

# Optika vaje

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Kot v opombo, jaz ne verjamem v imaginarni lomni kolicnik. Je tocka, kjer mi domisljija ne omogoca, da bi dvomila v svoj dobro preizkusen vid.

## 1 Uvod in ponovitev geometrijske optike

### 1.1 Opticno vlakno z parabolicnim refrakcijskim koeficientom $n(x, y) = n_0\sqrt{1 - \alpha^2(x^2 - y^2)}$ , $\alpha x \ll 1$ .

$$\nabla n = \frac{d}{ds}(n \frac{d\vec{r}}{ds}) \quad (1)$$

$$ds = \sqrt{dx^2 + dz^2} = dz\sqrt{1 + (\frac{dx}{dz})^2} \approx dz \quad (2)$$

$$\frac{dn}{dx} = \frac{d}{dz}(n \frac{dx}{dz}) = n \frac{d^2x}{dz^2} \quad (3)$$

$$\frac{d^2x}{dz^2} = \frac{1}{n} \frac{dn}{dx} = \frac{1}{n_0\sqrt{1 - \alpha^2(x^2 - y^2)}} n_0 \frac{1}{\sqrt{1 - \alpha^2(x^2 - y^2)}} (-2\alpha^2 x) = \frac{-2\alpha^2 x}{(1 - \alpha^2(x^2 - y^2))} = \frac{-2\alpha^2 x n_0^2}{n^2} \quad (4)$$

$$\frac{d^2x}{dz^2} = -\alpha^2 \gamma \Rightarrow x = x_0 \sin(\alpha z) \quad (5)$$

### 1.2 Curek svetlobe okrog Zemlje s polemerom $R = 6400\text{km}$

$$\vec{r} = (R + h)\sin\theta\hat{e}_x + (R + h)\cos\theta\hat{e}_y \quad (6)$$

$$ds = \sqrt{d\vec{r}d\vec{r}} = \sqrt{(R + h)^2(\sin^2\theta + \cos^2\theta)d\phi^2} = (R + h)d\theta \quad (7)$$

$$\nabla n = \frac{d}{ds}(n \frac{d\vec{r}}{ds}) = n \frac{d^2\vec{r}}{ds^2} = \frac{n}{(R + h)^2} \frac{d^2\vec{r}}{d\theta^2} = -\frac{n}{R + h}(\sin\theta\hat{e}_x + \cos\theta\hat{e}_y) \Rightarrow \frac{dn}{dy} = -\frac{n}{R + h} \quad (8)$$

$$4 \cdot \Delta n = \frac{dn}{dy} \Delta y = -\frac{n}{R + h} \Delta y \approx 1,56 \cdot 10^{-6}; h \ll R \quad (9)$$

### 1.3 Izracunaj ABCD matriko za prehod zarka iz ene snovi v drugo $[y_2, \theta_2]^T = M[y_1, \theta_1]^T$ , $M = \begin{pmatrix} A & B \\ C & D \end{pmatrix}$

$$y_2 = 1 \cdot y_1 + 0 \cdot \theta_1 \quad (10)$$

Snellov zakon:

$$n_1 \sin \theta_1 = n_2 \sin \theta_2 \Rightarrow n_1 \theta_1 = n_2 \theta_2 \quad (11)$$

$$\Phi_1 = \theta_1 + \frac{y_1}{R}, \Phi_2 = \theta_2 + \frac{y_1}{R} \quad (12)$$

$$\Phi_1 = \Phi_2 \Rightarrow n_1(\theta_1 + \frac{y_1}{R}) = n_2(\theta_2 + \frac{y_1}{R}) \quad (13)$$

$$\theta_2 = (\frac{n_1 - n_2}{n_2 R}) y_1 + \frac{n_1}{n_2} \theta_1; y_2 = 1 y_1 + 0 \theta_1 \quad (14)$$

$$n = \begin{pmatrix} A & B \\ C & D \end{pmatrix} = \begin{pmatrix} 1 & 0 \\ \frac{n_1 - n_2}{n_2 R} & \frac{n_1}{n_2} \end{pmatrix} \quad (15)$$

### 1.4 Matrika za debelo leco (prehod med sredstvi).

$$\begin{pmatrix} y_2 \\ \theta_2 \end{pmatrix} = M_3 M_2 M_1 \begin{pmatrix} y_1 \\ \theta_1 \end{pmatrix} \quad (16)$$

$$M_1 = \begin{pmatrix} 1 & 0 \\ \frac{n_1 - n_2}{n_2 R_1} & \frac{n_1}{n_2} \end{pmatrix} \quad (17)$$

$$M_2 = \begin{pmatrix} 1 & d \\ 0 & 1 \end{pmatrix} \quad (18)$$

$$M_3 = \begin{pmatrix} 1 & 0 \\ \frac{n_3 - n_2}{n_2 R_2} & \frac{n_3}{n_2} \end{pmatrix} \quad (19)$$

$$M = M_3 M_2 M_1 = \begin{pmatrix} A & B \\ C & D \end{pmatrix} \quad (20)$$

### 1.5 Matrika za tanko leco (prek fokusa leca)

Fokus (tanke) lece:  $\frac{1}{f_1} = \frac{n-1}{R_1}$  in  $\frac{1}{f_2} = \frac{n-1}{R_2}$ . Velja, da je f gorisce ali skupna locljivost dveh leca:

$$\frac{1}{f} = \frac{1}{f_1} + \frac{1}{f_2} = \frac{n-1}{R_1} + \frac{n-1}{R_2} = \frac{(n-1)R_2 + (n-1)R_1}{R_1 R_2} \quad (21)$$

Za elemente ABCD matrike za leco velja, da jih lahko prepisemo upostevajoc enacbi za fokus:

$$A = 1 + d \frac{n-1}{R_1} = 1 - \frac{n-1}{n R_1} = 1 - \frac{d}{n f_1} \quad (22)$$

$$B = \frac{d}{n} \quad (23)$$

$$C = \frac{2-n}{R_2} \left(1 + d \frac{1-n}{nR_1}\right) + n \frac{1-n}{nR_1} = -\frac{1}{f_1} \left(1 - \frac{d}{nf_1}\right) - \frac{1}{f_1} \quad (24)$$

$$D = d \frac{1}{n_2} \frac{1-n}{R_2} + 1 = 1 - \frac{d}{nf_2} \quad (25)$$

$$M_{\text{tankal-eca}} = \begin{pmatrix} 1, 0 \\ -\frac{2(n-1)}{R}, 1 \end{pmatrix} \quad (26)$$

**1.6 Obravnavamo mikroskop iz dveh lec z fokusoma  $f_1, f_2$  na razdalji  $d$ . Oddaljenost vzorca od 1. oznacuje  $f_1$ , oddaljenost detektorja od druge  $f_2$ .**

$$\text{povecava} = \frac{y_2}{y_1} \quad (27)$$

$$M = M_5 M_4 M_3 M_2 M_1 = \begin{pmatrix} 1, f_2 \\ 0, 1 \end{pmatrix} \begin{pmatrix} 1, 0 \\ -\frac{1}{f_2}, 1 \end{pmatrix} \begin{pmatrix} 1, d \\ 0, 1 \end{pmatrix} \begin{pmatrix} 1, 0 \\ -\frac{1}{f_1}, 1 \end{pmatrix} \begin{pmatrix} 1, f_1 \\ 0, 1 \end{pmatrix} \quad (28)$$

V razmislek, ce bi dogajanje na lecah opisali kot kaj se zgodi pred in po prehodu bi veljalo:  $Ay_1 + B\theta_1 = y_2$  in  $Cy_1 + D\theta_1 = \theta_2 \Rightarrow \frac{y_2}{y_1} = A$ , to se izkaze, da je res, ko 1. enacbo delimo z  $y_1$  in je  $\theta_1 = 0$  oz. ko je opticna os neodvisna od zacetnega kota.

$$M_{\text{tot}} = \begin{pmatrix} -\frac{f_2}{f_1}, 0 \\ -\frac{1}{f_2} \left(1 - \frac{d}{f_1}\right) - \frac{1}{f_3}, \frac{-f_1}{f_2} \end{pmatrix} \quad (29)$$

**1.7 Jonesove matrike za optice elemente a) linearen polarizator vzporeden x in y osi, b) rotiran za  $45^\circ$  glede na x, c) cetrtinska retardacijska ploscica vzporedna x in y osi, kjer je y hitra os, d) dve identicni retardacijski ploscici, obe zarotirani za  $\pm 45^\circ$  glede na x in y os.**

