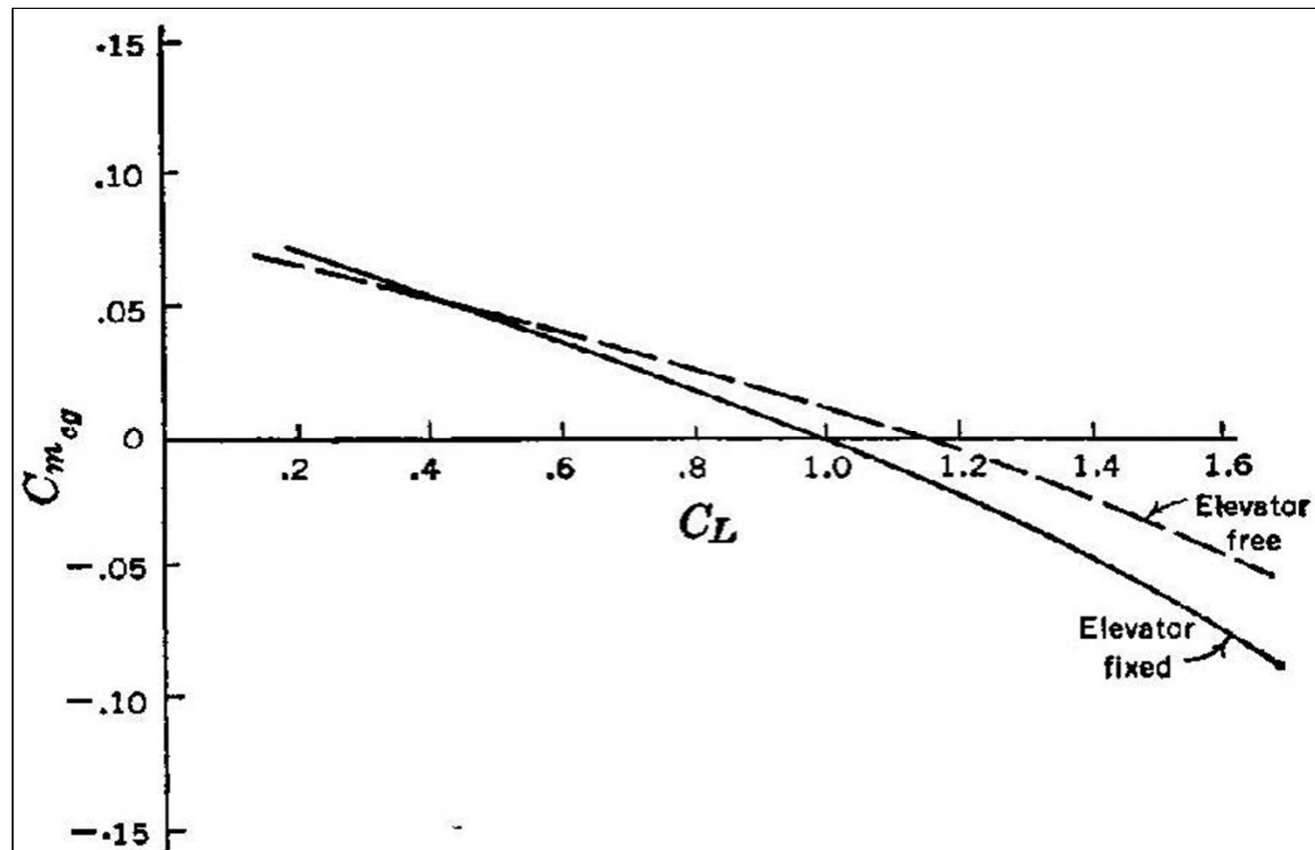




Typical Impact of Free Elevator



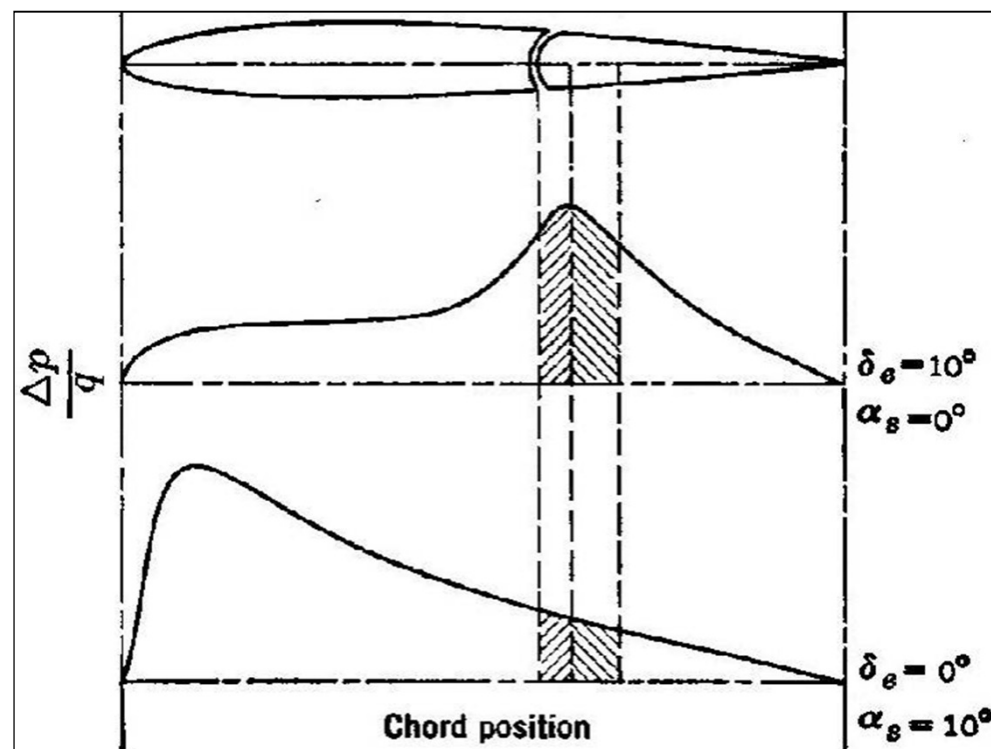


Aerodynamic Balancing Concept

In order to minimize the impact of a free **elevator** on the stability, there is a need to **minimize** its floating.

