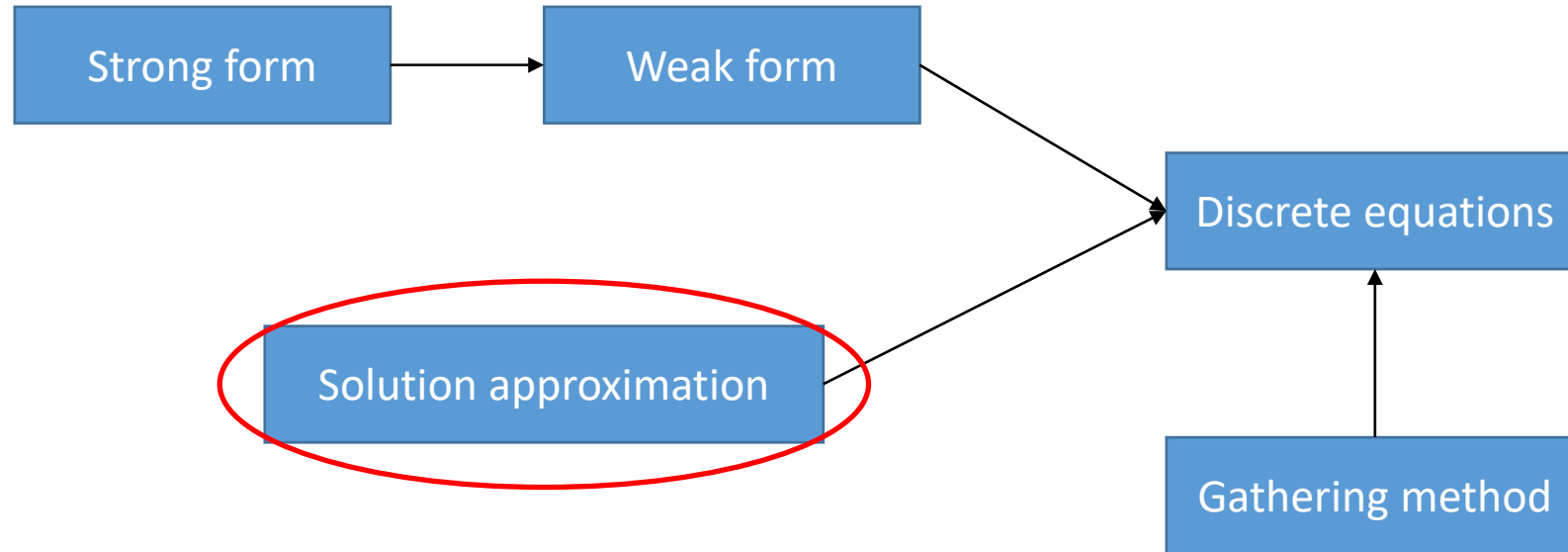


Computational Mechanics

Chapter 7 Trial Solutions, Weight Functions and Gauss Quadrature for Multidimensional Problems



Components for Formulation FEM Equations



Completeness and Continuity Requirement

- Completeness – approximation of solutions and (1st order) derivatives converge to arbitrary constants.
- 2D Completeness examination by the Pascal's triangle:

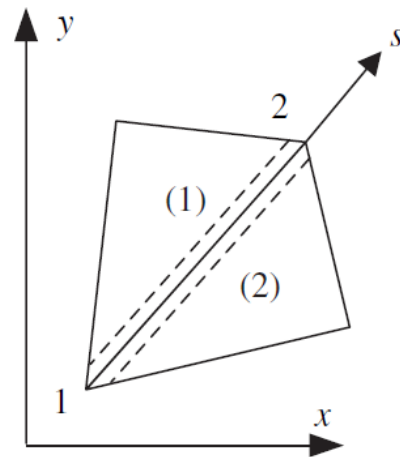
		1		constant
	x		y	linear
x ²		xy		quadratic
x ³	x ² y	xy ²	y ³	cubic

(a) $\theta^e(x, y) = \alpha_1^e + \alpha_2^e x + \alpha_3^e y$ ✓ Linear

(b) $\theta^e(x, y) = \alpha_1^e + \alpha_2^e x + \alpha_3^e y^2$ ✗

(c) $\theta^e(x, y) = \underbrace{\alpha_1^e + \alpha_2^e x + \alpha_3^e y}_{\text{Linear}} + \alpha_4^e x^2 y^2 + \alpha_5^e xy + \alpha_6^e y^3$ ✗

- Continuity - C^0 at the interfaces between elements:

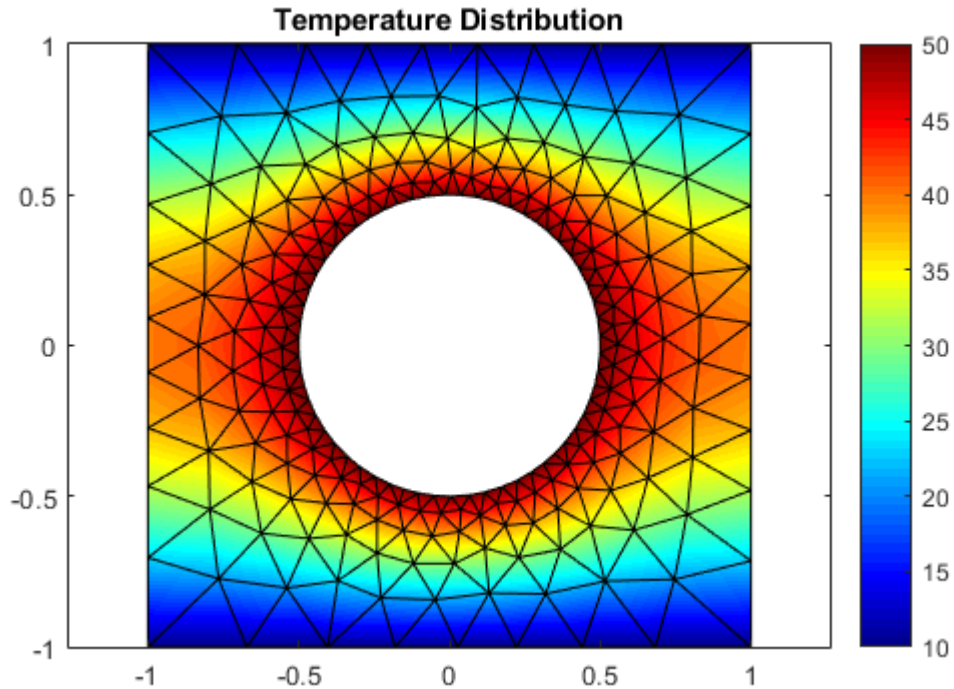


$$\theta^{(1)}(s) = \theta^{(2)}(s)$$

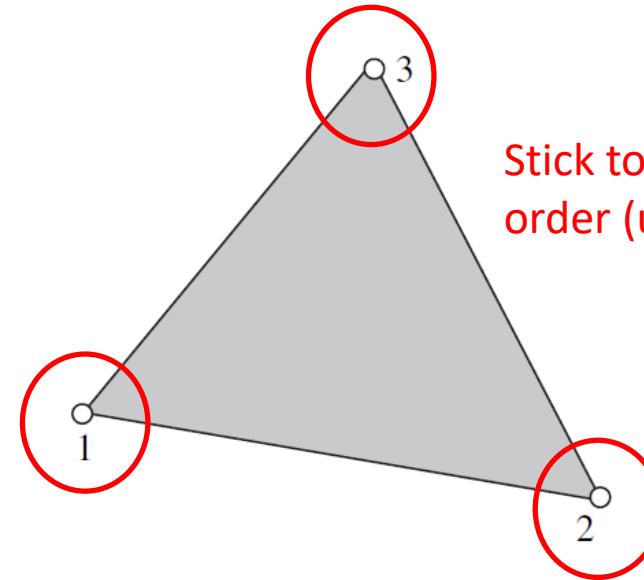


Introduction to 3-Node Triangular Elements

- Triangular elements handle **complex geometry**:



Triangular elements for heat conduction analysis [1]



Stick to the same numbering order (usually counterclockwise)

- Approximation of **linear** 2D elements:

$$\theta^e(x, y) = \alpha_0^e + \alpha_1^e x + \alpha_2^e y = [1 \quad x \quad y] \begin{bmatrix} \alpha_0^e \\ \alpha_1^e \\ \alpha_2^e \end{bmatrix} = \mathbf{p} \boldsymbol{\alpha}^e$$

3 constants – 3 nodes
in triangular elements



[1] <https://numfactory.upc.edu/web/FiniteElements.html>

Shape Functions of 3-Node Triangular Elements (1/2)

$$\theta^e(x, y) = [1 \quad x \quad y] \begin{bmatrix} \alpha_0^e \\ \alpha_1^e \\ \alpha_2^e \end{bmatrix} = \mathbf{p}(x, y) \cdot \boldsymbol{\alpha}^e$$

- Nodal value conditions:

$$\theta_1^e = [1 \quad x_1^e \quad y_1^e] \begin{bmatrix} \alpha_0^e \\ \alpha_1^e \\ \alpha_2^e \end{bmatrix}$$

$$\theta_2^e = [1 \quad x_2^e \quad y_2^e] \begin{bmatrix} \alpha_0^e \\ \alpha_1^e \\ \alpha_2^e \end{bmatrix}$$

$$\theta_3^e = [1 \quad x_3^e \quad y_3^e] \begin{bmatrix} \alpha_0^e \\ \alpha_1^e \\ \alpha_2^e \end{bmatrix}$$

$$\Rightarrow \underbrace{\begin{bmatrix} \theta_1^e \\ \theta_2^e \\ \theta_3^e \end{bmatrix}}_{\mathbf{d}^e} = \underbrace{\begin{bmatrix} 1 & x_1^e & y_1^e \\ 1 & x_2^e & y_2^e \\ 1 & x_3^e & y_3^e \end{bmatrix}}_{\mathbf{M}^e} \underbrace{\begin{bmatrix} \alpha_0^e \\ \alpha_1^e \\ \alpha_2^e \end{bmatrix}}_{\boldsymbol{\alpha}^e}$$

$$\Rightarrow \boldsymbol{\alpha}^e = (\mathbf{M}^e)^{-1} \cdot \mathbf{d}^e$$

$$\Rightarrow \theta^e(x, y) = \mathbf{p}(x, y) \cdot \boldsymbol{\alpha}^e = \underbrace{\mathbf{p}(x, y) \cdot (\mathbf{M}^e)^{-1}}_{\mathbf{N}^e(x, y)} \cdot \mathbf{d}^e$$

$$\Rightarrow \mathbf{p}_{1 \times 3} \cdot (\mathbf{M}^e)^{-1}_{3 \times 3} = \mathbf{N}^e_{1 \times 3} = [N_1^e \quad N_2^e \quad N_3^e]$$



Shape Functions of 3-Node Triangular Elements (2/2)

$$[N_1^e \quad N_2^e \quad N_3^e] = \mathbf{p} \cdot (\mathbf{M}^e)^{-1} = [1 \quad x \quad y] \begin{bmatrix} 1 & x_1^e & y_1^e \\ 1 & x_2^e & y_2^e \\ 1 & x_3^e & y_3^e \end{bmatrix}^{-1}$$

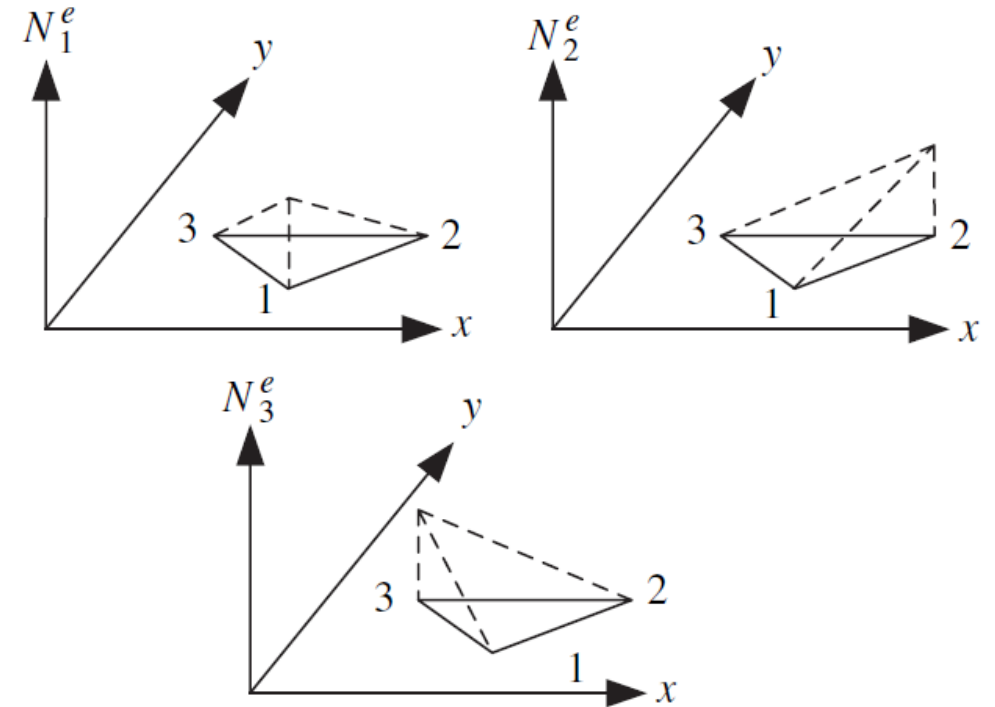
- **Kronecker delta** property of shape functions:

$$N_I^e(x_J^e, y_J^e) = \delta_{IJ}$$

$$\Rightarrow N_1^e = \frac{1}{2A^e} [x_2^e y_3^e - x_3^e y_2^e + (y_2^e - y_3^e)x + (x_3^e - x_2^e)y]$$

$$N_2^e = \frac{1}{2A^e} [x_3^e y_1^e - x_1^e y_3^e + (y_3^e - y_1^e)x + (x_1^e - x_3^e)y]$$

$$N_3^e = \frac{1}{2A^e} [x_1^e y_2^e - x_2^e y_1^e + (y_1^e - y_2^e)x + (x_2^e - x_1^e)y]$$



B^e of 3-Node Triangular Elements

$$\mathbf{N}^e = [N_1^e \quad N_2^e \quad N_3^e], \quad N_1^e = \frac{1}{2A^e} [x_2^e y_3^e - x_3^e y_2^e + (y_2^e - y_3^e)x + (x_3^e - x_2^e)y]$$

$$N_2^e = \frac{1}{2A^e} [x_3^e y_1^e - x_1^e y_3^e + (y_3^e - y_1^e)x + (x_1^e - x_3^e)y], N_3^e = \frac{1}{2A^e} [x_1^e y_2^e - x_2^e y_1^e + (y_1^e - y_2^e)x + (x_2^e - x_1^e)y]$$

$$\theta^e(x, y) = \mathbf{N}^e \cdot \mathbf{d}^e = N_1^e \theta_1 + N_2^e \theta_2 + N_3^e \theta_3$$

- Gradient of the trial solution:

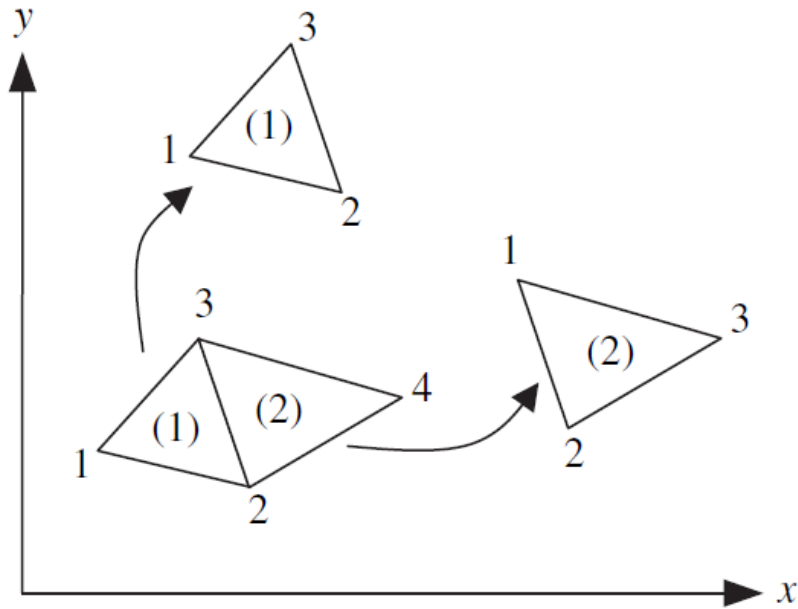
Linear elements lead to constant \mathbf{B}^e that are only dependent on element coordinates

$$\nabla \theta = \begin{bmatrix} \frac{\partial \theta}{\partial x} \\ \frac{\partial \theta}{\partial y} \end{bmatrix} = \begin{bmatrix} \frac{\partial N_1^e}{\partial x} \theta_1 + \frac{\partial N_2^e}{\partial x} \theta_2 + \frac{\partial N_3^e}{\partial x} \theta_3 \\ \frac{\partial N_1^e}{\partial y} \theta_1 + \frac{\partial N_2^e}{\partial y} \theta_2 + \frac{\partial N_3^e}{\partial y} \theta_3 \end{bmatrix} = \begin{bmatrix} \frac{\partial N_1^e}{\partial x} & \frac{\partial N_2^e}{\partial x} & \frac{\partial N_3^e}{\partial x} \\ \frac{\partial N_1^e}{\partial y} & \frac{\partial N_2^e}{\partial y} & \frac{\partial N_3^e}{\partial y} \end{bmatrix} \begin{bmatrix} \theta_1 \\ \theta_2 \\ \theta_3 \end{bmatrix} = \mathbf{B}^e \mathbf{d}^e$$

$$\frac{1}{2A^e} \begin{bmatrix} (y_2^e - y_3^e) & (y_3^e - y_1^e) & (y_1^e - y_2^e) \\ (x_3^e - x_2^e) & (x_1^e - x_3^e) & (x_2^e - x_1^e) \end{bmatrix}$$



Global Continuity of 3-Node Triangular Elements



- Parametric equations for global edge 2-3:

$$x = x_2 + (x_3 - x_2)s, \quad y = y_2 + (y_3 - y_2)s$$

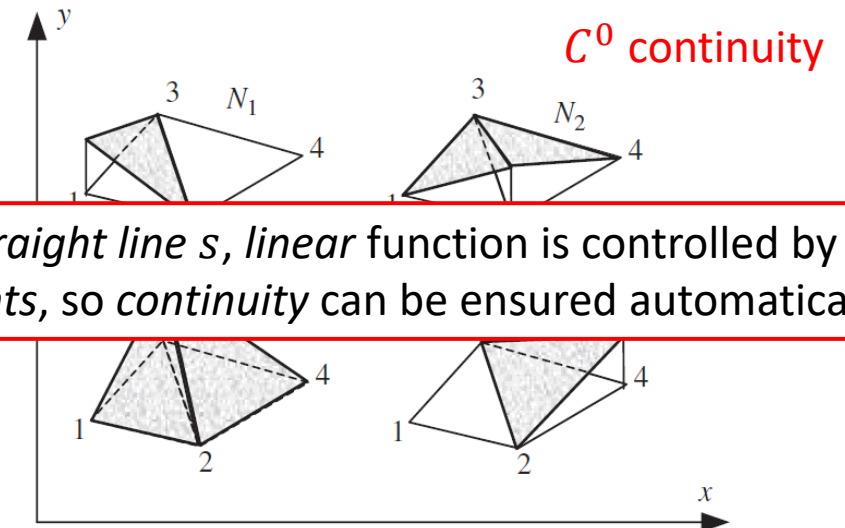
$$0 \leq s \leq 1$$

- Linear shape functions on global edge 2-3:

$$\theta^{(1)} = \beta_0^{(1)} + \beta_1^{(1)}s, \quad \theta^{(2)} = \beta_0^{(2)} + \beta_1^{(2)}s$$
- Nodal value conditions:

$$\theta_2 = \beta_0^{(1)} = \beta_0^{(2)}, \quad \theta_3 = \beta_0^{(1)} + \beta_1^{(1)} = \beta_0^{(2)} + \beta_1^{(2)}$$

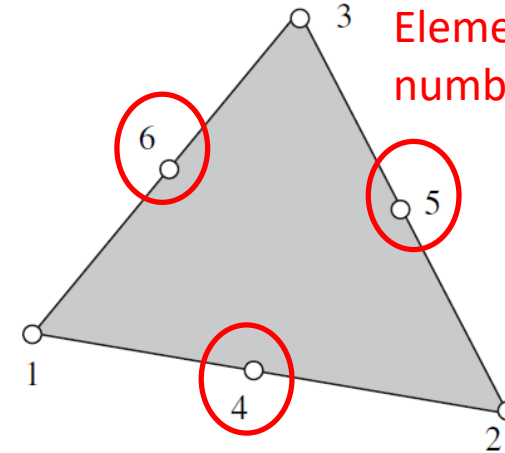
$$\Rightarrow \beta_0^{(1)} = \beta_0^{(2)} = \theta_2, \quad \beta_1^{(1)} = \beta_1^{(2)} = \theta_3 - \theta_2$$



Higher Order Triangular Elements

	1		constant
	x	y	linear
x^2	xy	y^2	quadratic
x^3	x^2y	xy^2	y^3 cubic

Similar format



Elements have the same numbering pattern

- Quadratic element:

$$\theta^e = \alpha_1^e + \alpha_2^e x + \alpha_3^e y + \alpha_4^e x^2 + \alpha_5^e xy + \alpha_6^e y^2$$

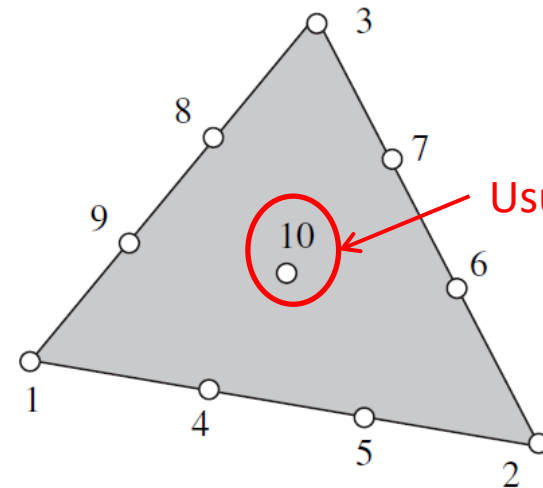
- Projection to a **straight line** along the edge:

$$x = a + bs, \quad y = c + ds$$

$$\Rightarrow \theta^e = \underline{\beta_0^e + \beta_1^e s + \beta_2^e s^2}$$

3 nodes on the edges are essential for continuity.

