
Calculation of Heat Conduction Utilizing Neural Networks

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(and whoever will work on this)

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Contents

1	Governing Equations	1
2	Discretization	2
3	Solving the Discrete Problem	4
3.1	Newton's Iteration	4
3.2	Boundary Conditions	4
4	The Linear Case	5

1 Governing Equations

We want to solve

$$\frac{d\varepsilon(x)}{dt} = -\vec{\nabla} \cdot \vec{q}(x), \quad (1)$$

where

$$\vec{q}(x) = -\alpha(x)\kappa(x)T(x)^{\beta(x)}\vec{\nabla}T(x), \quad (2)$$

and

$$\varepsilon(x) = C_V(x)T(x) = \frac{3}{2}n(x)k_B T(x). \quad (3)$$

The Gauss units are as following $\varepsilon \left[\frac{\text{erg}}{\text{cm}^3} \right], T[\text{eV}], q \left[\frac{\text{erg}}{\text{cm}^2} \right]$ with $k_B = 1.380649 \times 10^{-16} \frac{\text{erg}}{\text{K}} = 1.602178 \times 10^{-12} \frac{\text{erg}}{\text{eV}}$ and α, β are unitless. The conductivity κ in our model is defined in Gauss units as

$$\kappa(x) = \frac{Z(x) + 0.24}{Z(x) + 4.2} \frac{1.31 \times 10^{10}}{Z(x)\lambda_{ei}(x)} \tau^{\beta(x) - \frac{5}{2}}, \quad (4)$$

where Coulomb logarithm $\lambda_{ei}(x) = 23 - \ln \left(\frac{\sqrt{n(x)Z(x)}}{T(x)^{3/2}} \right)$ (see Plasma Formulary) and $\tau = \frac{1}{T_{\text{preheat}}}$.

We use $T_{\text{preheat}} = 1000$ eV to safely include the preheat region of the hohlraum wall simulation. Note that $1 \text{ erg} = 1 \frac{\text{g}\cdot\text{cm}^2}{\text{s}^2} = 10^{-7} \text{ J}$, which might be used to convert heat flux for benchmarking.

In order to solve (1), (2), and (3), we define

$$F := C_V \frac{dT}{dt} - \frac{d}{dx} \underbrace{\left(\alpha \kappa T^\beta \frac{dT}{dx} \right)}_q \quad (5)$$

and our task will be to find T that solves

$$F(T) = 0. \quad (6)$$

2 Discretization

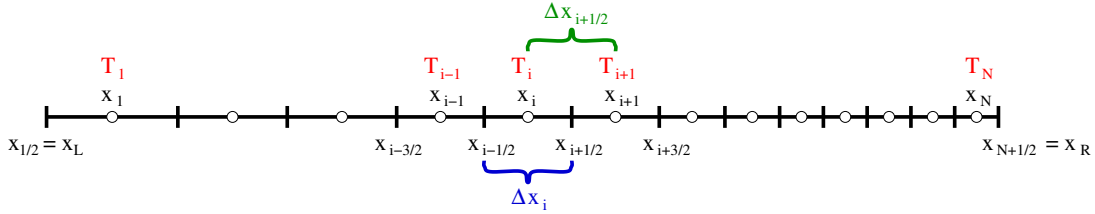


Figure 1: *Discretization of the 1D problem*

We discretize the problem on a general 1D mesh with cell-related variables indexed by integers and node-related ones by half-integers, as shown in Fig. 1.

Thus the cell volume is

$$\Delta x_i = x_{i+\frac{1}{2}} - x_{i-\frac{1}{2}}, \quad (7)$$

while the volume of the node-assigned dual cell (distance between neighboring cell centers) is

$$\Delta x_{i+\frac{1}{2}} = x_{i+1} - x_i = \frac{\Delta x_i + \Delta x_{i+1}}{2}. \quad (8)$$

The divergence of q in (1) is discretized on the primary cell by the finite difference

$$\vec{\nabla} \cdot \vec{q} \Big|_i \stackrel{1D}{=} \frac{dq}{dx} \Big|_i \approx \frac{q_{i+\frac{1}{2}} - q_{i-\frac{1}{2}}}{\Delta x_i}, \quad (9)$$

with the nodal value of the flux (2) being approximated as

$$q_{i+\frac{1}{2}} = \overline{(\alpha \kappa T^\beta)}_{i+\frac{1}{2}} \frac{T_{i+1} - T_i}{\Delta x_{i+\frac{1}{2}}}, \quad (10)$$

where $\overline{(\alpha\kappa T^\beta)}_{i+\frac{1}{2}}$ is obtained by some kind of averaging from the two connected cells, for example

$$\overline{(\alpha\kappa T^\beta)}_{i+\frac{1}{2}} = \frac{(\alpha\kappa T^\beta)_i + (\alpha\kappa T^\beta)_{i+1}}{2}, \quad (11a)$$

$$\overline{(\alpha\kappa T^\beta)}_{i+\frac{1}{2}} = \frac{\Delta x_i (\alpha\kappa T^\beta)_i + \Delta x_{i+1} (\alpha\kappa T^\beta)_{i+1}}{\Delta x_i + \Delta x_{i+1}}, \quad \text{or} \quad (11b)$$