Linearni polarizator vzporeden z x osjo  $M_{\text{lin}}^{(x)} = \begin{pmatrix} 1, 0 \\ 0, 0 \end{pmatrix} \rightarrow \begin{pmatrix} 1, 0 \\ 0, 0 \end{pmatrix} \begin{pmatrix} J_x \\ J_y \end{pmatrix} = \begin{pmatrix} J_x \\ 0 \end{pmatrix}$ , kjer vidimo, da prepusca svetlobo le v smeri x (enak postopek z y osjo). Primer, ko je rotiran linearni polarizator  $M_{\text{lin}}^{45} = \frac{1}{2} \begin{pmatrix} 1, \pm 1 \\ \pm 1, 1 \end{pmatrix} \rightarrow \frac{1}{2} \begin{pmatrix} 1, \pm 1 \\ \pm 1, 1 \end{pmatrix} \begin{pmatrix} J_x \\ J_y \end{pmatrix} = \frac{1}{2} \begin{pmatrix} J_x \pm J_y \\ \pm J_x + J_y \end{pmatrix}$ . Retardacijske ploscice: velja, da bo y komponenta deformirana zaradi lomnega kolicnika  $n_y$  in x zaradi  $n_x$ . Faktor  $\frac{\lambda}{4}$  oznacuje razliko v fazi med  $\phi_y - \phi_x = \frac{\pi}{2} = \frac{2\pi}{\lambda_0} z \Delta n$ , in izluscimo  $z = \frac{1}{\Delta n} \frac{\lambda_0}{4}$ .

$$M_{\lambda/4} = \begin{pmatrix} e^{2\pi i \frac{z}{\lambda_0} n_x}, 0 \\ 0, e^{2\pi i \frac{z}{\lambda_0} n_y} \end{pmatrix} = \begin{pmatrix} e^{i\phi_x}, 0 \\ 0, e^{i\phi_y} \end{pmatrix} \quad (30)$$

- Hitra os x:  $n_y < n_x, c_y > c_x$  in  $\phi_y < \phi_x \Rightarrow M_{\text{qw}}^{(y)} = e^{i\phi_x} \begin{pmatrix} 1, 0 \\ 0, e^{i(\phi_y - \phi_x)} \end{pmatrix} = e^{i\phi_x} \begin{pmatrix} 1, 0 \\ 0, +i \end{pmatrix}$

- Hitra os y:  $M_{qw}^{(y)} = \begin{pmatrix} 1, 0 \\ 0, -i \end{pmatrix}$

Retardacijske plosčice so lahko tudi zarotirane za poljuben kot  $\alpha$  :  $R(\alpha) = \begin{pmatrix} \cos(\alpha), \sin(\alpha) \\ -\sin(\alpha), \cos(\alpha) \end{pmatrix}$ ,  $R^T = R(-\alpha) = R^{-1}$ .

$$M_{qw'} = R^T M_{qw} R \Rightarrow M_{qw} R \begin{pmatrix} x_1 \\ y_1 \end{pmatrix} = R \begin{pmatrix} x_2 \\ y_2 \end{pmatrix} \Rightarrow R^T M_{qw} R \begin{pmatrix} x_1 \\ y_1 \end{pmatrix} = \begin{pmatrix} x_2 \\ y_2 \end{pmatrix} \quad (31)$$

$$\alpha = \frac{\pi}{4} \Rightarrow \begin{pmatrix} \cos^2(\alpha) + \sin^2(\alpha), \cos(\alpha)\sin(\alpha) - i\sin(\alpha)\cos(\alpha) \\ \cos(\alpha)\sin(\alpha) - i\sin(\alpha)\cos(\alpha), \sin^2(\alpha) + i\cos^2(\alpha) \end{pmatrix} = \frac{1}{2} \begin{pmatrix} 1+i, 1-i \\ 1-i, 1+i \end{pmatrix} = M_{qr'} \quad (32)$$

$$M_{qw'} = \frac{\sqrt{2}}{2} \begin{pmatrix} e^{i\pi/4}, e^{-i\pi/4} \\ e^{-i\pi/4}, e^{i\pi/4} \end{pmatrix} = \frac{\sqrt{2}}{2} e^{i\pi/4} \begin{pmatrix} 1, -i \\ -i, 1 \end{pmatrix} \quad (33)$$

Delovanje te plosčice na vpadni snop je torej  $M_{qw'} \begin{pmatrix} 0 \\ 1 \end{pmatrix} = \frac{\sqrt{2}}{2} \begin{pmatrix} 1, -1 \\ -i, 1 \end{pmatrix} \begin{pmatrix} 0 \\ 1 \end{pmatrix} = \frac{1}{\sqrt{2}} \begin{pmatrix} -i \\ 1 \end{pmatrix} = -\frac{i}{\sqrt{2}} \begin{pmatrix} 1 \\ i \end{pmatrix}$ .

Dve četrtinski retardacijski plosčici skupaj data polovicno:  $M_{hw'} = M_{qw'} \cdot M_{qw'} = \frac{1}{2} \begin{pmatrix} 1, -i \\ -i, 1 \end{pmatrix} \begin{pmatrix} 1, -i \\ -i, 1 \end{pmatrix} \xrightarrow{\text{ideja: poenostavimo}} \begin{pmatrix} 0, 1 \\ 1, 0 \end{pmatrix}$ .

$$M_{hw'} \begin{pmatrix} 0 \\ 1 \end{pmatrix} = \begin{pmatrix} 0, 1 \\ 1, 0 \end{pmatrix} \begin{pmatrix} 0 \\ 1 \end{pmatrix} = \begin{pmatrix} 1 \\ 0 \end{pmatrix} \quad (34)$$

**1.8 Podan je optični filter za določitev polarizacije prepuscene svetlobe in je zarotiran za  $\beta$ , interpretiraj rezultat.  $\beta$  vpliva le na amplitudo prepuscene svetlobe.**

$$T = \begin{pmatrix} \cos^2(\theta), \cos(\theta)\sin(\theta) \\ \cos(\theta)\sin(\theta), \sin^2(\theta) \end{pmatrix} \quad (35)$$

$$J_{in} = \cos(\beta)\hat{e}_x + \sin(\beta)\hat{e}_y = \begin{pmatrix} \cos(\beta) \\ \sin(\beta) \end{pmatrix} \quad (36)$$

$$J_{out} = T J_{in} = \begin{pmatrix} \cos^2(\theta), \cos(\theta)\sin(\theta) \\ \cos(\theta)\sin(\theta), \sin^2(\theta) \end{pmatrix} \begin{pmatrix} \cos(\beta) \\ \sin(\beta) \end{pmatrix} = \begin{pmatrix} \cos^2(\theta)\cos(\beta) + \cos(\theta)\sin(\theta)\sin(\beta) \\ \cos(\theta)\sin(\theta)\cos(\beta) + \sin^2(\theta)\sin(\beta) \end{pmatrix} \quad (37)$$

$$= \begin{pmatrix} \cos(\theta)\cos(\theta - \beta) \\ \sin(\theta)\cos(\theta - \beta) \end{pmatrix} = \cos(\theta - \beta) \begin{pmatrix} \cos(\theta) \\ \sin(\theta) \end{pmatrix} \quad (38)$$

Demonstracija rotacije optičnega elementa:

$$R^T M_{lin}^{(x)} R = \begin{pmatrix} c, -s \\ s, c \end{pmatrix} \begin{pmatrix} 1, 0 \\ 0, 0 \end{pmatrix} \begin{pmatrix} c, s \\ -s, c \end{pmatrix} = \begin{pmatrix} \cos^2(\theta), \cos(\theta)\sin(\theta) \\ \sin(\theta)\cos(\theta), \sin^2(\theta) \end{pmatrix} \quad (39)$$

- 1.9 Opticni izolator iz vec zaporednih elementov a) linearnega polarizatorja z osjo polarizacije v smeri y, b)  $\lambda/4$  retardacijska ploscica z glavno osjo rotirano  $\frac{\pi}{4}$  relativno na (x,y) in c) ogledalo

$$M_{lin}^{(y)} = \begin{pmatrix} 0, 0 \\ 0, 1 \end{pmatrix} \quad (40)$$

$$M_{qw}^+ = \frac{1}{\sqrt{2}} \begin{pmatrix} 1, -i \\ -i, 1 \end{pmatrix} \quad (41)$$

$$M_{qw}^- = \frac{1}{\sqrt{2}} \begin{pmatrix} 1, i \\ i, 1 \end{pmatrix} \quad (42)$$

Ogledalo obrne optico os  $M_{mirror} = \begin{pmatrix} -1, 0 \\ 0, 1 \end{pmatrix}$  (torej iz  $M_{qw}^+ \rightarrow M_{qw}^-$ ). Opticni izolator je taka kombinacija opticnih elementov, ki blokira svetlobo na poti nazaj:  $T_{tot} = \frac{1}{\sqrt{2}} M_{lin}^{(y)} M_{qw}^- M_{mirror} T_0 = \dots = \frac{1}{2} \begin{pmatrix} 0, 0 \\ 0, 0 \end{pmatrix}$

## 2 Jonesov kalkulus

- 2.1 Jonesovi vektorji elipticno polarizirane svetlobe, kjer je kot rotacije  $\pi/4$ .

Jonesov vektor v rotiranem sistemu S' prepisemo v sistem S, fazna razlika med sistemoma je kot rotacije.

$$J = R^T J' = \frac{1}{\sqrt{5}} \begin{pmatrix} \cos(\theta), -\sin(\theta) \\ \sin(\theta), \cos(\theta) \end{pmatrix} \begin{pmatrix} 2 \\ -i \end{pmatrix} = \frac{1}{\sqrt{5}} \begin{pmatrix} 2\cos(\theta) + i\sin(\theta) \\ 2\sin(\theta) - i\cos(\theta) \end{pmatrix} = \sqrt{\frac{2}{5}} \begin{pmatrix} 1 + \frac{i}{2} \\ 1 - \frac{i}{2} \end{pmatrix} \quad (43)$$

- 2.2 Elipticna polarizacija (desnosucna, kot  $\frac{\pi}{6}$  z dolzinami osi  $E_0, 2E_0$ ) Enkrat gre svetloba skozi vertikalno orientiran linearni polarizator in drugic skozi horizontalen. Posici razmerje intenzitet za prepusceno svetlobo, kjer je v prvem primeru rotacija polarizirane svetlobe Jonesovega vektorja taka, da je vzporeden ali x ali y osi in v drugem pa z rotacijo dveh linearnih polarizatorjev, da ta postaneta vzporedna elipticni polarizaciji sistema.

