

760-Heuristics-Assignment

Leo Mooney

March 2023

1 Question 1

Neighbors of the current solution can be found by swapping one pot in any crucible with a pot in any other crucible. This can be formally defined as following:

$N(\mathbf{x}) = \{\mathbf{y}(\mathbf{x}, k, l, m, n), k = 1, 2, 3, \dots, 16, l = k + 1, k + 2, k + 3, \dots, 17, m = 1, 2, 3, n = 1, 2, 3\}$ where

$$\mathbf{y}(\mathbf{x}, k, l, m, n) = (y_{1,1}, y_{1,2}, y_{1,3}; y_{2,1}y_{2,2}y_{2,3}; \dots y_{c,j}), y_{c,j} = \begin{cases} x_{l,n} & \text{if } c = k, j = m \\ x_{k,m} & \text{if } c = l, j = n \\ x_{c,j} & \text{otherwise} \end{cases}$$

2 Question 2

Let $h(x_c) = g(\overline{Al}[x_{c,avg}], \overline{Fe}[x_{c,avg}], \overline{Si}[x_{c,avg}])$ where

$$\overline{Al}[x_{c,avg}] = \frac{Al[x_{c,1}], Al[x_{c,2}], Al[x_{c,3}]}{3}$$

$$\overline{Fe}[x_{c,avg}] = \frac{Fe[x_{c,1}], Fe[x_{c,2}], Fe[x_{c,3}]}{3}$$

$$\overline{Si}[x_{c,avg}] = \frac{Si[x_{c,1}], Si[x_{c,2}], Si[x_{c,3}]}{3}$$

Algorithm 1 Sweep x

```

Let  $S$  contain all possible solutions of  $x$ 
Let  $x, x \in S$ , be some initial configuration
Let  $x^*$  be some configuration that maximizes  $f(x)$ 
Let  $I$  be the intermediate values
 $I_c := h(x_c)$ 
while not stopped do
  Compare each neighbor  $y(x, k, l, m, n) \in N(x)$ 
   $d = h(y_k) + h(y_l) - I_k - I_l$ 
  if  $d > 0$  for some  $y \in N(x)$  then
     $x := y$ 
     $I_k := h(y_k)$ 
     $I_l := h(y_l)$ 
  else if  $d \leq 0 \forall y \in N(x)$  then
    Stop
  end if
end while
 $x^* := x$ 

```

3 Question 3

See Appendix A for all code and plots.

3.1 Question 3E

Best solution found using repeated next ascents with $n = 200$.

```

1 [27  4 45 ] 99.261 %Al, 0.274 %Fe, 0.110 %Si, $41.53, spread = 41
2 [ 8 13 37 ] 99.508 %Al, 0.154 %Fe, 0.153 %Si, $48.71, spread = 29
3 [50 40 30 ] 99.504 %Al, 0.143 %Fe, 0.238 %Si, $48.71, spread = 20
4 [17 51 15 ] 99.268 %Al, 0.162 %Fe, 0.386 %Si, $41.53, spread = 36
5 [24 23 46 ] 99.512 %Al, 0.053 %Fe, 0.180 %Si, $48.71, spread = 23
6 [28 12 32 ] 99.358 %Al, 0.096 %Fe, 0.348 %Si, $44.53, spread = 20
7 [18  3 42 ] 99.760 %Al, 0.040 %Fe, 0.139 %Si, $57.35, spread = 39

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```

8 [19 41 20 ] 99.262 %Al, 0.212 %Fe, 0.249 %Si, $41.53, spread = 22
9 [11 25 5 ] 99.353 %Al, 0.185 %Fe, 0.325 %Si, $44.53, spread = 20
10 [ 9 6 21 ] 99.504 %Al, 0.139 %Fe, 0.253 %Si, $48.71, spread = 15
11 [ 7 36 26 ] 99.506 %Al, 0.098 %Fe, 0.268 %Si, $48.71, spread = 29
12 [47 39 2 ] 99.503 %Al, 0.114 %Fe, 0.270 %Si, $48.71, spread = 45
13 [22 33 10 ] 99.356 %Al, 0.187 %Fe, 0.219 %Si, $44.53, spread = 23
14 [34 29 38 ] 99.361 %Al, 0.209 %Fe, 0.241 %Si, $44.53, spread = 9
15 [14 43 49 ] 99.254 %Al, 0.224 %Fe, 0.307 %Si, $41.53, spread = 35
16 [ 1 35 31 ] 99.350 %Al, 0.075 %Fe, 0.336 %Si, $44.53, spread = 34
17 [48 44 16 ] 99.515 %Al, 0.143 %Fe, 0.241 %Si, $48.71, spread = 32
Sum = $787.09, MxSprd = 45

