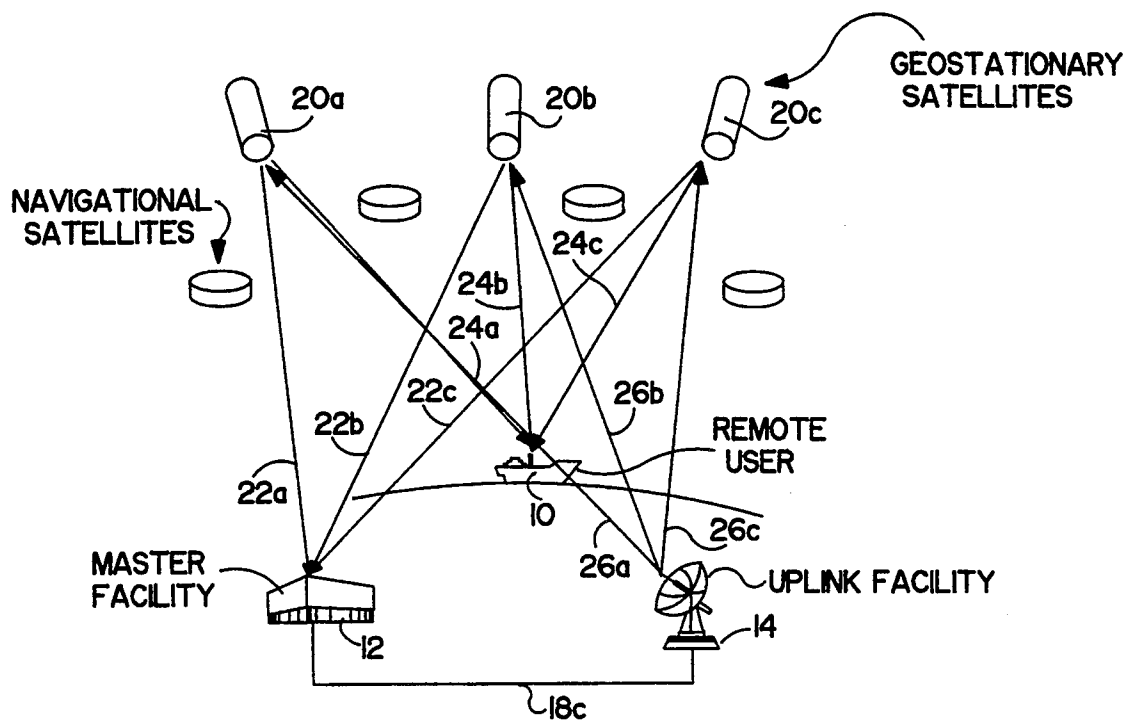


FIG. 2

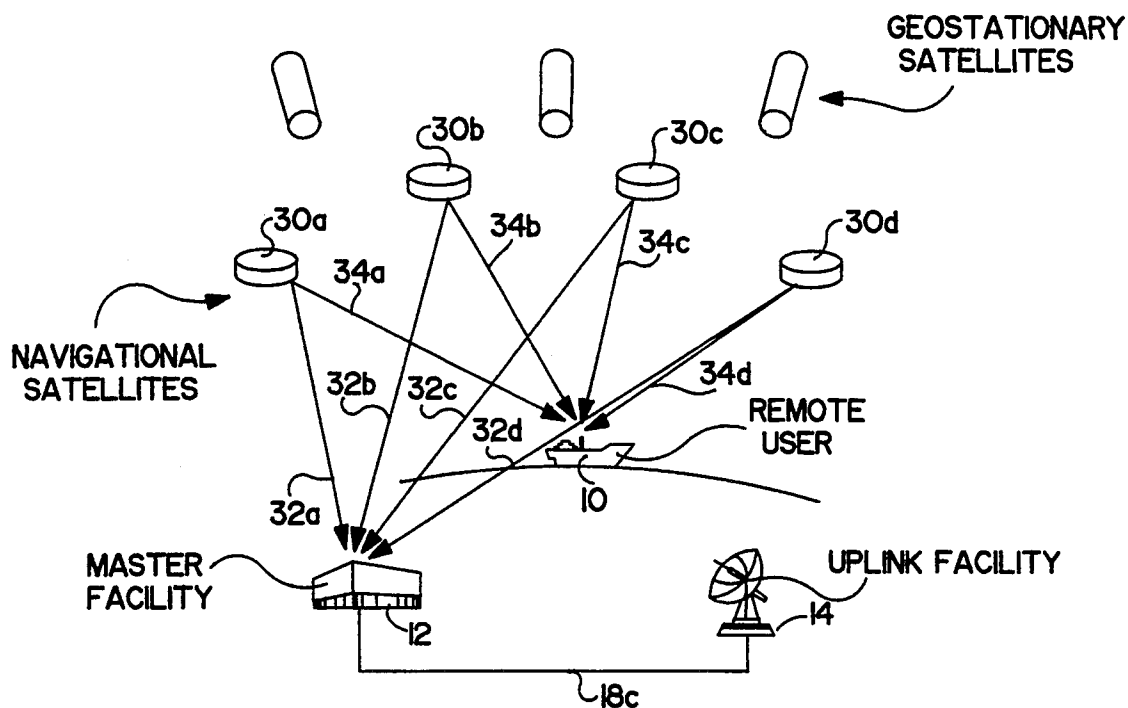


FIG. 3

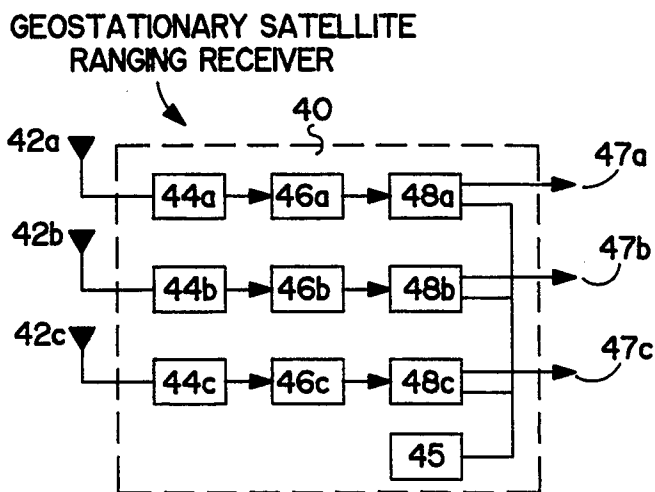
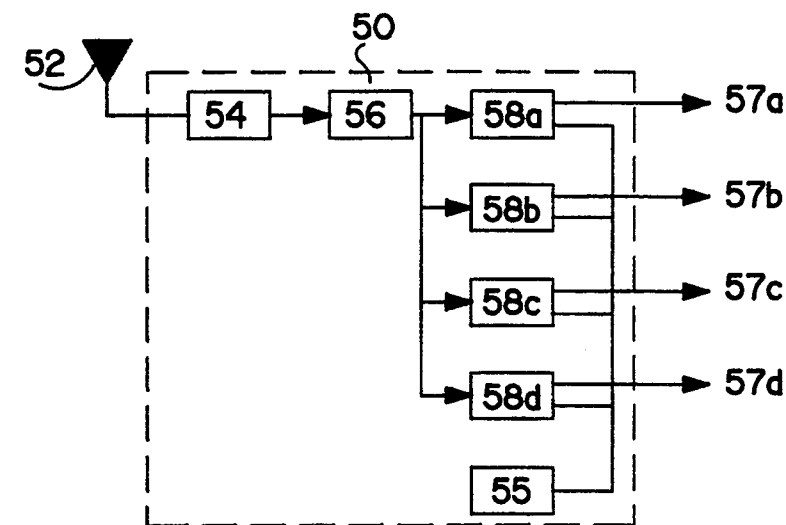