One way to achieve this is to 'aerodynamically **balance**' the elevator, by making ' $C_{h\alpha}$ ' nearly **zero**.

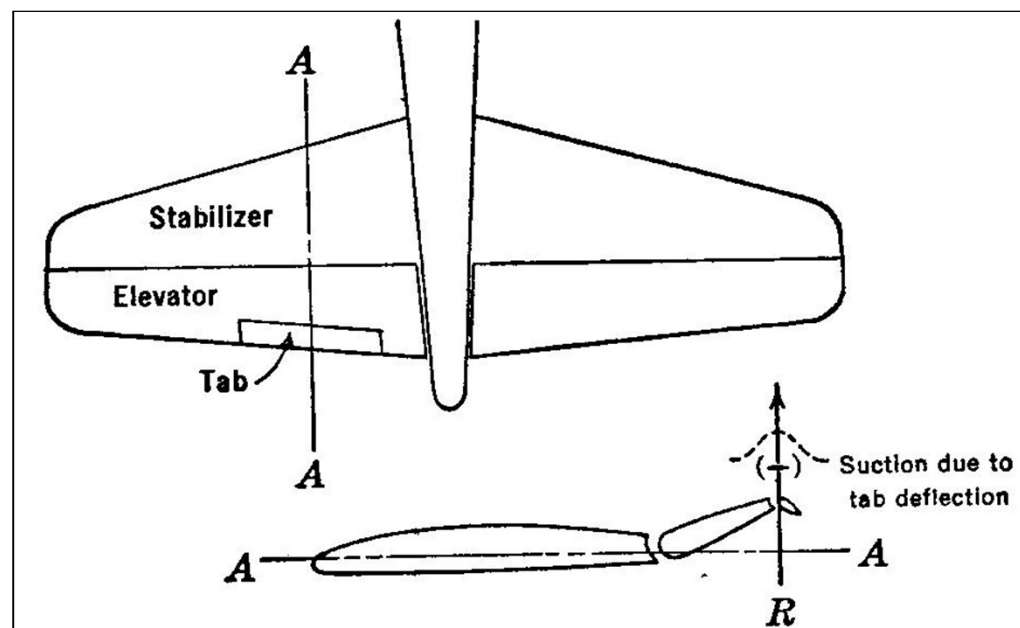
This is possible if the net resultant of forces **due** to ' α ' and ' δ ' passes through the hinge **line**, as shown alongside.