```

Best solution found using repeated steepest ascents with $n = 200$.

```

1 [ 1 48 15 ] 99.256 %Al, 0.121 %Fe, 0.300 %Si, $41.53, spread = 47
2 [29 36 10 ] 99.369 %Al, 0.216 %Fe, 0.272 %Si, $44.53, spread = 26
3 [33 6 34 ] 99.268 %Al, 0.253 %Fe, 0.272 %Si, $41.53, spread = 28
4 [42 16 49 ] 99.502 %Al, 0.161 %Fe, 0.163 %Si, $48.71, spread = 33
5 [43 24 39 ] 99.508 %Al, 0.067 %Fe, 0.243 %Si, $48.71, spread = 19
6 [47 8 5 ] 99.366 %Al, 0.188 %Fe, 0.317 %Si, $44.53, spread = 42
7 [ 4 26 19 ] 99.253 %Al, 0.243 %Fe, 0.283 %Si, $41.53, spread = 22
8 [31 28 46 ] 99.365 %Al, 0.139 %Fe, 0.196 %Si, $44.53, spread = 18
9 [ 3 11 23 ] 99.502 %Al, 0.058 %Fe, 0.246 %Si, $48.71, spread = 20
10 [32 27 35 ] 99.501 %Al, 0.087 %Fe, 0.224 %Si, $48.71, spread = 8
11 [22 40 51 ] 99.353 %Al, 0.122 %Fe, 0.349 %Si, $44.53, spread = 29
12 [13 38 2 ] 99.504 %Al, 0.177 %Fe, 0.160 %Si, $48.71, spread = 36
13 [50 25 37 ] 99.500 %Al, 0.188 %Fe, 0.231 %Si, $48.71, spread = 25
14 [20 30 17 ] 99.522 %Al, 0.111 %Fe, 0.277 %Si, $48.71, spread = 13
15 [ 9 18 44 ] 99.750 %Al, 0.037 %Fe, 0.099 %Si, $57.35, spread = 35
16 [45 41 12 ] 99.258 %Al, 0.171 %Fe, 0.284 %Si, $41.53, spread = 33
17 [21 7 14 ] 99.360 %Al, 0.168 %Fe, 0.347 %Si, $44.53, spread = 14
Sum = $787.09, MxSprd = 47

```

4 Question 4

There does not seem to be a significant difference in the objective value for next and steepest ascent. Steepest ascent also took far longer to converge on each local optimum. This means that fastest ascent is better than steepest ascent; however, this conclusion is from limited information so it not conclusive evidence.

5 Question 5

(a) You would expect the problem's objective function to have lots of plateaus because the objective function is not continuous. This means there will be lots

of cases where two pots are swapped and the quality, and thus value, will remain constant.

(b)

6 Question 6

$$g''(\overline{Al}, \overline{Fe}, \overline{Si}, x_{c1}, x_{c2}, x_{c3}, s) = \begin{cases} g(\overline{Al}, \overline{Fe}, \overline{Si}) - 20 * (s_c - s) & \text{if } s_c > s \\ g(\overline{Al}, \overline{Fe}, \overline{Si}) & \text{otherwise} \end{cases}$$

where $s_c = \max(x_{c1}, x_{c2}, x_{c3}) - \min(x_{c1}, x_{c2}, x_{c3})$

6.1 Task 6

See Appendix A for code.