FIG. 4



GPS RECEIVER

FIG. 5

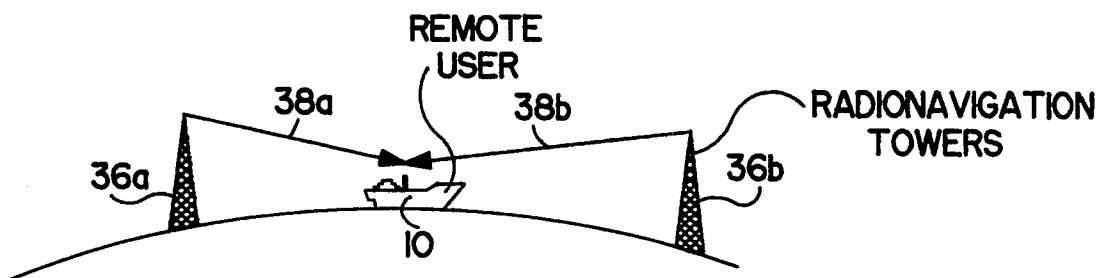


FIG. 6

CONDITIONAL ERROR
PROCESSING MODULE

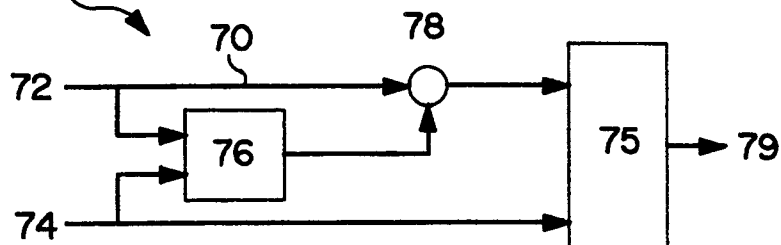


FIG. 7

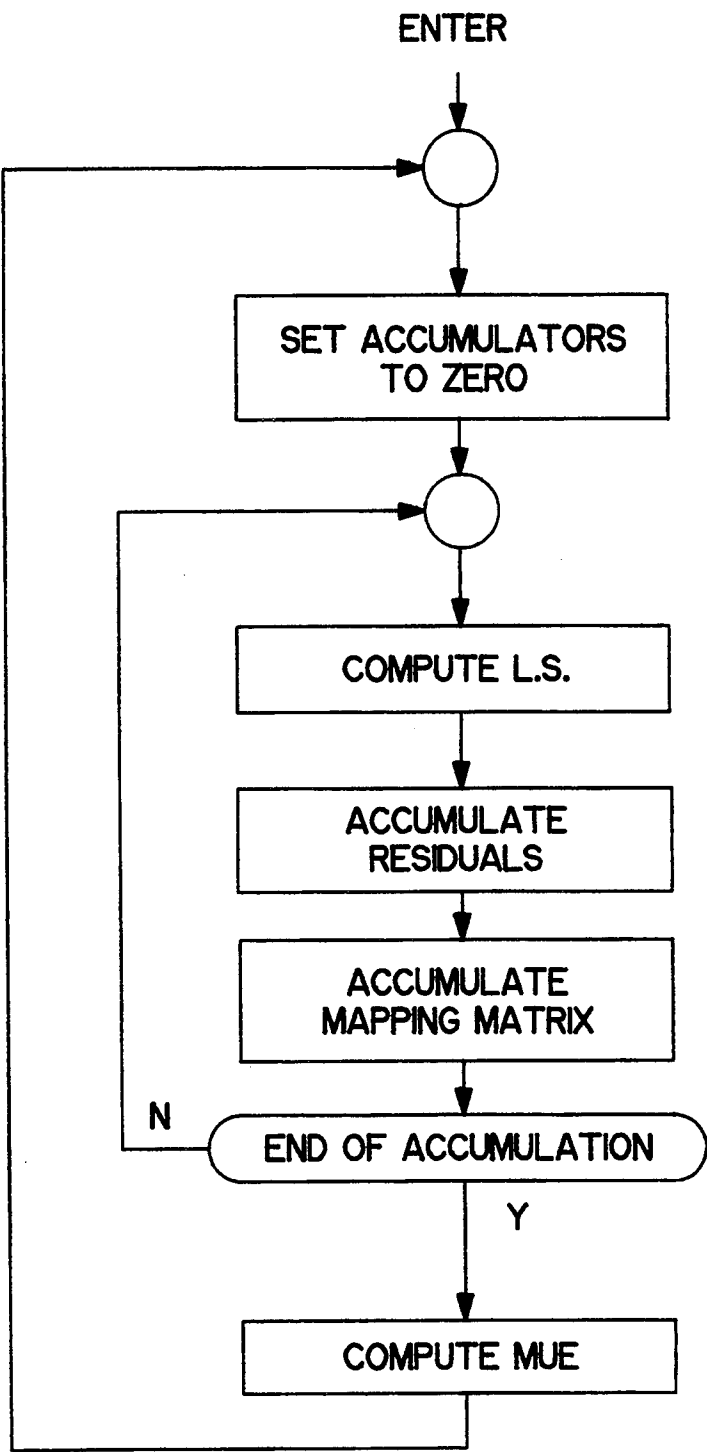


FIG. 8

GPS AND SATELLITE NAVIGATION SYSTEM

BACKGROUND OF THE INVENTION

1. Field of the Invention

This invention pertains to navigation and positioning systems. More particularly, this invention pertains to a positioning system incorporating navigational satellites and fixed relays in conjunction with a new calibration and processing system to minimize error and obtain more accurate positional coordinates than is possible under current systems.

2. Description of the Prior Art

Navigation by satellite began with the introduction of the U.S. Navy's TRANSIT system in the mid 1960's which is still in use. This system consists of seven polar-orbiting satellites at low-earth altitudes and can provide 20-50 m accuracy. The spread of the satellite orbits allows only one satellite to pass over a given geographic location at a time. Each satellite transmits a beacon-type signal that is received and converted into positional coordinates by analyzing the Doppler effect exhibited by the received signal plus additional navigational information (i.e., the actual satellite positions) transmitted to the TRANSIT user from another source.

A TRANSIT user typically computes a position fix only after each overhead pass is complete, which nominally occurs once every one and one-half hours. The TRANSIT system consequently cannot provide continuous navigational information and only allows the user to update another system, such as dead-reckoning, that provides continuous information. Technical constraints also make the system unusable for vehicles moving at high-speeds.

The United States Government began implementing the next-generation Global Positioning System (GPS) in the late 1970's to provide continuous updates and to service high speed vehicles. GPS employs satellites in 11,000 mile inclined circular orbits spaced 200 Km, 55° apart and will provide a user with continuous coverage anywhere on earth once the full constellation of satellites is properly placed in orbit. The orbits and operating parameters of GPS satellites are well known to those of ordinary skill in the art and are readily available to the public through various sources. One such reference is the *Interavia Space Directory* (1990-1991) available from Jane's Information Group and another is the *World Satellite Almanac* (2d Ed.) authored by Mark Long and published by Howard N. Sams & Co.

