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Assignment 1

Aero 707 Liam Hood

```
clear; close all; clc
global r2d
r2d = 180/pi;
% %% Problem 2
% problem_2()
%
```

Problem 3

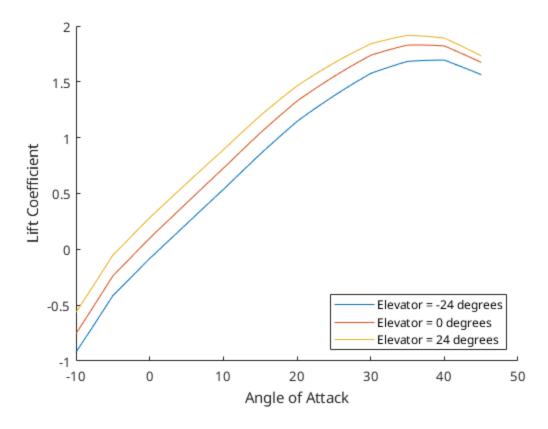
```
global r2d
    fprintf("\n*****Problem 3*****\n")
    % 2.3-1 Find instantaneous angle of attack and angle of side slip
    % in the gusts
    % Given starting conditions
   v = 500;
   alpha = 8/r2d;
   beta = -5/r2d;
    % Rotation matrices
    % stability from body fixed
    C_s_bf = [cos(alpha), 0, sin(alpha);
                0, 1, 0;
                -sin(alpha), 0, cos(alpha)];
    % wind from stability
    C_w_s = [\cos(beta), \sin(beta), 0;
            -sin(beta), cos(beta), 0;
            0, 0, 1];
    % wind from body fixed
   C_w_bf = C_w_s*C_s_bf;
    % starting V
   vw = [v;0;0];
   vbf = C w bf'*vw;
    % i
```

```
fprintf("i. Gust of 20 ft/s left to right (+velocity in y body fixed)\n")
    vbf1 = vbf + [0;20;0];
    disp("Don't know why this needs to be here")
    [alpha1, beta1] = find alpha beta(vbf1);
    disp("but it won't publish without these strings")
    fprintf("\tAngle of attack is now %f degrees\n", alpha1)
    fprintf("\tAngle of sideslip is now %f degrees\n", betal)
    fprintf("ii. Gust of 50 ft/s from dead astern(+velocity in x body
 fixed)\n")
    vbf2 = vbf + [50;0;0];
    [alpha2, beta2] = find_alpha_beta(vbf2);
    fprintf("\tAngle of attack is now %f degrees\n", alpha2)
    fprintf("\tAngle of sideslip is now %f degrees\n", beta2)
    % iii
    fprintf("iii. Gust of 30 ft/s from right and below (-velocity in y, -
velocity in z\n")
    vbf3 = vbf + [0;-30*cos(70/r2d);-30*sin(70/r2d)];
    [alpha3, beta3] = find_alpha_beta(vbf3);
    fprintf("\tAngle of attack is now %f degrees\n", alpha3)
    fprintf("\tAngle of sideslip is now %f degrees\n", beta3)
******Problem 3*****
i. Gust of 20 ft/s left to right (+velocity in y body fixed)
Don't know why this needs to be here
```

Problem 4

```
problem_4

*****Problem 4*****
Max lift occurs at an angle of attack of 35.000000 degrees
```

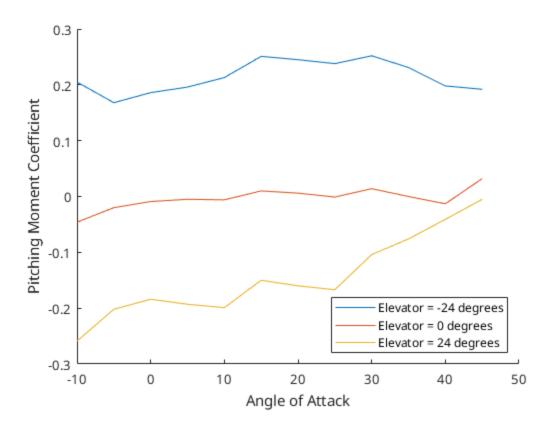


Problem 5

problem_5

*****Problem 5*****

We can see that the F16 lacks pitch stiffness as the curves all vary from flat to a slight slope up. The elevator does significantly shift the whole curve showing it has significant control power