6.1.1 Max Spread = 6

```

1 [38 34 40 ] 99.371 %Al, 0.241 %Fe, 0.163 %Si, $44.53, spread = 6
2 [17 13 19 ] 99.270 %Al, 0.297 %Fe, 0.234 %Si, $41.53, spread = 6
3 [35 36 39 ] 99.615 %Al, 0.043 %Fe, 0.196 %Si, $48.71, spread = 4
4 [ 6  8 10 ] 99.352 %Al, 0.257 %Fe, 0.275 %Si, $44.53, spread = 4
5 [30 32 27 ] 99.558 %Al, 0.093 %Fe, 0.170 %Si, $48.71, spread = 5
6 [37 42 41 ] 99.501 %Al, 0.115 %Fe, 0.198 %Si, $48.71, spread = 5
7 [24 22 21 ] 99.532 %Al, 0.037 %Fe, 0.276 %Si, $48.71, spread = 3
8 [33 29 28 ] 99.256 %Al, 0.151 %Fe, 0.303 %Si, $41.53, spread = 5
9 [11 14  9 ] 99.381 %Al, 0.080 %Fe, 0.297 %Si, $44.53, spread = 5
10 [ 5  7  3 ] 99.512 %Al, 0.188 %Fe, 0.212 %Si, $48.71, spread = 4
11 [46 47 43 ] 99.359 %Al, 0.172 %Fe, 0.315 %Si, $44.53, spread = 4
12 [26 25 31 ] 99.393 %Al, 0.138 %Fe, 0.325 %Si, $44.53, spread = 6
13 [49 48 44 ] 99.511 %Al, 0.169 %Fe, 0.145 %Si, $48.71, spread = 5
14 [20 18 23 ] 99.544 %Al, 0.057 %Fe, 0.220 %Si, $48.71, spread = 5
15 [15 16 12 ] 99.369 %Al, 0.127 %Fe, 0.302 %Si, $44.53, spread = 4
16 [ 2  4  1 ] 99.356 %Al, 0.144 %Fe, 0.280 %Si, $44.53, spread = 3
17 [50 51 45 ] 99.256 %Al, 0.198 %Fe, 0.351 %Si, $41.53, spread = 6
    Sum = $777.27, MxSprd = 6

```

6.1.2 Max Spread = 8

```

1 [15 13 11 ] 99.255 %Al, 0.157 %Fe, 0.277 %Si, $41.53, spread = 4
2 [ 2  1  4 ] 99.356 %Al, 0.144 %Fe, 0.280 %Si, $44.53, spread = 3
3 [46 49 51 ] 99.399 %Al, 0.152 %Fe, 0.259 %Si, $44.53, spread = 5
4 [26 19 24 ] 99.355 %Al, 0.140 %Fe, 0.305 %Si, $44.53, spread = 7
5 [32 29 36 ] 99.509 %Al, 0.087 %Fe, 0.197 %Si, $48.71, spread = 7
6 [34 35 33 ] 99.358 %Al, 0.156 %Fe, 0.278 %Si, $44.53, spread = 2
7 [ 8  3 10 ] 99.527 %Al, 0.176 %Fe, 0.194 %Si, $48.71, spread = 7
8 [48 50 44 ] 99.544 %Al, 0.129 %Fe, 0.241 %Si, $48.71, spread = 6

```

```

9 [14 6 7 ] 99.253 %Al, 0.249 %Fe, 0.360 %Si, $41.53, spread = 8
10 [16 18 17 ] 99.542 %Al, 0.132 %Fe, 0.258 %Si, $48.71, spread = 2
11 [30 27 23 ] 99.505 %Al, 0.105 %Fe, 0.199 %Si, $48.71, spread = 7
12 [20 22 21 ] 99.516 %Al, 0.060 %Fe, 0.277 %Si, $48.71, spread = 2
13 [43 45 38 ] 99.350 %Al, 0.226 %Fe, 0.125 %Si, $44.53, spread = 7
14 [ 9 5 12 ] 99.510 %Al, 0.106 %Fe, 0.258 %Si, $48.71, spread = 7
15 [40 39 47 ] 99.378 %Al, 0.169 %Fe, 0.269 %Si, $44.53, spread = 8
16 [28 25 31 ] 99.278 %Al, 0.204 %Fe, 0.285 %Si, $41.53, spread = 6
17 [42 41 37 ] 99.501 %Al, 0.115 %Fe, 0.198 %Si, $48.71, spread = 5
Sum = $781.45, MxSprd = 8