Each GPS satellite transmits an encrypted signal for military use and a degraded, unencrypted signal for civilian use. GPS satellites continuously broadcast signals that may be received by anyone with the proper equipment. These carrier signals are superimposed with the respective satellite's ephemeris that must be determined from the content of the GPS signal by the user's software in addition to the three dimensions of position. GPS operates on the principle of multilateration wherein a user determines the intersection of a plurality of range measurements derived from the GPS signals, the range measurements being made simultaneously to separate GPS satellites. The user then ascertains from this intersection his instantaneous latitude, longitude, and altitude.

The range measurements inherently contain an error called an offset bias common to all the measurements created by the unsynchronized operation of the satellite and user clocks. This error will yield an erroneous

range measurement, making it appear that the user is either closer to or farther from each of the satellites than is actually the case. These measurements are therefore more accurately termed pseudoranges. Four or more measurements are therefore to ascertain the unknown latitude, longitude, altitude, and offset bias required since the measurements are not truly ranges but are instead pseudoranges obtained from the signals of the respective GPS satellites.

GPS has some serious shortcomings, especially for continuous coverage with five meter accuracy, resulting from several factors. Physical factors include uncertainty in (1) atmospheric propagation delays, (2) precise GPS satellite locations, (which are required to determine a fix), and (3) the accuracy of the timing information that provides the basis of the pseudoranges. Induced errors include intentional degradation by the United States Department of Defense of the unencrypted signal for civilian users, from approximately 25 m accuracy to 100 m accuracy or worse for national security reasons. The best currently available techniques for overcoming this error can only reduce it to about 15 m.

One way of reducing the effects of the error in GPS produced by these factors utilizes differential corrections for the pseudoranges measured by the user to eliminate common errors, namely offset biases. Differential corrections are determined by placing a GPS receiver at a precisely known, fixed reference site, and then measuring the actual errors by comparing the received pseudoranges with the values expected for the known reference site. The differences between the received and expected values are then transmitted to users over a separate communication link to correct their pseudorange measurements before the user's position, i.e., the "fix", is computed.

However, some fix errors are residual and cannot be totally compensated for by differential correction. For example, atmospheric propagation delay errors and satellite

PATENT position errors will vary as the distance from the reference site increases and therefore will not be common to all measurements. A method for reducing the sensitivity of the user fix computation to residual error must also be employed in addition to differential correction.