Problem 6

```
problem_6
```

```
*****Problem 6*****

I did not see a what pitch or flight path was used for Table 3.6-1

so I adjusted pitch to match initial cost in the table

TAS: 170.000000 ft/s AOA: 0.385718 radians Pitch: 0.217817 radians

Pitch Rate: 0.000000 radians/s Altitude: 0.000000 ft Distance 0.000000 ft

Sum of Weighted Squares: 28.937859

TAS: 500.000000 ft/s AOA: 0.010123 radians Pitch: 0.068749 radians

Pitch Rate: 0.000000 radians/s Altitude: 0.000000 ft Distance 0.000000 ft

Sum of Weighted Squares: 3.542947

TAS: 500.000000 ft/s AOA: 0.094771 radians Pitch: 0.105418 radians

Pitch Rate: 0.000000 radians/s Altitude: 0.000000 ft Distance 0.000000 ft

Sum of Weighted Squares: 10.812971

****Find derivations for state equations*****
```

Problem 7

problem_7

*****Problem 7*****

```
Equilibrium Points:
x1 = -2
          x2 = 0
x1=1 - 3^{(1/2)*1i}
                     x2 = 0
x1=3^{(1/2)*1i} + 1
                     x2 = 0
         x2=-2*2^{(1/2)}
x1 = 0
x1 = 0
         x2=2*2^{(1/2)}
Linearize around x1=-2, x2=0 using first order Taylor series
The A matrix is:
[12, 0]
[ 0, -2]
The eigenvalues of this A matrix are lambda= -2.000000 and 12.000000
Linearize around x1=1-3^{(1/2)*i}, x2=0 using first order Taylor series
The A matrix is:
[3*(-1+3^{(1/2)*1i})^2,
                      0, 1 - 3^{(1/2)*1i}
The eigenvalues of this A matrix are lambda= 1.000000+-1.732051i and
 -6.000000+-10.392305i
Linearize around x1=1+3^{(1/2)*i}, x2=0 using first order Taylor series
The A matrix is:
[3*(1 + 3^{(1/2)*1i})^2,
                    0, 1 + 3^{(1/2)*1i}
Γ
The eigenvalues of this A matrix are lambda= 1.000000+1.732051i and
 -6.000000+10.392305i
Linearize around x1=0, x2=2*2^{(1/2)} using first order Taylor series
The A matrix is:
[
         0, -4*2^(1/2)]
[2*2^(1/2),
                     0]
 The eigenvalues of this A matrix are lambda= 0.000000+-4.000000i and
 0.000000+4.000000i
Linearize around x1=0, x2=-2*2^{(1/2)} using first order Taylor series
The A matrix is:
          0, 4*2^(1/2)]
[-2*2^{(1/2)}]
                  0]
The eigenvalues of this A matrix are lambda= 0.000000+-4.000000i and
0.000000+4.000000i
```