$$\overline{(\alpha\kappa T^\beta)}_{i+\frac{1}{2}} = \frac{\frac{1}{\Delta x_i} (\alpha\kappa T^\beta)_i + \frac{1}{\Delta x_{i+1}} (\alpha\kappa T^\beta)_{i+1}}{\frac{1}{\Delta x_i} + \frac{1}{\Delta x_{i+1}}}, \quad (11c)$$

where we denoted

$$(\alpha\kappa T^\beta)_j = \alpha_j \kappa_j T_j^{\beta_j}. \quad (12)$$

Discretizing (6), resp. (1), (2), and (3) over the i -th cell, we have

$$F_i := C_{Vi} \frac{dT_i}{dt} - \frac{\overline{(\alpha\kappa T^\beta)}_{i+\frac{1}{2}} \frac{T_{i+1}-T_i}{\Delta x_{i+\frac{1}{2}}} - \overline{(\alpha\kappa T^\beta)}_{i-\frac{1}{2}} \frac{T_i-T_{i-1}}{\Delta x_{i-\frac{1}{2}}}}{\Delta x_i} \quad (13)$$

with space-dependent α and β being provided by the neural network and k , C_V being also functions of x :

$$\alpha = \alpha(\text{NN}(x)), \quad \beta = \beta(\text{NN}(x)), \quad k = k(Z(x)), \quad C_V = C_V(n(x)). \quad (14)$$

At this point let us remark, that classical heat conductivity in plasma uses constant $\beta = 5/2$, which further simplifies the equations. This is the case for example in [Silar, vyzkumak, 2009]. However, there the problem is transformed using $\theta = T^{7/2}$ and solved by a mimetic scheme, whereas here we are going to proceed by Newton's iterative method.

For a regular mesh (i.e., with equidistant nodes), we have

$$\Delta x = \Delta x_i = \Delta x_{i+\frac{1}{2}}, \quad \forall i, \quad (15)$$

and thus (13) simplifies to

$$F_i = C_{Vi} \frac{dT_i}{dt} - \frac{1}{\Delta x^2} \left(\overline{(\alpha\kappa T^\beta)}_{i+\frac{1}{2}} (T_{i+1} - T_i) - \overline{(\alpha\kappa T^\beta)}_{i-\frac{1}{2}} (T_i - T_{i-1}) \right) \quad (16)$$

and all three types of averaging (11) are equivalent:

$$\overline{(\alpha\kappa T^\beta)}_{i+\frac{1}{2}} = \frac{(\alpha\kappa T^\beta)_i + (\alpha\kappa T^\beta)_{i+1}}{2}. \quad (17)$$

There are several ways to solve (6), that is, in the discrete case

$$F_i(\mathbf{T}) = 0, \quad \forall i. \quad (18)$$

Replacing also the time derivative by a finite difference, (16) becomes

$$F_i(\mathbf{T}) = C_{Vi} \frac{T_i - T_i^{[t-\Delta t]}}{\Delta t} - \frac{1}{\Delta x^2} \left(\overline{(\alpha\kappa T^\beta)}_{i+\frac{1}{2}} (T_{i+1} - T_i) - \overline{(\alpha\kappa T^\beta)}_{i-\frac{1}{2}} (T_i - T_{i-1}) \right), \quad (19)$$

where $T_i^{[t-\Delta t]}$ is the temperature at the previous time level $t - \Delta t$. Note that by using temperature at the actual time level t in the spatial difference (the term in parentheses), we are aiming at implicit schemes, so that the time step Δt is not overrestricted by stability requirements.

3 Solving the Discrete Problem

3.1 Newton's Iteration

For simplicity, let's take in each equation the value of $(\alpha k/\beta)$ from the actual cell instead of using nodal averages at its endpoints. Then we have a system similar to (18) with the i -th equation being

$$F_i^*(\mathbf{T}) = C_{Vi} \frac{T_i - T_i^{[t-\Delta t]}}{\Delta t} - \alpha_i \kappa_i T_i^{\beta_i} \frac{T_{i-1} - 2T_i + T_{i+1}}{\Delta x^2}. \quad (20)$$

The Jacobian of such system is a tridiagonal matrix with the elements

$$J_{i,i} = \frac{\partial F_i^*}{\partial T_i} = \frac{C_{Vi}}{\Delta t} + 2 \frac{\alpha_i \kappa_i}{\Delta x^2} (\beta_i + 1) T_i^{\beta_i} \quad (21a)$$

$$J_{i,i\pm 1} = \frac{\partial F_i^*}{\partial T_{i\pm 1}} = - \frac{\alpha_i \kappa_i T_i^{\beta_i}}{\Delta x^2}. \quad (21b)$$

Using precise definition of nonlinear functional F given by (19) and approximate Jacobian (21), we can now perform the k -th iteration of Newton's method:

$$\mathbf{T}^{(k+1)} = \mathbf{T}^{(k)} - \mathbf{J}^{-1} \mathbf{F}(\mathbf{T}^{(k)}). \quad (22)$$

Keep in mind, that the superscript $^{(k)}$ stands for Newton's iteration, not for the evolution in time! Therefore, $T_i^{[t-\Delta t]}$ in (20) stays the same in all iterations at given time t , until the solution \mathbf{T} at this time level has converged.

