Systèmes à base d'énergie pneumatique: de la robotique à l'énergie éolienne



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- Deux bancs d'essais électro-pneumatiques pour :
- application en aérodynamique : commande de la portance d'un pale éolienne par injection d'air comprimé
- application en robotique : contrôle en effort d'une pince à trois doigts à base de muscle pneumatique
- Carte E/S : électronique de commande des valves électro-pneumatiques binaires, un calculateur basé sur une carte STM Nucleo H743ZI2, acquisition sur 16 bits des données mesurées



Commande sans modèle (Fliess & Join, 2013)

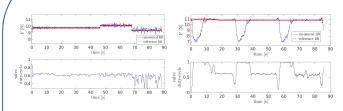
$$u_k = u_{k-1} - \frac{1}{\beta} \left(\frac{\mathrm{d}y}{\mathrm{d}t} \Big|_{k-1} - \left. \frac{\mathrm{d}y^*}{\mathrm{d}t} \right|_k \right) + K(y_k^* - y_k)$$

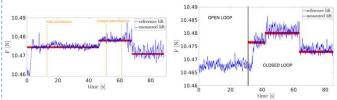
Commande super twisting adaptative (Taleb & Plestan, 2021)

$$\begin{array}{lll} u = -k_1 \, |\sigma|^{\frac{1}{2}} \mathrm{sgn}(\sigma) + v & & k_1 = \left\{ \begin{array}{lll} \frac{\alpha}{|\psi| + \epsilon} & \mathrm{if} & |\sigma| > \epsilon \\ -k_1 & \mathrm{if} & |\sigma| \leq \epsilon \end{array} \right. & k_2 = \left\{ \begin{array}{lll} \frac{\alpha}{2|\sigma|^{\frac{1}{2}}} & \mathrm{if} & |\sigma| > \epsilon \\ -k_2 & \mathrm{if} & |\sigma| \leq \epsilon \end{array} \right. & \left. \begin{array}{lll} k_2 = \left\{ \begin{array}{lll} \frac{\alpha}{2|\sigma|^{\frac{1}{2}}} & \mathrm{if} & |\sigma| > \epsilon \end{array} \right. & \left. \begin{array}{lll} k_2 = \left\{ \begin{array}{lll} \frac{\alpha}{2|\sigma|^{\frac{1}{2}}} & \mathrm{if} & |\sigma| > \epsilon \end{array} \right. & \left. \begin{array}{lll} k_2 = \left\{ \begin{array}{lll} \frac{\alpha}{2|\sigma|^{\frac{1}{2}}} & \mathrm{if} & |\sigma| > \epsilon \end{array} \right. & \left. \begin{array}{lll} k_2 = \left\{ \begin{array}{lll} \frac{\alpha}{2|\sigma|^{\frac{1}{2}}} & \mathrm{if} & |\sigma| > \epsilon \end{array} \right. & \left. \begin{array}{lll} k_2 = \left\{ \begin{array}{lll} \frac{\alpha}{2|\sigma|^{\frac{1}{2}}} & \mathrm{if} & |\sigma| > \epsilon \end{array} \right. & \left. \begin{array}{lll} k_2 = \left\{ \begin{array}{lll} \frac{\alpha}{2|\sigma|^{\frac{1}{2}}} & \mathrm{if} & |\sigma| > \epsilon \end{array} \right. & \left. \begin{array}{lll} k_2 = \left\{ \begin{array}{lll} \frac{\alpha}{2|\sigma|^{\frac{1}{2}}} & \mathrm{if} & |\sigma| > \epsilon \end{array} \right. & \left. \begin{array}{lll} k_2 = \left\{ \begin{array}{lll} \frac{\alpha}{2|\sigma|^{\frac{1}{2}}} & \mathrm{if} & |\sigma| > \epsilon \end{array} \right. & \left. \begin{array}{lll} k_2 = \left\{ \begin{array}{lll} \frac{\alpha}{2|\sigma|^{\frac{1}{2}}} & \mathrm{if} & |\sigma| > \epsilon \end{array} \right. & \left. \begin{array}{lll} k_2 = \left\{ \begin{array}{lll} \frac{\alpha}{2|\sigma|^{\frac{1}{2}}} & \mathrm{if} & |\sigma| > \epsilon \end{array} \right. & \left. \begin{array}{lll} k_2 = \left\{ \begin{array}{lll} \frac{\alpha}{2|\sigma|^{\frac{1}{2}}} & \mathrm{if} & |\sigma| > \epsilon \end{array} \right. & \left. \begin{array}{lll} k_2 = \left\{ \begin{array}{lll} \frac{\alpha}{2|\sigma|^{\frac{1}{2}}} & \mathrm{if} & |\sigma| > \epsilon \end{array} \right. & \left. \begin{array}{lll} k_2 = \left\{ \begin{array}{lll} \frac{\alpha}{2|\sigma|^{\frac{1}{2}}} & \mathrm{if} & |\sigma| > \epsilon \end{array} \right. & \left. \begin{array}{lll} k_2 = \left\{ \begin{array}{lll} \frac{\alpha}{2|\sigma|^{\frac{1}{2}}} & \mathrm{if} & |\sigma| > \epsilon \end{array} \right. & \left. \begin{array}{lll} k_2 = \left\{ \begin{array}{lll} \frac{\alpha}{2|\sigma|^{\frac{1}{2}}} & \mathrm{if} & |\sigma| > \epsilon \end{array} \right. & \left. \begin{array}{lll} k_2 = \left\{ \begin{array}{lll} \frac{\alpha}{2|\sigma|^{\frac{1}{2}}} & \mathrm{if} & |\sigma| > \epsilon \end{array} \right. & \left. \begin{array}{lll} k_2 = \left\{ \begin{array}{lll} \frac{\alpha}{2|\sigma|^{\frac{1}{2}}} & \mathrm{if} & |\sigma| > \epsilon \end{array} \right. & \left. \begin{array}{lll} k_2 = \left\{ \begin{array}{lll} \frac{\alpha}{2|\sigma|^{\frac{1}{2}}} & \mathrm{if} & |\sigma| > \epsilon \end{array} \right. & \left. \begin{array}{lll} k_2 = \left\{ \begin{array}{lll} \frac{\alpha}{2|\sigma|^{\frac{1}{2}}} & \mathrm{if} & |\sigma| > \epsilon \end{array} \right. & \left. \begin{array}{lll} k_2 = \left\{ \begin{array}{lll} \frac{\alpha}{2|\sigma|^{\frac{1}{2}}} & \mathrm{if} & |\sigma| > \epsilon \end{array} \right. & \left. \begin{array}{lll} k_2 = \left\{ \begin{array}{lll} \frac{\alpha}{2|\sigma|^{\frac{1}{2}}} & \mathrm{if} & |\sigma| > \epsilon \end{array} \right. & \left. \begin{array}{lll} k_2 = \left\{ \begin{array}{lll} \frac{\alpha}{2|\sigma|^{\frac{1}{2}}} & \mathrm{if} & |\sigma| > \epsilon \end{array} \right. & \left. \begin{array}{lll} k_2 = \left\{ \begin{array}{lll} \frac{\alpha}{2|\sigma|^{\frac{1}{2}}} & \mathrm{if} & |\sigma| > \epsilon \end{array} \right. & \left. \begin{array}{lll} k_2 = \left\{ \begin{array}{lll} \frac{\alpha}{2|\sigma|^{\frac{1}{2}}} & \mathrm{if} & |\sigma| > \epsilon \end{array} \right. & \left. \begin{array}{lll} k_2 = \left\{ \begin{array}{lll} \frac{\alpha}{2|\sigma|^{\frac{1}{2}}} & \mathrm{if} & |\sigma| > \epsilon \end{array} \right. & \left. \begin{array}{lll} k_2 = \left\{ \begin{array}{lll} \frac$$