Application of Trim Tabs

Another way to prevent floating, without **shifting** the hinge line, is to add a small surface **at** the elevator trailing edge called '**tab**' or 'trim tab', as shown alongside.



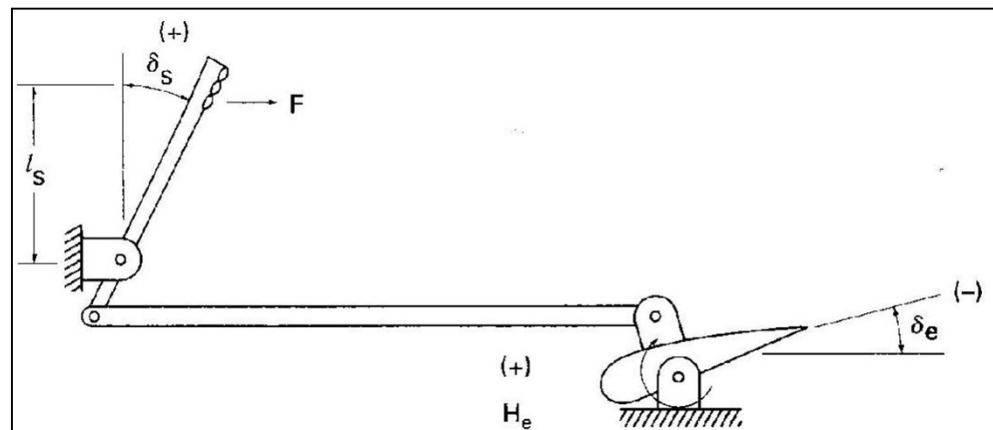


Stick Force Concept

In practice, HM is always kept small, which is **finally** cancelled through manual application of '**trim** tab'.

This is done to give the pilot a positive feel for **forces** required to change trim conditions, **which** is an important flight control system **design** criterion.

In view of the above, pilot experiences a **reaction** force while attempting to deflect the **stick**, as shown alongside.





Stick Force Formulation and Features

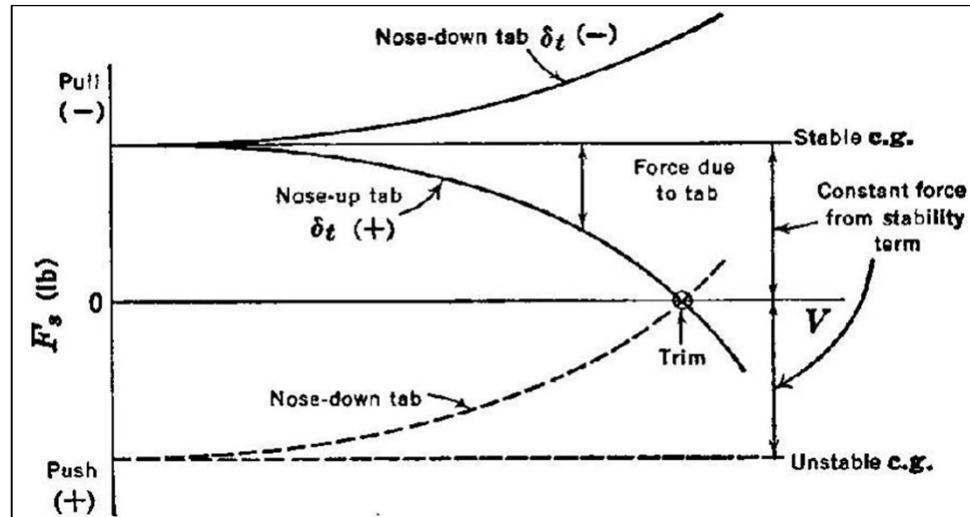
$$\text{Work Done} = \frac{F_s \times l_s \times \delta_s}{2} = \frac{HM \times \delta_e}{2} \rightarrow F_s = HM \frac{\delta_e}{\delta_s l_s} = -G \cdot HM$$

$$F_s = -GQ\eta_T S_e c_e C_h = -GQ\eta_T S_e c_e (C_{h0} + C_{h\alpha} \alpha + C_{h\delta} \delta_e + C_{h\delta_t} \delta_t)$$