```

6.1.3 Max Spread = 11

```

1 [40 49 51 ] 99.301 %Al, 0.205 %Fe, 0.295 %Si, $41.53, spread = 11
2 [35 33 34 ] 99.358 %Al, 0.156 %Fe, 0.278 %Si, $44.53, spread = 2
3 [ 5 3 7 ] 99.512 %Al, 0.188 %Fe, 0.212 %Si, $48.71, spread = 4
4 [29 31 28 ] 99.257 %Al, 0.160 %Fe, 0.310 %Si, $41.53, spread = 3
5 [ 4 6 9 ] 99.386 %Al, 0.217 %Fe, 0.204 %Si, $44.53, spread = 5
6 [36 32 26 ] 99.524 %Al, 0.048 %Fe, 0.266 %Si, $48.71, spread = 10
7 [39 44 47 ] 99.500 %Al, 0.124 %Fe, 0.270 %Si, $48.71, spread = 8
8 [25 18 16 ] 99.527 %Al, 0.153 %Fe, 0.256 %Si, $48.71, spread = 9
9 [41 50 48 ] 99.351 %Al, 0.151 %Fe, 0.329 %Si, $44.53, spread = 9
10 [14 22 24 ] 99.362 %Al, 0.083 %Fe, 0.335 %Si, $44.53, spread = 10
11 [13 23 19 ] 99.251 %Al, 0.258 %Fe, 0.213 %Si, $41.53, spread = 10
12 [30 27 20 ] 99.530 %Al, 0.104 %Fe, 0.212 %Si, $48.71, spread = 10
13 [46 42 45 ] 99.502 %Al, 0.140 %Fe, 0.056 %Si, $48.71, spread = 4
14 [21 10 17 ] 99.369 %Al, 0.239 %Fe, 0.344 %Si, $44.53, spread = 11
15 [37 43 38 ] 99.519 %Al, 0.169 %Fe, 0.143 %Si, $48.71, spread = 6
16 [11 12 15 ] 99.361 %Al, 0.068 %Fe, 0.309 %Si, $44.53, spread = 4
17 [ 8 1 2 ] 99.526 %Al, 0.042 %Fe, 0.230 %Si, $48.71, spread = 7
Sum = $781.45, MxSprd = 11

```

7 My Best Solutions

These were found by using standard simulated annealing in C.

7.1 No Max Spread

```

1 [13 4 26 ] 99.253 %Al, 0.210 %Fe, 0.373 %Si, $41.53, spread = 22
2 [31 46 17 ] 99.500 %Al, 0.135 %Fe, 0.144 %Si, $48.71, spread = 29
3 [49 14 29 ] 99.251 %Al, 0.207 %Fe, 0.314 %Si, $41.53, spread = 35
4 [23 27 30 ] 99.505 %Al, 0.105 %Fe, 0.199 %Si, $48.71, spread = 7
5 [20 50 10 ] 99.351 %Al, 0.220 %Fe, 0.327 %Si, $44.53, spread = 40
6 [ 8 34 19 ] 99.353 %Al, 0.244 %Fe, 0.155 %Si, $44.53, spread = 26
7 [ 1 48 24 ] 99.355 %Al, 0.069 %Fe, 0.342 %Si, $44.53, spread = 47

```

8	[32 6 2]	99.500	%Al,	0.146	%Fe,	0.227	%Si,	\$48.71,	spread = 30
9	[40 36 7]	99.501	%Al,	0.169	%Fe,	0.121	%Si,	\$48.71,	spread = 33
10	[28 25 43]	99.252	%Al,	0.218	%Fe,	0.369	%Si,	\$41.53,	spread = 18
11	[21 45 16]	99.357	%Al,	0.199	%Fe,	0.232	%Si,	\$44.53,	spread = 29
12	[9 47 39]	99.501	%Al,	0.095	%Fe,	0.228	%Si,	\$48.71,	spread = 38
13	[37 35 11]	99.501	%Al,	0.067	%Fe,	0.277	%Si,	\$48.71,	spread = 26
14	[22 15 3]	99.500	%Al,	0.089	%Fe,	0.165	%Si,	\$48.71,	spread = 19
15	[18 42 44]	99.750	%Al,	0.044	%Fe,	0.136	%Si,	\$57.35,	spread = 26
16	[51 5 38]	99.351	%Al,	0.192	%Fe,	0.349	%Si,	\$44.53,	spread = 46
17	[41 33 12]	99.353	%Al,	0.099	%Fe,	0.305	%Si,	\$44.53,	spread = 29
									Sum = \$790.09, MxSprd = 47