Les lois de commande sont échantillonnées à 20 kHz et la fréquence de service des valves est à 200 Hz

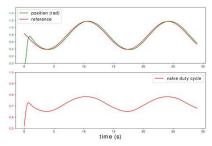
Contrôle de portance aérodynamique par injection d'air comprimé

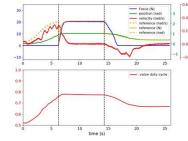


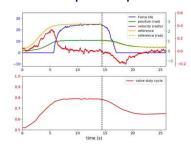


Commande sans modèle : perturbation chopper 'statique' et 'tournante' | Commande super twisting : perturbations chopper 'statique' et vitesse du vent

Asservissement hybride 1D pour préhension d'un objet à l'aide d'un muscle pneumatique



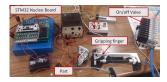


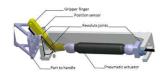


Commande sans modèle: asservissement de position angulaire (gauche) – asservissement hybride en vitesse, effort et position (droite)



Tunnel soufflerie & système chopper (LHEEA)





Boucle d'asservissement en position et détail muscle pneumatique

Perspectives:

- Côté aérodynamique : les travaux futurs se concentreront sur le pilotage de l'angle d'incidence de la pale de manière à permettre une meilleure contrôlabilité de la portance
- Côté robotique : les premiers résultats permettent d'envisager un système de préhension à trois doigts pour différents types de pièces mécaniques
- L. Michel et al., Model-free control of the dynamic lift on a wind turbine blade section: experimental results, J. Phys.: Conf. Ser. 2265, 2022.
- L. Michel et al., A novel lift controller for a wind turbine blade section using an active flow control device: experimental results, 2022 IEEE Conference on Control Technology and Applications, à paraître.
- P. Hamon, L. Michel, F. Plestan, D. Chablat, Control of a gripper finger actuated by a pneumatic muscle: a new scheme based on model-free approach, 2022 IFAC Symposium on Mechatronic Systems, à paraître.