Dynamics and Control presentation

Group 27 January 2019

1 Maths for 1D Motion

PID Controller

$$k_c = m_{eq}\omega_c^2 \sqrt{\alpha}, \qquad \tau_z = \frac{\sqrt{\alpha}}{\omega_c}$$

$$\tau_i = \beta \tau_z, \qquad \tau_p = \alpha \tau_z$$
(1)

A skew-sine reference profile has a maximum jerk at:

$$\ddot{r}_{max} = \frac{4\pi^2 h_m}{t_m^3} \tag{2}$$

$$\omega_c = \left(\frac{\ddot{r}_{max}\beta}{\alpha e_{LF}}\right)^{\frac{1}{3}} \tag{3}$$

$$= \left(\frac{4\pi^2 h_m \beta}{\alpha e_{LF}}\right)^{\frac{1}{3}} \frac{1}{t_m} \tag{4}$$

Our values.

Based off: https://new.abb.com/products/robotics/industrial-robots/irb-360. See IRB 360-1/1600 model.

Cycle from 0 mm $\rightarrow d_m \rightarrow 0$ mm

$$m_{eq} = 1 kg$$

$$e_{max} = 0.1 mm$$

$$d_m = 280 mm$$

$$h_m = \arctan\left(\frac{d_m}{L_u + L_l}\right)$$

$$= 0.1391 rad = 8^{\circ}$$

$$t_m = 0.35 s$$

2 Maths for 2D motion

Position

$$\Phi = \begin{bmatrix}
M_x \mp \frac{D}{2} - U_{j,x} - \frac{L_u}{2} cos(\theta_{U,j}) \\
M_y - U_{j,y} - \frac{L_u}{2} sin(\theta_{U,j}) \\
U_{j,x} - \frac{L_u}{2} cos(\theta_{U,j}) - L_{j,x} - \frac{L_l}{2} cos(\theta_{L,j}) \\
U_{j,y} - \frac{L_u}{2} sin(\theta_{U,j}) - L_{j,x} - \frac{L_l}{2} sin(\theta_{L,j}) \\
L_{j,x} - \frac{L_l}{2} cos(\theta_{L,j}) - P_x \pm \frac{L_e}{2} \\
L_{j,y} - \frac{L_l}{2} sin(\theta_{L,j}) - P_y \\
\vdots \\
\vdots
\end{cases}$$
(5)

$$\Phi^{driving} = \begin{bmatrix} \theta_{U,1} - \omega_1 t - (\theta_{U,1})_0 \\ \theta_{U,2} - \omega_2 t - (\theta_{U,2})_0 \end{bmatrix}$$

$$\tag{6}$$

Independent and Dependent Co-ordinates

$$q_i = \begin{bmatrix} \theta_{U,1} \\ \theta_{U,2} \end{bmatrix} \tag{7}$$

$$q_d = \left[\begin{array}{c} \vdots \end{array} \right] \tag{8}$$

$$J = \Phi_{q_d}^{-1} \Phi_{q_i} \tag{9}$$

$$\dot{q}_d = -J\dot{q}_i \tag{10}$$

$$\hat{M} = M_{ii} + J^T M_{dd} J \tag{11}$$

$$\hat{Q} = -J^T Q_{A,d} + J^T M_{dd} \Phi_{q_d}^{-1} \gamma \tag{12}$$

Inverse Kinematics

$$\Phi^{IK} = \begin{bmatrix} (\mp \frac{D}{2} - L_u cos(\theta_{U,j}) \pm \frac{L_e}{2} - P_x)^2 + (P_y + L_u sin(\theta_{U,j}))^2 - L_l^2 \\ \vdots \end{bmatrix}$$
(13)

$$\ddot{q}_i = -(\Phi_{q_i}^{IK})^{-1} (\Phi_{PP}^{IK} \dot{P} + 2\Phi_{q_iP}^{IK} \dot{q}_i \dot{P} + \Phi_{q_iq_i}^{IK} \dot{q}_i + \Phi_{P}^{IK} \ddot{P})$$
(14)