- Inner nodes** for higher order elements (seldomly used as not well conditioned):

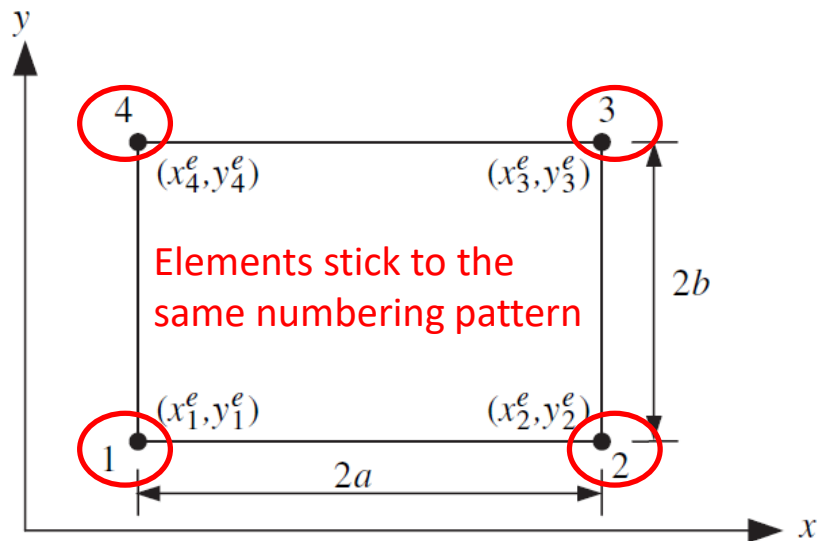


Usually centroid

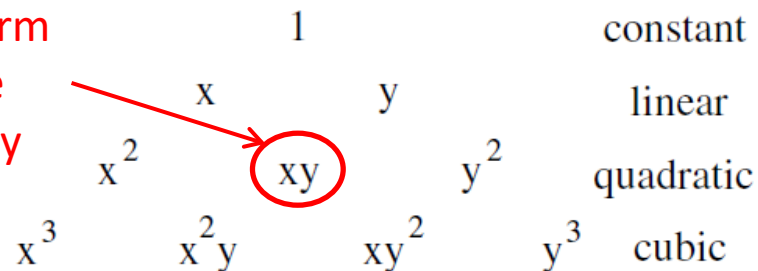


4-Node Rectangular Elements

- Avoid **shear locking** issue
- Counterclockwise nodal numbering is often used:



Bilinear term
for edge
continuity



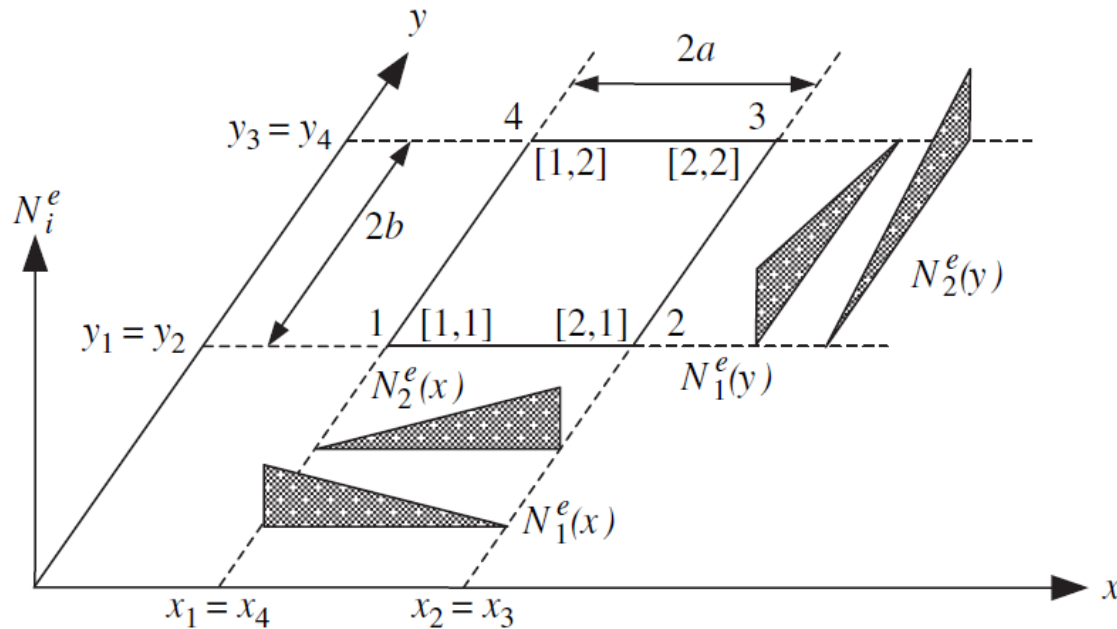
- Element approximation:

$$\theta^e(x, y) = \alpha_1^e + \alpha_2^e x + \alpha_3^e y + \alpha_4^e xy$$

- **Direct** shape function **construction** is essential to obtain $(\alpha_1^e, \alpha_2^e, \alpha_3^e, \alpha_4^e) = \alpha(\theta_1^e, \theta_2^e, \theta_3^e, \theta_4^e)$ for **manual calculation**.

Tensor Product Method

- **Increase dimension** and **keep interpolation** by multiplication of shape functions:



- Shape functions in **dyadic** notation:

$$N_{[I,J]}^e(x, y) = N_I^e(x)N_J^e(y)$$

- **Kronecker delta** properties:

$$N_{[I,J]}^e(x_M^e, y_L^e) = N_I^e(x_M^e)N_J^e(y_L^e) = \delta_{IM}\delta_{JL}$$

- Shape functions in regular notation:

$$N_1^e(x, y) = \frac{x - x_2^e}{x_1^e - x_2^e} \frac{y - y_4^e}{y_1^e - y_4^e} = \frac{1}{A^e} (x - x_2^e)(y - y_4^e)$$

$$N_2^e(x, y) = \frac{x - x_1^e}{x_2^e - x_1^e} \frac{y - y_4^e}{y_1^e - y_4^e} = \frac{-1}{A^e} (x - x_1^e)(y - y_4^e)$$

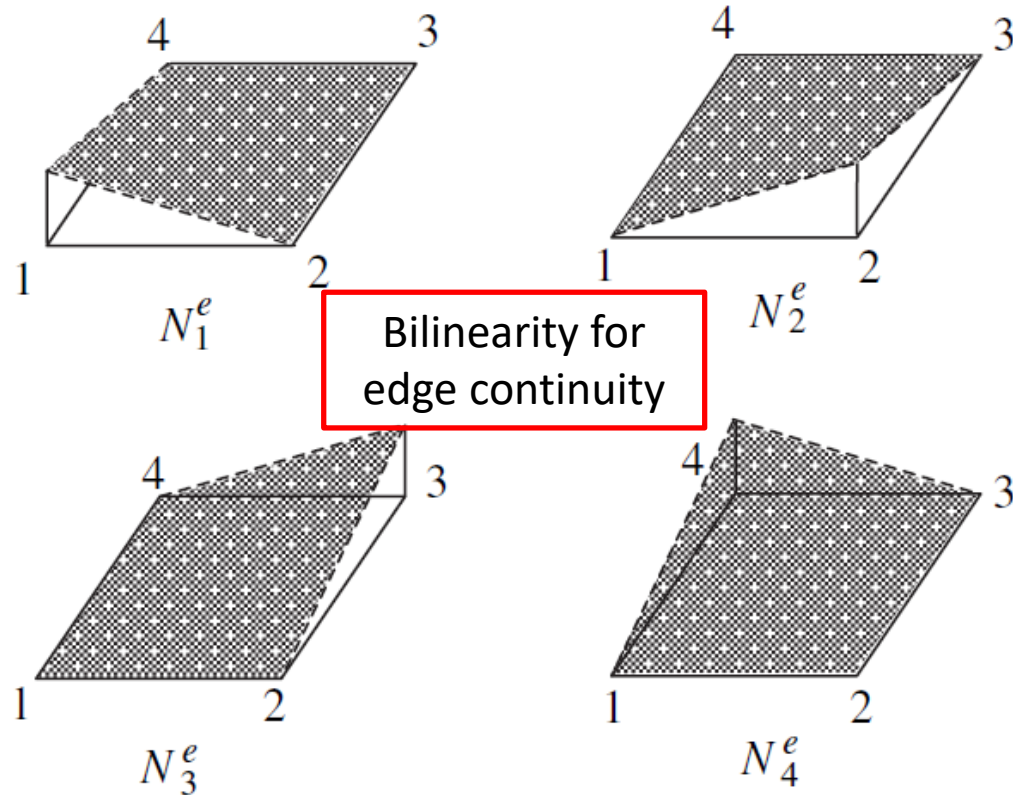
$$N_3^e(x, y) = \frac{x - x_1^e}{x_2^e - x_1^e} \frac{y - y_1^e}{y_4^e - y_1^e} = \frac{1}{A^e} (x - x_1^e)(y - y_1^e)$$

$$N_4^e(x, y) = \frac{x - x_2^e}{x_1^e - x_2^e} \frac{y - y_1^e}{y_4^e - y_1^e} = \frac{-1}{A^e} (x - x_2^e)(y - y_1^e)$$