Sensitivity to residual error depends on the satellite locations with respect to the user's location and the consequent mathematical relationship between basic pseudorange measurement errors and the position computation. This mathematical relationship is called the Position Dilution of Precision (PDOP) and its existence and affect are well known to those of ordinary skill in the art. One treatment of the topic may be found in the publication "Geometric Formulas for Dilution of Precision Calculations", authored by Paul Messett and Karl Rudnick, and published in Vol. 37., No. 4 at page 379 of the *Journal of the Institute of Navigation*. PDOP is a primarily scalar multiplier that allows the user to estimate fix uncertainty for a given measurement uncertainty. For example, if the measurement error is ± 10 meters and the PDOP is 3, the user can expect a fix error (i.e., error in calculated position) of ± 30 meters in a statistical sense.

GPS satellite locations are constantly changing as the satellites move across the sky and so the PDOP also constantly changes regardless of whether the user is

stationary. Minimum PDOP occurs when all satellites are uniformly distributed across the sky seen by the user but this does not occur all the time. Users sometimes experience very large PDOP, especially when the satellites become "grouped together", and fix errors correspondingly fluctuate.

There have been previous attempts to reduce PDOP or otherwise improve the accuracy of GPS-based positioning for remote moving users. U.S. Pat. No. 4,812,991 discloses a technique in which assorted GPS measurements are combined in a prescribed manner to reduce the effect of measurement errors. This technique does not reduce the effective PDOP governing the relationship between measurement errors and fix errors or extend the useful coverage of GPS as does the present invention.

U.S. Pat. No. 4,876,550 describes another data processing method which, although not specifically directed at GPS-based positioning, could be used to reduce the effect of nearly-singular geometry (large PDOP) on position fix computations. This method also does not reduce the typical effective PDOP but instead is applicable when the PDOP is so high that it is essentially infinitely large. This is not generally applicable to GPS which is designed to provide reasonable PDOP at all times although the PDOP will still be too large for accurate positioning because of measurement errors.

Alternative geostationary satellite-based systems have been proposed in order to minimize dependence on GPS with its attendant problems. These systems exhibit large latitudinal PDOP because all of the satellites necessarily reside in the earth's equatorial plane. The relatively large PDOP can magnify small errors in height calculation or instrument calibration to cause large latitudinal position errors. The achievable accuracy from these systems does not meet all needs but the coverage they provide is ideal since the satellites are always in view.

Some approaches have also attempted to use privately developed shore-based navigation systems. These systems can be very accurate but are affected by atmospheric variations, even to the extent that some longer range systems are unstable at night. Also, the construction and maintenance of shore based stations may be logistically or politically unfeasible in many parts of the world.

For some critical applications such as public safety and energy exploration, large increases in PDOP are intolerable. Occurrence of PDOP variations caused by changing satellite position can be reduced, as can PDOP itself, by integrating GPS measurements with those made to one or more commercial geostationary communication satellites. Since these geostationary satellites are earth-stationary, their effective PDOPs are virtually constant. Thus, when measurements from geostationary satellites are combined with those from GPS, the overall PDOP is "smoothed out" and large latitudinal errors inherent in geostationary satellite systems can be eliminated.

A system is described in United Kingdom Patent No. 2,180,426 that combines GPS with a geostationary communication satellite to provide a combined navigation/-communication capability. A GPS-like signal is transmitted from the communication satellite, presumably for navigational purposes. However, the requirement to synchronize the clock of this signal to the GPS clock is virtually impossible to realize because of circuit delays and other transponder limitations found in commercial

communication satellites. No description of how the combined positioning would be accomplished is provided even if satisfactory timing could be realized (e.g., how the location of the communication satellite derived). The concept is unworkable as described.

An intrinsic calibration problem arises when combining GPS and geostationary-based measurement. Unlike GPS where the carrier frequencies are all the same, geostationary satellite signals pass through different receiver and transponder circuits which necessarily create different time delays thereby introducing instrumental biases. These instrumental biases are difficult to determine for a moving user because each received signal has a different frequency requiring separate receiving and processing channels so that switching channels is impractical.

This calibration problem renders the usual software solution for determining common measurement delays applied to GPS signals ineffective. Although instrumental biases can be minimized through instrumentation calibration, they may change at any time afterwards due to environmental factors and dynamic effects for moving users. A new method must be found to eliminate instrumental biases in geostationary satellite measurements in realtime.

It is therefore a feature of this invention that it reduces PDOP variations in obtaining positional coordinates.

It is a further feature of this invention that it minimizes the affect of PDOP in obtaining measurements.

It is a still further feature of this invention that it both compensates for unequal instrument delays and determines and eliminates residual error in the measured data in real time.

It is another feature of this invention that it detects and eliminates instrument biases and residual errors using the entire measurement data set.

It is still another feature of this invention that it employs a unique statistically oriented method for detecting and eliminating error in the data set.

It is a further feature of this invention that it integrates navigational satellite data with geostationary satellite data to obtain more accurate positional coordinates.

It is yet another feature of this invention that it provides positional coordinates that are more accurate than can be obtained from conventional techniques.

It is a further feature of this invention that it relies primarily on existing satellite and telecommunication hardware to reduce the cost of implementing the system.

SUMMARY OF THE INVENTION

This invention improves the accuracy and reliability of satellite-based navigation by combining in its preferred embodiment measurements derived from GPS and commercial geostationary satellite systems in the position computation. Differential corrections are determined for both GPS and geostationary satellite signals and transmitted to the user. The use of geostationary satellites provides enhanced coverage and accuracy over the use of GPS alone since the signals emanate from stationary points rather than from moving satellites that rise and fall. The GPS satellite measurements increase positioning accuracy since they afford better spatial geometry. The measurements are then combined by the user employing a unique method that improves

error detection and removal as compared with previously used techniques.