- 2.2.1 a)

$$J = R^T(\theta) J' = \frac{1}{\sqrt{5}} \begin{pmatrix} 2\cos(\theta) + i\sin(\theta) \\ 2\sin(\theta) - i\cos(\theta) \end{pmatrix} \xrightarrow{\frac{\pi}{6}} J = \frac{1}{\sqrt{5}} \begin{pmatrix} \sqrt{3} + \frac{i}{2} \\ 1 - \frac{i\sqrt{3}}{2} \end{pmatrix} \quad (44)$$

Rotacija skozi horizontalni linearni polarizator  $J_X = \frac{1}{\sqrt{5}} \begin{pmatrix} \sqrt{3} + \frac{i}{2} \\ 0 \end{pmatrix}$  (horizontalni lin. pol.) in  $J_Y = \frac{1}{\sqrt{5}} \begin{pmatrix} 0 \\ 1 - \frac{i\sqrt{3}}{2} \end{pmatrix}$  (vertikalno skozi lin. pol v y smeri).

$$I \propto |J_X|^2 = J_X J_X^* = \frac{13}{20}; I_y \propto \frac{7}{20} \Rightarrow \frac{I_X}{I_Y} = 13/7 \quad (45)$$

### 2.2.2 b)

Jonesova matrika za zarotiran linearni polarizator iz laboratorijskega sistema v elipticni sistem  $T' = \begin{pmatrix} \cos^2(\theta), \sin(\theta)\cos(\theta) \\ \sin(\theta)\cos(\theta), \sin^2(\theta) \end{pmatrix}$ . Ko rotiramo iz laboratorijskega sistema v elipticni sistem uporabimo pri kotu rotacije oznako -, torej v tem primeru bi rotacijo za  $\frac{\pi}{6}$  označili za  $\theta = -\frac{\pi}{6}$ .

$$T'_X = \begin{pmatrix} \frac{3}{4}, \frac{\sqrt{3}}{4} \\ \frac{\sqrt{3}}{4}, \frac{3}{4} \end{pmatrix} \quad (46)$$

Za zasuk optične osi pristajemo kotu rotacije četrtno celotnega kota, za primer y-osi  $\theta = \frac{\pi}{2} + (-\frac{\pi}{6})$ :

$$T'_y = \begin{pmatrix} \frac{1}{4}, \frac{\sqrt{3}}{4} \\ \frac{\sqrt{3}}{4}, \frac{3}{4} \end{pmatrix} \quad (47)$$

$J'$  v sistemu vzporednih osi ( $\theta = 0$ ) =  $J' = \frac{1}{\sqrt{5}} \begin{pmatrix} 2 \\ -i \end{pmatrix}$ . Končni rezultat je torej  $J'_X = T'_X J' = \frac{1}{4\sqrt{5}} \begin{pmatrix} 6+i\sqrt{3} \\ -2\sqrt{3}-i \end{pmatrix}$ ,  $T'_Y J' = \frac{1}{4\sqrt{5}} \begin{pmatrix} 2-i\sqrt{3} \\ 2\sqrt{3}-3i \end{pmatrix}$ .  $I_X = \frac{31}{90}$ ,  $I_Y = \frac{14}{91} \Rightarrow \frac{I_X}{I_Y} = \frac{13}{7}$

## 3 EM valovanje v homogenih in prevodnih snoveh + EM valovanje v prevodnih snoveh

### 3.1 Orientacija elipticnega polarizatorja z fazno razliko $\delta = \frac{\pi}{4}$ , $\frac{E_X}{E_Y} = 2$ , a) $\theta$ je kot, za katerega je elipsa zarotirana glede na (x,y) in b) razmerje med elipsami dolge in kratke osi $\frac{x}{y} = ?$

Elipsa zarotirana za kot  $\theta$  relativno na (x,y) prek  $\tan(2\theta) = \frac{2E_{0x}E_{0y}\cos(\delta)}{E_{0x}^2 - E_{0y}^2}$ , vs-tavimo podatek o razmerju osi in  $\tan(2\theta) = \frac{2\sqrt{2}}{3}$ ,  $\theta = \frac{1}{2}\arctan(\frac{2\sqrt{2}}{3}) \approx 21,7^\circ$ .

$$\frac{b}{a} = \frac{E_{0y}\sin(\delta)\cos(\theta)}{E_{0x}\cos(\theta) + E_{0y}\cos(\delta)\sin(\theta)} = \frac{\frac{\sqrt{2}}{2}\cos(\theta)}{2\cos(\theta) + \frac{\sqrt{2}}{2}\sin(\theta)} = \frac{1}{\frac{4}{\sqrt{2}} + \tan(\theta)} \quad (48)$$

### 3.2 Globina pri koznem pojavu za elektrodo (ITD) specifikacij: $\lambda = 500nm$ , $R = 0,02\Omega m$ , $d = 50nm$ .

Za prevodne materiale uporabimo enacbe:  $k_0 = \frac{\omega}{c_0}$ ,  $\sigma_E = \frac{1}{\xi}$ ,  $d = \frac{1}{n_{im}k_0}$ .

$$\mathcal{N}^2 = \epsilon_\mu + \frac{i\sigma_E^2}{\epsilon_0\omega} = n_{Re}^2 - n_{Im}^2 + 2in_{Re}n_{Im} \quad (49)$$

$$n_R^2 - n_{Im}^2 = \epsilon_\mu; \frac{\sigma_E}{\epsilon_0\omega} = 2n_Rn_I; n_I = \frac{\sigma_E}{2n_R\epsilon_0\omega} \quad (50)$$

$$n_R^2 - \frac{\sigma_E^2}{4\epsilon_0\omega n_R^2} = \epsilon_E / \cdot n_R^2 \quad (51)$$

$$n_R^4 - \frac{\sigma_E^2}{4\epsilon_0\omega} - \epsilon_E n_R^2 = 0; t = n_R^2 \quad (52)$$

$$t^2 - \epsilon_E t - \alpha = 0; t_{1,2} = \frac{\epsilon_E \pm \sqrt{-4\alpha - \epsilon_E^2}}{2} = \frac{\epsilon_E \pm i\sqrt{4\alpha + \epsilon_E^2}}{2} \quad (53)$$

$$n_{Re}^2 = -\frac{1}{2}\epsilon_E + \frac{1}{2}\sqrt{\epsilon^2 + \frac{\sigma_n^2}{\epsilon_0^2\omega_2}} \quad (54)$$

$$n_{Im} = -\frac{\epsilon}{2} + \frac{1}{2}\sqrt{\epsilon^2 + \frac{\sigma_E^2}{\epsilon_0^2\omega}} = \sqrt{\frac{\sigma_E}{2\epsilon_0\omega}} \quad (55)$$

$$d = \frac{c_0}{\omega} \sqrt{\frac{2\epsilon_0\omega}{\sigma_E}} = \sqrt{\frac{2\xi}{\omega\mu_0}} \quad (56)$$

Za točne vrednosti vstavimo podatke.

### 3.3 Odbojnost; s pomočjo tabele izračunaj odbojnost obeh svetlob na materialih (iz zraka na material).

Au	1,4	1,9	Velja Snellov zakon $r = \frac{n_1 \cos(\alpha) - n_2 \cos(\beta)}{n_2 \cos(\alpha) + n_2 \cos(\beta)}$ in $n_1 = n_{air} = 1$ .
Ag	0,08	1,9	
Al	0,4	4,5	

$$r = \frac{1 - n \cos(\beta)}{1 + n \cos(\beta)} \quad (57)$$

$$R = |r|^2 = \frac{(1 - n_{Re})^2 + n_{Im}^2}{(1 + n_{Re})^2 + n_{Im}^2} \quad (58)$$

Iz tabele vzamemo podatke in jih "nasopamo" noter.

**3.4 Odbojnost za dobre prevodnike,  $\sigma_E \gg \omega\epsilon_0, n \gg 1$ . Izpelji odvisnost odbojnosti za normalno svetlobo na dobrem prevodniku!**

$$r_s = \frac{n_1 \cos(\theta_i) - n_2 \cos(\theta_t)}{n_1 \cos(\theta_i) + n_2 \cos(\theta_t)} \quad (59)$$

$$R = |r|^2 = \frac{(1 - n_{Re})^2 + n_{Im}^2}{(1 + n_{Re})^2 + n_{Im}^2} \quad (60)$$

$$n_{Re}^2 = \frac{1}{2}\epsilon + \frac{1}{2}\sqrt{\epsilon^2 + \frac{\sigma_E^2}{\epsilon_0^2\omega^2}}, n_{Im}^2 = -\frac{1}{2}\epsilon + \frac{1}{2}\sqrt{\epsilon^2 + \frac{\sigma_E^2}{\epsilon_0^2\omega^2}} \quad (61)$$

Za dobre prevodnike  $n_{Re}^2 \approx n_{Im}^2 \approx \frac{1}{2}\frac{\sigma_E}{\epsilon_0\omega}$  sta dela približno enaka. Odvisnost  $R(\lambda)$  za dobre prevodnike:  $R \approx 1 - \frac{2}{n+1} \approx 1 - 2\sqrt{\sigma_E/2\epsilon_0\omega}$ .

