

**Western New England University**  
**College of Engineering**  
**ECE Department**  
**Wave Transmission and Reception**  
**EE 457/557**  
**Fall 2023**  
**Design Project #2**  
**Due: November 13, 2023**

Name: \_\_\_\_\_

References: \_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

# Design Project #2

	Score	Max
Design		200
HFSS		300
Tables		100
Presentation		100
Total		700

1. Design a 16-GHz probe-fed microstrip patch antenna. The substrate is 20-mil thick ( $h = 20 \text{ mils} = 0.508 \text{ mm}$ ) Duroid 5880 ( $\epsilon_r = 2.2$ ). The probe formed by using the center conductor of a 0.085" semi-rigid copper coax cable. The dielectric of the coax is Teflon ( $\epsilon_r = 2.1$ ). The inner and outer radii of the coax are 10 mils ( $r_i = 10 \text{ mils}$ ) and 33 mils ( $r_o = 33 \text{ mils}$ ), respectively.
2. Simulate the 16-GHz probe-fed microstrip patch antenna using HFSS.
  - Tune the patch until the input return loss at 16 GHz is better than 25 dB ( $RL_{in} \geq +25 \text{ dB}$  or  $|\Gamma_{in}| \leq |S_{11}| \leq -25 \text{ dB}$ ).
  - Determine a value for the gain ( $G$ ) at a frequency of 16 GHz.
  - Determine a value for the E-Plane beamwidth ( $BW_{EP}$ ) at a frequency of 16 GHz.
  - Determine a value for the H-Plane beamwidth ( $BW_{HP}$ ) at a frequency of 16 GHz.
  - Plot  $|S_{11}|$  over the range of -40 to 0 dB. Employ a frequency range of 15 to 17 GHz.
  - Determine the bandwidth and percent bandwidth for which the input return loss is better than 10 dB ( $RL_{in} \geq +10 \text{ dB}$  or  $|\Gamma_{in}| \leq |S_{11}| \leq -10 \text{ dB}$ ).
3. Complete the following tables (Table 1, Table 2, Table 3, and Table 4).

Table 1 Summary of the calculated design parameters for the 16-GHz probe-fed microstrip patch antenna.

Parameter	Calculated	
$\lambda_g$		mm
$L_e$		mm
$\Delta L$		$\mu\text{m}$
$W$		mm
$\epsilon_r^{eff}$		
$\Delta L$		$\mu\text{m}$
$L_p$		mm
$G_1$		mS
$G_{12}$		$\mu\text{S}$
$B_1$		mS
$G_{Edge}$		mS
$R_{Edge}$		$\Omega$
$x_f$		mm

Table 2 Summary of the simulated design parameters for the 16-GHz probe-fed microstrip patch antenna.

Parameter	Initial Design	Final Design	
$W$			mm
$L_e$			mm
$\Delta L$			$\mu\text{m}$
$L_p$			mm
$x_f$			mm

Table 3 Summary of the simulated gain (at 16 GHz) for the 16-GHz probe-fed microstrip patch antenna.

