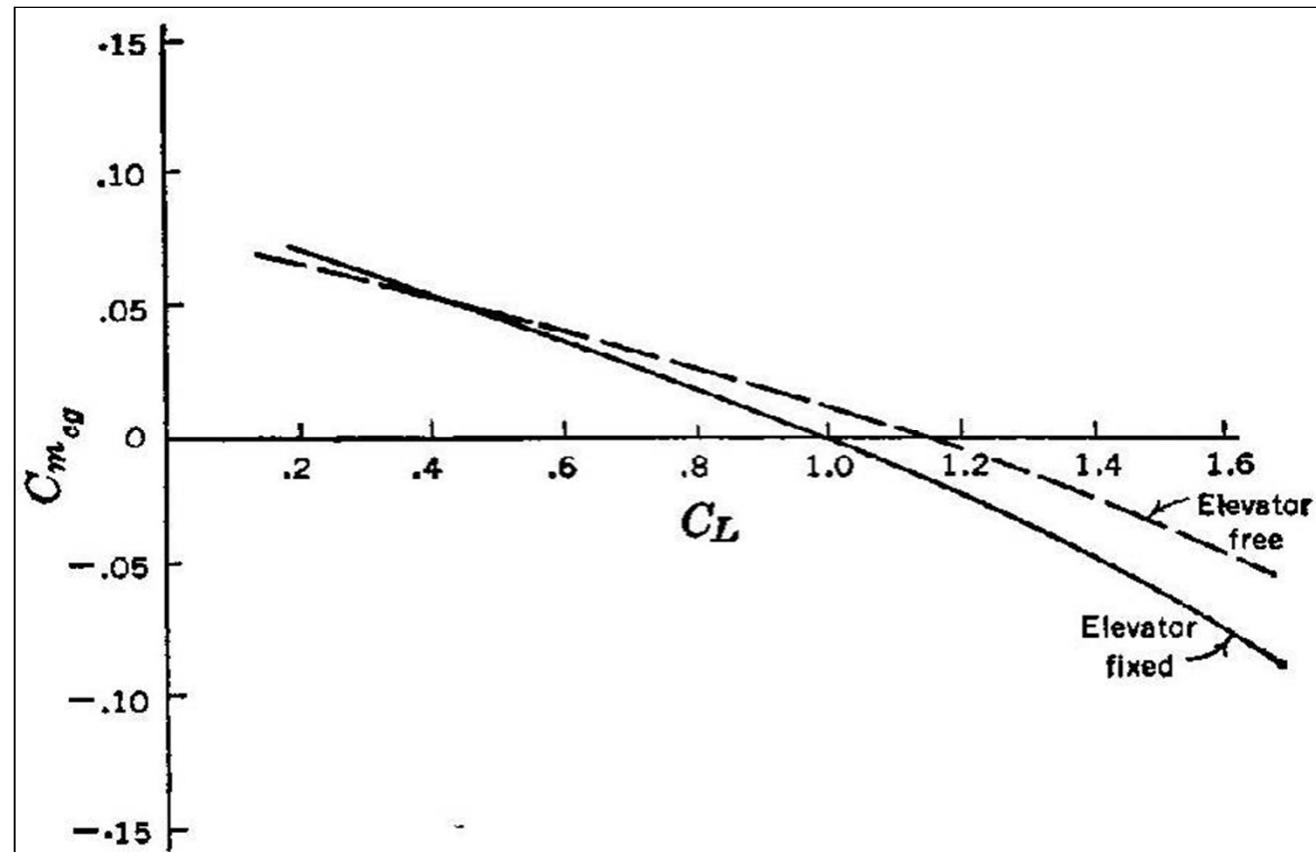




## *Typical Impact of Free Elevator*



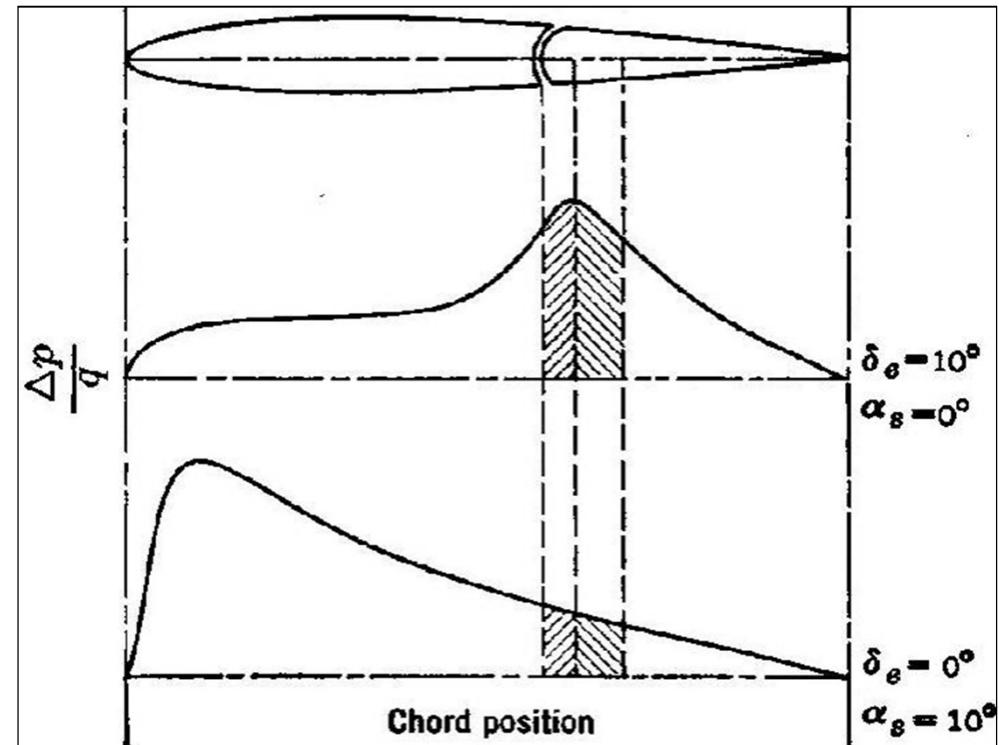


## Aerodynamic Balancing Concept

In order to minimize the impact of a free **elevator** on the stability, there is a need to **minimize** its floating.

One way to achieve this is to ‘aerodynamically **balance**’ the elevator, by making ‘ $C_{h\alpha}$ ’ nearly **zero**.