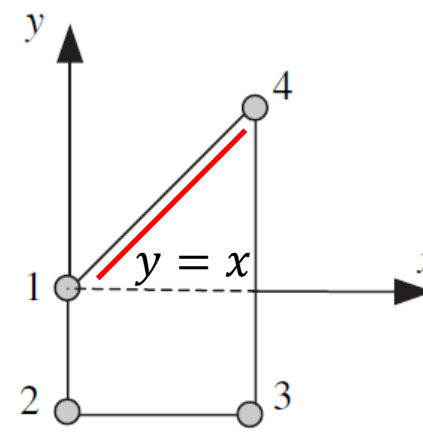


Properties of Bilinear Shape Functions

- Geometry of the shape functions:



- Drawbacks of the specific shape functions – cannot work for **arbitrary bilateral elements**:



$$N_1^e(x, y) = \frac{1}{A^e} (x - x_2^e)(y - y_4^e)$$

$$N_2^e(x, y) = \frac{-1}{A^e} (x - x_1^e)(y - y_4^e)$$

$$N_3^e(x, y) = \frac{1}{A^e} (x - x_1^e)(y - y_1^e)$$

$$N_4^e(x, y) = \frac{-1}{A^e} (x - x_2^e)(y - y_1^e)$$

The *quadratic function* N_4^e on the edge needs *3 nodes on the edge* to ensure continuity



Introduction to Isoparametric Elements

- Linear mapping from **physical domains** to a **regular parent domain**:

$$x = x_1^e N_1^e(\xi) + x_2^e N_2^e(\xi) = x_1^e \frac{1-\xi}{2} + x_2^e \frac{1+\xi}{2}, \quad \xi \in [-1, 1]$$

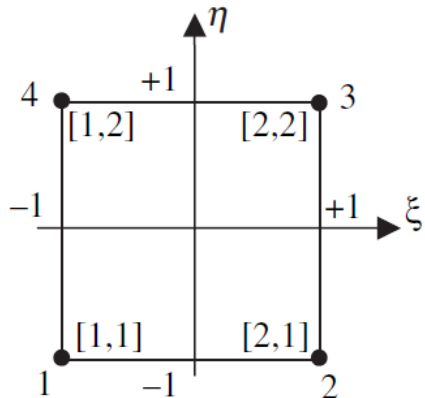
- Linear **approximation** of θ **by** ξ instead of x – direct construction:

$$\theta^e = \theta_1^e N_1^e(\xi) + \theta_2^e N_2^e(\xi) = \theta_1^e \frac{1-\xi}{2} + \theta_2^e \frac{1+\xi}{2}, \quad \xi \in [-1, 1]$$



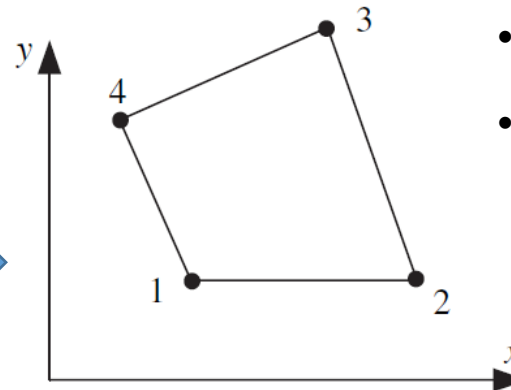
Isoparametric element

- Quadrilateral elements in the regular **parent domain**:



$$x = N^{4Q}(\xi, \eta) \mathbf{x}^e$$

$$y = N^{4Q}(\xi, \eta) \mathbf{y}^e$$



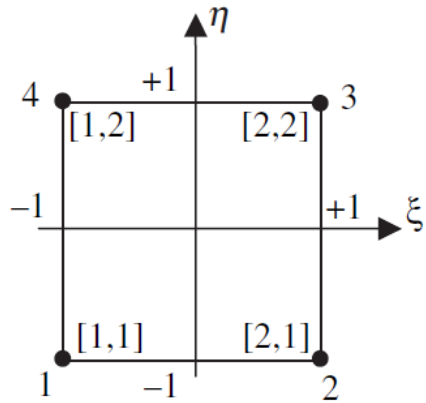
- $N^{4Q}(\xi, \eta)$: 4-node shape functions.

- $\mathbf{x}^e = [x_1^e \quad x_2^e \quad x_3^e \quad x_4^e]$

- $\mathbf{y}^e = [y_1^e \quad y_2^e \quad y_3^e \quad y_4^e]$

- Physical coordinates are mapped by the same functions as those for trial solutions
- Straight edges to straight edges

Components in $N^{4Q}(\xi, \eta)$



- Tensor product method for shape functions:

$$N_1^e(\xi, \eta) = \frac{1}{4}(\xi - 1)(\eta - 1)$$

$$N_2^e(\xi, \eta) = \frac{-1}{4}(\xi + 1)(\eta - 1)$$

$$N_3^e(\xi, \eta) = \frac{1}{4}(\xi + 1)(\eta + 1)$$

$$N_4^e(\xi, \eta) = \frac{-1}{4}(\xi - 1)(\eta + 1)$$

Independent of physical nodal positions.

- Trial solution approximation:

$$\theta^e = N^{4Q}(\xi, \eta) \mathbf{d}^e$$

Same as mapping – isoparametric.

- Bilinearity of shape functions:

$$\theta^e(\xi, \eta) = \alpha_1^e + \alpha_2^e \xi + \alpha_3^e \eta + \alpha_4^e \xi \eta$$

Linear on the edge – C^0 continuity along physical edges



Derivative of Isoparametric Shape Functions (1/2)

$$\theta^e = \mathbf{N}^{4Q}(\xi, \eta) \mathbf{d}^e = \sum_{i=1}^4 N_i^{4Q} d_i^e$$

- Gradient of the trial solution:

$$\nabla \theta^e = \begin{bmatrix} \frac{\partial \theta^e}{\partial x} \\ \frac{\partial \theta^e}{\partial y} \end{bmatrix} = \begin{bmatrix} \frac{\partial \sum_{i=1}^4 N_i^{4Q} d_i^e}{\partial x} \\ \frac{\partial \sum_{i=1}^4 N_i^{4Q} d_i^e}{\partial y} \end{bmatrix} = \begin{bmatrix} \frac{\partial N_1^{4Q}}{\partial x} & \frac{\partial N_2^{4Q}}{\partial x} & \frac{\partial N_3^{4Q}}{\partial x} & \frac{\partial N_4^{4Q}}{\partial x} \\ \frac{\partial N_1^{4Q}}{\partial y} & \frac{\partial N_2^{4Q}}{\partial y} & \frac{\partial N_3^{4Q}}{\partial y} & \frac{\partial N_4^{4Q}}{\partial y} \end{bmatrix} \begin{bmatrix} d_1^e \\ d_2^e \\ d_3^e \\ d_4^e \end{bmatrix} = \mathbf{B}^e \mathbf{d}^e$$