7.2 Max Spread = 6

1	[44,49,48,]	99.511	%Al,	0.169	%Fe,	0.145	%Si,	\$48.71,	spread=5
2	[18,19,21,]	99.512	%Al,	0.163	%Fe,	0.187	%Si,	\$48.71,	spread=3
3	[43,47,46,]	99.359	%Al,	0.172	%Fe,	0.315	%Si,	\$44.53,	spread=4
4	[9,11,12,]	99.535	%Al,	0.015	%Fe,	0.265	%Si,	\$48.71,	spread=3
5	[27,24,22,]	99.502	%Al,	0.068	%Fe,	0.194	%Si,	\$48.71,	spread=5
6	[36,39,34,]	99.502	%Al,	0.139	%Fe,	0.173	%Si,	\$48.71,	spread=5
7	[25,23,28,]	99.267	%Al,	0.185	%Fe,	0.332	%Si,	\$41.53,	spread=5
8	[38,37,42,]	99.650	%Al,	0.118	%Fe,	0.067	%Si,	\$52.44,	spread=5
9	[51,50,45,]	99.256	%Al,	0.198	%Fe,	0.351	%Si,	\$41.53,	spread=6
10	[2,7,5,]	99.505	%Al,	0.182	%Fe,	0.208	%Si,	\$48.71,	spread=5
11	[29,26,31,]	99.372	%Al,	0.094	%Fe,	0.350	%Si,	\$44.53,	spread=5
12	[16,14,20,]	99.298	%Al,	0.164	%Fe,	0.379	%Si,	\$41.53,	spread=6
13	[33,32,30,]	99.541	%Al,	0.070	%Fe,	0.160	%Si,	\$48.71,	spread=3
14	[6,8,10,]	99.352	%Al,	0.257	%Fe,	0.275	%Si,	\$44.53,	spread=4
15	[3,1,4,]	99.363	%Al,	0.151	%Fe,	0.284	%Si,	\$44.53,	spread=3
16	[13,15,17,]	99.276	%Al,	0.220	%Fe,	0.261	%Si,	\$41.53,	spread=4
17	[35,40,41,]	99.335	%Al,	0.141	%Fe,	0.317	%Si,	\$41.53,	spread=6
									Sum = \$779.18, MxSprd = 6

7.3 Max Spread = 8

1	[8,1,6,]	99.358	%Al,	0.130	%Fe,	0.315	%Si,	\$44.53,	spread=7
2	[24,27,21,]	99.506	%Al,	0.091	%Fe,	0.245	%Si,	\$48.71,	spread=6
3	[26,31,29,]	99.372	%Al,	0.094	%Fe,	0.350	%Si,	\$44.53,	spread=5
4	[32,40,34,]	99.353	%Al,	0.199	%Fe,	0.210	%Si,	\$44.53,	spread=8
5	[46,44,41,]	99.507	%Al,	0.108	%Fe,	0.191	%Si,	\$48.71,	spread=5
6	[22,15,18,]	99.514	%Al,	0.064	%Fe,	0.164	%Si,	\$48.71,	spread=7
7	[17,13,20,]	99.359	%Al,	0.191	%Fe,	0.305	%Si,	\$44.53,	spread=7
8	[38,33,35,]	99.501	%Al,	0.105	%Fe,	0.167	%Si,	\$48.71,	spread=5
9	[47,39,43,]	99.370	%Al,	0.153	%Fe,	0.341	%Si,	\$44.53,	spread=8
10	[7,2,5,]	99.505	%Al,	0.182	%Fe,	0.208	%Si,	\$48.71,	spread=5
11	[51,45,50,]	99.256	%Al,	0.198	%Fe,	0.351	%Si,	\$41.53,	spread=6

```

12 [12,16,19,] 99.362 %Al, 0.204 %Fe, 0.275 %Si, $44.53, spread=7
13 [11,9,14,] 99.381 %Al, 0.080 %Fe, 0.297 %Si, $44.53, spread=5
14 [36,30,37,] 99.654 %Al, 0.098 %Fe, 0.129 %Si, $52.44, spread=7
15 [10,3,4,] 99.357 %Al, 0.278 %Fe, 0.244 %Si, $44.53, spread=7
16 [49,48,42,] 99.513 %Al, 0.147 %Fe, 0.139 %Si, $48.71, spread=7
17 [28,25,23,] 99.267 %Al, 0.185 %Fe, 0.332 %Si, $41.53, spread=5
Sum = $784.00, MxSprd = 8