Problems

```
7, 9, 10];
      B = [2; 1; 5];
응
응
      y = C*x+D*u
응
      C = [2, 1, 3];
응
      D = 0;
응
ွ
      % Transfer function G(s)
    fprintf("Transfer Function\n")
응
      syms s
응
      G = collect(C*inv((s*eye(3)-A))*B);
응
      fprintf("From formula\n")
응
      fprintf("G(s) = %s\n", G)
      fprintf("Built in Function\n")
응
응
      [b,a] = ss2tf(A,B,C,D);
응
      G builtin = collect((b(1)*s^3 + b(2)*s^2 + b(3)*s + b(4))/...
응
          (a(1)*s^3 + a(2)*s^2 + a(3)*s + a(4)));
응
      fprintf("G(s) = %s\n", G_builtin)
응
      % Poles
응
      fprintf("\nPoles\n")
응
      poles builtin = eig(A);
응
      poles = vpasolve(det(s*eye(3)-A)==0,s);
응
      fprintf("From formula\n")
      fprintf("Poles %f, %f, %f \n", poles)
응
      fprintf("Built in Function\n")
왕
      fprintf("Poles %f, %f, %f \n", poles_builtin)
end
function problem_3()
    global r2d
    fprintf("\n*****Problem 3*****\n")
    % 2.3-1 Find instantaneous angle of attack and angle of side slip
    % in the gusts
    % Given starting conditions
    v = 500;
    alpha = 8/r2d;
    beta = -5/r2d;
    % Rotation matrices
    % stability from body fixed
    C_s_bf = [cos(alpha), 0, sin(alpha);
                0, 1, 0;
                -sin(alpha), 0, cos(alpha)];
    % wind from stability
    C_w_s = [\cos(beta), \sin(beta), 0;
            -sin(beta), cos(beta), 0;
            0, 0, 1];
    % wind from body fixed
    C_w_bf = C_w_s*C_s_bf;
    % starting V
    vw = [v;0;0];
    vbf = C_w_bf'*vw;
    % i
    fprintf("i. Gust of 20 ft/s left to right (+velocity in y body fixed)\n")
```

```
vbf1 = vbf + [0;20;0];
    disp("Don't know why this needs to be here")
    [alpha1, beta1] = find_alpha_beta(vbf1);
    disp("but it won't publish without these strings")
    fprintf("\tAngle of attack is now %f degrees\n", alpha1)
    fprintf("\tAngle of sideslip is now %f degrees\n", betal)
    fprintf("ii. Gust of 50 ft/s from dead astern(+velocity in x body
 fixed)\n"
    vbf2 = vbf + [50;0;0];
    [alpha2, beta2] = find_alpha_beta(vbf2);
    fprintf("\tAngle of attack is now %f degrees\n", alpha2)
    fprintf("\tAngle of sideslip is now %f degrees\n", beta2)
    % iii
    fprintf("iii. Gust of 30 ft/s from right and below (-velocity in y, -
velocity in z\n")
    vbf3 = vbf + [0;-30*cos(70/r2d);-30*sin(70/r2d)];
    [alpha3, beta3] = find alpha beta(vbf3);
    fprintf("\tAngle of attack is now %f degrees\n", alpha3)
    fprintf("\tAngle of sideslip is now %f degrees\n", beta3)
end
function problem_4()
    fprintf("\n*****Problem 4*****\n")
    % 2.3-4 Find instantaneous angle of attack and angle of side slip