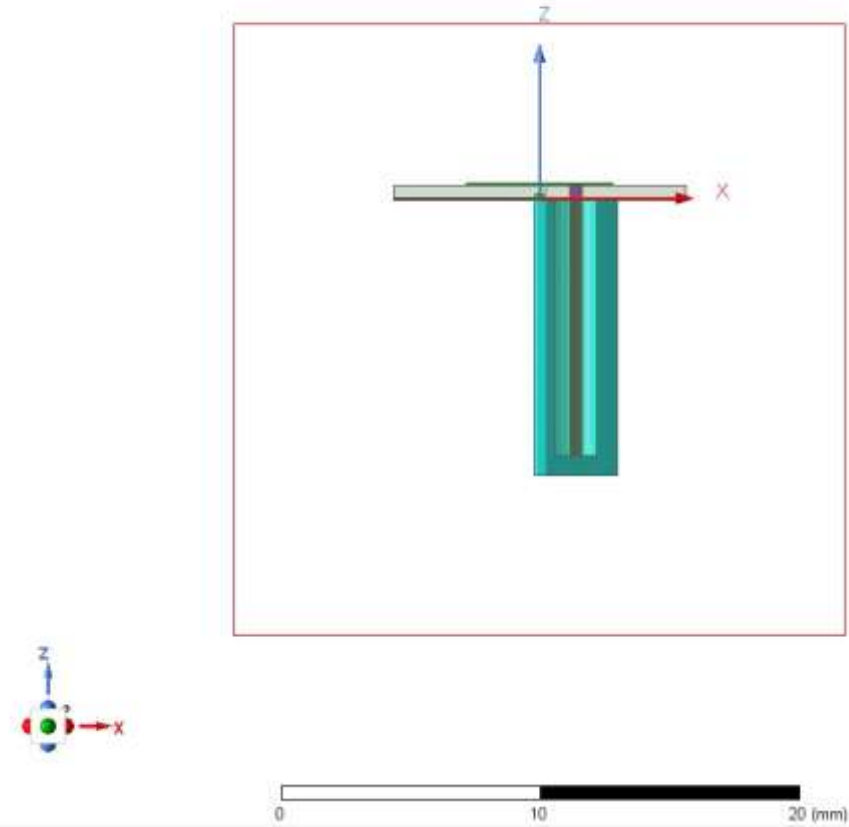
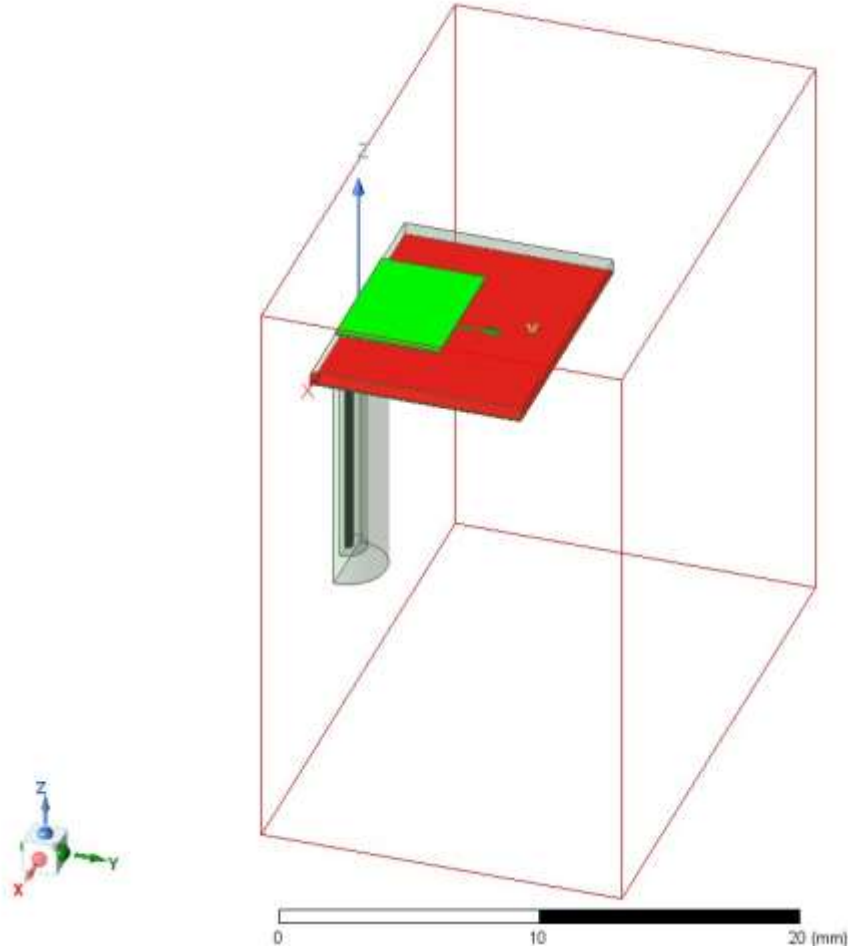
Parameter	HFSS	
$G$		W/W
$G$		dB
$BW_{EP}$		°
$BW_{HP}$		°

Table 4 Summary of the calculated and simulated frequency response for the 16-GHz probe-fed microstrip patch antenna.