- Derivatives on different domains – **chain rule**:

$$\frac{\partial N_I^{4Q}}{\partial \xi} = \frac{\partial N_I^{4Q}}{\partial x} \frac{\partial x}{\partial \xi} + \frac{\partial N_I^{4Q}}{\partial y} \frac{\partial y}{\partial \xi}, \quad \frac{\partial N_I^{4Q}}{\partial \eta} = \frac{\partial N_I^{4Q}}{\partial x} \frac{\partial x}{\partial \eta} + \frac{\partial N_I^{4Q}}{\partial y} \frac{\partial y}{\partial \eta}$$

$$\Rightarrow \begin{bmatrix} \frac{\partial N_I^{4Q}}{\partial \xi} \\ \frac{\partial N_I^{4Q}}{\partial \eta} \end{bmatrix} = \underbrace{\begin{bmatrix} \frac{\partial x}{\partial \xi} & \frac{\partial y}{\partial \xi} \\ \frac{\partial x}{\partial \eta} & \frac{\partial y}{\partial \eta} \end{bmatrix}}_{\text{Jacobian } \mathbf{J}^e} \begin{bmatrix} \frac{\partial N_I^{4Q}}{\partial x} \\ \frac{\partial N_I^{4Q}}{\partial y} \end{bmatrix}$$



Derivative of Isoparametric Shape Functions (2/2)

$$\begin{bmatrix} \frac{\partial N_I^{4Q}}{\partial \xi} \\ \frac{\partial N_I^{4Q}}{\partial \eta} \end{bmatrix} = \begin{bmatrix} \frac{\partial x}{\partial \xi} & \frac{\partial y}{\partial \xi} \\ \frac{\partial x}{\partial \eta} & \frac{\partial y}{\partial \eta} \end{bmatrix} \begin{bmatrix} \frac{\partial N_I^{4Q}}{\partial x} \\ \frac{\partial N_I^{4Q}}{\partial y} \end{bmatrix} = \mathbf{J}^e \begin{bmatrix} \frac{\partial N_I^{4Q}}{\partial x} \\ \frac{\partial N_I^{4Q}}{\partial y} \end{bmatrix}$$

$$\Rightarrow \underbrace{\begin{bmatrix} \frac{\partial N_I^{4Q}}{\partial x} \\ \frac{\partial N_I^{4Q}}{\partial y} \end{bmatrix}}_{\nabla N_I^{4Q}} = (\mathbf{J}^e)^{-1} \underbrace{\begin{bmatrix} \frac{\partial N_I^{4Q}}{\partial \xi} \\ \frac{\partial N_I^{4Q}}{\partial \eta} \end{bmatrix}}_{\mathbf{G} N_I^{4Q}}$$

$$\Rightarrow \nabla N^{4Q} = (\mathbf{J}^e)^{-1} \mathbf{G} N^{4Q}$$

$$x = \mathbf{N}^{4Q}(\xi, \eta) \mathbf{x}^e, \quad y = \mathbf{N}^{4Q}(\xi, \eta) \mathbf{y}^e$$

$$\Rightarrow \mathbf{J}^e = \begin{bmatrix} \frac{\partial \mathbf{N}^{4Q} \mathbf{x}^e}{\partial \xi} & \frac{\partial \mathbf{N}^{4Q} \mathbf{y}^e}{\partial \xi} \\ \frac{\partial \mathbf{N}^{4Q} \mathbf{x}^e}{\partial \eta} & \frac{\partial \mathbf{N}^{4Q} \mathbf{y}^e}{\partial \eta} \end{bmatrix} = \mathbf{G} \mathbf{N}^{4Q} [\mathbf{x}^e \quad \mathbf{y}^e]$$

$$\mathbf{B}^e = \begin{bmatrix} \frac{\partial N_1^{4Q}}{\partial x} & \frac{\partial N_2^{4Q}}{\partial x} & \frac{\partial N_3^{4Q}}{\partial x} & \frac{\partial N_4^{4Q}}{\partial x} \\ \frac{\partial N_1^{4Q}}{\partial y} & \frac{\partial N_2^{4Q}}{\partial y} & \frac{\partial N_3^{4Q}}{\partial y} & \frac{\partial N_4^{4Q}}{\partial y} \end{bmatrix} = \nabla \mathbf{N}^{4Q}$$

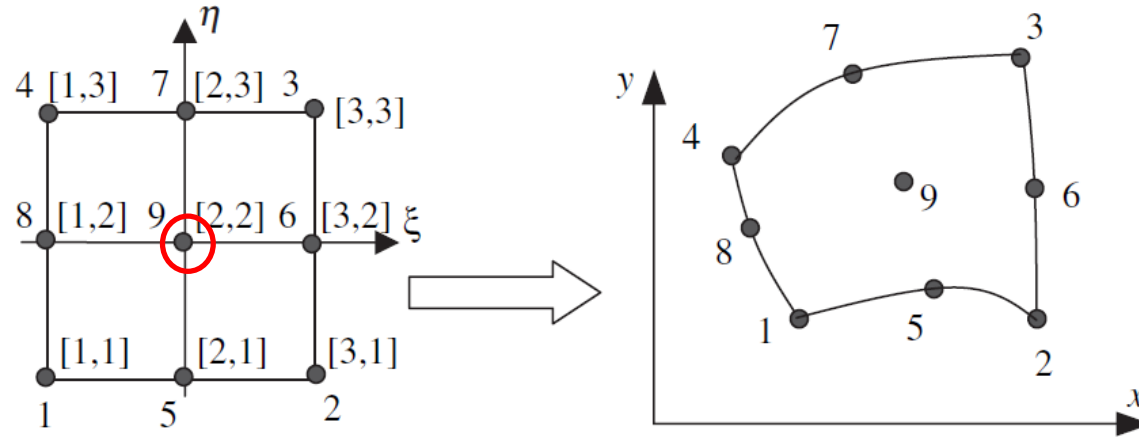
$$\Rightarrow \underline{\mathbf{B}^e} = \nabla \mathbf{N}^{4Q} = \underline{(\mathbf{J}^e)^{-1}} \mathbf{G} \mathbf{N}^{4Q}$$

Depend on physical domains



Higher Order (Quadratic) Quadrilateral Elements

- 3 nodes on *edges* for continuity
- Node 9 for unique solution and *physical coordinates*



$$N_K^{9Q}(\xi, \eta) = N_I^{3L}(\xi) N_J^{3L}(\eta)$$

$$x(\xi, \eta) = N^{9Q}(\xi, \eta) \mathbf{x}^e, \quad y(\xi, \eta) = N^{9Q}(\xi, \eta) \mathbf{y}^e$$

- Mapping of **curved edges** (1-2 edge as an example):

$$x(\xi, \eta = \text{const}) = \alpha_0^x + \alpha_1^x \xi + \alpha_2^x \xi^2, \quad y(\xi, \eta = \text{const}) = \alpha_0^y + \alpha_1^y \xi + \alpha_2^y \xi^2$$

Nonlinear (quadratic) relationship between x and y , leading to fewer elements for curved boundary *approximation*



Completeness of Isoparametric Elements

- Isoparametric elements are **at least** linear complete – **1D** quadratic element example:

$$x(\xi) = \sum_{I=1}^3 x_I^e N_I^{3L}(\xi) = x_1^e \frac{1}{2} \xi(\xi - 1) + x_2^e (1 - \xi^2) + x_3^e \frac{1}{2} \xi(\xi + 1)$$

$$\theta^e(\xi) = \sum_{I=1}^3 \theta_I^e N_I^{3L}(\xi) = \theta_1^e \frac{1}{2} \xi(\xi - 1) + \theta_2^e (1 - \xi^2) + \theta_3^e \frac{1}{2} \xi(\xi + 1) \quad \boxed{\text{Linear terms?}}$$

