

Contents

1	Schematics and Simulation Results	1
1.1	Frequency response at the ADC input	1
1.2	Frequency response at the input to the anti-aliasing filter	2
1.3	Input impedance at the BNC	3
1.4	Clamper	4
1.5	Power dissipation	5
1.6	10 kHz input signal at the input to the ADC	5
2	Discussion	7
2.1	Power Block	7
2.2	Clamper Block	7
2.3	Scaling Block	9
2.4	Buffer Block	11
2.5	Anti-aliasing Filter	12
2.6	Inverting Level Shifter Block	14
3	Observation	16
4	Summary	17
	Appendix	18

1 Schematics and Simulation Results

The front end design including power, clamper, scaling, buffer, anti-aliasing filter and inverting level shifter is shown in figure 1.1.

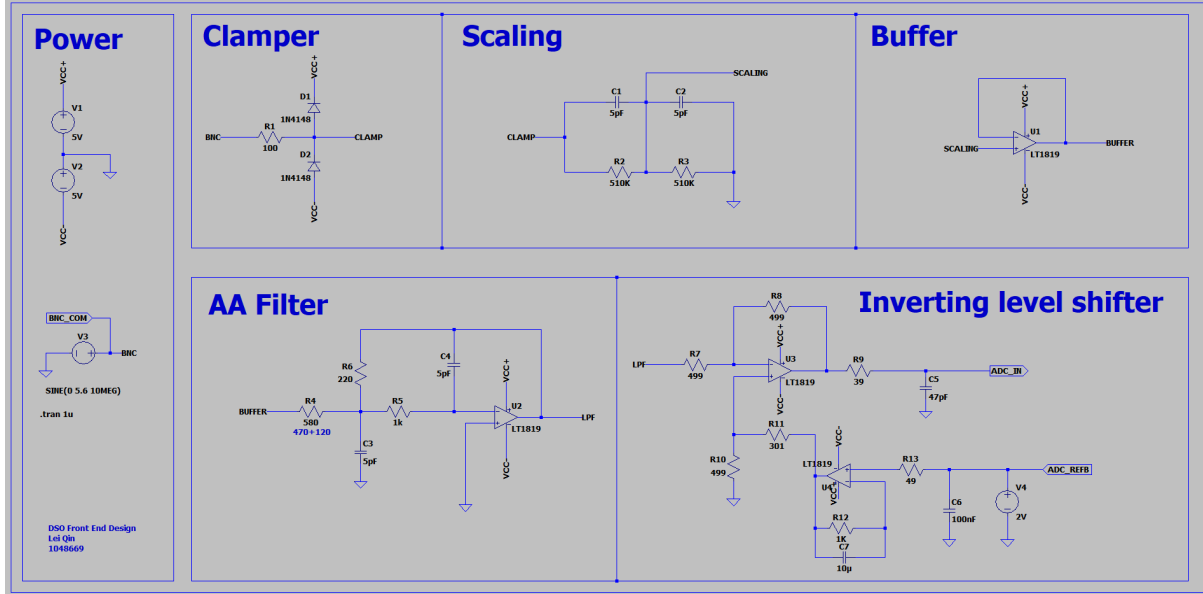


Figure 1.1: Front End design schematic.

1.1 Frequency response at the ADC input

The magnitude and phase response at the ADC input are shown in figure 1.2 and figure 1.3. The magnitude at 1Hz and 18.72MHz are about -14.68dB and -17.67dB . Thus , the cut off frequency is about 18.72MHz . The phase at 18.72MHz is about -73.755° which is larger than -180° . The response is of more than 20dB per decade and less than 2dB ripple.

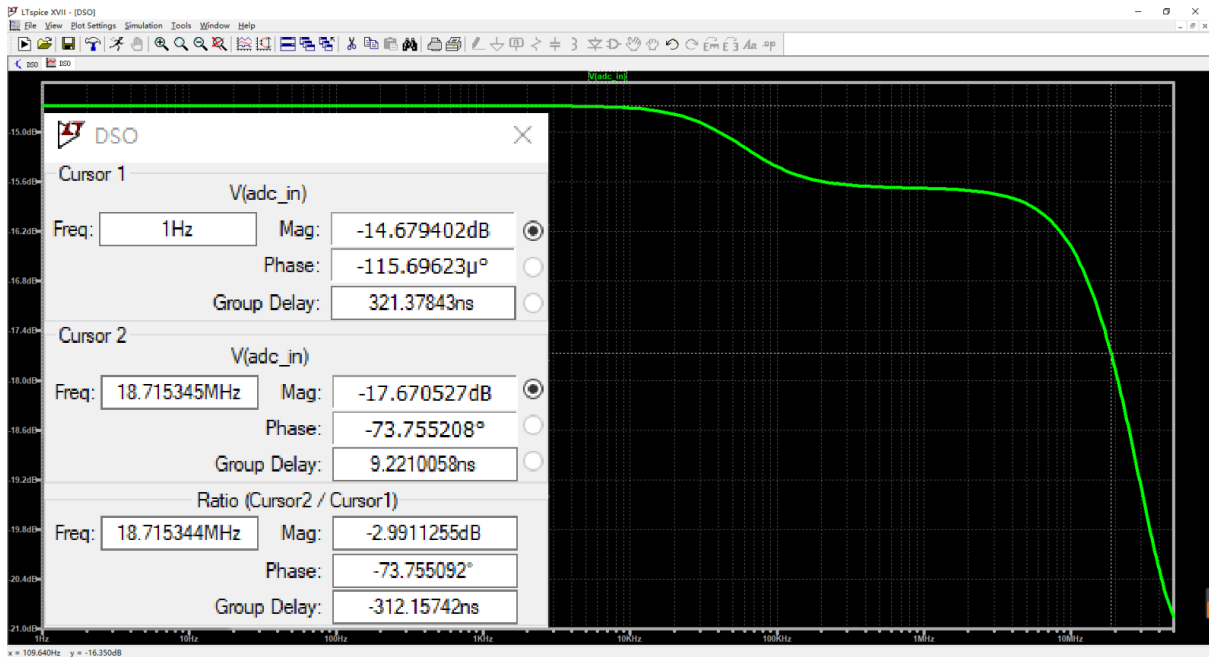


Figure 1.2: Magnitude response at the ADC input.

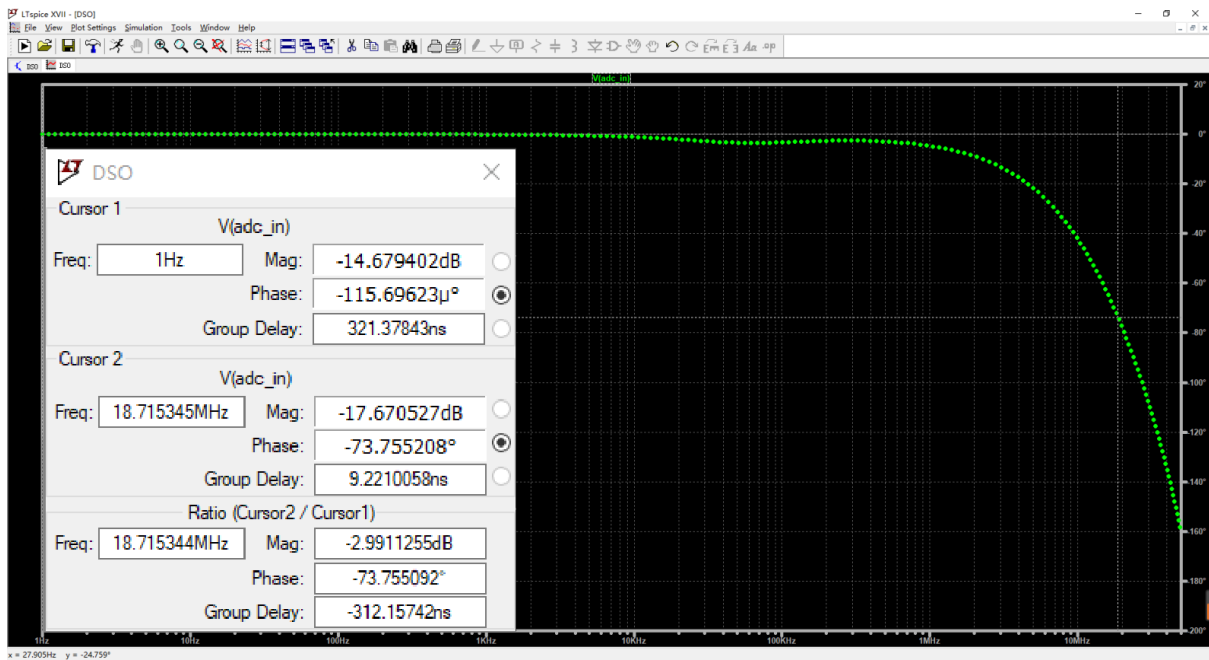


Figure 1.3: Phase response at the ADC input.