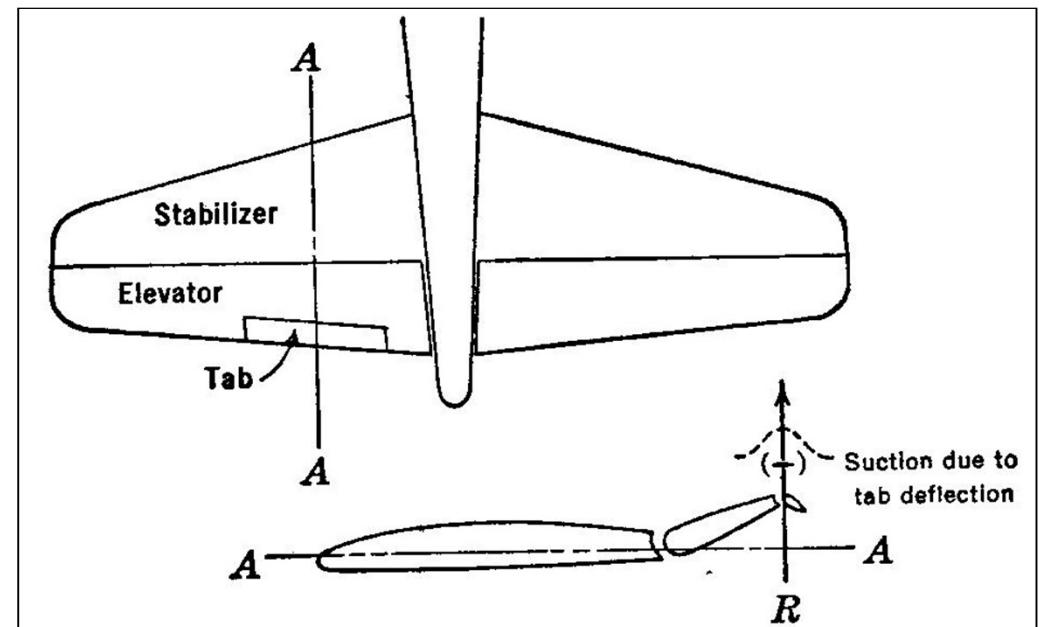
This is possible if the net resultant of forces **due** to ‘ $\alpha$ ’ and ‘ $\delta$ ’ passes through the hinge **line**, as shown alongside.





## *Application of Trim Tabs*

Another way to prevent floating, without shifting the hinge line, is to add a small surface at the elevator trailing edge called ‘tab’ or ‘trim tab’, as shown alongside.