    % in the gusts
    n = 1e2;
    alpha = linspace(-10, 45, n);
    elev = [-24,0,24];
    for ii = 1:3
        cl(ii,:) = zeros(1,n);
        for jj = 1:n
            cl(ii,jj) = CX(alpha(jj),elev(ii))*sind(alpha(jj)) - ...
                CZ(alpha(jj),0,elev(ii))*cosd(alpha(jj));
        end
    end
    figure
   hold on
   plot(alpha, cl(1,:))
   plot(alpha, cl(2,:))
    plot(alpha, cl(3,:))
    legend("Elevator = -24 degrees", "Elevator = 0 degrees", ...
        "Elevator = 24 degrees", "Location", "southeast")
    xlabel("Angle of Attack")
    ylabel("Lift Coefficient")
    hold off
    [~,~I] = \max(cl(3,:));
    fprintf("Max lift occurs at an angle of attack of %f degrees\n", alpha(I))
end
function problem_5()
```

```
fprintf("\n*****Problem 5*****\n")
    % 2.3-5
   n = 1e2;
    alpha = linspace(-10,45,n);
    elev = [-24,0,24];
    for ii = 1:3
        cm(ii,:) = zeros(1,n);
        for jj = 1:n
            cm(ii,jj) = CM(alpha(jj),elev(ii));
        end
    end
    figure
   hold on
   plot(alpha, cm(1,:))
   plot(alpha, cm(2,:))
   plot(alpha, cm(3,:))
    legend("Elevator = -24 degrees", "Elevator = 0 degrees", ...
        "Elevator = 24 degrees", "Location", "southeast")
   xlabel("Angle of Attack")
    ylabel("Pitching Moment Coefficient")
    hold off
    fprintf("We can see that the F16 lacks pitch stiffness as the curves all
\n")
    fprintf("vary from flat to a slight slope up. The elevator does
 significantly \n")
    fprintf("shift the whole curve showing it has significant control power
\n")
end
function problem 6()
    fprintf("\n*****Problem 6*****\n")
    global r2d
    % 3.5-1
    fprintf("I did not see a what pitch or flight path was used for Table
 3.6-1\n")
    fprintf("so I adjusted pitch to match initial cost in the table \n")
    x1 = [170; 22.1/r2d; 12.48/r2d; 0; 0; 0];
    u1 = [.297, -25.7, .25, 0];
    [xd1] = transp(x1,u1);
    sos1 = xd1(1)^2 + 100*xd1(2)^2 + 10*xd1(4)^4;
    fprintf("TAS: %f ft/s AOA: %f radians Pitch: %f radians \n", x1(1:3))
    fprintf("Pitch Rate: %f radians/s Altitude: %f ft Distance %f ft\n",
 x1(4:6)
    fprintf("\tSum of Weighted Squares: %f\n", sos1)
    x2 = [500; .58/r2d; 3.939/r2d; 0; 0; 0];
    u2 = [.293, 2.46, .25, 0];
    [xd2] = transp(x2,u2);
    sos2 = xd2(1)^2 + 100*xd2(2)^2 + 10*xd2(4)^4;
    fprintf("TAS: %f ft/s AOA: %f radians Pitch: %f radians \n", x2(1:3))
    fprintf("Pitch Rate: %f radians/s Altitude: %f ft Distance %f ft\n",
    fprintf("\tSum of Weighted Squares: %f\n", sos2)
```

```
x3 = [500; 5.43/r2d; 6.04/r2d; 0; 0; 0];
    u3 = [.204, -4.10, .25, 0];
    [xd3] = transp(x3,u3);