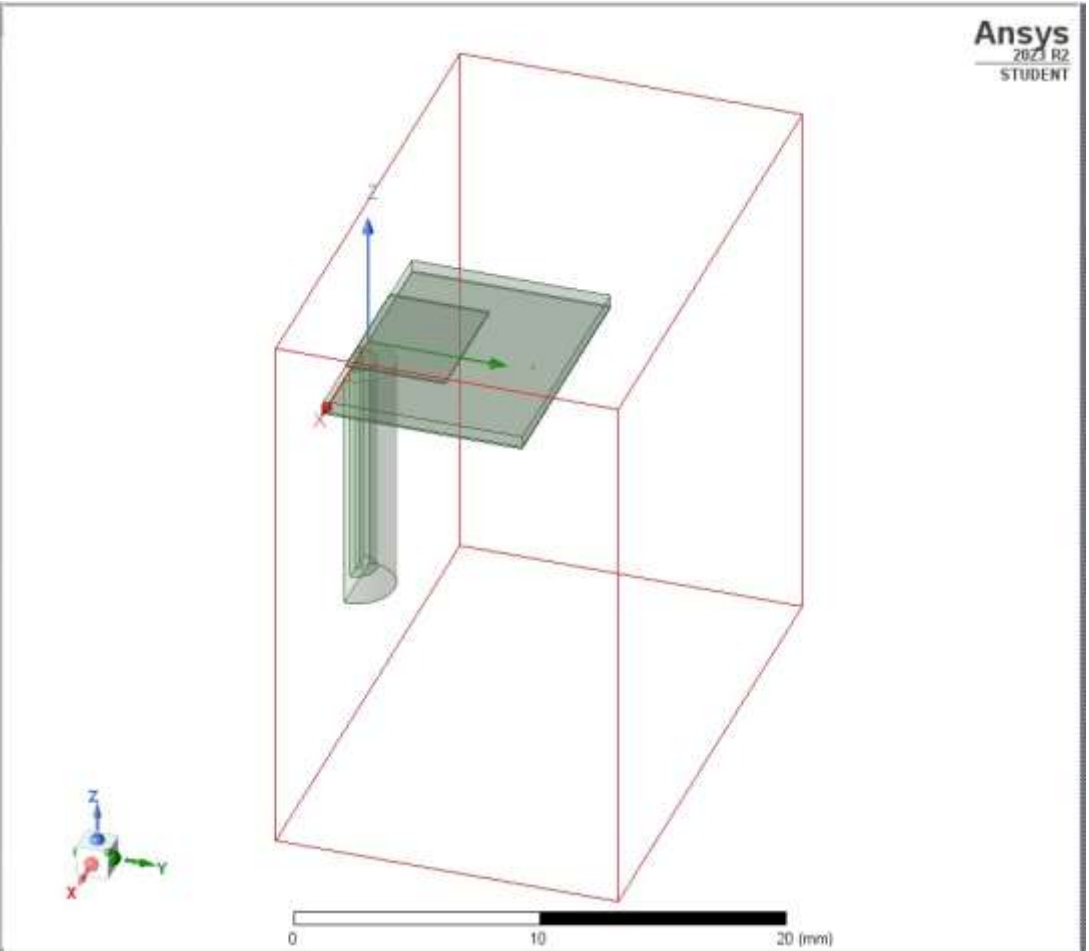
Parameter	Calculated	HFSS	
$BW_f$			MHz
$BW_f$			%

# Design Project 2

## 16GHz Patch Antenna



Properties				
Name	Value	Unit	Evaluated V...	Type
h	0.508	mm	0.508mm	Design
Le	6.262947717	mm	6.2629477mm	Design
del_L	266.272104	um	266.2721um	Design
L	$Le - 2 \cdot del\_L$		5.7304035mm	Design
W	$1.5 \cdot L$		8.5956053mm	Design
Ls	$2 \cdot L$		11.460807mm	Design
Ws	$2 \cdot W$		17.191211mm	Design
t	80	um	80um	Design
SCALE	0.825		0.825	Design
Xf	$2.07 \cdot SCALE$	mm	1.70775mm	Design
X0	$(1/2) \cdot Le - Xf$		1.4237239mm	Design
r_i	10	mil	10mil	Design
r_o	33	mil	33mil	Design
r_o2	$r_o + 10 \cdot t$		1.6382mm	Design
Lc	10	mm	10mm	Design
d_cap	$10 \cdot t$		800um	Design