3 Maths for 3D motion

Position

$$\Phi = \begin{bmatrix}
M + R_{A,j} \begin{bmatrix} \frac{D}{2} \\ 0 \\ 0 \end{bmatrix} - U_j - R_{U,j} \begin{bmatrix} 0 \\ 0 \\ \frac{L_u}{2} \end{bmatrix} \\
U_j + R_{U,j} \begin{bmatrix} 0 \\ 0 \\ -\frac{L_u}{2} \end{bmatrix} - L_j - R_{L,j} \begin{bmatrix} 0 \\ 0 \\ \frac{L_l}{2} \end{bmatrix} \\
L_j + R_{L,j} \begin{bmatrix} 0 \\ 0 \\ -\frac{L_l}{2} \end{bmatrix} - P - R_{A,j} \begin{bmatrix} \frac{L_e}{2} \\ 0 \\ 0 \end{bmatrix} \\
\begin{bmatrix} 0 & 1 & 0 \end{bmatrix} R_{L,j}^T (R_{L,j})_0 \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix} \\
\vdots$$
(15)

$$\Phi^{driving} = \begin{bmatrix} (\theta_{U,j})_x + \sin((\theta_{a,j})_0)\omega_j t - 0\\ (\theta_{U,j})_y - \cos((\theta_{a,j})_0)\omega_j t - (\theta_{a,j})_0\\ (\theta_{U,j})_z - (\theta_{U,j})_{z,0} \\ \vdots \end{bmatrix}$$
(16)

$$\Phi_{q}\dot{q} = \begin{bmatrix}
I & -I & -R_{U,j}\tilde{r}_{U}^{U,A}R_{U,j}^{T} & 0 & 0 & \dots \\
0 & I & +R_{U,j}\tilde{r}_{U}^{U,B}R_{U,j}^{T} & -I & -R_{L,j}\tilde{r}_{L}^{L,B}R_{L,j}^{T} & \dots \\
0 & 0 & 0 & I & +R_{L,j}\tilde{r}_{L}^{L,C}R_{L,j}^{T} & \dots \\
0 & 0 & 0 & 0 & e_{y}^{0}R_{L,j}^{T}\tilde{e}_{x}^{U} & \dots \\
\vdots & \vdots & & & \end{bmatrix} \begin{bmatrix} \dot{M} \\ \dot{U}_{j} \\ \dot{\omega}_{U,j} \\ \dot{L}_{J} \\ \omega_{L,j} \\ \vdots \end{bmatrix}$$
(17)

Independent and Dependent Co-ordinates

$$q_{i} = \begin{bmatrix} (\theta_{U,1})_{x} \\ (\theta_{U,1})_{y} \\ (\theta_{U,1})_{z} \\ \vdots \end{bmatrix}$$

$$(18)$$

$$q_a = \begin{bmatrix} \theta_{a,1} \\ \theta_{a,2} \\ \theta_{a,3} \end{bmatrix} \tag{19}$$

$$\omega_{a}^{0,U} = R_{U}^{0} \omega_{a}^{U,U}$$

$$= \begin{bmatrix} \cos(\theta_{a})\cos(\psi_{0}) & -\sin(\psi_{0}) & \cos(\psi_{0})\sin(\theta_{a}) \\ \cos(\theta_{a})\sin(\psi_{0}) & \cos(\psi_{0}) & \sin(\psi_{0})\sin(\theta_{a}) \\ -\sin(\theta_{a}) & 0 & \cos(\theta_{a}) \end{bmatrix} \begin{bmatrix} 0 \\ \omega_{a} \\ 0 \end{bmatrix}$$

$$= \begin{bmatrix} -\sin(\psi_{0})\omega_{a} \\ \cos(\psi_{0})\omega_{a} \\ 0 \end{bmatrix}$$
(20)

$$\int \omega_a^{0,U} = \int R_U^0 \omega_a^{U,U}$$

$$\theta_U = \begin{bmatrix} -\sin(\psi_0)\theta_a - \theta_{a,0} \\ \cos(\psi_0)\theta_a \\ \psi_0 \end{bmatrix}$$
(21)

Inverse kinematics

$$r = R_{A,j} \begin{bmatrix} \frac{D-L_e}{2} \\ 0 \\ 0 \end{bmatrix} - R_{U,j} \begin{bmatrix} 0 \\ 0 \\ L_u \end{bmatrix} - P = R_{L,j} \begin{bmatrix} 0 \\ 0 \\ L_l \end{bmatrix}$$

$$(22)$$

$$r^T r = r^T R^T R r$$

$$\left(\left(\frac{D - L_e}{2} - L_u sin(\theta_{a,j}) \right) cos(\psi_0) - P_x \right)^2 + \left(\left(\frac{D - L_e}{2} - L_u sin(\theta_{a,j}) \right) sin(\psi_0) - P_y \right)^2 + \left(-L_u cos(\theta_{a,j}) - P_z \right)^2 = L_l^2$$
(23)

$$\ddot{q}_{a} = -(\Phi_{q_{a}}^{IK})^{-1}(\Phi_{PP}^{IK}\dot{P} + 2\Phi_{q_{a}P}^{IK}\dot{q}_{a}\dot{P} + \Phi_{q_{a}q_{a}}^{IK}\dot{q}_{a} + \Phi_{P}^{IK}\ddot{P})$$
 (24)