PART I: Waves

Simple harmonic oscillator

Spring-block system:

$$F = -kx$$

$$= ma = m\frac{\mathrm{d}^2 x}{\mathrm{d}t^2}$$

$$m\frac{\mathrm{d}^2 x}{\mathrm{d}t^2} = -kx$$

$$x(t) = A\cos(\omega_0 t + \phi) \quad \text{with} \quad \omega = \sqrt{k/m}$$

$$v(t) = \frac{\mathrm{d}x}{\mathrm{d}t} = -A\omega_0 \sin(\omega_0 t + \phi)$$

$$a(t) = \frac{\mathrm{d}v}{\mathrm{d}t} = \frac{\mathrm{d}^2 x}{\mathrm{d}t^2} = -A\omega_0^2 \cos(\omega_0 t + \phi)$$

$$K = \frac{1}{2}mv^2 = \frac{1}{2}mA^2\omega_0^2 \sin^2(\omega_0 t + \phi)$$

$$U = \frac{1}{2}kx^2 = \frac{1}{2}kA^2\cos^2(\omega_0 t + \phi)$$

$$E = \frac{1}{2}mA^2\omega_0^2$$

Phasors, complex exponential notation, addition

$$x + iy = a\cos(\omega_0 t + \phi) + ia\sin(\omega_0 t + \phi)$$
$$= ae^{i(\omega_0 t + \phi)}.$$

Beats

$$A\cos 2\pi f_1 + A\cos 2\pi f_2 = 2A\cos 2\pi \frac{f_1 - f_2}{2}\cos 2\pi \frac{f_1 + f_2}{2}$$
$$f_{\text{beat}} = |f_1 - f_2|$$

Wave equation

$$\frac{\partial^2 \psi(x,t)}{\partial t^2} = v^2 \frac{\partial^2 \psi(x,t)}{\partial x^2}$$

Solutions

$$\psi(x,t) = h(x - ct) + g(x + ct)$$
$$f(x,t) = A\cos(kx - \omega t + \phi)$$

Speed

$$v = \sqrt{\frac{T}{\mu}}$$
$$v = f\lambda$$

Linearity and principle of superposition

Travelling Waves

Energy transfer - reflection and transmission

Phase changes at boundaries

$$\begin{split} K_{\lambda} &= \frac{1}{4}\mu\omega^2A^2\lambda \\ E_{\lambda} &= U_{\lambda} + K_{\lambda} = \frac{1}{2}\mu\omega^2A^2\lambda. \\ P &= \frac{1}{2}\mu\omega^2A^2v \end{split}$$

Longitudinal and transverse waves

Carrier and envelope

$$\psi_1(x,t) + \psi_2(x,t) = a\cos(\omega_1 t - k_1 x) + a\cos(\omega_2 t - k_2 x)$$

$$= 2a\cos\left[\frac{\omega_1 + \omega_2}{2}t - \frac{k_1 + k_2}{2}x\right]\cos\left[\frac{\omega_1 - \omega_2}{2}t - \frac{k_1 - k_2}{2}x\right]$$

Phase and group velocities (dispersion)

$$v_{p} = \frac{\omega}{k}$$

$$v_{g} = \frac{\partial \omega}{\partial k} = \frac{\partial (v_{p}k)}{\partial k} = v_{p} + k \frac{\partial v_{p}}{\partial k}.$$

Standing waves

$$y_1 + y_2 = Ae^{i(kx - \omega t + \pi)} + Ae^{i(kx + \omega t)}$$
$$= -2A\sin kx \sin \omega t$$