$$\delta_e = \delta_{e0} - \left(\frac{dC_m}{dC_L} \right)_{\text{fixed}} \times \frac{C_L}{C_{m\delta}}; \quad K = -G\eta_T S_e c_e; \quad A = C_{h0} + C_{h\alpha} \alpha + C_{h\delta} \delta_{e0}$$

$$F_s = KQ \left[A + \frac{C_{h\alpha} C_L}{a_w} (1 - \varepsilon_\alpha) - \left(\frac{dC_m}{dC_L} \right)_{\text{fixed}} \times \frac{C_{h\delta} C_L}{C_{m\delta}} + C_{h\delta_t} \delta_t \right]$$

$$F_s = KQA - K \frac{W}{S} \frac{C_{h\delta}}{C_{m\delta}} \left(\frac{dC_m}{dC_L} \right)_{\text{free}} + KQC_{h\delta_t} \delta_t; \quad \frac{dF_s}{dV} = K\rho V (A + C_{h\delta_t} \delta_t)$$





Stick Force Trim Solution

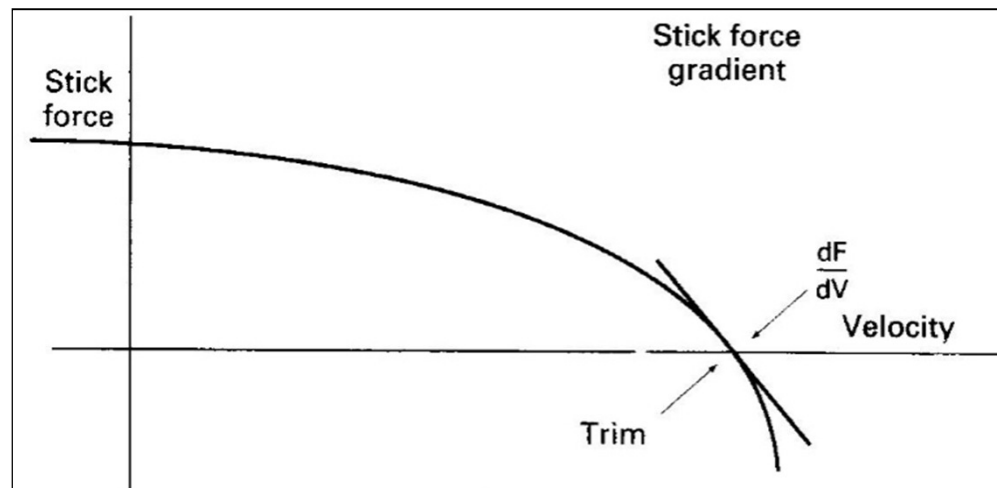
$$F_s = KQ_{trim}A - K \frac{W}{S} \frac{C_{h\delta}}{C_{m\delta}} \left(\frac{dC_m}{dC_L} \right)_{free} + KQ_{trim}C_{h\delta_t}\delta_t = 0$$

$$C_{h\delta_t}\delta_t = \frac{W}{Q_{trim}S} \frac{C_{h\delta}}{C_{m\delta}} \left(\frac{dC_m}{dC_L} \right)_{free} - A$$

$$F_s = KQ \times \left(\frac{W}{Q_{trim}S} \frac{C_{h\delta}}{C_{m\delta}} \left(\frac{dC_m}{dC_L} \right)_{free} \right) A - K \frac{W}{S} \frac{C_{h\delta}}{C_{m\delta}} \left(\frac{dC_m}{dC_L} \right)_{free}$$

$$F_s = K \frac{W}{S} \frac{C_{h\delta}}{C_{m\delta}} \left(\frac{dC_m}{dC_L} \right)_{free} \times \left(\frac{V^2}{V_{trim}^2} - 1 \right)$$

$$\frac{dF_s}{dV} = K \frac{2W}{S} \frac{C_{h\delta}}{C_{m\delta}} \left(\frac{dC_m}{dC_L} \right)_{free} \times \frac{V}{V_{trim}^2}$$





Stick Force Stability

Stick force gradient with speed is a measure of **change** in stick force needed to **change** the aircraft speed.

If the gradient is < 0 , then if the aircraft slows **down**, a positive stick force is **generated**, which creates a nose down **moment**, leading to higher speed, and vice versa.

This behaviour helps the pilot to fly hands-off **even** in the presence of speed **disturbances**.