1.2 Frequency response at the input to the anti-aliasing filter

The frequency response at the input to the anti-aliasing filter is shown in figure 1.4.

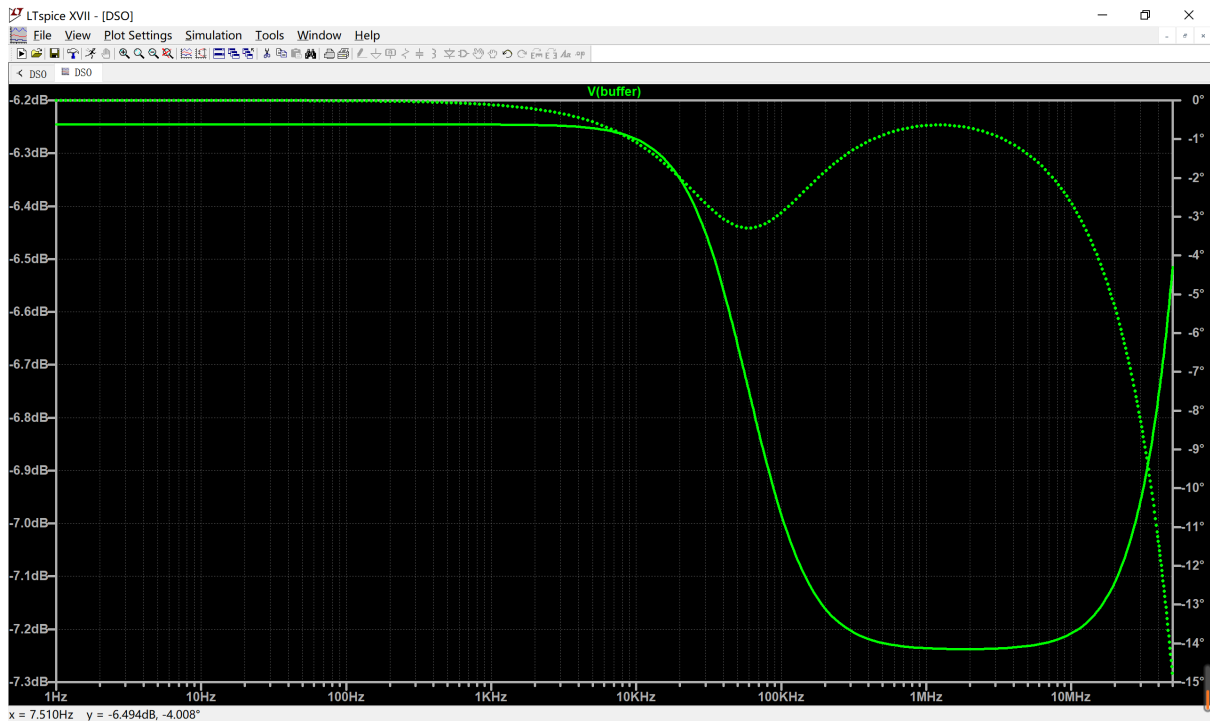


Figure 1.4: Frequency response at the input to the anti-aliasing filter.

1.3 Input impedance at the BNC

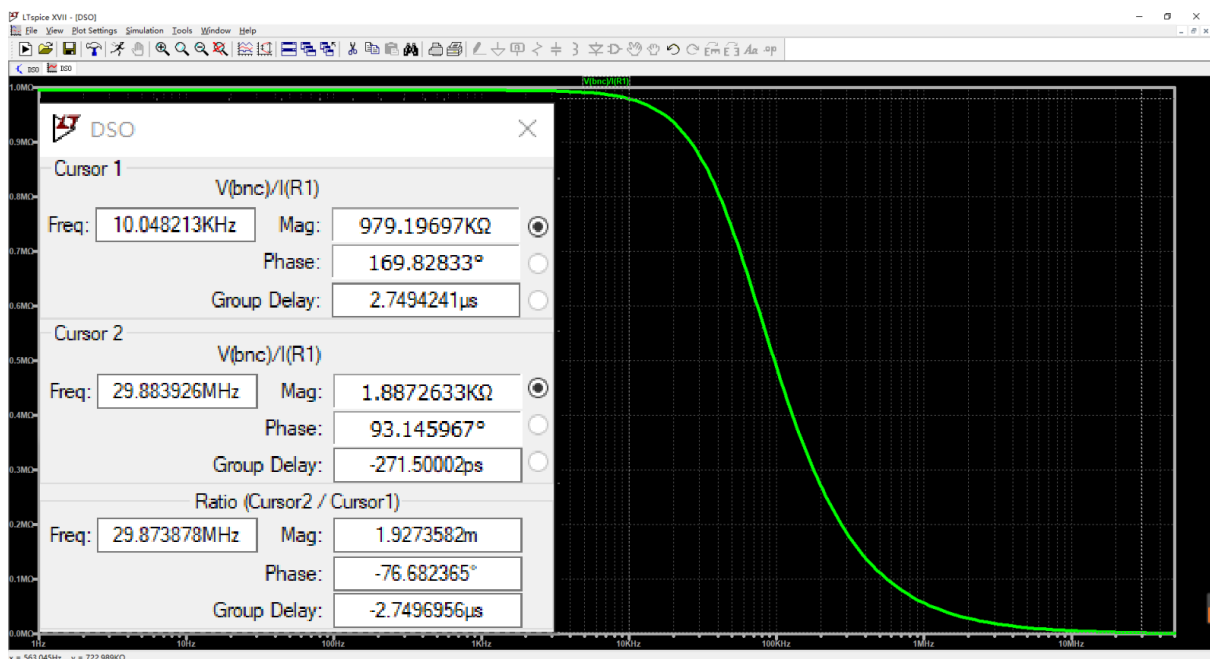


Figure 1.5: Input impedance at the BNC.

The input impedance at the BNC is shown in figure 1.5. We can the input impedance from DC to 10kHz is at least 0.979MΩ; the input impedance from 10kHz to 30MHz is at least

1.887k Ω .

1.4 Clamper

The clamping output signals with 5V and 10V input are shown in figure 1.6 and 1.7.

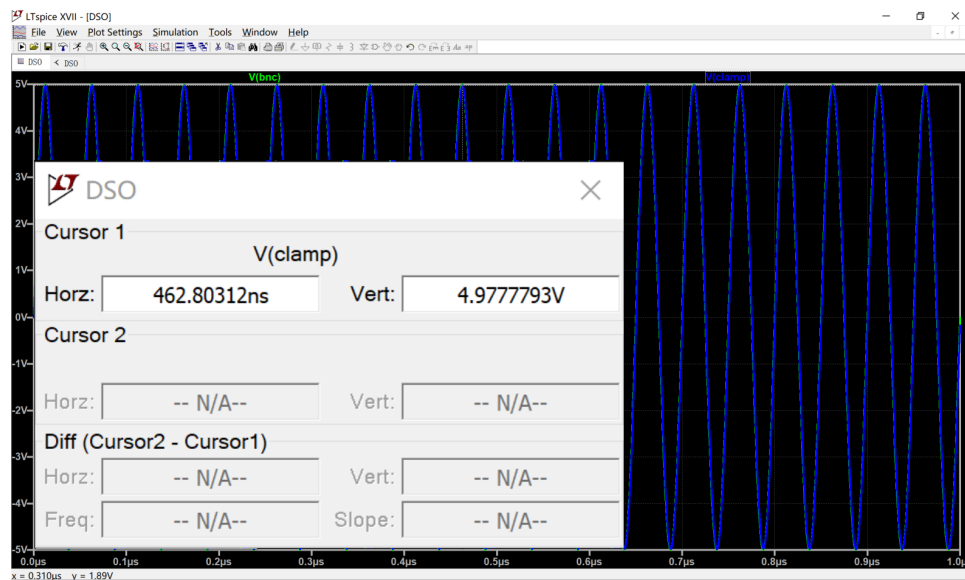


Figure 1.6: Clamping circuit with 5 V input.