BRIEF DESCRIPTION OF THE DRAWINGS

A more particular description of the invention briefly summarized above may be had by reference to the exemplary preferred embodiments illustrated in the drawings of this specification so that the manner in which the above cited features, as well as others which will become apparent, are obtained and can be understood in detail. The drawings nevertheless illustrate only typical, preferred embodiments of the invention and are not to be considered limiting of its scope as the invention may admit to other equally effective embodiments.

In the Drawings:

FIG. 1 illustrates the major components of the preferred embodiments;

FIG. 2 depicts the use of geostationary communication satellites to comprise a subsystem of fixed relays in accord with the first preferred embodiment of the invention;

FIG. 3 depicts the use of navigational satellites to comprise a subsystem in accord with both preferred embodiments of the invention;

FIG. 4 is a block diagram of a geostationary satellite signal receiver for use with the invention;

FIG. 5 is a block diagram of a GPS signal receiver for use with the invention;

FIG. 6 shows an alternative preferred embodiment employing radionavigation towers rather than geostationary communications satellites;

FIG. 7 is a block diagram of the conditional error processor of the preferred embodiment of the invention; and

FIG. 8 is a flow diagram of the steps performed by the conditional error processor of FIG. 7.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

Most of the major components of the present invention are illustrated in FIG. 1. Remote user 10 is located at some uncertain position and may be relatively rapidly moving. Remote user 10 has at least one geostationary satellite signal receiver 40 as is diagrammed in FIG. 4 and at least one GPS signal receiver 50 as is diagrammed in FIG. 5. Remote user 10 receives signals from each of geostationary satellites 20a-c via receiver 40 and from each of navigational satellites 30a-d via receiver 50.

Geostationary telecommunication satellites 20a-c may be any of several types well known to those of ordinary skill in the art whose services are commercially available for lease. Geostationary satellites are in a fixed relationship to a particular location or the earth and consequently operate as "fixed relays" receiving signals and relaying them to a predetermined location. The commercial services of the Galaxy, Westar, Satcom, and Spacenet satellites are all suitable for implementing the present invention.

Telecommunication satellites 20a-c receive and transmit spread spectrum signals modulated with a pseudorandom (PRN) code sequence at prescribed chipping and code repetition rates to prevent interference with other signals within the carrier band. These spread spectrum signals must be authorized common carrier signals duly licensed for transmission and receipt by the appropriate governmental entities. In the United

States, this is primarily the Federal Communications Commission (FCC).

Modulation of spread spectrum signals associated with satellites 20a-c includes low frequency biphasic modulation of the carrier signal containing information necessary for performing navigational computations aboard remote user 10. The information bandwidth of the signals received and transmitted by geostationary satellites 20a-c in the preferred embodiment of the invention is on the order of 100 Hz. The pseudorandom code sequence chipping rates are typically in the range of 2.5 MHz and code repetition rates are typically in the range of 150 Hz. Satellites 20a-c receive signals from uplink facility 14 and transmit signals to both remote user 10 and master facility 12 as shown in FIG. 2.

Navigational satellites 30a-d in the preferred embodiment are GPS satellites whose operating parameters were discussed in part above. Additionally, the carrier signals from each GPS satellite are modulated with a unique pseudo-random (PRN) code sequence, one at chipping rates of 1.023 MHz and the other at 10.23 MHz. Each carrier signal also contains its respective satellite's ephemeris containing its precise location at any given time.

Master facility 12, uplink facility 14, and tracking stations 16a-b comprise a means for receiving and transmitting signals to and from satellites 30a-d and 20a-c and to remote user 10. Tracking stations 16a-b and uplink facility 14 are linked to master facility 12 via communication links 18a-c, respectively. The means for receiving and transmitting necessarily has a GPS receiver 50 and a geostationary satellite signal receiver 40, generally located at master control facility 12, for receiving signals.

Tracking station 16a-b are representative of a remote tracking network that may be comprised of as many such tracking stations as is required, but all embodiments require at least four tracking stations. Neither the tracking network nor uplink facility 14 need necessarily be in close physical proximity with master control facility 12. It is generally desirable that the tracking network have a high number of tracking stations widely distributed throughout the coverage area.

Master facility 12 coordinates receipt and transmission of the various signals received by and transmitted from tracking stations 16a-b and uplink facility 14 as well as modulation and error correction of data in selected signals as described below. Uplink facility 14 transmits timing-based, modulated, conventional common carrier frequency signals such as C-band or Ku-band signals. This modulation in the preferred embodiment of the invention is a spread spectrum pseudorandom code (PRC) originating in a stable oscillator such as an atomic clock.

One important aspect of the invention is that little or no capital is required to implement the most expensive equipment necessary for the practice of the invention. The GPS satellite system is largely in place and is a project of the United States federal government. The geostationary telecommunication satellites are also in place and their services are readily obtainable along with equipment for receipt, processing and transmission of signals. Access to and use of equipment comprising geostationary satellites 20a-d, master control facility 12, tracking stations 16a-b, communications links 18a-c, and uplink facility 14 can be obtained by contacting a single sales representative at a commercial teleport as

may commonly be found in many major American metropolitan areas.

Another important feature is that the receipt, processing and transmission of all signals employs standard spread spectrum signal technology and so can be used with "off-the-shelf" technology. The sole exception is the conditional error processing described below that is performed by the user. Thus, most of the technology for implementing the invention is readily accessible to the public in sources such as *World Satellite Almanac* published by Howard W. Sams & Company and *Spread Spectrum Systems* authored by Robert C. Dixon and published by John Wiley & Sons in addition to commercial teleports and the *Interavia Space Flight Directory* mentioned above.

Receivers 40 and 50 aboard remote user 10 and located at master control facility 12 track the PRC signals generated at uplink facility 14 and, through correlation techniques, generate a signal that accurately tracks the timing provided by uplink facility 14. The output generated by receivers 40 and 50 contains the measured pseudoranges that are proportional to the range from user 10 to the fixed relays and navigational satellites, respectively. These signals also include errors created by offsets between the clocks of uplink facility 14 and remote user 10 as well as propagation errors incurred in the earth's atmosphere and satellite transponders.