Harmonics

On a fixed string:

$$f_n = n \frac{v}{2L}, \quad n = 1, 2, 3, \dots$$

Pipe open at both ends:

$$f_n = n \frac{v}{2L}, \quad n = 1, 2, 3, \dots$$

Pipe closed at one end:

$$f_n = n \frac{v}{4L}, \quad n = 1, 3, 5, \dots$$

Nodes and antinodes

On a fixed string:

$$x = n\frac{\lambda}{2}, \ n = 0, 1, 2, \dots$$
 nodes

$$x = n \frac{(2n+1)\lambda}{4}, \ n = 0, 1, 2, \dots$$
 antinodes

Sound

$$s(x,t) = s_{\text{max}} \cos(kx - \omega t) \Delta P = \Delta P_{\text{max}} \sin(kx - \omega t)$$

$$v_{\rm sound\ in\ air} \approx 340\ {\rm ms}^{-1}$$

Measurement of sound

The *sound level*, β , is measured in decibels (dB).

$$\beta = 10 \log \frac{I}{I_0}$$

Doppler effect

Observer moving with respect to stationary source

$$f' = \left(\frac{v \pm v_0}{v}\right) f$$

Source moving towards stationary observer

$$f' = \left(\frac{v}{v \mp v_s}\right) f$$

Both source/observer moving

$$f' = \left(\frac{v \pm v_{\rm O}}{v \mp v_{\rm S}}\right) f$$

Relativistic Doppler effect

$$f_{\rm obs} = \frac{\sqrt{1 + v/c}}{\sqrt{1 - v/c}} f_{\rm source}$$

For $v \ll c$ this is equivalent to the "normal" Doppler effect.

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PART II: Light

General nature

$$c = f\lambda$$

electromagnetic spectrum, especially visible light

$$\mathbf{E} = \mathbf{E}_0 e^{i(\omega t - \mathbf{k}.\mathbf{x})}$$

$$\mathbf{H} = \mathbf{H}_0 e^{i(\omega t - \mathbf{k}.\mathbf{x})}$$

Optical Path Length = $n_{\alpha}d$

= index of refraction \times distance travelled

Associated phase = $kn_{\alpha}d$ where $k = \frac{2\pi}{\lambda}$

$$n_{\alpha} = \frac{\text{speed of light in vacuum}}{\text{speed of light in medium } \alpha}$$

$$=\frac{c}{v_{\alpha}}$$

$$\lambda_n = \frac{\lambda_0}{n}$$

Polarization

Types of polarization

Methods of producing polarizations

Brewster angle

$$\tan \theta_p = \frac{n_2}{n_1}$$

Malus' law

$$I = I_0 \cos^2 \theta$$

Propagation

Fermat's and Huygens' principles

Reflection

$$\theta_i = \theta_r$$

Refraction

$$n_i \sin \theta_i = n_t \sin \theta_t$$

Total Internal Reflection and the Critical Angle

$$\sin \theta_c = \frac{n_1}{n_2}$$

Interference

Coherence

Fraunhöfer and Fresnel limits

Constructive and destructive interference

$$d_2 - d_1 = n\lambda$$
, $n = 0, 1, 2, 3, \dots$ (constructive interference)

Young's double slit experiment

$$d\sin\theta = m\lambda$$

$$y_m = m \frac{\lambda D}{d}$$

Thin films

Change of phase upon reflection

Soap bubble

$$2nd\cos\beta = \left(m - \frac{1}{2}\right)\lambda$$
 (constructive interference)

Oil film

$$2nd\cos\beta = \left(m - \frac{1}{2}\right)\lambda$$
 (constructive interference)

Anti-reflection coating

Thin film wedge

$$(p + \frac{1}{2})\lambda = 2\alpha x$$
 - bright fringes

Newton's rings

$$2t = (p + \frac{1}{2})\lambda$$
 (constructive interference)

$$r^2 = (p + \frac{1}{2})\lambda R$$

Interferometers

Michelson interferometer

The distance d associated with m fringes is $d = m\lambda/2$.