    sos3 = xd3(1)^2 + 100*xd3(2)^2 + 10*xd3(4)^4;
    fprintf("TAS: %f ft/s AOA: %f radians Pitch: %f radians \n", x3(1:3))
    fprintf("Pitch Rate: %f radians/s Altitude: %f ft Distance %f ft\n",
 x3(4:6))
    fprintf("\tSum of Weighted Squares: %f\n", sos3)
    fprintf("****Find derivations for state equations*****\n")
end
function problem_7()
    fprintf("\n*****Problem 7*****\n")
    global r2d
    % 3.7-1
    syms x1 x2
   x1dot = x1^3-x2^2+8;
   x2dot = x1*x2;
    sol = solve(x1dot==0,x2dot==0,x1,x2);
    fprintf("Equilibrium Points:\n")
    for ii = 1:5
        fprintf("\tx1=%s
                           x2=%s\n",[sol.x1(ii),sol.x2(ii)])
    end
    fprintf("Linearize around x1=-2, x2=0 using first order Taylor series\n")
    A = subs([diff(x1dot,x1), diff(x1dot,x2); diff(x2dot,x1), diff(x2dot,x2)],
[x1,x2],[-2,0]);
    fprintf("The A matrix is:\n")
    disp(A)
    [\sim,D] = eig(A);
    fprintf("\tThe eigenvalues of this A matrix are lambda= %f and %f\n\n",
[D(1,1),D(2,2)])
    fprintf("Linearize around x1=1-3^(1/2)*i, x2=0 using first order Taylor
 series\n")
    A = subs([diff(x1dot,x1), diff(x1dot,x2); diff(x2dot,x1), diff(x2dot,x2)],
[x1,x2],[1-3^{(1/2)*i,0]};
    fprintf("The A matrix is:\n")
    disp(A)
    [\sim,D] = eig(A);
    fprintf("\tThe eigenvalues of this A matrix are lambda= %f+%fi and %f+%fi
n^n, [real(D(1,1)), imag(D(1,1)), real(D(2,2)), imag(D(2,2))])
    fprintf("Linearize around x1=1+3^{(1/2)*i}, x2=0 using first order Taylor
 series\n")
    A = subs([diff(x1dot,x1), diff(x1dot,x2); diff(x2dot,x1), diff(x2dot,x2)],
[x1,x2],[1+3^{(1/2)*i,0]};
    fprintf("The A matrix is:\n")
    disp(A)
    [\sim,D] = eig(A);
    fprintf("\tThe eigenvalues of this A matrix are lambda= %f+%fi and %f+%fi
n^n, [real(D(1,1)), imag(D(1,1)), real(D(2,2)), imag(D(2,2))])
```

```
fprintf("Linearize around x1=0, x2=2*2^(1/2) using first order Taylor
 series\n")
    A = subs([diff(x1dot,x1), diff(x1dot,x2); diff(x2dot,x1), diff(x2dot,x2)],
[x1,x2],[0,2*2^{(1/2)}]);
    fprintf("The A matrix is:\n")
    disp(A)
    [\sim,D] = eig(A);
    fprintf("\tThe eigenvalues of this A matrix are lambda= %f+%fi and %f+%fi
n^n, [real(D(1,1)), imag(D(1,1)), real(D(2,2)), imag(D(2,2))])
    fprintf("Linearize around x1=0, x2=-2*2^(1/2) using first order Taylor
 series\n")
    A = subs([diff(x1dot,x1), diff(x1dot,x2); diff(x2dot,x1), diff(x2dot,x2)],
[x1,x2],[0,-2*2^{(1/2)}]);
    fprintf("The A matrix is:\n")
    disp(A)
    [\sim,D] = eig(A);
    fprintf("\tThe eigenvalues of this A matrix are lambda= %f+%fi and %f+%fi
n^n, [real(D(1,1)), imag(D(1,1)), real(D(2,2)), imag(D(2,2))])
end
```