The geostationary satellite ranging receiver, generally denoted 40, is illustrated in FIG. 4 in block diagram form. Antennas 42a-c are, in the preferred embodiment, small directional antennas that must be pointed at satellites 20a-c to achieve the highest gain and background signal rejection. Antennas 42a-c receive signals broadcast by each of satellites 20a-c, respectively, which signals are then amplified and converted by RF sections 44a-c, respectively. The PRN code sequence is tracked in code tracking loops 46a-c, respectively, and the code phase is measured in code phase loops 48a-c, respectively, with respect to local oscillator 45.

Outputs 47a-c consist of pseudorange signals transmitted by satellites 20a-c and received by antennas 42a-c, after data receipt and processing. Multiple antennas, channels, and outputs are necessary because each geostationary satellite will typically transmit on different frequencies and will thus necessitate separate circuits for receipt and processing. Receiver 40 will also output data representing the referenced pseudoranges received from master control facility 12 and the position of satellites 20a-c.

The GPS receiver of the preferred embodiment of the invention, generally denoted 50, is illustrated in block diagram form in FIG. 5. A single omni-directional antenna 52a, radio frequency amplifier 54a, and code tracking loop 56a are employed because satellites 30a-c transmit on the same frequencies. Code tracking loop 56a then discriminates between signals originating from each of satellites 30a-d by virtue of their unique PRN code sequences and separates them out for transmission to their respective code phase loops 58a-d. Code phase loops 58a-d also compare their respective signals to local oscillator 55 for operational purposes to provide the pseudorange measurements output at 57a-d.

There are commercial products available that may be used to implement receivers 40 and 50 of the invention. Geostationary satellite receiver 40 can be one of many c-band communication receivers capable of handling spread-spectrum downlink signals. The preferred em-

bodiment employs the VSAT receiver manufactured by Contel for their VSAT point-to-multipoint low data rate communications services. GPS receiver 50 similarly may be one of many commercial products, and GPS receivers manufactured by Trimble, Magnavox, and Motorola are preferable.

Turning to the operation of the geostationary communication satellite subsystem shown in FIG. 2, uplink facility 14 transmits spread spectrum signals via signal paths 26a-c to satellites 20a-c, respectively, in a common carrier, uplink frequency band. Satellites 20a-c then retransmit them as relay signals via signal paths 22a-c, respectively, to master control facility 12 and as relay signals via signal paths 24a-c, respectively, to remote user 10 at different downlink frequencies. The relay signals are received at master control facility 12 and remote user 10 via signal paths 22a-c and 24a-c simultaneously. These relay signals may be of differing carrier frequencies within the downlink carrier frequency band that are modulated with the same pseudorandom code sequences and at the same chipping and code repetition rate.

Tracking stations 16 and 18 are also employed in conjunction with the geostationary satellite subsystem of FIG. 2. Signals are transmitted from uplink facility 14 to satellites 20a-c whereupon they are relayed to tracking stations 16a-b. Tracking stations 16a-b each have at least one receiver 40. Information generated at tracking stations 16a-b is transmitted to master control facility 12 via communication links 18a-b, respectively.

The operation of the navigational satellite subsystem is illustrated in FIG. 3. Each of satellites 30a-d transmits a signal that is received simultaneously at remote user 10 and master control facility 12 via signal paths 32a-d and 34a-d. As previously mentioned, master control facility 12 has a GPS receiver such as receiver 50 in FIG. 5 that receives the signal broadcast by each of satellites 30a-d to provide pseudorange measurements for each satellite relative to a precisely known antenna location at master control facility 12. Differential corrections to the pseudoranges are then computed to obtain new values for the pseudoranges so that they are accurate at the known location.

These differential corrections are periodically transmitted by master control facility 12 to uplink facility 14 via communication link 18a where they are transmitted to user 10 via telecommunication satellites 20a-c. Remote user 10 then receives those corrections via receiver 40 in FIG. 4 and applies the corrections to his measured pseudoranges obtained from the signal broadcast by satellite 30a-d before processing.

Calibration to eliminate instrumental biases introduced by separate channels in receiver 50 tends to eliminate such biases because each of satellites 30a-d effectively transmits its signal at the same time and at the same frequency. Remote user 10 can compare each of the signals to insure that they exhibit the same delay with respect to the GPS receiver clock 55 and adjust them accordingly utilizing differential correction techniques. Thus the output of any GPS receiver at user 10 master control facility 12 will be largely free of instrumental biases and is self-calibrating in this respect.

Master control facility 12 receives signals relayed from each of geostationary satellites 20a-c and transmitted from navigational satellites 30a-d as previously described. Master control facility 12 has at least one receiver akin to receiver 40 in FIG. 4 and one akin to receiver 50 in FIG. 5 for this purpose. Each receiver

generates a pseudorange measurement by measuring the epoch of the received code sequence with respect to an independent oscillator or clock (not shown) at master facility 12. The measurement is a code phase measurement proportional to the range from master facility 12 to the respective satellite but contains an arbitrary offset introduced by the clock of master control facility 12.

Five sets of pseudoranges are generated in the preferred embodiment of this invention:

- (1) geostationary satellites 20a-c relative to user 10;
- (2) geostationary satellites 20a-c relative to master control facility 12;
- (3) geostationary satellites 20a-c relative to tracking stations 16a-b;
- (4) navigational satellites 30a-d relative to user 10;
- (5) navigational satellites 30a-d relative to master control facility 12.

Once generated, those pseudoranges not generated at user 10 but needed to generate correction data are transmitted to user 10 for use in computing a fix.