- Assumption of a linear field:

$$\theta^e(x) = \alpha_0 + \alpha_1 x \Rightarrow \theta_I^e = \alpha_0 + \alpha_1 x_I^e$$

$$\Rightarrow \theta^e(x) = \sum_{I=1}^3 (\alpha_0 + \alpha_1 x_I^e) N_I^{3L}(\xi) = \underbrace{\alpha_0 \sum_{I=1}^3 N_I^{3L}(\xi)}_1 + \alpha_1 \underbrace{\sum_{I=1}^3 x_I^e N_I^{3L}(\xi)}_x$$

1D linear completeness satisfied, higher order may be possible



Completeness of 2D Isoparametric Elements

- Coordinate mapping and solution approximation:

$$x = \sum_{I=1}^{n_{en}} x_I^e N_I^e, \quad y = \sum_{I=1}^{n_{en}} y_I^e N_I^e, \quad \theta^e = \sum_{I=1}^{n_{en}} \theta_I^e N_I^e, \quad N_I^e = N_I^e(\xi, \eta)$$

- Assumption of a linear field:

$$\theta^e(x) = \alpha_0 + \alpha_1 x + \alpha_2 y \Rightarrow \theta_I^e = \alpha_0 + \alpha_1 x_I^e + \alpha_2 y_I^e$$

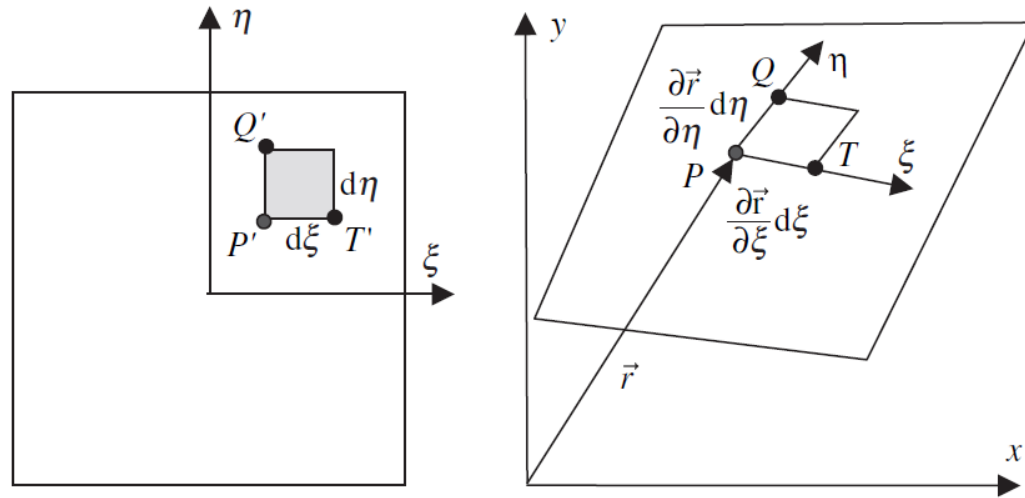
$$\theta^e = \sum_{I=1}^{n_{en}} \theta_I^e N_I^e = \sum_{I=1}^{n_{en}} (\alpha_0 + \alpha_1 x_I^e + \alpha_2 y_I^e) N_I^e = \alpha_0 \underbrace{\sum_{I=1}^{n_{en}} N_I^e}_1 + \alpha_1 \underbrace{\sum_{I=1}^{n_{en}} x_I^e N_I^e}_x + \alpha_2 \underbrace{\sum_{I=1}^{n_{en}} y_I^e N_I^e}_y$$

2D linear completeness satisfied, higher order may be possible



Gauss Quadrature for Quadrilateral Elements

- Area mapping:



$$\mathbf{r} = x\mathbf{i} + y\mathbf{j}$$

- Infinitesimal area $d\Omega$:

$$\mathbf{PT} = \frac{\partial \mathbf{r}}{\partial \xi} d\xi = \frac{\partial x}{\partial \xi} d\xi \mathbf{i} + \frac{\partial y}{\partial \xi} d\xi \mathbf{j}$$

$$\mathbf{PQ} = \frac{\partial \mathbf{r}}{\partial \eta} d\eta = \frac{\partial x}{\partial \eta} d\eta \mathbf{i} + \frac{\partial y}{\partial \eta} d\eta \mathbf{j}$$

$$\Rightarrow d\Omega = |\mathbf{PT} \times \mathbf{PQ}| = \left| \frac{\partial x}{\partial \xi} \frac{\partial y}{\partial \eta} - \frac{\partial y}{\partial \xi} \frac{\partial x}{\partial \eta} \right| d\xi d\eta = \underbrace{\begin{vmatrix} \frac{\partial x}{\partial \xi} & \frac{\partial y}{\partial \xi} \\ \frac{\partial x}{\partial \eta} & \frac{\partial y}{\partial \eta} \end{vmatrix}}_{J^e} d\xi d\eta$$

$$\Rightarrow I = \iint f(x, y) d\Omega = \iint_{(-1,1)}^{(-1,1)} f(\xi, \eta) |J^e| d\xi d\eta$$

$$\Rightarrow I = \int_{-1}^1 \left(\sum_{i=1}^{n_{gp}} W_i f(\xi_i, \eta) |J^e(\xi_i, \eta)| \right) d\eta = \dots$$

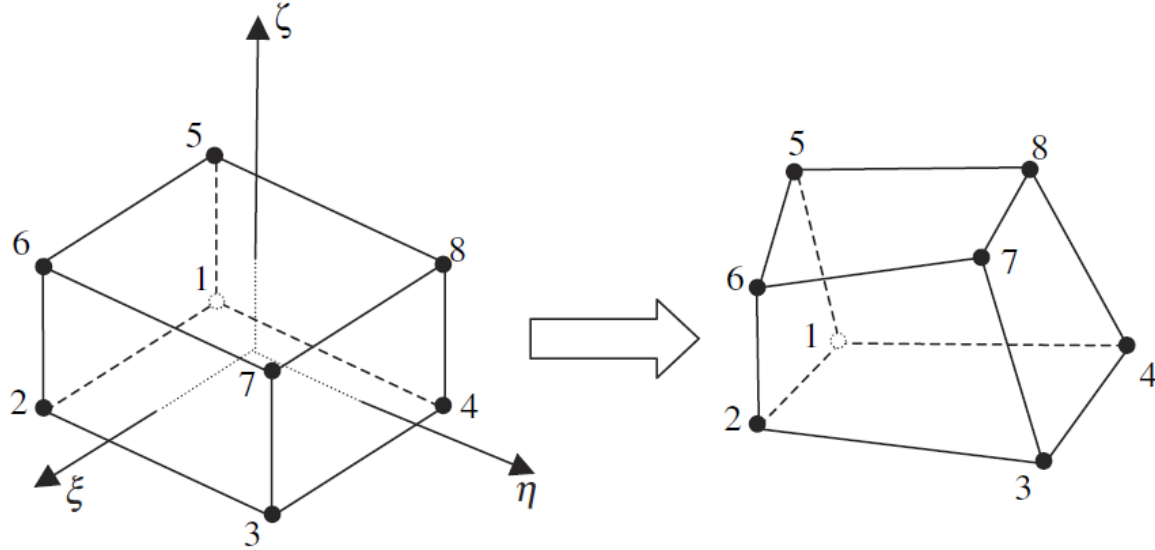
Same as 1D Gauss Quadrature



Hexahedra Elements

- Hexahedra elements are 3D expansion of 2D quadrilateral elements.
- Mapping from **regular parent** to physical domains:

$$x = N^{8H} \mathbf{x}^e, \quad y = N^{8H} \mathbf{y}^e, \quad z = N^{8H} \mathbf{z}^e$$



