$\mathbf{H}\mathbf{A}\mathbf{M}\mathbf{T}$

Heat and Mass Transfer

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1 Introduction

 ${\rm Text}\ [1].$

2 Boundary Conditions

2.1 Radiation

The net radiation heat flux from surface 1 to surface 2 using grey body radiation can be calculated as

$$\dot{Q}_{1\to 2} = A_1 F_{1\to 2} E_1 - A_2 F_{2\to 1} E_2. \tag{2.1}$$

using the formula for emission of grey bodies

$$E_i = \epsilon_i \sigma T_i^4 \tag{2.2}$$

and the reciprocity rule for configuration factors $A_1F_{1\rightarrow 2}=A_2F_{2\rightarrow 1}$ we can write

$$\dot{Q}_{1\to 2} = \sigma A_1 F_{1\to 2} \left(\epsilon_1 T 1^4 - \epsilon_2 T_2^4 \right) \tag{2.3}$$

and $\dot{Q}_{1\rightarrow 2}=-\dot{Q}_{2\rightarrow 1}.$ Given two line segments as seen in Fig. 2.1

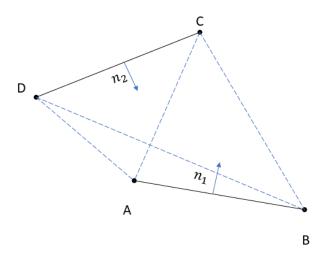


Figure 2.1: Radiation.

the configuration factor from surface \overline{AB} to surface \overline{CD} can be calculated as

$$F_{\overline{\rm AB} \to \overline{\rm CD}} = \frac{\overline{\rm AC} + \overline{\rm BD} - \overline{\rm AD} - \overline{\rm BC}}{2\overline{\rm AB}} \tag{2.4}$$

where \overline{XY} is the distance from X to Y.

In terms of boundary conditions we ca write

$$\lambda \left(\vec{n} \cdot \nabla T \right) = \frac{\dot{Q}_{1 \to 2}}{A_1} = \sigma F_{1 \to 2} \left(\epsilon_1 T 1^4 - \epsilon_2 T_2^4 \right) \tag{2.5}$$

and using a Taylor series

$$T[T^4] \approx T_0^4 + 4T_0^3 (T - T_0) = 4T_0^3 T - 3T_0^4$$
 (2.6)

and the shorthand $\tilde{\epsilon}_i = \epsilon_i \sigma F_{1\rightarrow 2}$ we get

$$\lambda \left(\vec{n} \cdot \nabla T \right) - 4\tilde{\epsilon}_1 T_{1,0}^3 T_1 + 4\tilde{\epsilon}_2 T_{2,0}^3 T_2 = 3\tilde{\epsilon}_2 T_{2,0}^4 - 3\tilde{\epsilon}_1 T_{1,0}^4. \tag{2.7}$$

Bibliography

[1] Hans Dieter Baehr and Karl Stephan. Wärme- und Stoffübertragung. Berlin, Heidelberg: Springer Berlin Heidelberg, 2019. ISBN: 978-3-662-58440-8 978-3-662-58441-5. DOI: 10.1007/978-3-662-58441-5. URL: http://link.springer.com/10.1007/978-3-662-58441-5 (visited on 10/20/2024).