The pseudorange measurements with respect to geostationary satellites 20a-c relative to master control facility 12 are made simultaneously, thereby obtaining a set of data represented by Equation 1:

$$Z_M = R_M + D_M + D_U + N_M \quad [1]$$

where

Z_M = the vector of the measured pseudoranges at master control facility 12;

R_M = the vector of ranges from master control facility 12 to the respective geostationary satellites;

D_M = the vector of common clock offsets by the clock of master facility 12;

D_U = the vector of transponder delays in respective geostationary satellites; and

N_M = vector of the measured random noise at master control facility 12.

Pseudorange measurements made at master control facility 12 using Eq. 1 are reference pseudorange measurements that are sent to uplink facility 14 via communication link 18c. Uplink facility 14 also has a local clock (not shown) from which the PRN codes are derived, as well as a modulator (also not shown). The modulator of uplink facility 14 accepts the data from master control facility 12 and modulates it onto the uplink carrier signal in a manner well known to those of ordinary skill in the art. The clock of uplink facility 14 does not introduce error or delay and consequently has no bearing on the generation of user measurements, but should nevertheless be stable enough to create slowly varying pseudorange measurements of both master control facility 12 and remote user 10. A carrier signal modulated with the master pseudorange data is then transmitted to remote user 10.

Simultaneously, pseudorange measurements with signals from the geostationary satellites 20a-c are calculated at remote user 10. These measurements can be represented by Eq. 2:

$$Z_U = R_U + D_U + D_U + N_U \quad [2]$$

where

Z_U = the vector of measured pseudoranges at remote user 10;

R_U = vector of ranges from user 10 to the respective geostationary satellite;

D_U = vector of the common clock offsets of the clock at remote user 10;

D_{UG} = vector of transponders delays at the respective geostationary satellites; and

N_U = vector of measurement of random noise at remote user 10.

Transponder delay D_U is common to Eqs. (1) and (2) and can be eliminated by taking their difference to obtain:

$$Z_D = (R_U - R_M) + (D_U - D_M) + (N_U - N_M) \quad [3]$$

A major source of instrumental bias is thereby eliminated, including all delays and offsets produced at master control facility 12, uplink facility 14, and propagation delays incurred in signal transmission along signal paths associated with satellites 20a-c. This significantly eliminates the need to transmit timing information and overcomes synchronization problems found in the art.

Eq. (3) shows that the Z_D is a function of four unknowns: the three cartesian coordinates latitude, longitude, and altitude of user 10's position and the common clock differences offset ($D_U - D_M$). When using three geostationary satellites as described above, the additional measurement required is the altitude of user 10 measured from a reference datum. This altitude is accurately predictable for most users on the Earth's surface. However, knowing the user's altitude is not a critical requirement of this invention since additional satellite measurements are used as is described elsewhere.

Finally, in order to provide user 10 with the precise locations of geostationary satellites 20a-c as required for Eq. (3), pseudorange measurements of geostationary satellites 20a-c are made with reference to at least four remote tracking stations such as remote tracking stations 16a-b of FIG. 1. The measurements are made by receivers located at these fixed known sites and are transmitted to master control facility 12. Master control facility 12 then computes from pseudorange measurements made at tracking stations 16a-b and those at master control facility 12 to accurately determine the position of each of satellites 20a-c. The positions of satellites 20a-c once calculated are then transmitted via communication link 18c to uplink facility 14 for modulation onto a carrier signal and transmission to remote user 10. Pseudorange data is calculated from signals received from the navigation satellites which take the form of Equations 1-2 above and common pseudorange errors likewise be eliminated by differentially correcting.

Remote user 10 receives pseudoranges measured at master control facility 12 with respect to geostationary satellites 20a-c, at tracking stations 16a-b with respect to geostationary satellites 20a-c, and at master control facility 12 with respect to navigational satellites 30a-d. User 10 collects these measurements along with the pseudorange measurements made at remote user 10 with respect to geostationary satellites 20a-c and with regard to navigational satellites 30a-d to create a single user data set. This user data set is then separated into subsets.

The first subset contains unknown errors which must be determined from the data and can be considered a trial group. The second subset contains data with much smaller errors relative to the trial group such that it can be considered a control group. The data of both groups is applied to conditional error processing module wherein very accurate estimates of the error in the trial group are determined.

The conditional error process can be explained from a mathematical perspective. Assuming the vector Z to be defined as:

$$Z = HX + V \quad [5]$$

where

X = an unknown vector representing the user's location

H = the linear relationship between X and Z ; and

V = a vector comprised of random errors, the least squares solution for X is:

$$X^* = (H^T H)^{-1} H^T Z, \quad [6]$$

where H^T is the transposition of H . The residual after the least squares fit is:

$$R = Z - HX^* = (I - H(H^T H)^{-1} H^T) Z = MZ \quad [7]$$

where I is the identity matrix and M is an idempotent transformation.

The residual vector R is defined by the single user data set comprised of differentially corrected GPS measurements and geostationary satellite measurements. Thus, when the user data set is partitioned into control and trial subsets, this is a partitioning of the vector components of the residual vector R . The differentially corrected GPS measurements are almost always the most accurate because the reference signal is visible both the user's location and at the known reference site. Longitudinal measurements to geostationary satellite such as satellites 20a-c could, however, be substituted as a control group in an alternative, lesser preferred embodiment. The differentially corrected GPS measurement are consequently used as the control group.

The residuals for the control group are assumed to be zero and are used to minimize the residuals for the entire data set based on that assumption. Z^* is obtained by accumulating the elements of M in Eq. (7) over a prescribed period of time and then partitioning the accumulated M and culling the submatrices resulting from the control group residuals. Z^* then is comprised of "conditional errors" in the trial group measurements and can be applied to the trial group subset (i.e., geostationary satellite measurements) to obtain more accurate measurements and, hence a "fix".