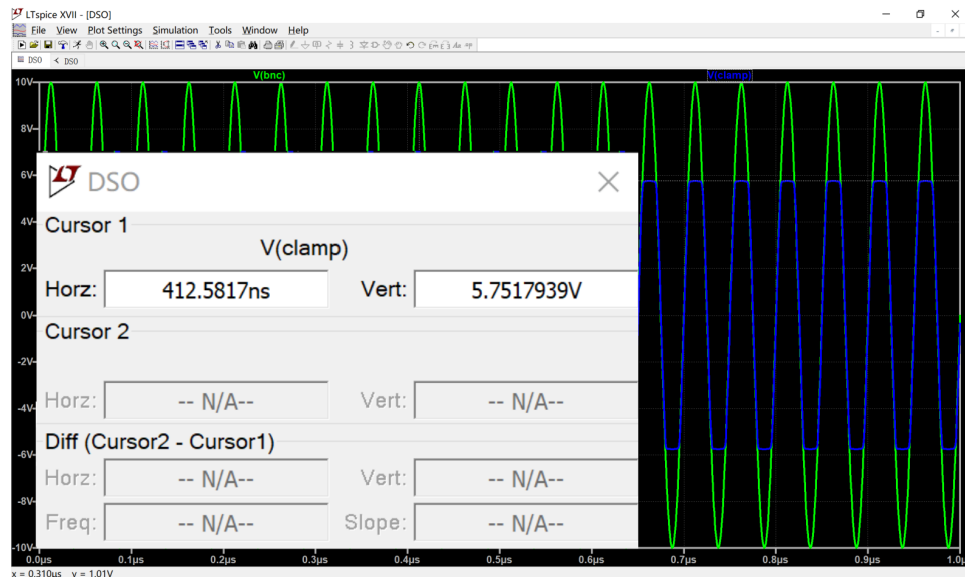


Figure 1.7: Clamping circuit with 10 V input.

1.5 Power dissipation

Given that the the device must draw less than 150mA per rail when running a maximum sampling rate, the maximum power at 5V is:

$$P_{max} = 150m \times 5 = 750mW$$

From the operating point information in Appendix and the formulation for power consumption of Op-Amp in figure 1.8, we can calculate the total power dissipation in figure 1.9 is about 387.964mW which is less than the requirement.

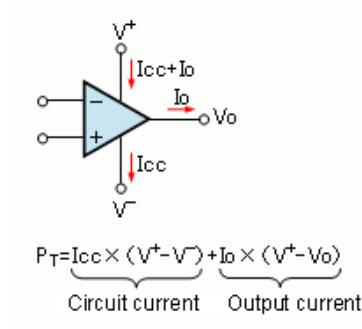


Figure 1.8: Power consumption of Op-Amp.

Component	Vo	Io	Icc	Max power consumed (mW)
				(5.6V, 20MHz)
Buffer OpAmp (U1)	0.497	-8.581E-04	9.05E-03	86.671
AA Filter OpAmp (U2)	-0.192	3.741E-03	9.43E-03	113.705
ADC In OpAmp (U3)	2.681	-2.877E-03	9.38E-03	87.126
Level Shifter OpAmp (U4)	1.997	2.494E-03	9.30E-03	100.462
Sum				387.964

Figure 1.9: Power dissipation table.

1.6 10 kHz input signal at the input to the ADC

The input to the ADC in time domain with 10 kHz 5.6V input signal is shown in figure 1.10. We can see the signal goes from 1.834V to 3.529V.

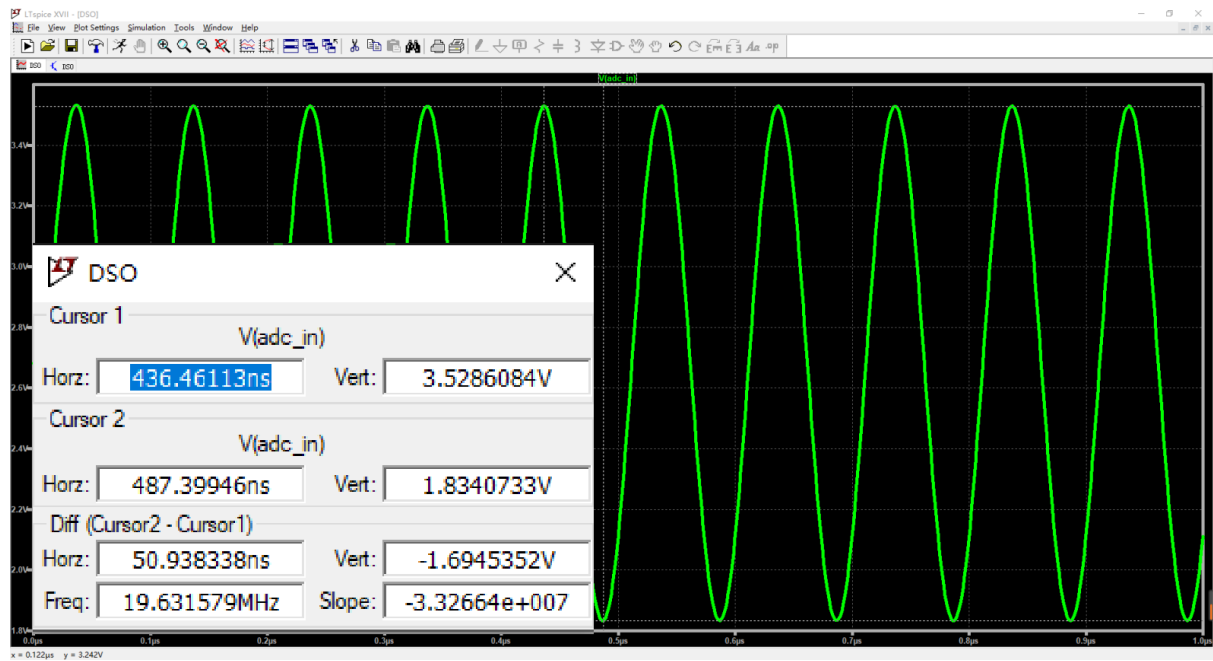


Figure 1.10: Time domain 10 kHz input signal at the input to the ADC.

2 Discussion

2.1 Power Block

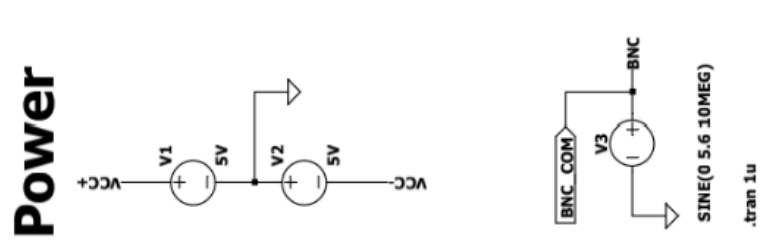


Figure 2.1: Power.

$V_{cc+} = 5V$, $V_{cc-} = -5V$. The input signal is through a BNC connector.

2.2 Clamper Block

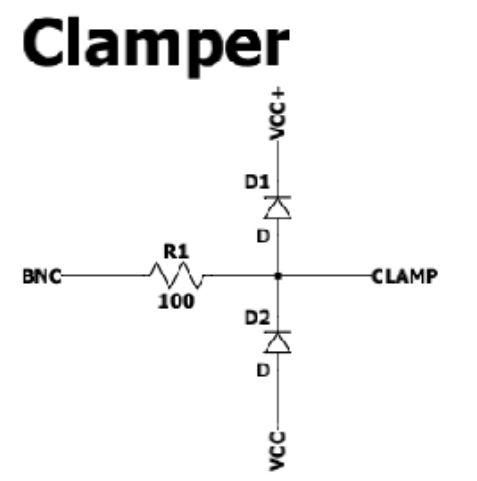


Figure 2.2: Clamper.