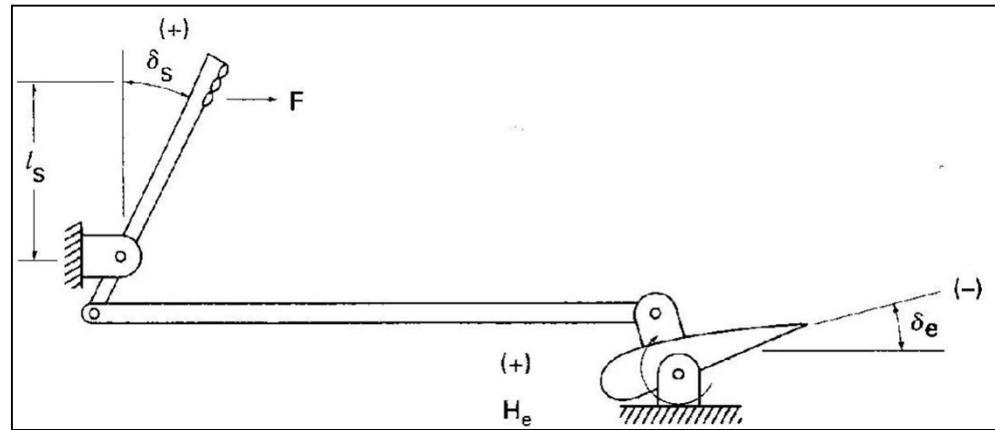


## Stick Force Concept

In practice, HM is always kept small, which is finally cancelled through manual application of ‘trim tab’.

This is done to give the pilot a positive feel for forces required to change trim conditions, which is an important flight control system design criterion.

In view of the above, pilot experiences a reaction force while attempting to deflect the stick, as shown alongside.





# Stick Force Formulation and Features

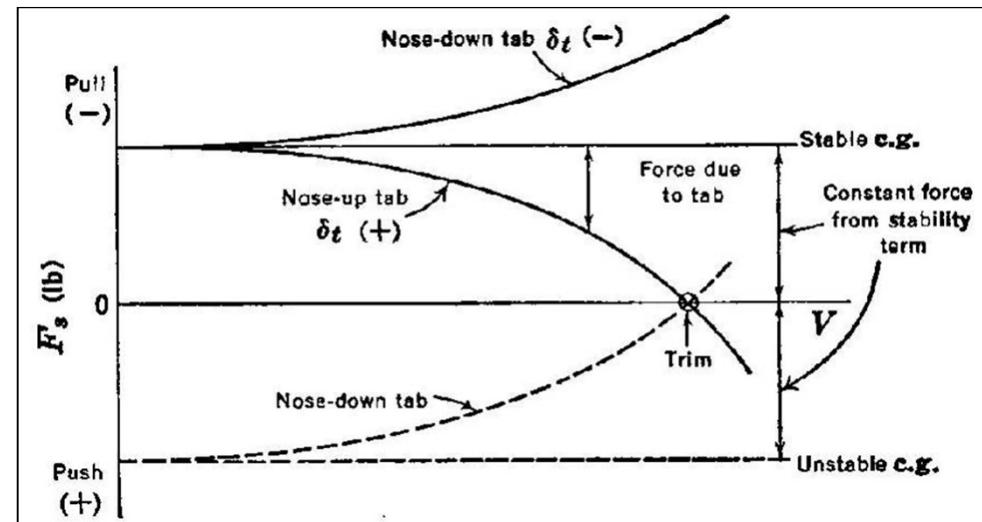
Work Done =  $\frac{F_s \times l_s \times \delta_s}{2} = \frac{HM \times \delta_e}{2} \rightarrow F_s = HM \frac{\delta_e}{\delta_s l_s} = -G \cdot HM$

$$F_s = -GQ\eta_T S_e C_e C_h = -GQ\eta_T S_e C_e (C_{h0} + C_{h\alpha}\alpha + C_{h\delta}\delta_e + C_{h\delta_t}\delta_t)$$

$$\delta_e = \delta_{e0} - \left( \frac{dC_m}{dC_L} \right)_{fixed} \times \frac{C_L}{C_{m\delta}}; \quad K = -G\eta_T S_e C_e; \quad A = C_{h0} + C_{h\alpha}\alpha + C_{h\delta}\delta_{e0}$$

$$F_s = KQ \left[ A + \frac{C_{h\alpha} C_L}{a_w} (1 - \varepsilon_\alpha) - \left( \frac{dC_m}{dC_L} \right)_{fixed} \times \frac{C_{h\delta} C_L}{C_{m\delta}} + C_{h\delta_t} \delta_t \right]$$

$$F_s = KQA - K \frac{W}{S} \frac{C_{h\delta}}{C_{m\delta}} \left( \frac{dC_m}{dC_L} \right)_{free} + KQC_{h\delta_t} \delta_t; \quad \frac{dF_s}{dV} = K\rho V (A + C_{h\delta_t} \delta_t)$$