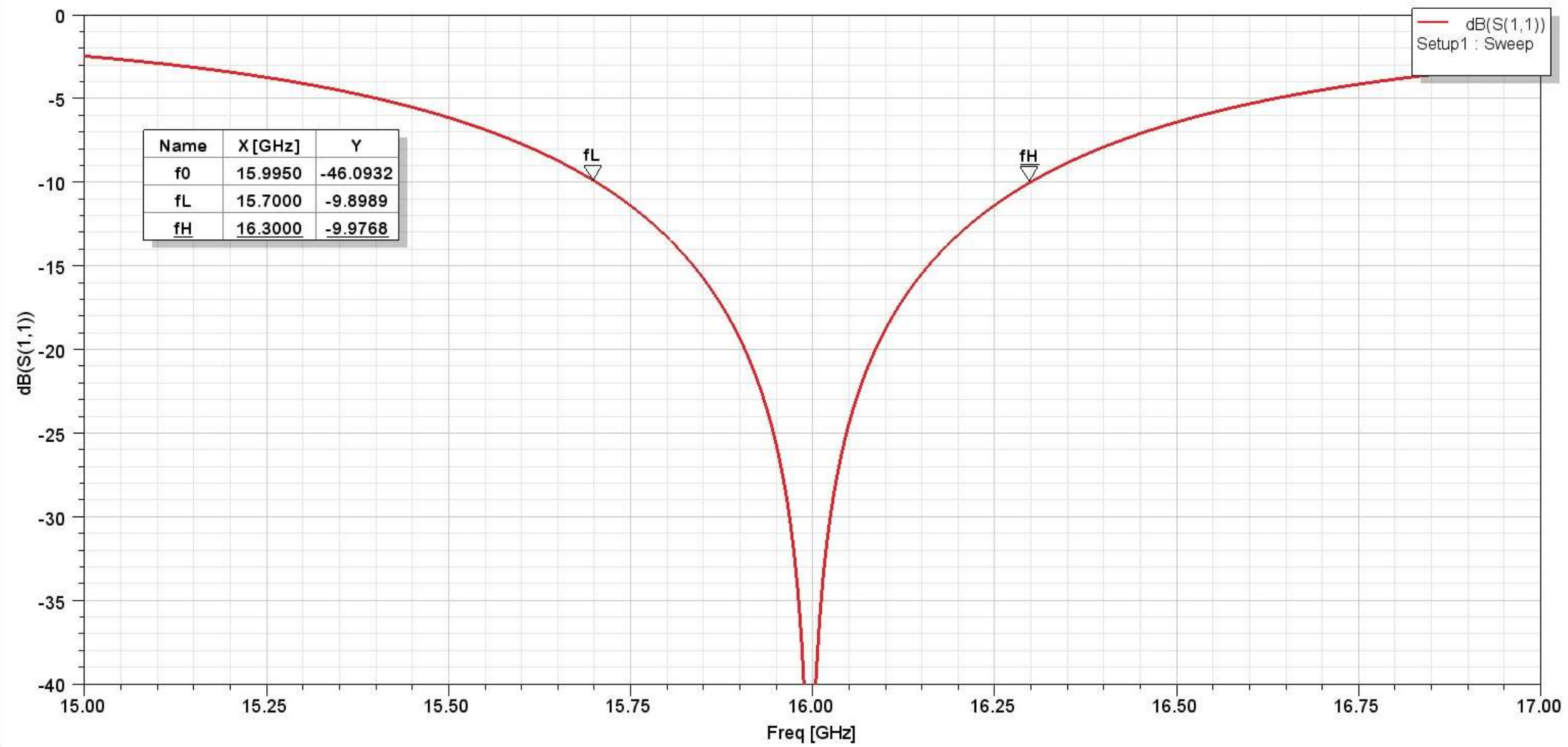


# Calculations

$$\begin{aligned}
 \textcircled{1} \quad \lambda_{FS} &= \mu c / f_0 \\
 &= \frac{2.99792 \times 10^8 \times 10^2}{16 \times 10^9} = \frac{2.99792 \times 10^{10}}{16 \times 10^9} = 0.18737 \times 10^3 \\
 \lambda_{FS} &= 18.737 \\
 \textcircled{2} \quad \lambda_g &= \frac{18.737}{\sqrt{2.2}} = 12.632482 \text{ mm} \\
 \textcircled{3} \quad L_e &= \frac{1}{2} \cdot \lambda_g \\
 &= \frac{1}{2} \times 12.632482 \\
 &= 6.316241 \text{ mm} \\
 \textcircled{4} \quad W' &= 1.5 \times L_e \\
 &= 1.5 \times 6.316241 \\
 &= 9.4743615 \text{ mm} \\
 \textcircled{5} \quad \epsilon_{eff} &= \left[ \left( \frac{1}{2} \right) (\epsilon_r + 1) \right] + \left[ \left( \frac{1}{2} \right) (\epsilon_r - 1) \right] \left[ 1 + 12 \left( \frac{h}{W'} \right) \right]^{-1} \\
 &= \left[ \left( \frac{1}{2} \right) (2.2 + 1) \right] + \left[ \left( \frac{1}{2} \right) (2.2 - 1) \right] \left[ 1 + 12 \left( \frac{0.508}{9.4743615} \right) \right]^{-1} \\
 &= 1.6 + 0.6 [1.643420]^{-1/2} \\
 &= 2.068033
 \end{aligned}$$