The BNC input can accept a maximum input of $\pm 5.6V$ after which the input voltage is clamped. The clamper circuit is to protect the front end circuit by clipping the input signal if it exceeds $\pm 5.6V$.

Resistor $R_1 = 100\Omega$ is to absorb the divided voltage when clamping. A small value is chosen because when there is a high frequency input signal, the total impedance would become very small which would increase the total current of the circuit. Since we do not want many voltages drop on R_1 , we need to choose a small value for that.

The clamping output signals with 5V and 10V input are shown in figure 2.3 and 2.4. We can see if the magnitude of input is larger than 5.6V, it would be clamped by this part circuit to around 5.6V.

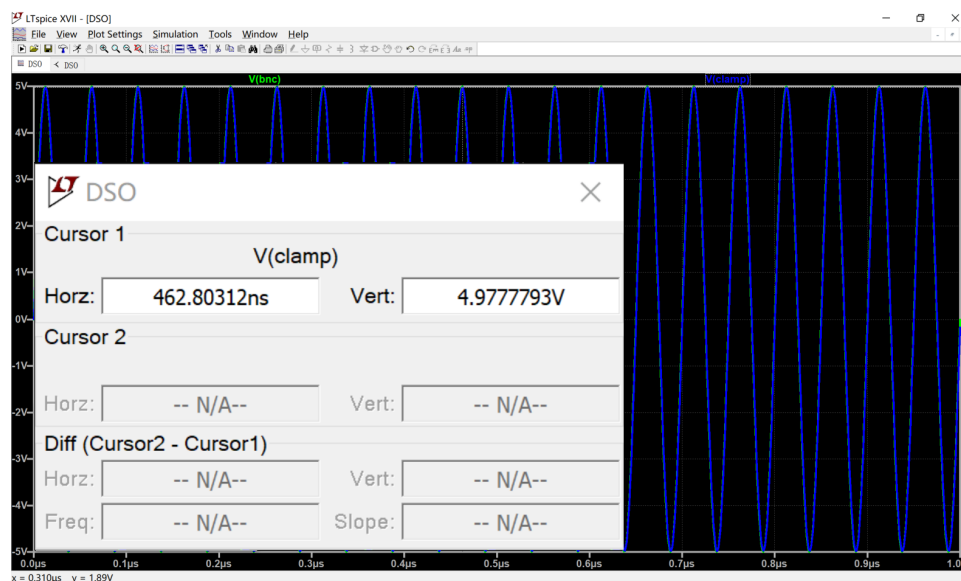


Figure 2.3: Clamping circuit with 5 V input.

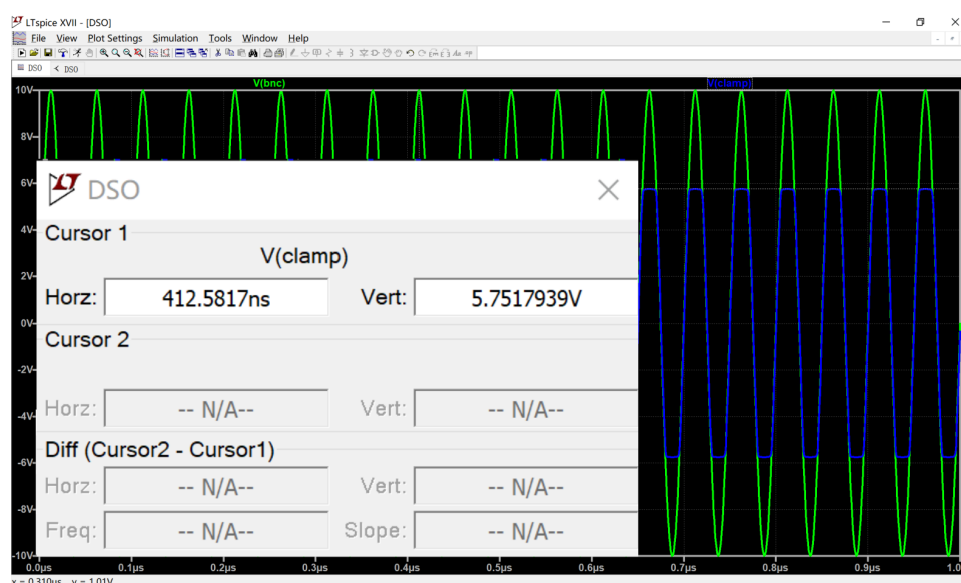


Figure 2.4: Clamping circuit with 10 V input.

2.3 Scaling Block

Scaling

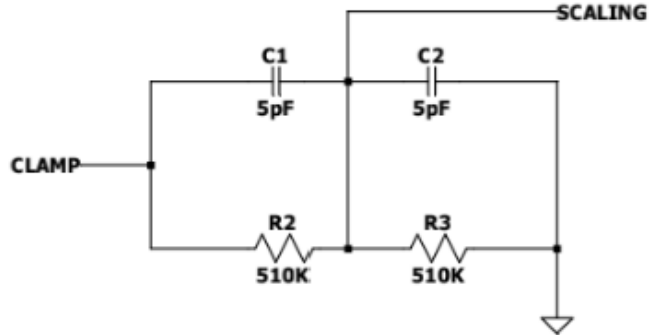


Figure 2.5: Scaling.

The scaling circuit is to provide enough impedance for the whole circuit and scale the input signal for later use.

$R_2 = R_3 510k\Omega$, $C_1 = C_2 = 5pF$ are to ensure the input has a $1M\Omega \pm 10\%$ input impedance from DC to $10kHz$ and at least 100Ω input impedance from $10kHz$ to $30MHz$. The total impedance can be calculated by:

$$Z_{total} = (X_{C1} || R_2) + (X_{C2} || R_3)$$

For $10kHz$: $Z_{total} = 2 * (\frac{1}{2\pi f C_1} || R_2) \approx 1.02M\omega$;

For $30MHz$: $Z_{total} = 2 * (\frac{1}{2\pi f C_1} || R_2) \approx 2.12k\omega$.

The input impedance at the BNC is shown in figure 2.6. We can the input impedance from DC to $10kHz$ is at least $0.979M\Omega$; the input impedance from $10kHz$ to $30MHz$ is at least $1.887k\Omega$.

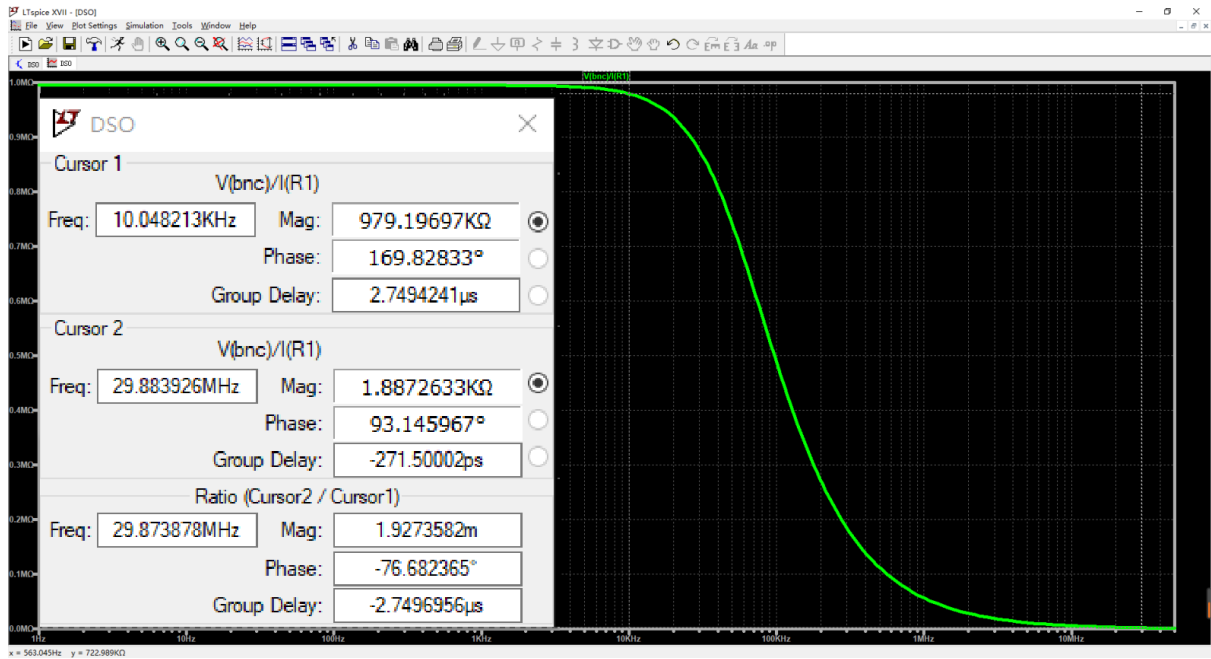


Figure 2.6: Input impedance at the BNC.