3.2 Boundary Conditions

We will enforce

$$\nabla T = 0 \quad (23)$$

on both ends of the domain. To do this on a mesh of N cells indexed from 1 to N (see Fig. 1), we formally introduce the ghost values

$$T_0 = T_1, \quad T_{N+1} = T_N. \quad (24)$$

Inserting them into the equations (20) for the boundary cells ($i = 1$ resp. $i = N$), we get

$$F_1(\mathbf{T}) := C_{V1} \frac{T_1 - T_1^{[t-\Delta t]}}{\Delta t} - \frac{(\overline{\alpha \kappa T^\beta})_{\frac{3}{2}} (T_2 - T_1)}{\Delta x^2}, \quad (25a)$$

$$F_N(\mathbf{T}) := C_{VN} \frac{T_N - T_N^{[t-\Delta t]}}{\Delta t} + \frac{(\overline{\alpha \kappa T^\beta})_{N-\frac{1}{2}} (T_N - T_{N-1})}{\Delta x^2}, \quad (25b)$$

which immediately yields the first and last row of the Jacobian matrix

$$J_{1,1} = \frac{\partial F_1^*}{\partial T_1} = \frac{C_{V_1}}{\Delta t} + \frac{\alpha_1 \kappa_1}{\Delta x^2} (\beta_1 + 1) T_1^{\beta_1}, \quad (26a)$$

$$J_{1,2} = \frac{\partial F_1^*}{\partial T_2} = - \frac{\alpha_1 \kappa_1 T_1^{\beta_1}}{\Delta x^2}, \quad (26b)$$

$$J_{N,N-1} = \frac{\partial F_N^*}{\partial T_{N-1}} = - \frac{\alpha_N \kappa_N T_N^{\beta_N}}{\Delta x^2}, \quad (26c)$$

$$J_{N,N} = \frac{\partial F_N^*}{\partial T_N} = \frac{C_{V_N}}{\Delta t} + \frac{\alpha_N \kappa_N}{\Delta x^2} (\beta_N + 1) T_N^{\beta_N}. \quad (26d)$$

4 The Linear Case

Let us now look at the special case of linear heat conduction, that is,

$$\beta_i \equiv 0, \forall i \quad (27)$$

and for simplicity let us also use a constant coefficient

$$a = \alpha_i \kappa_i, \forall i \quad (28)$$

and constant heat capacity. In other words, we are solving

$$C_V \frac{dT}{dt} = a \frac{d^2 T}{dx^2}, \quad (29)$$

which we discretize (again aiming at the implicit scheme), define the functional

$$F_i = C_V \frac{T_i - T_i^{[t-\Delta t]}}{\Delta t} - a \frac{T_{i-1} - 2T_i + T_{i+1}}{\Delta x^2} \quad (30)$$

and calculate

$$F_i = 0, \forall i. \quad (31)$$

If Newton's iteration was to be used, the Jacobian would be a constant tridiagonal matrix with elements

$$J_{i,i} = \frac{\partial F_i}{\partial T_i} = \frac{C_V}{\Delta t} + 2 \frac{a}{\Delta x^2} \quad (32a)$$

$$J_{i,i\pm 1} = \frac{\partial F_i}{\partial T_{i\pm 1}} = - \frac{a}{\Delta x^2}. \quad (32b)$$

However, for such a simple problem it is not necessary to iterate or even explicitly formulate the Jacobian. We can simply rewrite (basically just reorder) (31) with (30) as

$$T_i - \frac{a}{C_V} \frac{\Delta t}{\Delta x^2} (T_{i-1} - 2T_i + T_{i+1}) = T_i^{[t-\Delta t]}, \quad (33)$$

that is,

$$-\frac{a}{C_V} \frac{\Delta t}{\Delta x^2} T_{i-1} + \left(1 + 2\frac{a}{C_V} \frac{\Delta t}{\Delta x^2}\right) T_i - \frac{a}{C_V} \frac{\Delta t}{\Delta x^2} T_{i+1} = T_i^{[t-\Delta t]}, \quad (34)$$

and denoting

$$b = \frac{a}{C_V} \quad (35)$$

we recover

$$-b \frac{\Delta t}{\Delta x^2} T_{i-1} + \left(1 + 2b \frac{\Delta t}{\Delta x^2}\right) T_i - b \frac{\Delta t}{\Delta x^2} T_{i+1} = T_i^{[t-\Delta t]}, \quad (36)$$

which yields a simple linear system

$$\mathbf{A} \mathbf{T} = \mathbf{T}^{[t-\Delta t]}, \quad (37)$$

with a tridiagonal constant matrix \mathbf{A} as it can be found in many textbooks on implicit methods for parabolic problems.