Functions

```
function [alpha, beta] = find alpha beta(vbf)
    global r2d
    syms alphas betas V
    C_s_bf = [cos(alphas), 0, sin(alphas);
                0, 1, 0;
                -sin(alphas), 0, cos(alphas)];
    % wind from stability
    C_w_s = [\cos(betas), \sin(betas), 0;
            -sin(betas), cos(betas), 0;
            0, 0, 1];
    % wind from body fixed
    C w bf = C w s*C s bf;
    sol = vpasolve([V;0;0]==C_w_bf*vbf,[alphas,betas,V]);
    alpha = sol.alphas*r2d;
    beta = sol.betas*r2d;
end
function [CXI]=CX(alpha,elev)
    % Data and interpolation for F-16 Axial force coefficient.
    alphtabl=[-10,-5,0,5,10,15,20,25,30,35,40,45];
    elevtabl=[-24, -12, 0, 12, 24];
    cxtabl=[-.099, -.081, -.081, -.063, -.025, .044, .097...
    .113, .145, .167, .174, .166;
    -.048, -.038, -.040, -.021, .016, .083, .127...
    .137, .162, .177, .179, .167;
    -.022, -.020, -.021, -.004, .032, .094, .128...
    .130, .154, .161, .155, .138;
    -.040, -.038, -.039, -.025, .006, .062, .087...
    .085, .100, .110, .104, .091;
```

```
-.083, -.073, -.076, -.072, -.046, .012, .024...
    .025, .043, .053, .047, .040];
    CXI= interp2(alphtabl,elevtabl,cxtabl,alpha,elev);
end
function [CZI]=CZ(alpha,beta,elev)
    % Data and interpolation for F-16 z-force coefficient
    alphtabl=[-10,-5,0,5,10,15,20,25,30,35,40,45];
    cztabl=[.770, .241, -.100, -.416, -.731, -1.053, -1.366...
    -1.646, -1.917, -2.120, -2.248, -2.229];
    C1= interp1(alphtabl,cztabl,alpha);
    CZI = C1*(1-(beta/57.3)^2) - .19*(elev/25.0);
end
function [CMI]=CM(alpha,elev)
    % F-16 model pitching-moment data and interpolation
    alphtabl=[-10,-5,0,5,10,15,20,25,30,35,40,45];
    elevtabl = [-24, -12, 0, 12, 24];
    cmtabl=[.205, .168, .186, .196, .213, .251, .245...
    .238, .252, .231, .198, .192;
    .081, .077, .107, .110, .110, .141, .127...
    .119, .133, .108, .081, .093;
    -.046, -.020, -.009, -.005, -.006, .010, .006...
    -.001, .014, .000, -.013, .032;
    -.174, -.145, -.121, -.127, -.129, -.102, -.097...
    -.113, -.087, -.084, -.069, -.006;
    -.259, -.202, -.184, -.193, -.199, -.150, -.160...
    -.167, -.104, -.076, -.041, -.005];
    CMI = interp2(alphtabl,elevtabl,cmtabl,alpha,elev);
end
function [xd] = transp(x,u)
    % Medium-sized transport aircraft, longitudinal dynamics
    S = 2170.0; CBAR = 17.5; MASS = 5e3; IYY = 4.1e6;
    TSTAT = 6e4; DTDV = -38; ZE = 2; CDCLS = .042;
    CLA = .085; CMA = -.022; CMDE = -.016; % per degree
    CMQ = -16; CMADOT = -6; CLADOT = 0; % per radian
   RTOD = 57.29578; GD = 32.17;
    THTL = u(1);
    ELEV = u(2);
    XCG =
            u(3);
    LAND = u(4);
    VT =
            x(1);
                        % TAS in fps
    ALPHA = RTOD*x(2); % A. O. A.
   THETA = x(3);
                        % PITCH ATTITUDE
    O =
            x(4);
                        % PITCH RATE
   H =
            x(5);
                        % ALTITUDE
    [\sim,QBAR] = ADC(VT,H);
    QS = QBAR*S;
    SALP = sin(x(2)); CALP = cos(x(2));
    GAM = THETA - x(2); SGAM = sin(GAM); CGAM = cos(GAM);
    if LAND == 0
                        % clean
        CLO = .2; CDO = .016;
        CMO = .05; DCDG = 0; DCMG = 0;
```

```
elseif LAND == 1 % landing flap and gear
        CLO = 1; CDO = .08;
        CMO = -.2; DCDG = .02; DCMG = -.05;
       disp("Landing Gear & Flaps")
    end
    THR = (TSTAT+VT*DTDV) * max(THTL,0);
                                                    % THR
   CL = CLO+CLA*ALPHA;
                                                    % NONDIM LIFT
   CM = DCMG+CMO+CMA*ALPHA+CMDE*ELEV+CL*(XCG-.25); % MOMENT
   CD = DCDG+CDO+CDCLS*CL*CL;
                                                     % DRAG POLAR
    % State Equations
   xd(1) = (THR*CALP-QS*CD)/MASS - GD*SGAM;
   xd(2) = (-THR*SALP-QS*CL+MASS*(VT*Q+GD*CGAM))/(MASS*VT+QS*CLADOT);
   xd(3) = Q;
   D = .5*CBAR*(CMQ*Q+CMADOT*xd(2))/VT;
   xd(4) = (QS*CBAR*(CM+D)+THR*ZE)/IYY;
   xd(5) = VT*SGAM;
   xd(6) = VT*CGAM;
end
function [MACH,QBAR] = ADC(VT,H)
   R0 = 2.377e-3i
   TFAC = 1 - .703e - 5*H;
   T = 519*TFAC;
    if H >= 35000
        T = 390;
    end
   RHO = R0*(TFAC^4.14);
   MACH = VT/sqrt(1.4*1716.3*T);
    OBAR = .5*RHO*VT*VT;
end
but it won't publish without these strings
Angle of attack is now 8.000000 degrees
Angle of sideslip is now -2.710123 degrees
ii. Gust of 50 ft/s from dead astern(+velocity in x body fixed)
Angle of attack is now 7.271964 degrees
Angle of sideslip is now -4.549540 degrees
iii. Gust of 30 ft/s from right and below (-velocity in y, -velocity in z
Angle of attack is now 4.766735 degrees
Angle of sideslip is now -6.207827 degrees
```

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