## Stick Force Trim Solution

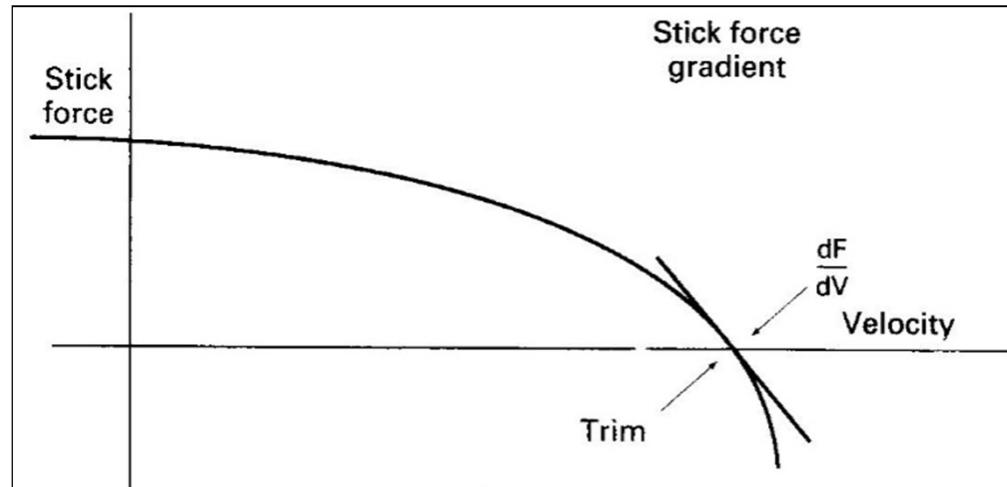
$$F_s = KQ_{trim}A - K \frac{W}{S} \frac{C_{h\delta}}{C_{m\delta}} \left( \frac{dC_m}{dC_L} \right)_{free} + KQ_{trim} C_{h\delta_t} \delta_t = 0$$

$$C_{h\delta_t} \delta_t = \frac{W}{Q_{trim} S} \frac{C_{h\delta}}{C_{m\delta}} \left( \frac{dC_m}{dC_L} \right)_{free} - A$$

$$F_s = KQ \times \left( \frac{W}{Q_{trim} S} \frac{C_{h\delta}}{C_{m\delta}} \left( \frac{dC_m}{dC_L} \right)_{free} \right) A - K \frac{W}{S} \frac{C_{h\delta}}{C_{m\delta}} \left( \frac{dC_m}{dC_L} \right)_{free}$$

$$F_s = K \frac{W}{S} \frac{C_{h\delta}}{C_{m\delta}} \left( \frac{dC_m}{dC_L} \right)_{free} \times \left( \frac{V^2}{V_{trim}^2} - 1 \right)$$

$$\frac{dF_s}{dV} = K \frac{2W}{S} \frac{C_{h\delta}}{C_{m\delta}} \left( \frac{dC_m}{dC_L} \right)_{free} \times \frac{V}{V_{trim}^2}$$





## ***Stick Force Stability***

**Stick** force gradient with speed is a measure of **change** in stick force needed to **change** the aircraft speed.

If the gradient is  $< 0$ , then if the aircraft slows **down**, a positive stick force is **generated**, which creates a nose down **moment**, leading to higher speed, and vice versa.

This behaviour helps the pilot to fly hands-off **even** in the presence of speed **disturbances**.



## *Stick Forces Under Manoeuvre*

**It** is known that during a trimmed flight, stick forces are **driven** to zero, in order to reduce the pilot effort.

**However**, when performing manoeuvres (particularly **in** fighter aircraft), pilot effort for a specific ‘n’ is an **important** design input.

**It** has been found through studies that pilots rate the **manoeuvring** capability of an aircraft through the stick force **gradients**, which need to be suitably moderated.

$$\begin{aligned} F_s &= K \left( \frac{W}{S} \right) \times \frac{C_{h\delta}}{C_{m\delta}} \left( \frac{dC_m}{dC_L} \right)_{free} \times \left( \frac{V^2}{V_{trim}^2} - n \right) \\ &\quad + K g l_T \frac{\rho}{2} (n-1) \times \left( C_{h\alpha} - \frac{1.1 C_{h\delta}}{\tau} \right) \\ \left( \frac{dF_s}{dn} \right)_{pull-up} &= K \left( \frac{W}{S} \right) \frac{C_{h\delta}}{C_{m\delta}} \left( \frac{dC_m}{dC_L} \right)_{free} \\ &\quad + K g l_T \frac{\rho}{2} \times \left( C_{h\alpha} - \frac{1.1 C_{h\delta}}{\tau} \right) \end{aligned}$$



# Aircraft Symmetric Stability and Control Summary