**3.5 Odbojnost v prevodniku za določene kote - svetloba preide iz zraka na aluminij pod kotom  $\theta = 30$ . Velikost in smer kompleksnega valovnega vektorja aluminija:  $n_{Re} = 0, 4; n_{Im} = 4, 5$**

**3.5.1 Velikost in smer kompleksnega valovnega vektorja  $\mathcal{K} = k_{Re} + k_{Im} \cdot i$**

$$e^{i\vec{k}\vec{r}} = e^{-ik_{Re}\vec{r}} e^{-k_{Im}\vec{r}} \quad (62)$$

$$e^{ik\vec{r}} = e^{ik_{Re}\vec{r} - k_{Im}\vec{r}} = e^{ik_{Re}r - k_{Im}r} \Rightarrow ik_i r = ik_{Re}r - k_{Im}r \quad (63)$$

$$\mathcal{K}\mathcal{K} = k_0^2 \mathcal{N}^2 = k_{Re}^2 + 2ik_{Im}k_{Re} - k_{Im}^2 \quad (64)$$

Upostevamo  $k_0 = \frac{\omega}{c_0}$  in zvezo  $\cos^2(\beta) + \sin^2(\beta) = 1$  in nadalje uporabimo  $k_0 \sin(\alpha) = k_{Re} \sin(\beta)$ :

$$k_0^2 \mathcal{N}^2 = k_{Re}^2 (\cos^2(\beta) + \sin^2(\beta)) + 2ik_{Im}k_{Re} \cos(\beta) - k_{Im}^2 = k_{Re}^2 \cos^2(\beta) + 2ik_{Im}k_{Re} \cos(\beta) - k_{Im}^2 + k_{Re}^2 \sin^2(\beta) \quad (65)$$

$$= (k_{Re} \cos(\beta) + ik_{Im})^2 + k_{Re}^2 \sin^2(\beta) \quad (66)$$

$$\Rightarrow k_0^2 (\mathcal{N} - \sin^2(\alpha)) = (k_{Re} \cos(\beta) + ik_{Im}) / \cdot \sqrt{\quad}$$

(67)

$$k_{Re} \sin(\beta) = k_0 \sin(\alpha) \Rightarrow \sin(\beta) = \frac{k_0}{k_{Re}} \sin(\alpha) = \dots \Rightarrow \beta \approx 51,7 \quad (68)$$



**3.5.2 Odbojnost za TE polarizacijo na aluminiju pod kotom 30°, Rs(TE)=?, Aluminij je prevodnik zato je lahko  $\theta_z$  kompleksen.**

$$r_s = \frac{n_1 \cos(\theta_i) - n_2 \cos(\theta_t)}{n_1 \cos(\theta_i) + n_2 \cos(\theta_t)} = \frac{\cos(\alpha) - \mathcal{N} \sqrt{1 - \sin^2(\theta_t)}}{\cos(\alpha) + \mathcal{N} \sqrt{1 - \sin^2(\theta_t)}} \quad (69)$$

$$\sin(\theta_t) = \frac{\sin(\alpha)}{\mathcal{N}} \quad (70)$$

## 4 Fresnelove enacbe in Fraunhoferjev ter Fresnelov uklon

**4.1 Globina pri koznem pojavu pri diamantu z  $\lambda = 600nm$ ,  $n = 2,417$  in kote  $\theta_i = [24, 5, 25, 50]$**

Poglejmo  $\sin \theta_c = \frac{n_2}{n_1} = \frac{1}{2,417}$  in  $d = \frac{1}{\kappa_0 n_2 \mathcal{K}} = \frac{\lambda}{2\pi n_2} (\frac{\sin^2(\theta_i)}{\sin^2(\theta_c)} - 1)^{-1/2} = 1,4\mu m$

**4.2 Fraunhoferjev uklon na pravokotni zaslon ( $R_0, a, b, \mathcal{K}_x = \frac{k_\xi}{R_0}, \mathcal{K}_y = \frac{k_\eta}{R_0}$ )**

Za izracun upostevamo definicijo  $\sin(cx) = \frac{\sin(x)}{x}$  in vrednost funkcije f, ki je 1 na pravokotnem območju in 0 zunaj.

$$E(\mathcal{K}_x, \mathcal{K}_y, R_0) = \frac{iE_0}{\lambda} \frac{e^{ikR_0}}{R_0} \iint f(x) e^{-i\kappa_x x} e^{-i\kappa_y y} dx dy \quad (71)$$

$$= \frac{iE_0}{\lambda} \frac{e^{ikR_0}}{R_0} \int_{-\frac{a}{2}}^{\frac{a}{2}} \int_{-\frac{b}{2}}^{\frac{b}{2}} e^{-i\kappa_x x} e^{-i\kappa_y y} dx dy \quad (72)$$

Resimo po delih, za x koordinato  $I_X(\frac{a}{2}) = \int_{-\frac{a}{2}}^{\frac{a}{2}} e^{-i\kappa_x x} dx = -\frac{1}{i\kappa_x} e^{-i\kappa_x x} \Big|_{-\frac{a}{2}}^{\frac{a}{2}} = \frac{2}{\kappa_x} \text{sinc}(\frac{\kappa_x a}{2})$  in  $I_Y(\frac{b}{2}) = b \cdot \text{sinc}(\frac{\kappa_y b}{2})$ .

$$E = \frac{iE_0 e^{ikR_0}}{\lambda R_0} a b \text{sinc}(\frac{\kappa_x a}{2}) \text{sinc}(\frac{\kappa_y b}{2}); I = |E|^2 \quad (73)$$

Naprej lahko racunamo  $I(\theta_x, 0) = I_0 \text{sinc}(\frac{\kappa_x a \sin \theta_x}{2})$ , kar je difrakcija po kotu. Minimum za sinc(x) je, ko je x = 0. Torej je x veckratnik  $\pi = \frac{\kappa_x a \sin \theta_x}{2} = n\pi$   $\Rightarrow \theta_x = \sin^{-1}(\frac{2n\pi}{\kappa_x a})$ .

**4.3 Fraunhoferjev uklon na difrakcijski resetki**

$$E_0(\mathcal{K}_x, \mathcal{K}_y) = \alpha \int f(x, y) e^{-i\kappa_x x} dx = e^{-i\kappa_x x_0} E_0(\kappa_x, \kappa_y) \quad (74)$$

$$E = \sum_j^{\frac{N}{2}} E_0 e^{-i\kappa_x D_j} e^{-j \frac{\kappa_x D}{2}} + \sum_j^{\frac{N}{2}} E_0 e^{i\kappa_x D_j} e^{j \frac{\kappa_x D}{2}} \quad (75)$$

Uporabimo razvoj v vrsto  $\sum_{j=0}^N x^j = \frac{1-x^{N+1}}{1-x}$ ,

$$E = E_0 e^{-i \frac{\kappa_x D}{2}} \left( \frac{1 - e^{-i \frac{\kappa_x D N}{2}}}{1 - e^{-i \kappa_x D}} \right) + E_0 e^{i \frac{\kappa_x D}{2}} \left( \frac{1 - e^{i \frac{\kappa_x D N}{2}}}{1 - e^{i \kappa_x D}} \right) = \dots = 2E_0 \frac{\sin(\frac{\kappa_x D N}{2})}{\sin(\frac{\kappa_x D}{2})} \quad (76)$$

#### 4.4 Resolucija difrakcijskih resetek

Podana sta  $\lambda_1 = 589,0nm$ ,  $\lambda_2 = 589,6nm$  in:

$$E \propto \text{sinc}\left(\frac{\kappa_x d}{2}\right) \cdot \frac{\sin(\frac{\kappa_x D N}{2})}{\sin(\frac{\kappa_x D}{2})} \propto \sigma(\theta) \cdot \Gamma(\theta) \quad (77)$$

$$I(\theta) = |E|^2 = I_0 \text{sinc}\left(\frac{\kappa_x d}{2}\right) \frac{\sin^2(\frac{\kappa_x D N}{2})}{\sin^2(\frac{\kappa_x D}{2})} \quad (78)$$

Za primer  $N \gg 1$   $I(\theta)$  zgleda tako, da pocasi oscilira zaradi  $\text{sinc}^2 \alpha$  in hitro zaradi  $\frac{\sin^2(\frac{\kappa_x D N}{2})}{\sin^2(\frac{\kappa_x D}{2})}$ , kjer zgornjemu clenu dolocimo minimum in spodnjemu maksimum za najhitrejsje mozno pojevanje.