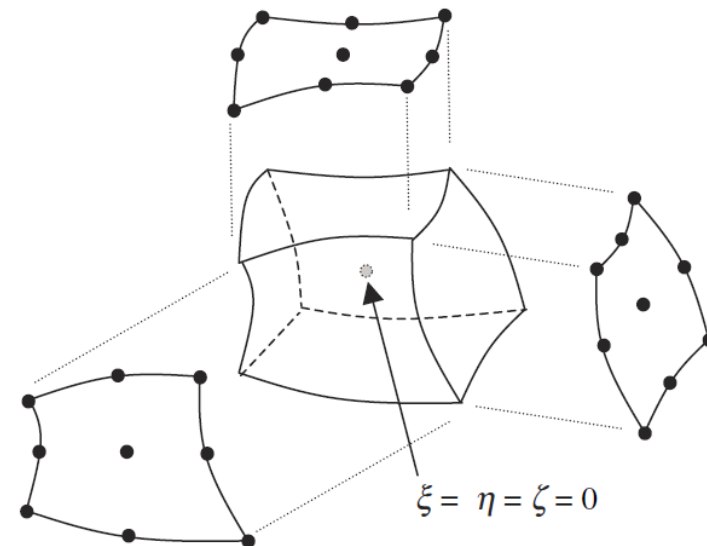
- Construction of shape functions – linear example:

$$N_L^{8H}(\xi, \eta, \varsigma) = N_I^{2L}(\xi)N_J^{2L}(\eta)N_K^{2L}(\varsigma)$$

- Solution approximation:

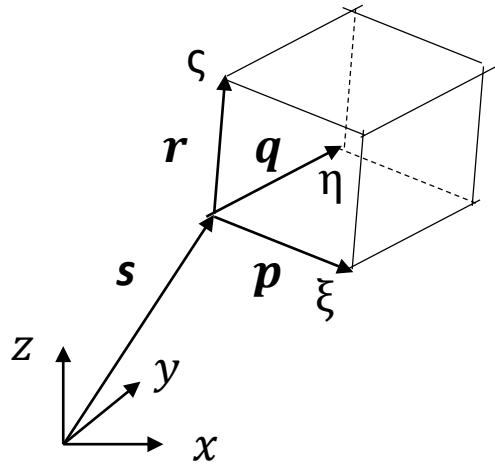
$$\theta^e = N^{8H} \mathbf{d}^e$$

- Higher order elements **approximate** curved surfaces:



Gauss integration for Hexahedral elements

- Infinitesimal volume $d\Omega$ mapping:



$$\mathbf{s} = x\mathbf{i} + y\mathbf{j} + z\mathbf{k}$$

$$\Rightarrow \mathbf{p} = \frac{\partial \mathbf{s}}{\partial \xi} d\xi = \left(\frac{\partial x}{\partial \xi} \mathbf{i} + \frac{\partial y}{\partial \xi} \mathbf{j} + \frac{\partial z}{\partial \xi} \mathbf{k} \right) d\xi$$

$$\mathbf{q} = \frac{\partial \mathbf{s}}{\partial \eta} d\eta = \left(\frac{\partial x}{\partial \eta} \mathbf{i} + \frac{\partial y}{\partial \eta} \mathbf{j} + \frac{\partial z}{\partial \eta} \mathbf{k} \right) d\eta$$

$$\mathbf{r} = \frac{\partial \mathbf{s}}{\partial \zeta} d\zeta = \left(\frac{\partial x}{\partial \zeta} \mathbf{i} + \frac{\partial y}{\partial \zeta} \mathbf{j} + \frac{\partial z}{\partial \zeta} \mathbf{k} \right) d\zeta$$

$$\Rightarrow d\Omega = |\mathbf{r} \cdot (\mathbf{p} \times \mathbf{q})| = |\mathbf{J}^e| d\xi d\eta d\zeta$$

- Gauss integration:

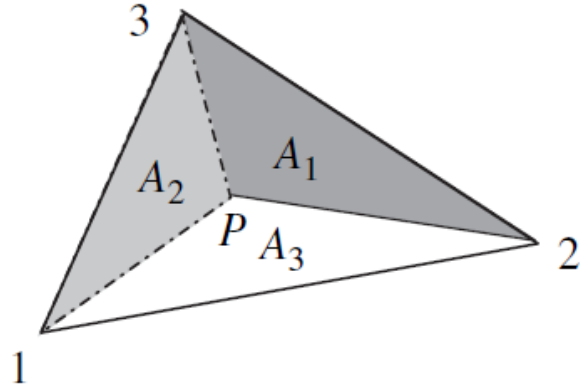
$$I = \int_{(-1,-1,-1)}^{(1,1,1)} f(\xi, \eta, \zeta) |\mathbf{J}^e| d\xi d\eta d\zeta = \dots$$

Utilize 1D Gauss Quadrature for each dimension



Triangular Coordinates for Linear Elements

- Definition of triangular coordinates:



$$\xi_I = \frac{A_I}{A} \Rightarrow \underline{\xi_1 + \xi_2 + \xi_3 = 1}$$

- Kronecker delta property:

$$\xi_I(x_j^e, y_j^e) = \delta_{IJ}$$

- Linear mapping:

$$\underline{x = x_1^e \xi_1 + x_2^e \xi_2 + x_3^e \xi_3, y = y_1^e \xi_1 + y_2^e \xi_2 + y_3^e \xi_3}$$

Linear combination of two variables
in the parent domain

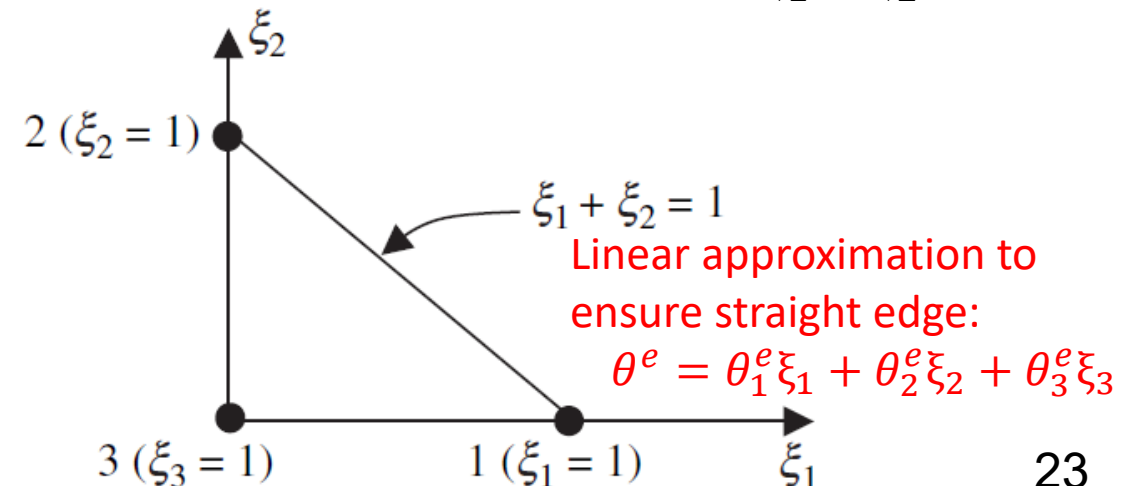
- Mapping between physical and parent domains:

$$\begin{bmatrix} 1 \\ x \\ y \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 \\ x_1^e & x_2^e & x_3^e \\ y_1^e & y_2^e & y_3^e \end{bmatrix} \begin{bmatrix} \xi_1 \\ \xi_2 \\ \xi_3 \end{bmatrix}$$

$(\mathbf{M}^e)^T$

$$\Rightarrow \begin{bmatrix} \xi_1 \\ \xi_2 \\ \xi_3 \end{bmatrix} = (\mathbf{M}^e)^{-T} \begin{bmatrix} 1 \\ x \\ y \end{bmatrix}$$

- Geometry of the parent domain on $\xi_1 - \xi_2$ plane:



The End