The conditional error processing module is illustrated in FIG. 7 and the processing algorithm in flow chart form in FIG. 8. Conditional error processor 76 in FIG. 7 receives its input data from both groups, the trial group at input 72 and the control group at input 74. The control group at input 74 in the preferred embodiment is the subset comprised of differentially corrected GPS measurements and the trial group at input 72 is the geostationary satellite measurements. Conditional error processor 76 then zeros out a set of accumulators and begins the iterative process for a predetermined period of time.

The iterative process begins by performing a least squares solution for all measurements including those in both the trial group and the control group. The differences (residuals) between the data in the trial group and the solution is determined from a linear mapping of all data, and the differences are stored and accumulated as a linear mapping of the raw data. The differences between the data in the control group and the solution are assumed to be zero and are also accumulated as a linear mapping. This iterative process in the preferred em-

bodiment is performed for a period of approximately one to two minutes.

At the end of the iterative process, the conditional errors are computed by appropriately partitioning the accumulated linear mappings of raw data so that the differences of the control data are culled, inverting the resulting matrix, and then processing the accumulated residuals to determine the errors in the data of the trial group. The result is a new data set containing "conditional errors" that are applied to the original trial group subject (i.e., geostationary satellite measurements) to minimize the overall residuals. Processing then returns to the next accumulation cycle.

The output of conditional error processor 76 then consists of corrections 78 for the trial data 72. The corrected trial data is then grouped again with the control group data and processed using a conventional standard processor 75. Statistical processor 75 in the preferred embodiment implements a Kalman filter as is well known to those of ordinary skill in the art. Output 79 of statistical processor 75 then consists of accurate positional coordinates as a function of time.

It is an essential characteristic of the conditional error processing that the accuracies of the error estimates must be the highest possible given the total amount of data available to remote user 10. They must be higher, for example, than if a simple comparison was made between the trial and control group of measurements. This is accomplished in conditional error processing by comparing the errors of all data that has been optimally combined via least square fitting procedure thus insuring the results will have to smallest possible statistical uncertainty.

By using the pseudoranges measured at remote control facility 12 with respect to navigational satellites 30a-c as the control group, the uncertainties in the error estimates will be several times less than the readout associated with the measurements in the control group, i.e., the differentially corrected GPS pseudo-ranges alone. Thus, the effects of residual unknown errors in the GPS data will have minimum effect on the accuracy of the error estimate corrections.

Geostationary satellites 20a-c function as fixed relays and can be replaced by radio navigation towers 36a-b shown in FIG. 1 in an alternative preferred embodiment. As shown in FIG. 6, radio navigation towers 36a-b transmit signals via signal paths 38a-b to remote user 10 whereupon remote user 10 extracts measurements from the system that are proportional to the range of each shore station. Measurements extracted from signals 38a-b can be represented by Equation 4 below:

$$Z_S = R_S + N_S + B_S \quad [4]$$

where

Z_S = vector of the measured ranges;

R_S = vector of the true ranges to shore stations 36a-b;

N_S = measurement noise; and

B_S = instrumental biases.

Since the exact locations of radio navigation towers 36a-b are known, there are three unknowns and the users coordinate position can be determined therefrom without the need for tracking stations 16a-b or associated measurements. This information is then used along with GPS measurements taken as previously described

to establish the single user data set for the conditional error processor.

It is therefore evident that the invention claimed herein may be embodied in alternative and equally satisfactory embodiments without departing from the spirit or essential characteristics thereof. The preferred embodiments disclosed above must consequently be considered illustrative and not limiting of the scope of the invention.

What is claimed is:

1. A method for determining positional coordinates, comprising the steps of:

transmitting an unmodulated first plurality of signals to a plurality of fixed relays from a control facility; receiving the unmodulated first plurality of signals from the fixed relays and an unmodulated second plurality of signals from a plurality of navigational satellites at the control facility and at a remote location;

modulating the unmodulated first plurality of signals and the unmodulated second plurality of signals received at the control facility and retransmitting the modulated first plurality of signals and the modulated second plurality of signals to the remote location;

receiving the modulated first plurality of signals and the modulated second plurality of signals from the control facility at the remote location; and

processing the unmodulated first plurality of signals, the modulated first plurality of signals, the unmodulated second plurality of signals, and the modulated second plurality of signals received at the remote location to minimize errors in the data in the unmodulated first plurality of signals and in the modulated first plurality of signals with the data in the unmodulated second plurality of signals and in the modulated second plurality of signals to obtain accurate positional coordinates.

2. The method of claim 1, wherein the step of processing to obtain positional coordinates further comprises the steps of:

performing a least-squares fit with the ranging data from said modulated second plurality of signals and from said unmodulated second plurality of signals and the positioning data from said unmodulated first plurality of signals and said modulated first plurality of signals;

accumulating the differences between the ranging data and the positioning data and the data obtained for the least-squares fit;

storing the differences between the ranging data and the positioning data and the data obtained from the least-squares fit;

accumulating the data obtained for the least-squares fit;

storing the data obtained for the least-squares fit;

partitioning the accumulated least-squares fit data to segregate the ranging data;

inverting and operating on the accumulated differences to determine the errors in the segregated data;

correcting the errors in the segregated data to obtain accurate positional coordinates.

3. The method of claim 1, wherein the plurality of fixed relays are further comprised of at least one of a geostationary satellite or a shore-based radio navigation station.

4. The method of claim 1, wherein the step of modulating relayed ranging data comprises modulating the relayed ranging data using spread-spectrum techniques to include pseudorandom code modulation at preselected chipping and code repetition rates.

5. The method of claim 1, wherein the unmodulated first plurality of signals, the modulated first plurality of signals, the unmodulated second plurality of signals, and the modulated second plurality of signals are transmitted as spread-spectrum signals.

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