- maksimum:  $\sin^2 \Gamma = 0 \Rightarrow \Gamma = \frac{kD}{2} \sin \theta = m\pi \Rightarrow \sin \theta_m = \frac{2\pi m}{kD} = \frac{m\lambda}{D} \Rightarrow \frac{d}{dt} \Rightarrow \cos \theta \Delta \theta = \frac{m}{D} \Delta \lambda_C$
- minimum:  $\sin^2 \Gamma N = 0 \Rightarrow \Gamma N = \frac{kDN}{2} \sin \theta = n\pi \Rightarrow \sin \theta_N = \frac{k\pi m}{kDN}$   
1. minimum se zgodi pri  $n+1$ , torej:

$$(n+1)\pi - n\pi = \frac{kDN}{2} (\sin \theta_{min} - \sin \theta_{max}) \approx \frac{kDN}{2} (\theta_{min} - \theta_{max}) \quad (79)$$

$$\pi = \frac{kD}{2} N \Delta(\sin \theta) = \frac{kDN}{2} \cos \theta d\theta \quad (80)$$

$$\Delta \theta = \frac{2\pi}{kDN \cos \theta} = \frac{\lambda}{ND \cos \theta_{max}} \Rightarrow \frac{\lambda}{\Delta \lambda} = mN \quad (81)$$

**4.5 Fresnelove cone so okrogle cone radija  $a$ , nakopocene ena za drugo z drugacnimi polmeri. V primeru dveh je notranji radij  $a_1 = \sqrt{\lambda L}$  in zunanji  $a_2 = \sqrt{2\lambda L}$ . Lahko racunamo za vsako cono posamicno ali skupaj z  $\frac{1}{L} = \frac{1}{z'_0} + \frac{1}{z_0}$**

Poenostavitev je sicer ta, da je vse na opticni osi  $(x', y') = (\xi', \eta') = (0, 0)$ ,  $R_0 = z_0$ ,  $R'_0 = z'_0$ :

$$E = \frac{E_0}{i\lambda} \frac{e^{ikz'_0}}{z'_0} \frac{e^{ikz_0}}{z_0} \iint f(x, y) e^{\frac{ik}{2z'_0}(x^2+y^2)} e^{\frac{ik}{2z_0}(x^2+y^2)} dx dy = \frac{c}{i\lambda} \iint f(x, y) e^{\frac{ik}{2L}(x^2+y^2)} dx dy \quad (82)$$

$$E = \frac{C}{i\lambda} \int_0^{2\pi} d\phi \int_0^{a_1} e^{\frac{ik}{2L}\rho^2} \rho d\rho = \frac{2\pi ic}{\lambda} \int_0^{a_1} e^{\frac{ik}{2L}\rho^2} \rho d\rho = \frac{2\pi c}{i\lambda} \frac{L}{k} \int_0^{\frac{ka_1^2}{2L}} e^{iu} du = \quad (83)$$

$$= \frac{CL}{i} \int_0^{\frac{ka_1^2}{2L}} e^{iu} du \xrightarrow{a_1,0} -CL(e^{i\pi} - 1) = 2CL \quad (84)$$

V tem primeru sta za podatka vstavljeni kolicini  $(a_1, 0)$ , naprej pa za  $(a_2, 0)$  dobimo 0 in  $(a_1, a_2) - 2CL$ .

#### 4.6 Fresnelova leca, kjer je podan rekurzivni zapis za električno poljsko jakost $E_n = 2(-1)^n E_0$ , $a_1 = \sqrt{n\pi L}$ , $a_2 = \sqrt{(n+1)\lambda L}$

Velja, da sodo/liho stevilo takih odprtih deluje kot leca z fokusom  $f = L = (a_2^2 - a_1^2)/\lambda$ .

$$E_0 = \frac{\tilde{E}_0 e^{ik(z'_0 + z_0)}}{z'_0 + z_0}; u = \frac{k\rho}{2L} \quad (85)$$

Za nadaljne cene upostevamo v mejah integrala vbistvu je  $u(a_2) = \frac{k}{2L}[(n+1)\lambda L] = (n+1)\pi$  in  $u(a_1) = n\pi$ .

$$E_n = -CL e^{in\pi} e^{i(n+1)\pi} = -CL(e^{in\pi} e^{i\pi} - e^{in\pi}) = 2CL e^{in\pi} = (-1)^n 2CL \quad (86)$$

$$= (-1)^n 2CL = (-1)^n \cdot 2 \cdot \frac{E_0 e^{ik(z'_0 + z_0)}}{z_0 + z'_0} \Rightarrow E_n = (-1)^n 2E_0 \quad (87)$$

## 5 Interferenca

### 5.1 Interferenca na tanki rezi z debelino odprtine $D = 0,54mm$ , $\lambda = 600nm$ . Zanima nas kolikсна je oddaljenost od zalona, da bo razdalja med interferencnima vzorcema $\xi = 1mm$ .

$$2\pi m = k_0 D \sin(\theta) = k_0 D \theta \Rightarrow \tan(\theta) = \frac{\xi}{z_0} \Rightarrow \xi = z_0 \tan(\theta) \approx z_0 \theta \quad (88)$$

$$\text{Za } m=1: \theta = \frac{2\pi}{k_0 D} \Rightarrow z_0 = \frac{\xi}{\theta} = 0,9m$$

### 5.2 Fresnelova bipiramida za $n = 1, 5$ , $\lambda = 633nm$ , $\xi = 0,5nm$ . Z $\alpha$ je označen prizmin kot, z $\beta$ kot odboja.

Interferenčni vzorec z  $E = E_0 e^{i(\vec{k}_1 \vec{r} - \omega t)} + E_0 e^{i(\vec{k}_2 \vec{r} - \omega t)}$ ;  $k_1 = (-k_x, 0, k_y)$ ,  $k_z = (k_x, 0, k_y)$ .

$$E(x, z) = E_0 (e^{-ik_x x} + e^{ik_x z}) e^{i(k_z z - \omega t)} \quad (89)$$

$$I \propto |E|^2 = |E_0|^2 \cos^2(k_x x) \quad (90)$$

Maksimum intenzitete nastopi pri  $\cos(k_x x) = \pm 1 \Rightarrow \pi$ . Snellov zakon je  $n_{steklo} \sin(\alpha) = n_{zrak} \sin(\beta)$  postopoma privede do  $n\alpha \approx \beta$ :

$$k_x = k_0 \sin(\beta - \alpha) = \frac{2\pi}{\lambda} \sin(\beta - \alpha) \Rightarrow \frac{2\pi x}{\lambda} \sin(\beta - \alpha) = \pi \Rightarrow \sin(\alpha(n-1)) \approx \frac{\lambda}{2x} \quad (91)$$

$$\alpha = \frac{\lambda}{2x(n-1)} \quad (92)$$

**5.3 Fabry-Perrotov interferometer z  $n = 1,5, R = 0,95$  in  $\lambda_0 = 656,28nm, \Delta\lambda = 0,016nm$ . Doloci visino h, da bo lahko interferometer locil neodvisni crti.**

$$E_{out} = E_0 \frac{t_{12}t_{21}}{1 - r_{21}^2 e^{i\phi}}; \phi = 2k_0 n d \cos(\alpha); R = |r_{21}|^2 \quad (93)$$

$$T = \frac{1}{1 + \frac{4R}{(1-R)^2} \sin^2(\frac{\theta}{2})} = \frac{1}{1 + F \sin^2(\theta/2)} \quad (94)$$

Kriterij za dolocitev je, da sta dva  $T(\lambda)$  vrha locena, ko sta se vedno locena, ce v ' $\lambda$ ' prostoru individualne vrh zadane svojo polovico maksimalno vrednost.

$$T = \frac{1}{2} \Rightarrow F \sin^2 \frac{\theta}{2} = 1 \Rightarrow \frac{\theta}{2} = \arcsin \frac{1}{\sqrt{F}} \quad (95)$$

$$d\lambda = -\frac{c}{\nu^2} d\nu \Rightarrow \frac{d\lambda}{\lambda} = -\frac{d\nu}{\nu} \quad (96)$$

$$\frac{\phi}{2} = \arcsin\left(\frac{1}{\sqrt{F}}\right) = k_0 n d = \frac{\Delta\omega n d}{c} \Rightarrow \frac{1}{\sqrt{F}} = \frac{n d \omega \Delta\lambda}{c \lambda} \Rightarrow d = \frac{1}{2\pi n \sqrt{F}} \frac{\lambda^2}{\Delta\lambda} = 73\mu m \quad (97)$$

## 6 Vecplastni nanosi in sipanje

**6.1 Popolna prepustnost skozi tanko plast (zrak-TP-steklo).** Opazujemo svetlobo valovne dolzine  $\lambda=540nm$ , TP je debeline  $d_2$  in ima neznani lomni kolicnik  $n_2$ , steklo ima  $n_3 = 1,54$ . Zanima nas najmanjsa globina  $d_2$  in  $n_2$ , da struktura prepusca svetlobo.