Dark fringes

$$\cos \theta = p \frac{\lambda}{2d}$$

Doublet source

$$\Delta \lambda = \lambda_2 - \lambda_1 = \frac{\lambda_1 \lambda_2}{2\Delta d} \approx \frac{\lambda^2}{2\Delta d}$$

Fabry-Perot interferometer

Etalon

Diffraction

Single-slit diffraction

$$a\sin\theta = n\lambda$$

Multiple slits

$$I = I_0 \frac{\sin^2 \alpha}{\alpha^2} \times \frac{\sin^2 N\beta}{\sin^2 \beta}$$

$$\alpha = \frac{\pi}{\lambda} a \sin \theta$$
 and $\beta = \frac{\pi}{\lambda} d \sin \theta$

Interference Maxima

Maxima when
$$\frac{\sin N\beta}{\sin \beta} = N$$
 or when $\beta = 0, \pm \pi, \pm 2\pi, \dots$

Interference Minima

Minima when $\frac{\sin N\beta}{\sin \beta} = 0$ or

$$\beta = \pm \frac{\pi}{N}, \pm \frac{2\pi}{N}, \dots, \pm \frac{(N-1)\pi}{N}, \pm \frac{(N+1)\pi}{N}, \dots$$

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N-2 subsidiary maxima.

Subsidiary Interference Maxima

$$\beta = \pm \frac{3\pi}{2N}, \pm \frac{5\pi}{2N}, \dots$$

Missing peaks

$$\frac{d}{a} = \frac{m}{n}$$

Instrumental broadening

$$\Delta\theta = \frac{2\lambda}{ND\cos\theta_{\rm m}}$$

Circular apertures

Rayleigh criterion

$$\sin\theta \approx \theta \ge \frac{\lambda}{a}$$

$$\sin \theta \approx \theta \ge 1.22 \frac{\lambda}{D}$$

Gratings

Dispersion relation

$$\frac{\mathrm{d}\theta}{\mathrm{d}\lambda} = \frac{m}{d\cos\theta} \approx \frac{m}{d}$$

Resolving power

$$R = \frac{\lambda}{\Delta \lambda} = Nm$$

PART III: Optics

Real and virtual images

Mirrors

Magnification

$$M = -\frac{q}{p} = \frac{h_{\rm i}}{h_{\rm o}}$$

Plane mirrors

Mirror equation

$$\frac{1}{p} + \frac{1}{q} = \frac{1}{f}$$

Sign conventions

Convex mirrors

$$\begin{array}{l} f < 0 \\ p \text{ anywhere} \end{array}$$

Concave mirrors

$$f > 0$$

$$p > f$$

$$p < f$$

Ray tracing

Lenses

Refraction at a spherical surface

Lens-makers' equation

$$\frac{1}{f} = (n-1)\left(\frac{1}{R_1} - \frac{1}{R_2}\right)$$

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Thin lenses

Thin-lens equation

$$\frac{1}{p} + \frac{1}{q} = \frac{1}{f}$$

Magnification

$$M = -\frac{q}{p} = \frac{h_{i}}{h_{o}}$$

Sign conventions

Positive, converging, bi-convex lens

$$f > 0$$

$$p > f$$

$$p < f$$

Negative, diverging, bi-concave lens

$$f < 0$$
 p anywhere

Ray tracing

Aberrations

Spherical Chromatic

Compound lenses

$$M_T = M_1 M_2 \dots M_N$$

Optical systems and instruments

Camera

f-number

$$f$$
 – number $\equiv \frac{f}{D}$

The human eye

Near point
$$\equiv 25 \text{ cm}$$

Far point $\equiv \infty$

The simple magnifier

$$m_{\min} = \frac{\theta}{\theta_0} = \frac{25 \text{ cm}}{f}$$

$$m_{\text{max}} = 1 + \frac{25 \text{ cm}}{f}$$

The compound microscope

$$M = M_1 m_e = -\frac{L}{f_o} \left(\frac{25 \text{ cm}}{f_e} \right)$$

The refracting telescope

The astronomical telescope

$$L \approx f_o + f_e$$

$$m = -\frac{f_o}{f_e}$$

The terrestrial telescope

$$L = f_o - |f_e|$$

$$m = -\frac{f_o}{f_e}$$

The reflecting telescope

The Hubble space telescope

COSTAR