

Some techniques for compensating the defects:	
- linearization processes are realizable with digital efectronics	
- the material forming the sensor is physically organ	ized
- the material forming the sensor is physically organ to maximize the pensitivity of the device to the target variable and to minimize the response t	5
- Use sensor array approach	
e.g. chemiresistors	
Solder pads  Laser slots Dielectric layer	
Platinum heater Electrode	
Fig. 7.2. An example of an array of chemiresistors fabricated using thick-film techniques. The slots are cut by a laser and help to isolate each sensor site from its neighbors	
neignors	
- use filters (analog or digital)	
- positioning is critical	ALPS
- the entire compensation and communications system can be constructed in single-chip form	7
- prefer self-test and auto-calibration features	2

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- · Actuators: - output quantity is an energy or power, - input of the actuator is driven electrically whenever possible connected in series with a power provider (power amplifier) considerations required control authority (amount of control force, moment, strain or displacement, etc.) power consumption, frequency response, and physical constraints such as size and mounting requirements, · Smart Actuators: -solid-state actuators: piezoelectric actuators,
  shape memory actuators, magnetostrictive actuators
  - actuators with controllable fluido (smart fluido):
    magnetorheological fluid actuators,
    electrorheological fluid actuators

## **Transduction Devices for Adaptive Structures**

- Accelerometer (sensor)
- Electrodynamic shaker (actuator)
- Electrorheological fluid (actuator)
- Electrostrictive material (actuator)
- Magnetorheological fluid (actuator)
- Magnetostrictive material (actuator)
- Optical fibers (sensor)
- Piezoelectric material (actuator or sensor)
- Shape memory alloy (actuator or sensor)
- Strain gauge (sensor)

· Piezoelectric Actuators / Sensors

Constitutive egs:

$$\begin{cases} D = dT + \mathcal{E}^T E \\ S = s^E T + d^t E \end{cases}$$

 $\begin{cases}
E = -gT + \beta^T D \\
S = S^p T + g^t D
\end{cases}$ 

where g piezoelectric constants

PT impermittivity constants for constant T

50 elasticity matrix for constant D

From eg	(2)		
indi	uced strain	$S_j = dij E_i$	(a)
From eq.	(/)		
whe	E = 0	(short circuit)	
		$D_{\lambda} = d_{\lambda} \nabla_{\lambda}$	(6)
		Di=dy Ti	(b)
4/ 1/	- ( "		
/ne s	train" cons	stante d	,
·			
- an	neasure of the	he strain produced	ey an applied electric
	Lie	eld ( The Motor (	Effect)
-an	reasure of	the short wrecut	charge density to
The second secon	the applica	ed stress (The Ge	nerator Effect)
Ex. 10 00 (3	?)		
From eq. (3			
	7-0	(2404 (2) (4)	
wher	) - 0 (	open circuit)	
	T		
		E = - 9 1/1 /	(C)
The "	voltage" c	onstants g	
		•	(1 (
- a )	measure of	the electric field	d (open circuit)
	by an appli	ed mechanical str	ess.
	• •		

From eq. (4),

induced strain

Sj= gij Di

(d)

From (a) - (d).

d = strawn developed
opplied electric field

= short circuit charge density

applied mechanical stress

g = Open circuit electric field

applied mechanical stress

= Strain developed applied charge density

\* Actuators need high "strain" constants d

\* Sensors need high "voltage" constants g

$$933 = 24 \times 10^{-3} \text{ V·m/N}$$

$$d_{33} = 390 \times 10^{-12} \text{ m/V}$$

## Voltage-Force relationship

$$V = EL$$
 and  $T = \frac{F}{A}$ 

$$E = -g_{33}T \Rightarrow V = -g_{33} \stackrel{L}{=} F$$

$$S = d_{33} \in = d_{33} \frac{V}{L} = \frac{\Delta L}{L}$$

$$\Rightarrow \Delta L = d_{33} V$$