Additionally, $C_1 = C_2 = 5\text{ pF}$ is chosen to ensure that the input capacitance is less than 60 pF .

Then the input signal is halved after the scaling circuit shown in figure 2.7

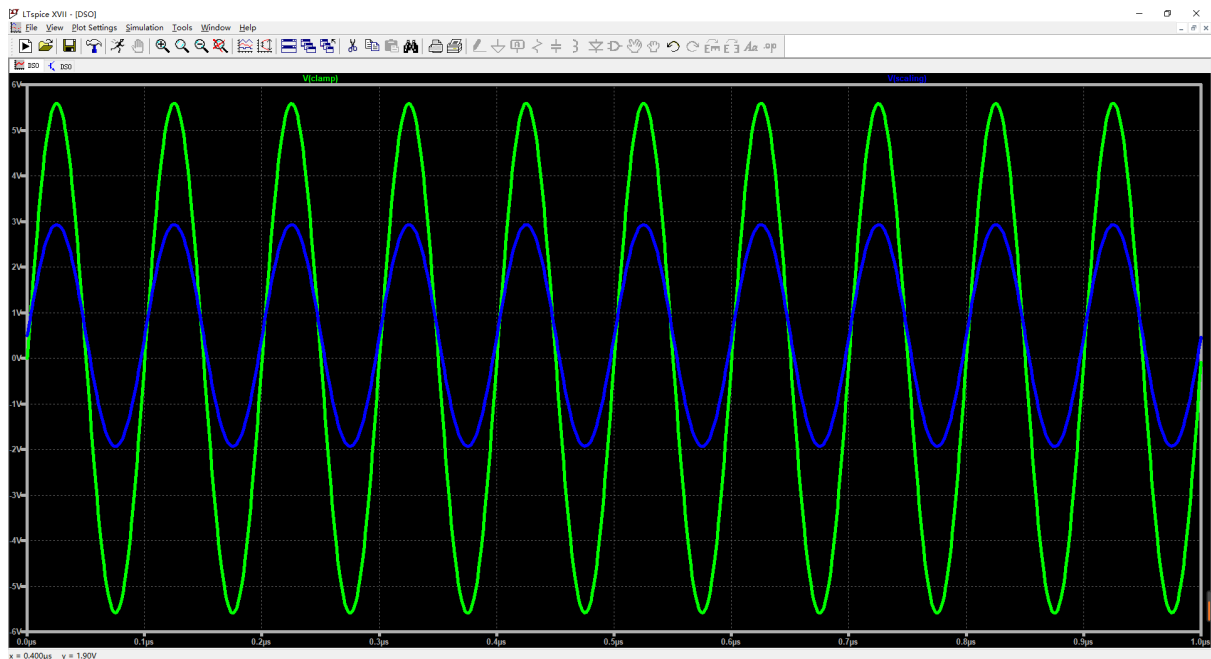


Figure 2.7: Scaling v.s. Camping.

2.4 Buffer Block

Buffer

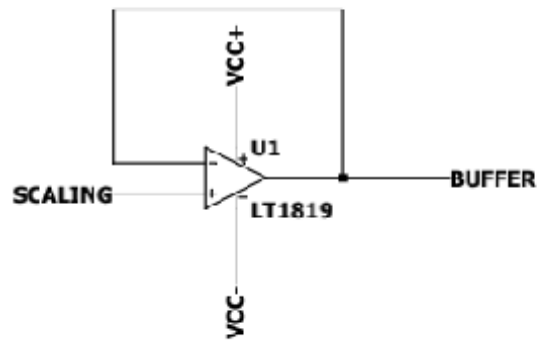


Figure 2.8: Buffer.

The buffer is used to decouple the front and back circuits. So it can keep the impedance of the previous design unchanged.

The frequency response at the input to the anti-aliasing filter is shown in figure 2.9.

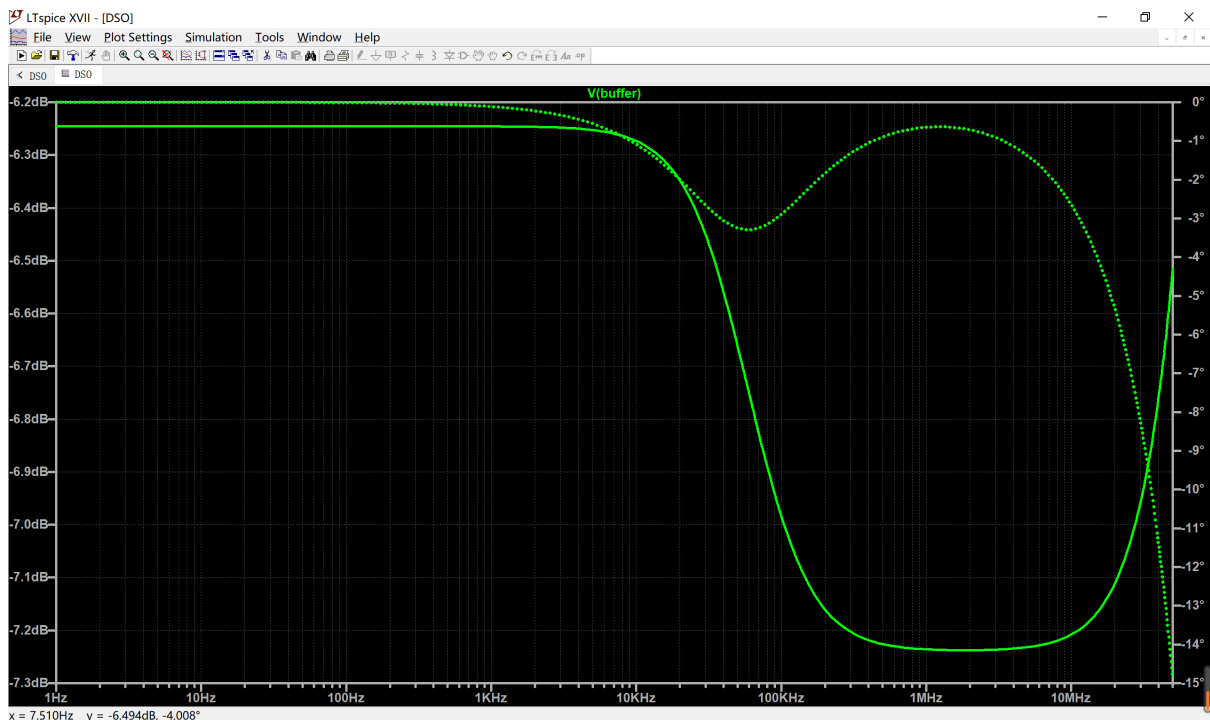


Figure 2.9: Frequency response at the input to the anti-aliasing filter.