Stick Forces Under Manoeuvre

It is known that during a trimmed flight, stick forces are **driven** to zero, in order to reduce the pilot effort.

However, when performing manoeuvres (particularly **in** fighter aircraft), pilot effort for a specific ‘n’ is an **important** design input.

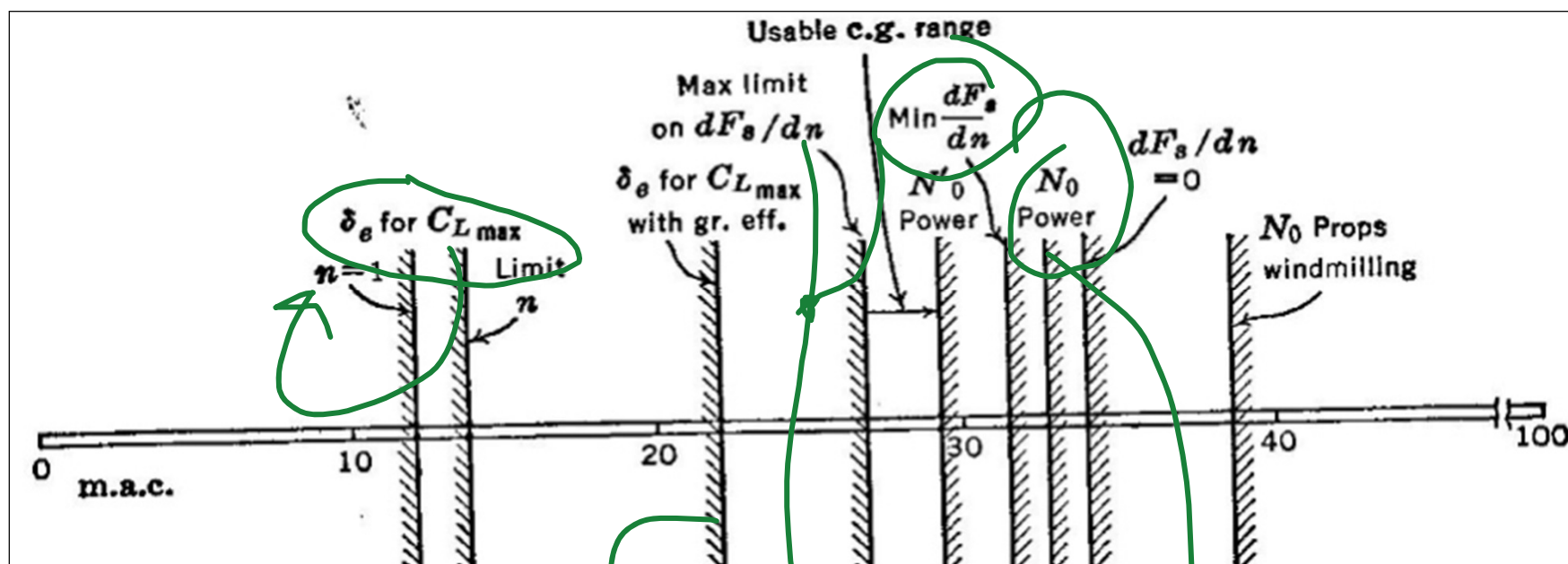
It has been found through studies that pilots rate the **manoeuvring** capability of an aircraft through the stick force **gradients**, which need to be suitably moderated.

$$F_s = K \left(\frac{W}{S} \right) \times \frac{C_{h\delta}}{C_{m\delta}} \left(\frac{dC_m}{dC_L} \right)_{free} \times \left(\frac{V^2}{V_{trim}^2} - n \right) + Kgl_T \frac{\rho}{2} (n-1) \times \left(C_{h\alpha} - \frac{1.1C_{h\delta}}{\tau} \right)$$

$$\left(\frac{dF_s}{dn} \right)_{pull-up} = K \left(\frac{W}{S} \right) \frac{C_{h\delta}}{C_{m\delta}} \left(\frac{dC_m}{dC_L} \right)_{free} + Kgl_T \frac{\rho}{2} \times \left(C_{h\alpha} - \frac{1.1C_{h\delta}}{\tau} \right)$$



Aircraft Symmetric Stability and Control Summary



landing gear down effect
 F_s per g limit
 no rotation