```

7.4 Max Spread = 11

```

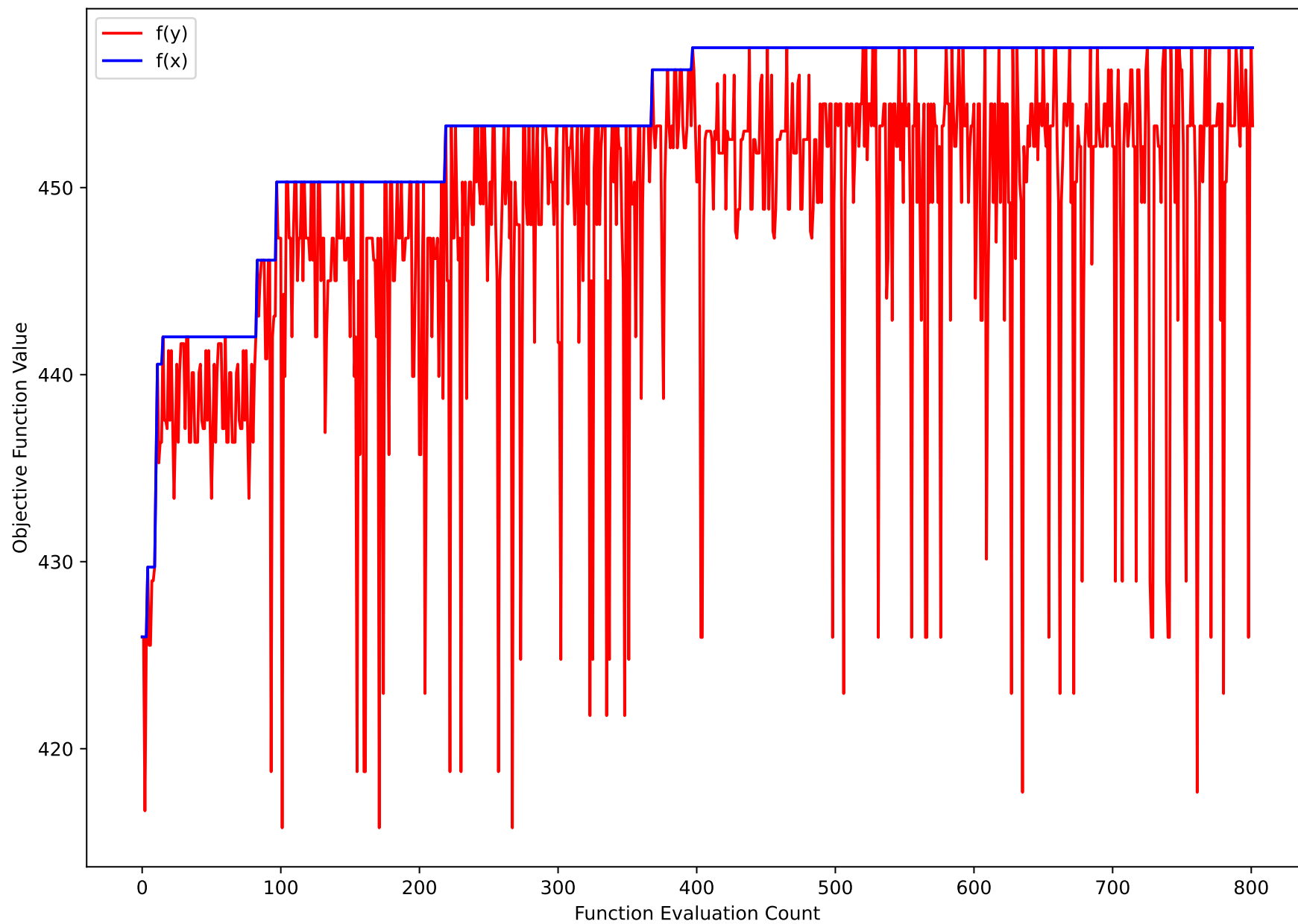
1 [24,19,26,] 99.355 %Al, 0.140 %Fe, 0.305 %Si, $44.53, spread=7
2 [27,33,37,] 99.500 %Al, 0.148 %Fe, 0.086 %Si, $48.71, spread=10
3 [38,28,34,] 99.262 %Al, 0.236 %Fe, 0.270 %Si, $41.53, spread=10
4 [48,50,41,] 99.351 %Al, 0.151 %Fe, 0.329 %Si, $44.53, spread=9
5 [49,43,51,] 99.294 %Al, 0.189 %Fe, 0.367 %Si, $41.53, spread=8
6 [44,47,39,] 99.500 %Al, 0.124 %Fe, 0.270 %Si, $48.71, spread=8
7 [42,36,45,] 99.504 %Al, 0.145 %Fe, 0.069 %Si, $48.71, spread=9
8 [35,46,40,] 99.504 %Al, 0.110 %Fe, 0.193 %Si, $48.71, spread=11
9 [4,3,1,] 99.363 %Al, 0.151 %Fe, 0.284 %Si, $44.53, spread=3
10 [10,6,8,] 99.352 %Al, 0.257 %Fe, 0.275 %Si, $44.53, spread=4
11 [32,31,21,] 99.501 %Al, 0.089 %Fe, 0.201 %Si, $48.71, spread=11
12 [14,15,12,] 99.251 %Al, 0.139 %Fe, 0.370 %Si, $41.53, spread=3
13 [9,11,17,] 99.512 %Al, 0.072 %Fe, 0.221 %Si, $48.71, spread=8
14 [30,20,23,] 99.503 %Al, 0.072 %Fe, 0.255 %Si, $48.71, spread=10
15 [29,25,18,] 99.505 %Al, 0.134 %Fe, 0.271 %Si, $48.71, spread=11
16 [16,13,22,] 99.374 %Al, 0.167 %Fe, 0.288 %Si, $44.53, spread=9
17 [7,2,5,] 99.505 %Al, 0.182 %Fe, 0.208 %Si, $48.71, spread=5
Sum = $785.63, MxSprd = 11