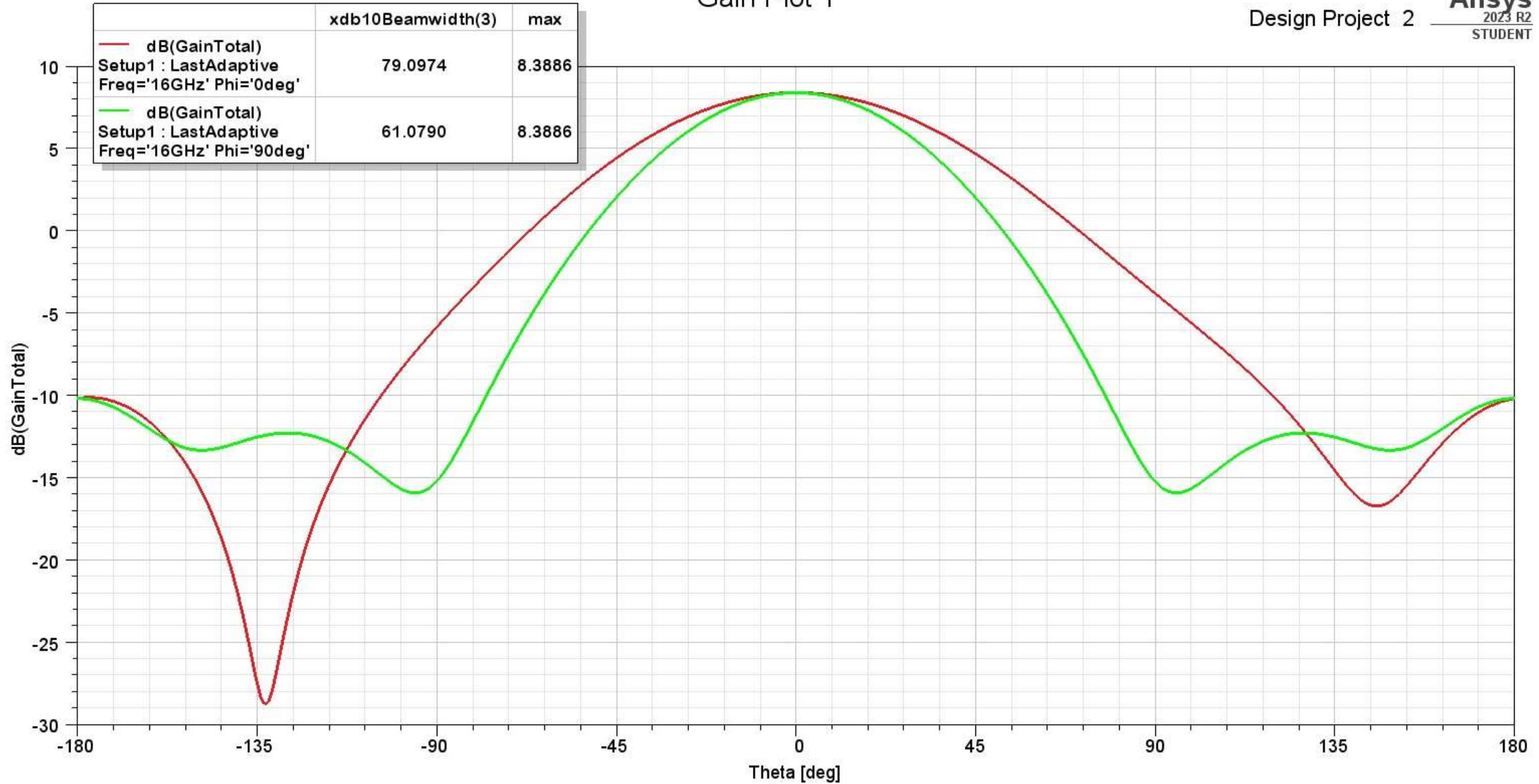
$$\begin{aligned}
 \textcircled{6} \quad \Delta L &= 0.412h \left[ \frac{\epsilon_{eff} + 0.3}{\epsilon_{eff} - 0.258} \right] \left[ \frac{(W'/h) + 0.264}{(W'/h) + 0.8} \right] \\
 &= 0.412 (0.508) \left[ \frac{2.068033 + 0.3}{2.068033 - 0.258} \right] \left[ \frac{18.65031 + 0.264}{18.65031 + 0.8} \right] \\
 &= 0.209296 [1.308281] [0.972442] \times 10^3 \\
 &= 0.266272104 \times 10^3 \\
 &= 266.272104 \text{ } \mu\text{m} \\
 \textcircled{7} \quad L_p &= L_e - \Delta L \\
 &= 6.316241 - [266.272104] \\
 &= 6.316241 - 1.065088 \\
 &= 5.78369 \text{ mm} \\
 \textcircled{8} \quad W &= 1.5 \times L_p \\
 &= 1.5 \times 5.78365 \\
 &= 8.67554 \text{ mm}
 \end{aligned}$$