2.5 Anti-aliasing Filter

AA Filter

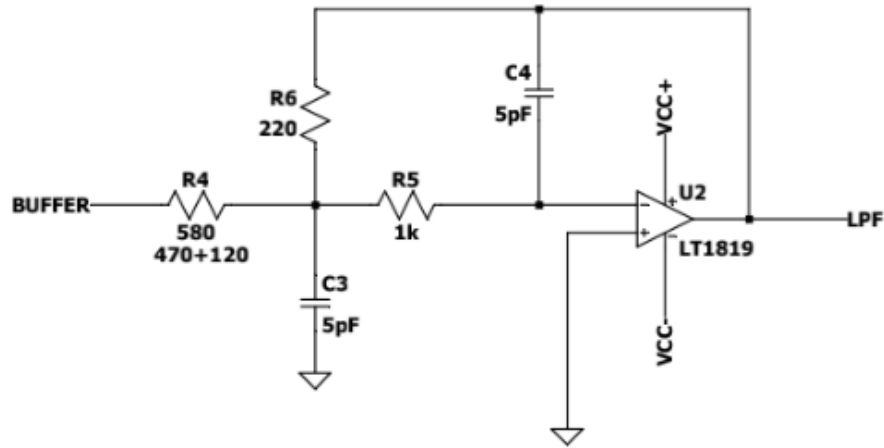


Figure 2.10: AA Filter.

The anti-aliasing filter is designed as a multiple feedback low-pass filter (2nd order Butterworth). The cut off frequency is designed as 20MHz to prevent aliasing of the input signal. The DC Amplitude of the circuit is designed to satisfy the requirement of ADC input $V_{pp} = 2\text{V}$ with $\pm 2\text{dB}$ maximum ripple.

We use online low-pass filter design tool with requirements to get initial values for components, then continue to tune these values to meet all requirements: 1) $f_o = 20\text{MHz}$, 2) $H = \frac{2}{5.6} = 0.3571$, 3) $\pm 2\text{dB}$ maximum ripple in passband and 4) values from BOM list.

Finally, $R_4 = 580\Omega$, $R_5 = 1\text{k}\Omega$, $R_6 = 220\Omega$ and $C_3 = C_4 = 5\text{pF}$. The magnitude and phase response at the ADC input are shown in figure 2.11 and figure 2.12. The magnitude at 1Hz and 18.72MHz are about -14.68dB and -17.67dB . Thus, the cut off frequency is about 18.72MHz . The phase at 18.72MHz is about -73.755° which is larger than -180° . The response is of more than 20dB per decade and less than 2dB ripple.

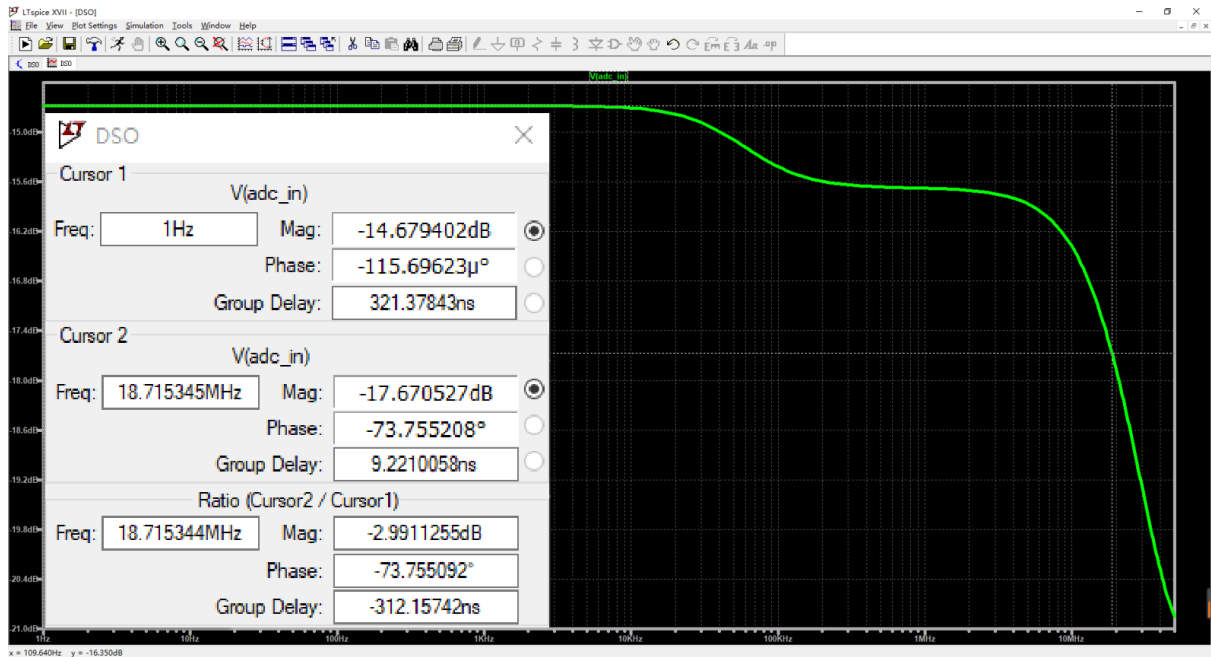


Figure 2.11: Magnitude response at the ADC input.

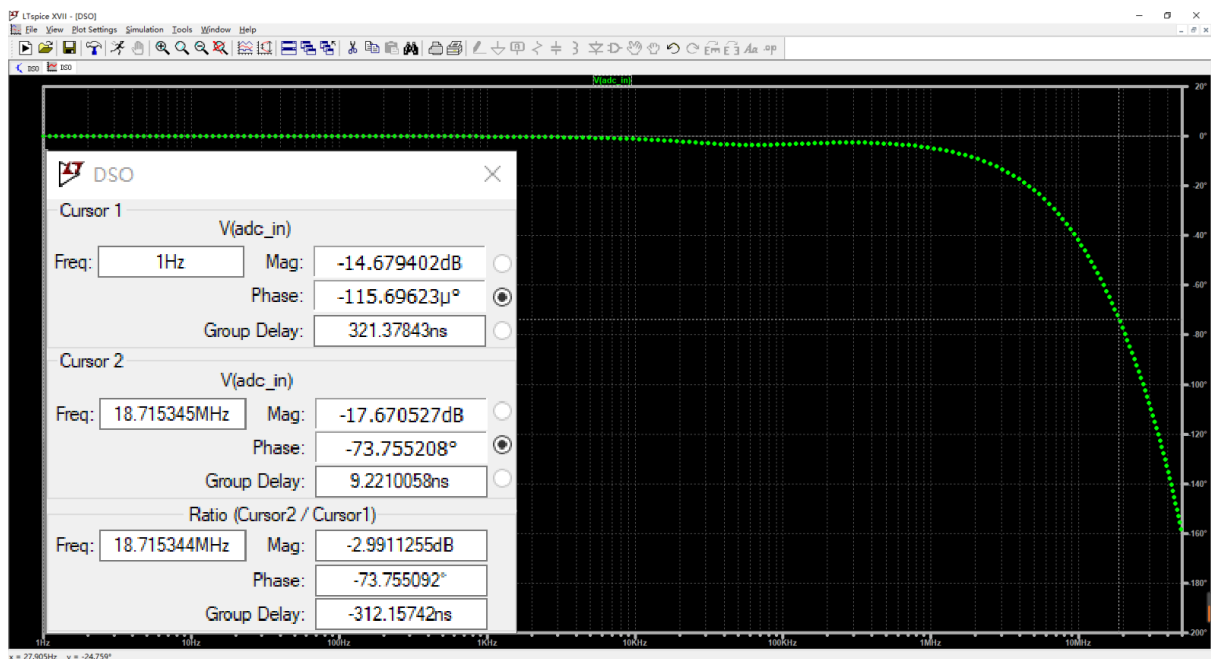


Figure 2.12: Phase response at the ADC input.

The output with 10MHz and 5.6V input signal before and after the anti-aliasing filter is shown in figure 2.13.