$$M = \begin{pmatrix} M_{11} & M_{12} \\ M_{21} & M_{22} \end{pmatrix} = M_{12} P M_{23} = M_{12} \begin{pmatrix} e^{-i\delta} & 0 \\ 0 & e^{i\delta} \end{pmatrix} M_{23} = \frac{1}{t_{12}} \begin{pmatrix} 1 & r_{12} \\ r_{12} & 1 \end{pmatrix} \begin{pmatrix} e^{-i\delta} & 0 \\ 0 & e^{i\delta} \end{pmatrix} \frac{1}{t_{23}} \begin{pmatrix} 1 & r_{23} \\ r_{23} & 1 \end{pmatrix} \quad (98)$$

$$= \frac{1}{t_{12}t_{23}} \begin{pmatrix} r_{12} + r_{23}e^{i\delta} & r_{23}e^{-i\delta} + r_{12}e^{i\delta} \\ r_{12}e^{-i\delta} + r_{23}e^{i\delta} & r_{12}r_{23}e^{-i\delta} + e^{i\delta} \end{pmatrix} \quad (99)$$

$$T = \frac{n_3}{n_1} \frac{|t_{12}t_{23}|^2}{1 + |r_{12}r_{23}|^2 + 2r_{12}r_{23}\cos(2\delta)}; T_{max} \Rightarrow \cos(2\delta_{min}) \Rightarrow 2\delta = (2m-1)\pi \quad (100)$$

$$M_{11} = \frac{1}{t_{12}t_{23}}(e^{-i\delta} + r_{12}r_{23}e^{i\delta}), M_{21} = \dots \quad (101)$$

$$t = \frac{1}{M_{11}} = \frac{t_{12}t_{23}}{e^{-i\delta} + r_{12}r_{23}e^{i\delta}} \quad (102)$$

$$r = \frac{M_{21}}{M_{11}} = \frac{r_{12}e^{-i\delta} + r_{23}e^{i\delta}}{e^{-i\delta} + r_{12}r_{23}e^{i\delta}} \quad (103)$$

Maksimalna prepustnost je, ko je prepustnost  $T=1$  in odbojnost  $R=0$ . Pri teh pogojih je  $r_{12} = r_{23}$  in  $n_2 = 1, 24$ .

**6.2 Vecplastno dielektricno steklo z 17 plastmi z alternirajocimi lomnimi kolicniki  $n_a = 1, 38$  in  $n_b = 2, 32$  na steklu z  $n_3 = 1, 52$ . Koliksna je odbojnost?**

$$a = \frac{\lambda}{4na}, b = \frac{\lambda}{4nb} \quad (104)$$

$$M_{tot} = M_{1a}P_aM_{ab}P_b\dots P_aM_{a3} = M_{1a} \cdot M_N \cdot P_aM_{a3} \quad (105)$$

$$M_{1a} = \frac{1}{t_{1a}} \begin{pmatrix} 1, r_{1a} \\ r_{1a}, 1 \end{pmatrix}; r_{1a} = \frac{1-na}{1+na} \quad (106)$$

$$M_{a3} = \frac{1}{t_{a3}} \begin{pmatrix} 1, r_{a3} \\ r_{a3}, 1 \end{pmatrix} \quad (107)$$

$$P_{ab} = \begin{pmatrix} e^{-i\delta_{ab,0}} \\ 0, e^{i\delta_{ab}} \end{pmatrix} = \begin{pmatrix} -i, 0 \\ 0, i \end{pmatrix}; \delta_{ab} = n_{a,b}k_0d_{a,b} = \frac{\pi}{2} \quad (108)$$

## 7 Koherenca svetlobe

**7.1 Mikelsonov interferometer z  $\lambda_1 = 588, 995nm$  in  $\lambda_2 = 589, 592nm$ . Kako dalec od ogledala moramo opazovati, da ju locimo?**

$$\Delta\omega = |\omega_1 - \omega_2| \quad (109)$$

$$S(\omega) = \frac{I}{2}[\delta(\omega - (\omega_0 - \frac{\Delta\omega}{2})) + \delta(\omega - (\omega_0 + \frac{\Delta\omega}{2}))] = \frac{I_0}{2}|\delta(\omega - \omega_0) + \delta(\omega - (\omega_0 + \Delta\omega))| \quad (110)$$

$$G^{(1)}(\tau) = \int_{-\infty}^{\infty} S(\omega)e^{i\omega\tau}d\omega = \frac{I_0}{2}[e^{i(\omega_0 - \frac{\Delta\omega}{2})\tau} + e^{i(\omega_0 + \frac{\Delta\omega}{2})\tau}] \quad (111)$$

$$I_{det} = 2I_0 + 2Re(G^{(1)}) = 2I_0 + I_0(\cos((\omega_0 - \frac{\Delta\omega}{2})\tau)) = 2I_0(1 + \cos(\omega_0\tau)\cos(\frac{\Delta\tau}{2})) \quad (112)$$

Da poiscemo minimum, upostevamo, da bo to tam kjer je oscilajoc clen  $\cos(\frac{\Delta\omega\tau}{2}) = 0 \Rightarrow \Delta\omega = \pi \Rightarrow \pi = \frac{2\Delta\omega x}{c_0}$ :

$$\Delta x = \frac{\pi c_0}{2\Delta\omega} = \frac{\pi c_0}{2} \frac{1}{2\pi c_0(\frac{1}{\lambda_1} - \frac{1}{\lambda_2})} \quad (113)$$

## 7.2 Spekter in avtokorelacija Gavsovega paketa $E(t) = E_0 e^{-\pi(\frac{t}{t_c})^2} e^{-i\omega_0 t}$ , doloci $S(\omega) = ?$

Zacetni nastavek je avtokorelacijska funkcija  $G^{(1)}(\tau) = \lim_{T \rightarrow \infty} \frac{1}{T} \int_{-\frac{T}{2}}^{\frac{T}{2}} E(t) E^*(t+\tau) dt$  in njeno normalizirano vrednostjo  $g(\tau)$ .

$$g(\tau) = \frac{G^{(1)}(\tau)}{G^{(1)}(0)} = \lim_{T \rightarrow \infty} \frac{\int_{-\frac{T}{2}}^{\frac{T}{2}} E(t) E^*(t+\tau) dt}{\int_{-\frac{T}{2}}^{\frac{T}{2}} |E(t)|^2 dt} = \frac{1}{C} \lim_{T \rightarrow \infty} \int_{-\frac{T}{2}}^{\frac{T}{2}} E(t) E^*(t+\tau) dt \quad (114)$$

Nato izracunamo normalizacijsko konstanto  $C = \lim_{T \rightarrow \infty} \int_{-\frac{T}{2}}^{\frac{T}{2}} |E(t)|^2 dt = \dots = |E_0|^2 \frac{t_c}{\sqrt{2}}$ :

$$= \frac{1}{C} \lim_{T \rightarrow \infty} \int_{-\frac{T}{2}}^{\frac{T}{2}} E_0 e^{-\pi(\frac{t}{t_c})^2} e^{-i\omega_0 t} E_0^* e^{i\omega_0(t+\tau)} e^{-\pi(\frac{t+\tau}{t_c})^2} dt \quad (115)$$

$$= \frac{|E_0|^2}{C} \lim_{T \rightarrow \infty} \int_{-\frac{T}{2}}^{\frac{T}{2}} e^{-\pi(\frac{t}{t_c})^2} e^{-\pi(\frac{t+\tau}{t_c})^2} e^{i\omega_0 \tau} dt \quad (116)$$

$$= \frac{\sqrt{2}}{t_c} \lim_{T \rightarrow \infty} \int_{-\frac{T}{2}}^{\frac{T}{2}} e^{-\frac{2\pi}{t_c^2}(t^2+t\tau+\frac{\tau^2}{2})} e^{i\omega_0 \tau} dt \quad (117)$$

$$= \frac{\sqrt{2}}{t_c} \lim_{T \rightarrow \infty} \int_{-\frac{T}{2}}^{\frac{T}{2}} e^{-\frac{2\pi}{t_c^2}(t^2+t\tau+\frac{\tau^2}{2})} e^{-\frac{2\pi\tau^2}{4t_c^2}} e^{i\omega_0 \tau} dt \quad (118)$$

$$= \frac{\sqrt{2}}{t_c} e^{-\frac{2\pi\tau^2}{4t_c^2}} e^{i\omega_0 \tau} \lim_{T \rightarrow \infty} \int_{-\frac{T}{2}}^{\frac{T}{2}} e^{-\frac{2\pi}{t_c^2}(t+\frac{\tau}{2})^2} dt \quad (119)$$

$$=_{NS} \frac{\sqrt{2}}{t_c} e^{-\frac{2\pi\tau^2}{4t_c^2}} e^{i\omega_0 \tau} \int_{-\infty}^{\infty} e^{-\frac{2\pi}{t_c^2}(x)^2} dx = e^{-\frac{2\pi\tau^2}{2t_c^2}} e^{i\omega_0 \tau} \quad (120)$$

Po Fourierovi transformaciji dobimo:

$$S(\omega) = \frac{1}{2\pi} \int_{-\infty}^{\infty} G^{(1)}(\tau) E^{-i\omega\tau} d\tau = \frac{1}{2\pi} \int_{-\infty}^{\infty} g(\tau) e^{-i\omega\tau} d\tau \quad (121)$$

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**7.3** Spekter in avtokorelacija eksponentnega pulza  $E = E_0 e^{-t/t_c} e^{-i\omega_0 t} : t > 0$  in 0 sicer.