```

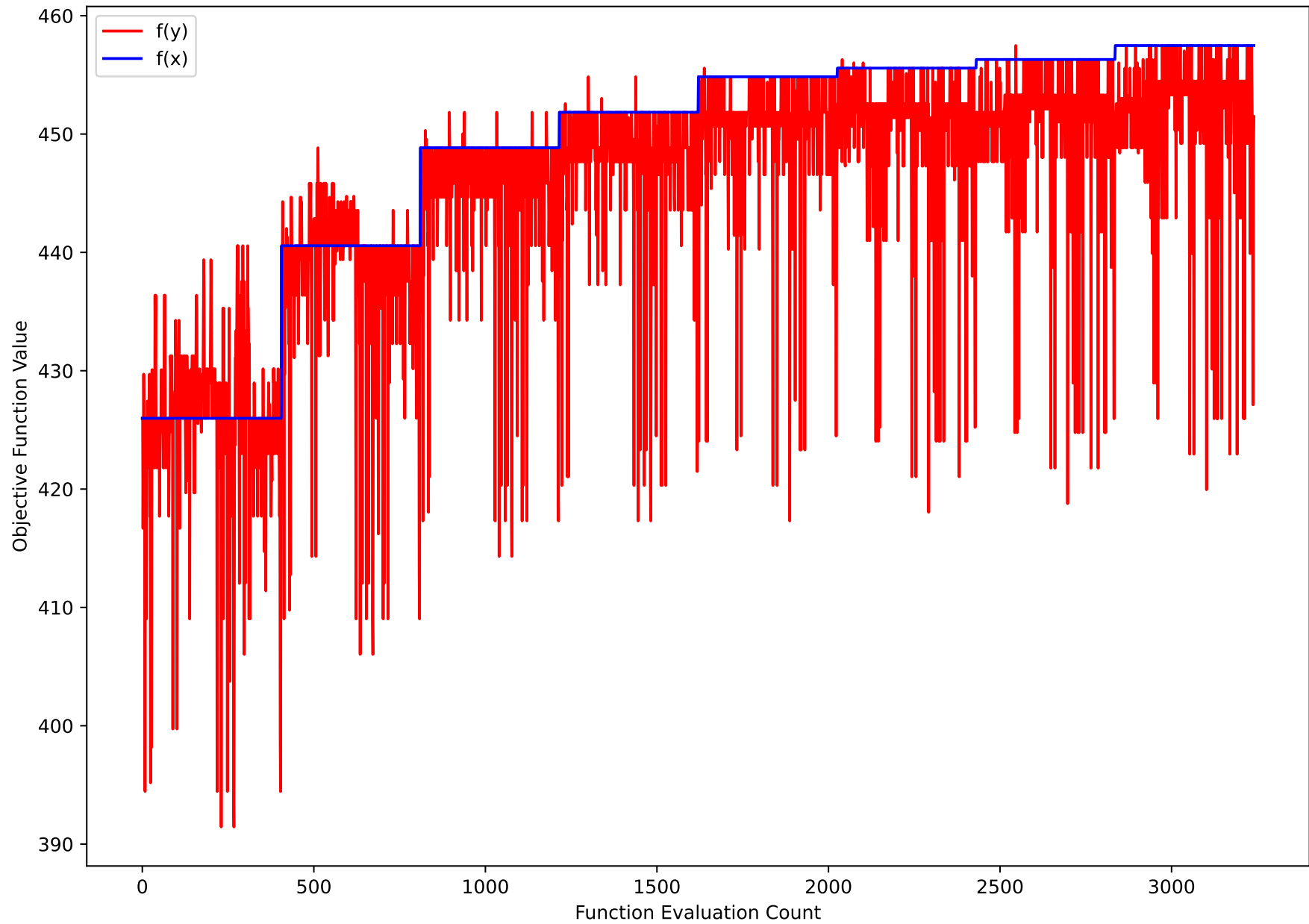
8 Appendix A

See overleaf

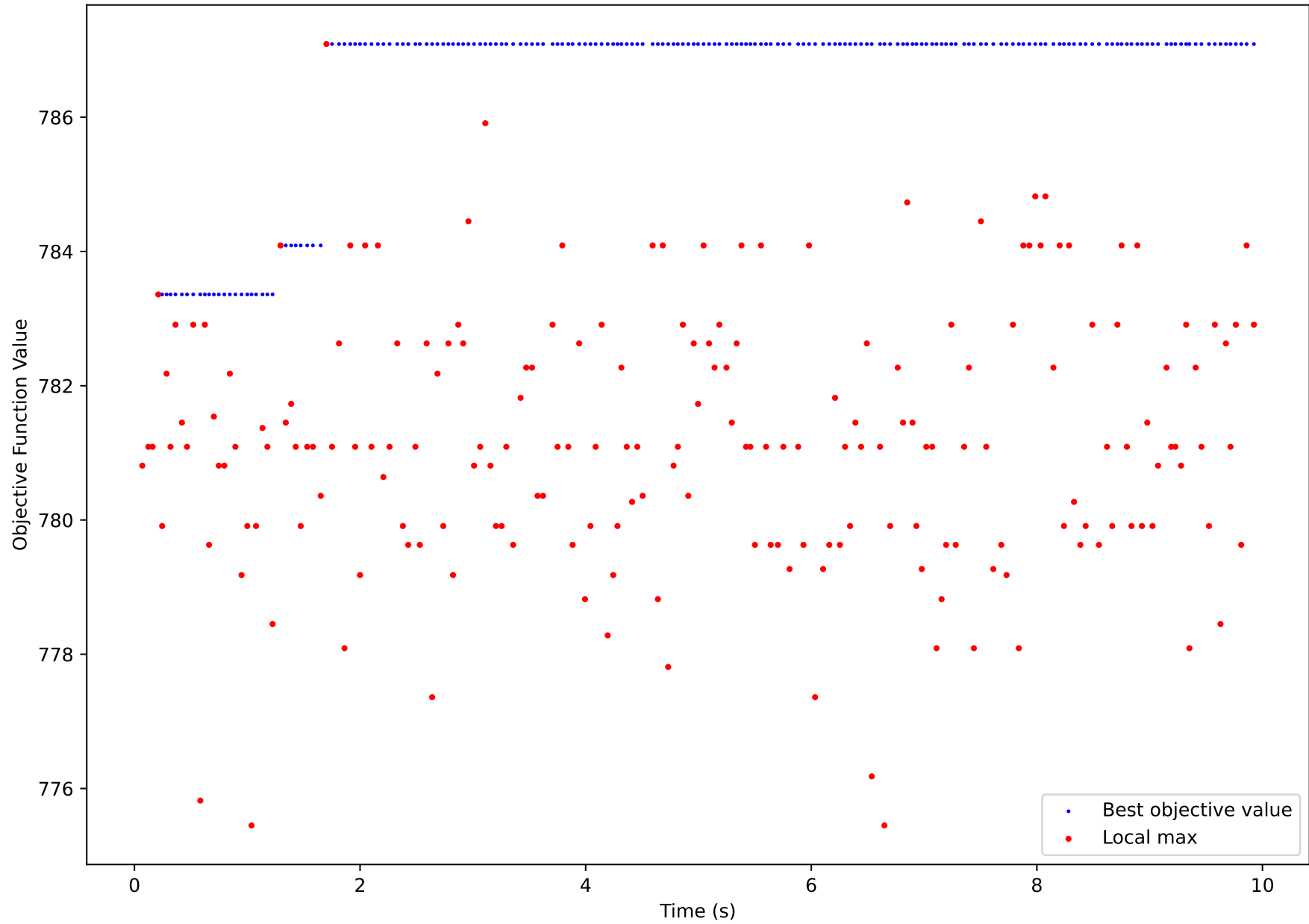
Task 3C



Task 3D



Task 3E Repeated Next Ascents (n=200)



Task 3E Repeated Steepest Ascents (n=200)