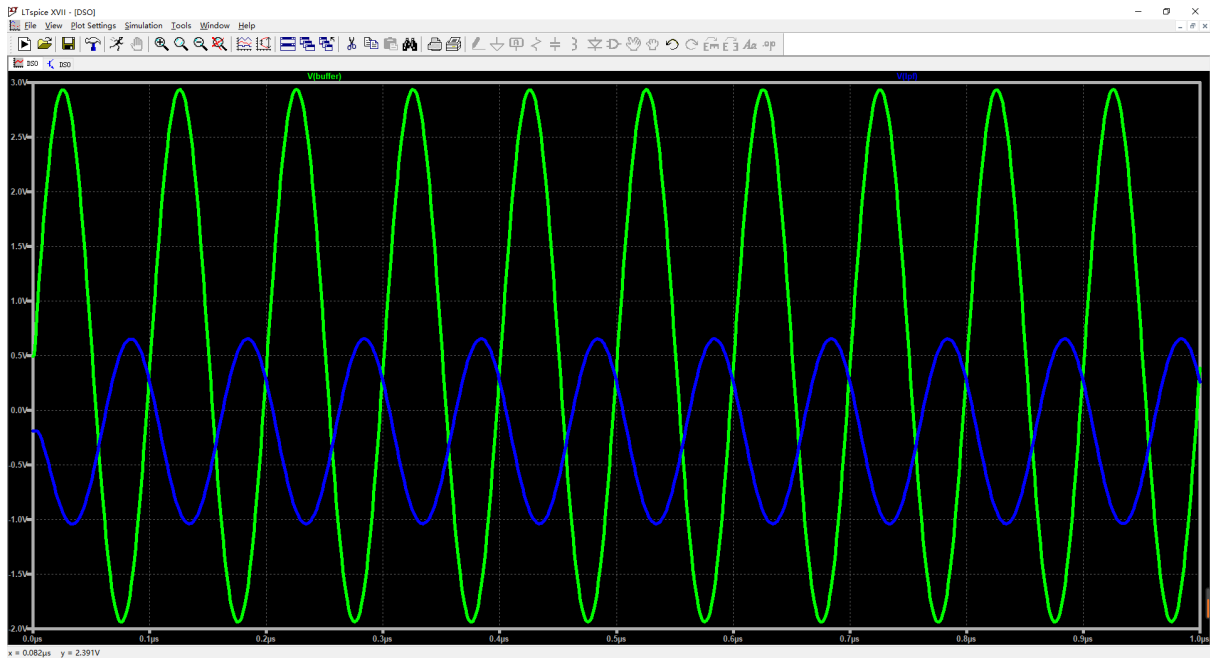


Figure 2.13: LPF v.s. Buffer.

2.6 Inverting Level Shifter Block

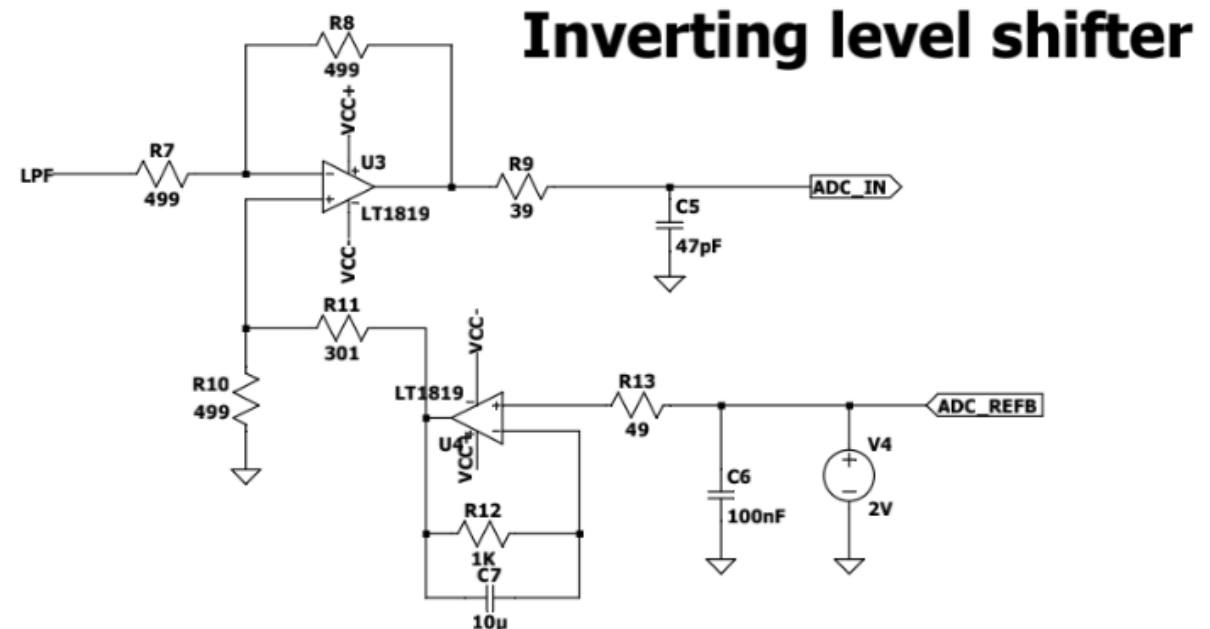
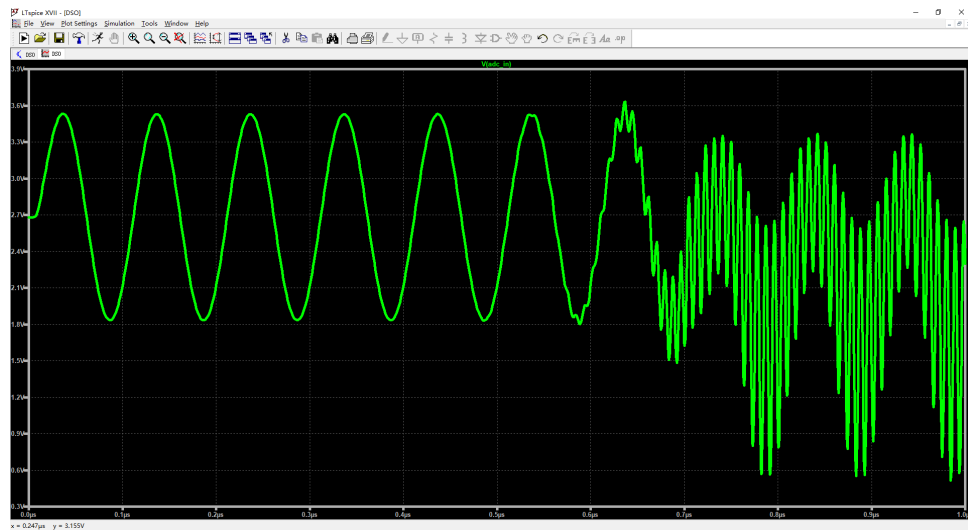
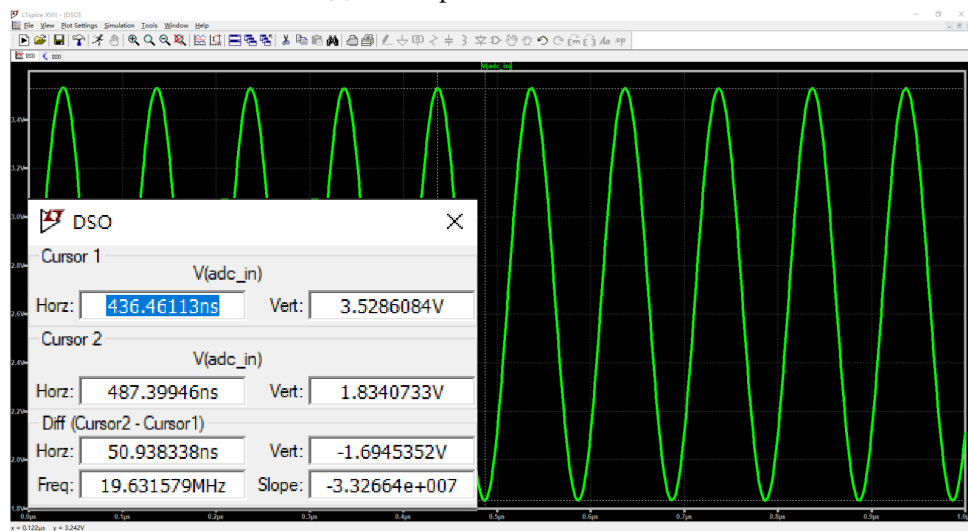


Figure 2.14: Inverting Level Shifter.

The inverting Level Shifter is designed from ADS830E data sheet with C_7 to prevent the high frequency oscillation, the output signal comparison is shown in 2.15.



(a) ADC input with oscillation.



(b) ADC input without oscillation.

Figure 2.15: Comparison of circuits with or without C_7

3 Observation

All core requirements are satisfied and discussed in last section. Since there might be a DC offset due to OpAmps in the final design, we can add trim pots to adjust that.