## 8 Lomni kolicnik

**8.1** Koeficienti v Cauchyjevi formuli za  $\lambda \gg \lambda_0$ , doloci formuli za koeficienta  $C_1, C_2$  prek Sellmarjevih koeficientov  $A$  in  $G$  za material z eno resonanco  $\lambda_0$  v zunanem magnetnem polju. + Z podatki  $A=1, G=1,17, \lambda_0 = 500nm$  in  $\lambda = 800nm$  lahko vrednosti izracunas.

$$\mathcal{N} = C_1 + \frac{C_2}{\lambda^2} \Rightarrow \mathcal{N}^2 = A + \frac{C\lambda^2}{\lambda^2 - \lambda_0^2} = A + \frac{G}{1 - (\frac{\lambda_0}{\lambda})^2} = C_1^2 + 2\frac{C_1 C_2}{\lambda^2} + \frac{C_2^2}{\lambda^4} \quad (122)$$

$$C_1^2 + 2\frac{C_1 C_2}{\lambda^2} + \frac{C_2^2}{\lambda^4} = A + \frac{G}{1 - (\frac{\lambda_0}{\lambda})^2} =_{\lambda \gg \lambda_0} A + G + G(\frac{\lambda_0^2}{\lambda^2}) \quad (123)$$

Z enacenjem koeficientov pri enakih vrednostih  $\lambda$  dobimo, da je  $C_1^2 = A + G$  in  $2C_1 C_2 = G\lambda_0^2$  ter izrazimo iskane vrednosti.

$$\mathcal{N} = \sqrt{A + G} + \frac{G}{2\sqrt{A + G}} \frac{\lambda_0^2}{\lambda^2} \quad (124)$$

## 9 Opticno anizotropne snovi

**9.1** Opticno aktivni materiali in cirkularni dihroizem; obravnavaj Jonesovo matriko, matriko, ki opise opticni fenomen cirkularnega dihroizma in matriko, ki opise prehod skozi material, ki je hkrati opticno aktiven in 'ima' cirkularni dihroizem.

### 9.1.1 Jonesova matrika

Linearno polarizirano svetlobo razdelimo na levo in desno sucno polarizacijo ( $\tilde{n} = \frac{n_{LCP} + n_{RCP}}{2}, \Delta n = n_{RCP} - n_{LCP}$ ), ki je pred in po prehodu skozi opticno aktiven material:

$$J_{in} = \begin{pmatrix} 1 \\ 0 \end{pmatrix} = \frac{1}{2} \begin{pmatrix} 1 \\ i \end{pmatrix} + \frac{1}{2} \begin{pmatrix} 1 \\ -i \end{pmatrix} \quad (125)$$

$$J_{out} = \frac{1}{2} \begin{pmatrix} 1 \\ i \end{pmatrix} e^{in_{LCP} k_0 d} + \frac{1}{2} \begin{pmatrix} 1 \\ -i \end{pmatrix} e^{in_{RCP} k_0 d} = \frac{1}{2} \begin{pmatrix} e^{ik_0 \tilde{n} d} e^{-ik_0 \frac{\Delta n}{2} d} + e^{ik_0 \tilde{n} d} e^{ik_0 \frac{\Delta n}{2} d} \\ i e^{ik_0 \tilde{n} d} e^{-ik_0 \frac{\Delta n}{2} d} - i e^{-ik_0 \tilde{n} d} e^{ik_0 \frac{\Delta n}{2} d} \end{pmatrix} = \quad (126)$$

$$= \frac{e^{ik_0 \tilde{n} d}}{2} \begin{pmatrix} e^{-ik_0 \frac{\Delta n}{2} d} + e^{ik_0 \frac{\Delta n}{2} d} \\ i e^{-ik_0 \frac{\Delta n}{2} d} - i e^{ik_0 \frac{\Delta n}{2} d} \end{pmatrix} = e^{ik_0 \tilde{n} d} \begin{pmatrix} \cos(k_0 \frac{\Delta n}{2} d) \\ \sin(k_0 \frac{\Delta n}{2} d) \end{pmatrix} = e^{ik_0 \tilde{n} d} \begin{pmatrix} \cos(\theta) & -\sin(\theta) \\ \sin(\theta) & \cos(\theta) \end{pmatrix} = \quad (127)$$

$$J_{out} = R_{0A} J_{in} \quad (128)$$

### 9.1.2 Cirkularni dihiroizem

- $\kappa_{LCP} = n_{Im}^{LCP} \cdot k$ ,  $\kappa_{RCP} = n_{Im}^{RCP} \cdot k$
- $\bar{\kappa} = \frac{\kappa_{LCP} + \kappa_{RCP}}{2}$ ,  $\Delta\kappa = \kappa_{RCP} - \kappa_{LCP}$
- $\kappa_{RCP} = \bar{\kappa} + \frac{\Delta\kappa}{2}$ ,  $\kappa_{LCP} = \bar{\kappa} - \frac{\Delta\kappa}{2}$

$$J_{in} = \begin{pmatrix} 1 \\ 0 \end{pmatrix} = \frac{1}{2} \begin{pmatrix} 1 \\ i \end{pmatrix} + \frac{1}{2} \begin{pmatrix} 1 \\ -i \end{pmatrix} \quad (129)$$

$$J_{out} = \frac{1}{2} \begin{pmatrix} 1 \\ i \end{pmatrix} e^{-\kappa_{LCP}d} + \frac{1}{2} \begin{pmatrix} 1 \\ -i \end{pmatrix} e^{-\kappa_{RCP}d} = \frac{e^{-\frac{\bar{\kappa}d}{2}}}{2} \left( e^{\frac{\Delta\kappa d}{2}} + e^{\frac{\Delta\kappa d}{2}} \right) = \quad (130)$$

$$= e^{-\bar{\kappa}d} \begin{pmatrix} \cosh\left(\frac{\Delta\kappa d}{2}\right) \\ i \sinh\left(\frac{\Delta\kappa d}{2}\right) \end{pmatrix} = e^{-\bar{\kappa}d} \begin{pmatrix} \cos\left(\frac{i\Delta\kappa d}{2}\right) \\ \sin\left(\frac{i\Delta\kappa d}{2}\right) \end{pmatrix} \quad (131)$$

$$R_{C,D.} = e^{-\bar{\kappa}d} \begin{pmatrix} \cos(\theta), \sin(\theta) \\ \sin(\theta), \cos(\theta) \end{pmatrix} : \theta = i \frac{\Delta\kappa d}{2} \quad (132)$$

### 9.1.3 Opticno aktiven material z cirkularnim dihiroizmom (matriki zmnozimo)

- $n_{Re}^{LCP} \neq n_{Re}^{RCP}$ ,  $n_{Im}^{LCP} \neq n_{Im}^{RCP}$

$$R_{both} = R_{0A} R_{CD} - e^{ik_0 \bar{n}d} e^{-\bar{\kappa}d} \begin{pmatrix} \cos(\theta), -\sin(\theta) \\ \sin(\theta), \cos(\theta) \end{pmatrix}; \theta = \frac{\Delta n Re k_0 d}{2} + i \frac{\Delta\kappa d}{2} \quad (133)$$

## 9.2 Rotacija polarizacije v magneto-opticnem pojavu z

$$\theta = \frac{k_0 \Delta n d}{2}, \Delta n = n_{RCP} - n_{LCP}$$

Resujemo enačbi za magneto optični efekt za  $\Omega \ll \omega$  oz. majhna magnetna polja:

$$n_{RCP} = 1 + \frac{1}{2} \frac{\omega_p^2}{\omega_0^2 - \omega^2 + \omega\Omega} = 1 + \frac{1}{2} \frac{\omega_p^2}{\omega_0^2 - \omega^2} \frac{1}{1 + \frac{\omega\Omega}{\omega_0^2 - \omega^2}} = 1 + \frac{1}{2} \frac{\omega_p^2}{\omega_0^2 - \omega^2} \left(1 - \frac{\omega\Omega}{\omega_0^2 - \omega^2}\right) \quad (134)$$

$$n_{LCP} = 1 + \frac{1}{2} \frac{\omega_p^2}{\omega_0^2 - \omega^2 - \omega\Omega} = 1 + \frac{1}{2} \frac{\omega_p^2}{\omega_0^2 - \omega^2} \frac{1}{1 - \frac{\omega\Omega}{\omega_0^2 - \omega^2}} = 1 + \frac{1}{2} \frac{\omega_p^2}{\omega_0^2 - \omega^2} \left(1 + \frac{\omega\Omega}{\omega_0^2 - \omega^2}\right) \quad (135)$$

$$\Omega \ll \omega \Rightarrow \frac{1}{1 + \frac{\omega\Omega}{\omega_0^2 - \omega^2}} = 1 + \frac{\omega\Omega}{\omega_0^2 - \omega^2} \quad (136)$$

$$\Delta n = n_{RCP} - n_{LCP} = -\frac{\omega_p^2 \Omega \omega}{(\omega_0^2 - \omega^2)^2}; \Omega = \frac{e_0 B_0}{me}, \omega_p^2 = \frac{\rho e_0^2}{m\epsilon_0}, k = \frac{\omega}{c} \quad (137)$$

$$\theta = \frac{k_0 \Delta n d}{2} = -\frac{1}{2} k_0 d \frac{\omega_p^2 \omega \Omega}{(\omega_0^2 - \omega^2)^2} \quad (138)$$



## 10 Indeks elipsoida, sipanje svetlobe in laserji

### 10.1 Izracunaj in skiciraj indeks elipsoida in valovni vektor za prehod svetlobe skozi biaksialen kristal z lomnimi kolicniki $n_{xx}, n_{yy}, n_{zz}$ v $xz, xy$ in $yz$ ravninah

Navadno je  $\vec{k} \cdot \vec{E} = 0$  oziroma nista vzporedna v izotropnih materialih.

$$(k^2 l - k_0^2 \epsilon) \vec{E} = (\vec{k} \vec{E}) \vec{k} \quad (139)$$

V lastnem sistemu je matrika taka in sicer pogosto velja  $\epsilon_{xx} < \epsilon_{yy} < \epsilon_{zz}$ :

$$\epsilon = \begin{bmatrix} \epsilon_{xx} & 0 & 0 \\ 0 & \epsilon_{yy} & 0 \\ 0 & 0 & \epsilon_{zz} \end{bmatrix} \quad (140)$$

$$\begin{bmatrix} k_y^2 + k_z^2 - k_0^2 \epsilon_{xx} & -k_x k_y & -k_x k_z \\ -k_x k_y & k_x^2 + k_y^2 - k_0^2 \epsilon_{yy} & -k_y k_z \\ -k_z k_x & -k_y k_z & k_x^2 + k_y^2 - k_0^2 \epsilon_{zz} \end{bmatrix} \vec{E} = \underline{\underline{M}} \vec{E} = 0 \quad (141)$$

$$\det \underline{\underline{M}} = \begin{bmatrix} k_y^2 + k_z^2 - k_0^2 \epsilon_{xx} & -k_x k_y & -k_x k_z \\ -k_x k_y & k_x^2 + k_y^2 - k_0^2 \epsilon_{yy} & -k_y k_z \\ -k_z k_x & -k_y k_z & k_x^2 + k_y^2 - k_0^2 \epsilon_{zz} \end{bmatrix} = 0 \quad (142)$$

Za lazi izracun gremo v podane ravnine, za primer bo izracun v  $xy$  ravnini.

#### 10.1.1 $xy$ -ravnina $\vec{k} = (k_x, k_y, 0)$

$$\underline{\underline{M}} = \begin{bmatrix} k_y^2 - k_0^2 \epsilon_{xx} & -k_x k_y & 0 \\ -k_x k_y & k_x^2 - k_0^2 \epsilon_{yy} & 0 \\ 0 & 0 & k_x^2 + k_y^2 - k_0^2 \epsilon_{zz} \end{bmatrix} \quad (143)$$

$$\det \underline{\underline{M}} = (k_x^2 + k_y^2 - k_0^2 \epsilon_{zz}) [k_0^4 \epsilon_{xx} \epsilon_{yy} - k_0^2 k_x^2 \epsilon_{xx} - k_0^2 k_y^2 \epsilon_{yy}] \quad (144)$$

1.  $k_x^2 + k_y^2 = k_0^2 \epsilon_{zz} \Rightarrow \kappa_x^2 + \kappa_y^2 = \epsilon_{zz} \Rightarrow$ graficno kroznica
2.  $k_0^2 k_x^2 \epsilon_{xx} + k_0^2 k_y^2 \epsilon_{yy} = k_0^4 \epsilon_{xx} \epsilon_{yy} \Rightarrow \frac{\kappa_x^2}{\epsilon_{yy}} + \frac{\kappa_y^2}{\epsilon_{xx}} = 1 \Rightarrow$ graficno elipsa

V  $yz$  ravnini naredimo enak korak in ta da pride enak par resitev. Naprej se nekaj o polarizaciji na primeru  $xy$  ravnine:

- Vsaka resitev pripada določenemu kolicniku  $n$  in svoji polarizaciji
- Ena polarizacija je vzporedna na elipso, druga pravokotna "ven"
- Ena polarizacija kaze v  $\kappa_z$  smer:  $k_x^2 + k_y^2 - k_0^2 \epsilon_{zz} = 0$ ;  $\vec{E} = (0, 0, E_0)$

## 10.2 Smer $\vec{E}, \vec{k}$ na površini indeksnega elipsoida.

### 10.2.1 xy ravnina

$$\tilde{M} = \frac{M}{k_0^2} = \begin{bmatrix} \kappa_y^2 - \epsilon_{xx} & -\kappa_x \kappa_y & 0 \\ -\kappa_x \kappa_y & \kappa_x^2 - \epsilon_{yy} & 0 \\ 0 & 0 & \kappa_x^2 + \kappa_y^2 - \epsilon_{zz} \end{bmatrix} \begin{bmatrix} E_x \\ E_y \\ E_z \end{bmatrix} = 0 \quad (145)$$

$$(\kappa_y^2 - \epsilon_{xx})E_x - \kappa_x \kappa_y E_y = 0 \Rightarrow \frac{E_y}{E_x} = \frac{\kappa_y^2 - \epsilon_{xx}}{\kappa_x \kappa_y} \quad (146)$$

$$\frac{\kappa_y^2}{\epsilon_{xx}} + \frac{\kappa_x^2}{\epsilon_{yy}} = 1 \Rightarrow \kappa_y^2 = \epsilon_{xx} - \kappa_x^2 \frac{\epsilon_{xx}}{\epsilon_{yy}} \quad (147)$$

Enacbi združimo v  $\frac{E_y}{E_x} = \frac{\kappa_y^2 - \epsilon_{xx}}{\kappa_x \kappa_y} = -\frac{\epsilon_{xx} \kappa_x}{\epsilon_{yy} \kappa_y}$  in tangentno linijo za resitev dobimo prek odvoda  $\frac{d\kappa_y}{d\kappa_x}$ :

$$0 = \frac{2\kappa_x}{\epsilon_{yy}} + \frac{2\kappa_y}{\epsilon_{xx}} \frac{d\kappa_y}{d\kappa_x} \Rightarrow \frac{d\kappa_y}{d\kappa_x} = -\frac{\epsilon_{xx}}{\epsilon_{yy}} \frac{\kappa_x}{\kappa_y} \quad (148)$$

### 10.2.2 xz ravnina

$$\tilde{M} = \frac{M}{k_0^2} = \begin{bmatrix} \kappa_z^2 - \epsilon_{xx} & 0 & -\kappa_x \kappa_z \\ 0 & \kappa_x^2 + \kappa_z^2 - \epsilon_{yy} & 0 \\ -\kappa_z \kappa_x & 0 & \kappa_x^2 - \epsilon_{zz} \end{bmatrix} \begin{bmatrix} E_x \\ E_y \\ E_z \end{bmatrix} = 0 \quad (149)$$

$$(\kappa_z^2 - \epsilon_{xx})E_x - \kappa_x \kappa_z E_z = 0 \Rightarrow \frac{E_z}{E_x} = \frac{\kappa_z^2 - \epsilon_{xx}}{\kappa_x \kappa_z} \quad (150)$$

**10.3 Glavna polarizacija v biaksialnem materialu z  $n_{xx} = 1,619$ ;  $n_{yy} = 1,620$ ;  $n_{zz} = 1,627$ . Material osvetimo tako, da svetloba lezi v xz ravnini pod kotom  $30^\circ$  glede na os z. Analiziraj polarizacijo svetlobe, izračunaj n, smeri E in D polj ter kot med njima in poyntingov vektor S ter določi kot med njima.**

Ce vektor lezi v xz ravnini uporabimo ze dobljene resitve  $\kappa_x^2 + \kappa_y^2 = \epsilon_{yy}$  in  $\frac{\kappa_x^2}{\epsilon_{zz}} + \frac{\kappa_z^2}{\epsilon_{xx}} = 1$ . Pripravimo podatke za izracun elipticne resitve:

- $\epsilon_{xx} = n_{xx}^2 = 2,62$  enako za  $\epsilon_{yy}, \epsilon_{zz}$
- $\epsilon_{yy} = \kappa_x^2 + \kappa_y^2 \Rightarrow k_x^2 + k_z^2 = \epsilon_{yy} k_0^2$

### 10.3.1 Elipticna resitev

(151)

### 10.3.2 Resitev za električno polje in Poytingov vektor

#### 10.3.3 Opticne osi

Cilj je najti kot med  $(\vec{k}, \vec{z})$ , da sta  $n_1, n_2$  enaka.

$$n_1 = n_{yy} \quad (152)$$

$$n_2 = \sqrt{\frac{\epsilon_{xx}\epsilon_{zz}}{\epsilon_{xx}\sin^2(\theta) + \epsilon_{yy}\cos^2(\theta)}} \quad (153)$$

$$n_1 = n_2 \Rightarrow n_{yy} = \sqrt{\frac{\epsilon_{xx}\epsilon_{zz}}{\epsilon_{xx}\sin^2(\theta) + \epsilon_{yy}\cos^2(\theta)}} = \sqrt{\frac{\epsilon_{xx}\epsilon_{zz}}{\epsilon_{xx}(1 - \cos^2(\theta)) + \epsilon_{yy}\cos^2(\theta)}} \quad (154)$$

$$\sin^2(\theta) = \frac{1}{\epsilon_{zz} - \epsilon_{xx}} \left( \epsilon_{zz} - \frac{\epsilon_{xx}\epsilon_{zz}}{\epsilon_{yy}} \right) \approx 0,128 \quad (155)$$