4 Summary

The performance can be expected that: 1) Signal from DC to 1MHz would be presented well; 2) Signal from 1MHz to 20MHz would be shifted in phase; 3) Signal larger than 20MHz could not be presented.

Appendix

Operating point

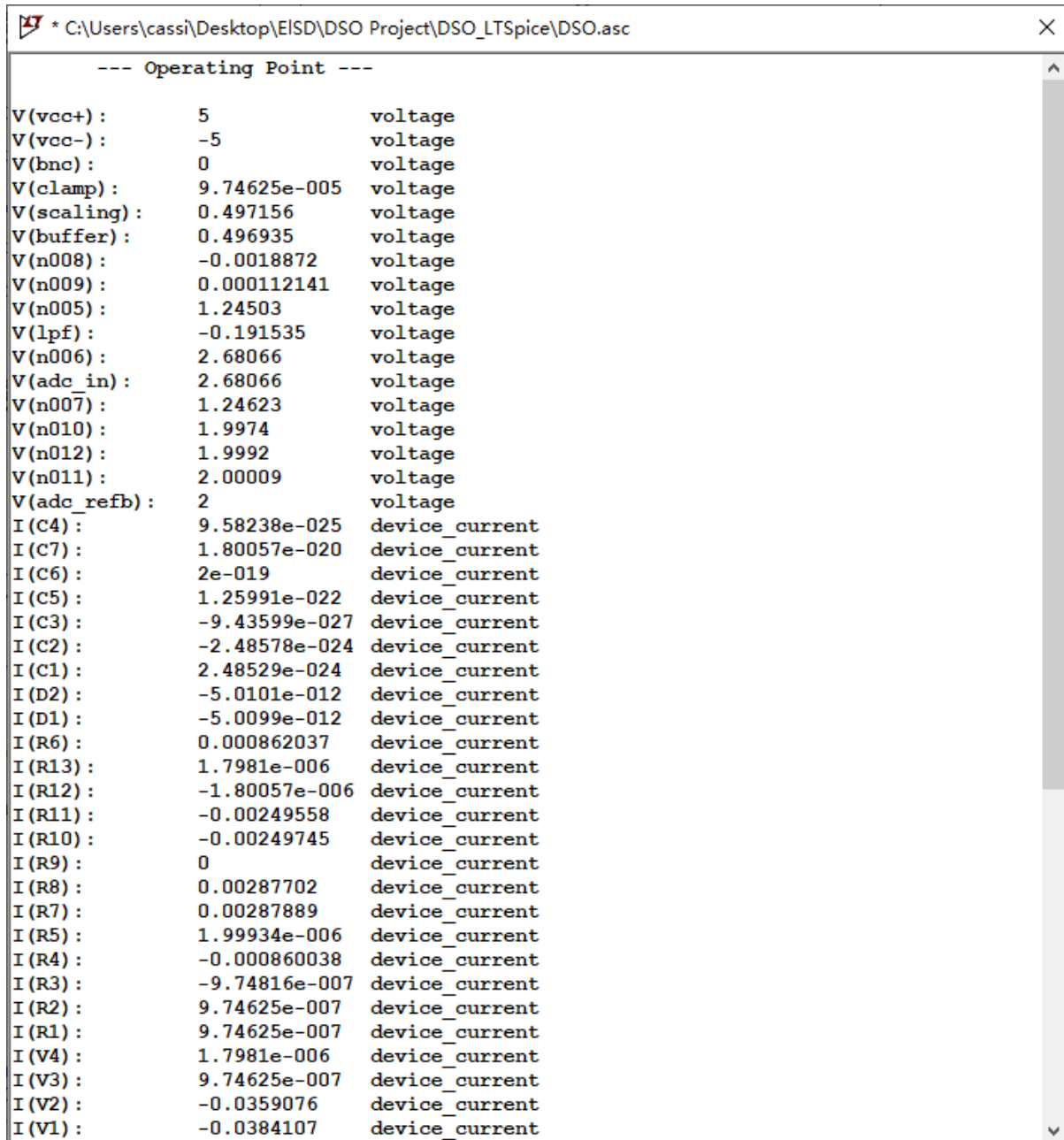
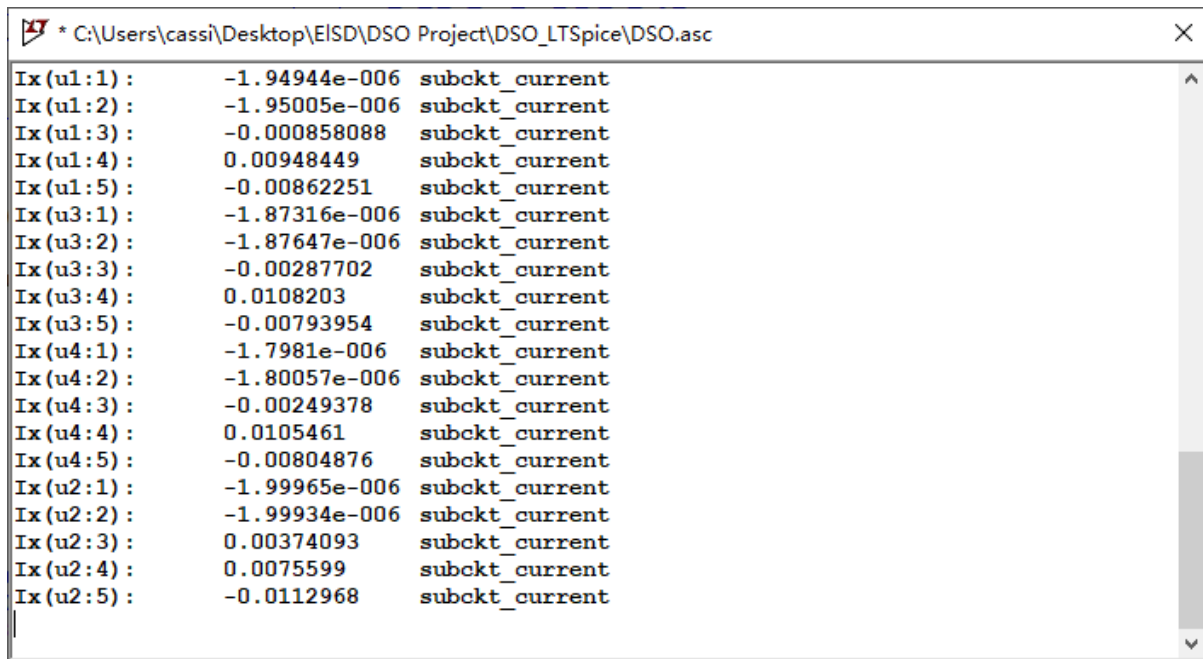


Figure 1: Operating point 1.



The image shows a screenshot of a text editor window with the title bar: * C:\Users\cassi\Desktop\EISD\DSO Project\DSO_LTSpice\DSO.asc. The window contains a list of simulation results for 'Operating point 2'. Each line consists of a node identifier, a numerical value, and the variable name 'subckt_current'. The results are organized by node groups: u1, u3, u4, and u2, each with five sub-entries. The values are in scientific notation, mostly negative, with some positive values for u1:4, u3:4, u4:4, and u2:3.

Node	Value	Variable
u1:1	-1.94944e-006	subckt_current
u1:2	-1.95005e-006	subckt_current
u1:3	-0.000858088	subckt_current
u1:4	0.00948449	subckt_current
u1:5	-0.00862251	subckt_current
u3:1	-1.87316e-006	subckt_current
u3:2	-1.87647e-006	subckt_current
u3:3	-0.00287702	subckt_current
u3:4	0.0108203	subckt_current
u3:5	-0.00793954	subckt_current
u4:1	-1.7981e-006	subckt_current
u4:2	-1.80057e-006	subckt_current
u4:3	-0.00249378	subckt_current
u4:4	0.0105461	subckt_current
u4:5	-0.00804876	subckt_current
u2:1	-1.99965e-006	subckt_current
u2:2	-1.99934e-006	subckt_current
u2:3	0.00374093	subckt_current
u2:4	0.0075599	subckt_current
u2:5	-0.0112968	subckt_current

Figure 2: Operating point 2.