# S Parameter Plot 5



Gain Plot 1

Design Project 2



# Table 1

Parameter	Calculated	
$f_0$	16	GHz
$h$	0.508	mm
$\varepsilon_r$	2.2	
$\lambda_g$	12.632482	mm
$L_e$	6.316241	mm
$W'$	9.4743615	mm
$\varepsilon_r^{eff}$	2.068033	
$\Delta L$	266.272104	$\mu\text{m}$
$L_p$	5.78369	mm
$W$	8.67554	mm
$R_{edge}$	189.33921	$\Omega$
$x_f$	0.270	mm

# Table 2

Parameter	Initial Design	Final Design	
$W$	8.67554	8.5956033	mm
$L_e$	6.316241	6.262947717	mm
$\Delta L$	266.272104	266.2721	$\mu\text{m}$
$L_p$	5.78369	5.7304033	mm
$x_f$	0.270	1.70775	mm

### Table 3

Parameter	HFSS	
$G$	6.9002	W/W
$G$	8.3886	dB
$BW_{EP}$	61.0790	°
$BW_{HP}$	79.0974	°

### Table 4

Parameter	Calculated	HFSS	
$BW_f$	628.492714	625.00000	MHz
$BW_f$	3.92807	3.8824	%



$$\textcircled{1} \lambda_{FS} = \mu c / f_0$$

$$= \frac{2.99792 \times 10^8 \times 10^3}{16 \times 10^9} = \frac{2.99792 \times 10^{11}}{16 \times 10^9} = 0.18737 \times 10^2$$

$$\lambda_{FS} = 18.737$$

$$\textcircled{2} \lambda_g = \frac{18.737}{\sqrt{2.2}} = 12.632482 \text{ mm.}$$

$$\begin{aligned} \textcircled{3} L_e &= \frac{1}{2} \cdot \lambda_g \\ &= \frac{1}{2} \times 12.632482 \\ &= 6.316241 \text{ mm.} \end{aligned}$$

$$\begin{aligned} \textcircled{4} W' &= 1.5 \times L_e \\ &= 1.5 \times 6.316241 \\ &= 9.4743615 \text{ mm.} \end{aligned}$$

$$\begin{aligned} \textcircled{5} \epsilon_r^{eff} &= \left[ \left( \frac{1}{2} \right) (\epsilon_r + 1) \right] + \left[ \left( \frac{1}{2} \right) (\epsilon_r - 1) \right] \left[ 1 + 12 \left( h / W' \right) \right]^{-1/2} \\ &= \left[ \left( \frac{1}{2} \right) (2.2 + 1) \right] + \left[ \left( \frac{1}{2} \right) (2.2 - 1) \right] \left[ 1 + 12 \left( \frac{0.508}{9.4743615} \right) \right]^{-1/2} \\ &= 1.6 + 0.6 \left[ 1.643420 \right]^{-1/2} \\ &= 2.068033 \end{aligned}$$

$$\textcircled{6} \Delta L = 0.412h \left[ \frac{\epsilon_{x266} + 0.3}{\epsilon_{x266} - 0.258} \right] \left[ \frac{(\dot{w}/h) + 0.264}{(\dot{w}/h) + 0.8} \right]$$

$$= 0.412 (0.508) \left[ \frac{2.068033 + 0.3}{2.068033 - 0.258} \right] \left[ \frac{18.65031 + 0.264}{18.65031 + 0.8} \right]$$

$$= 0.209296 [1.308281] [0.472442] \times 10^3$$

$$= 0.266272104 \times 10^3$$

$$= 266.272104 \mu\text{m}.$$

$$\textcircled{7} L_p = L_e - 2\Delta L$$

$$= 6.316241 - [2(0.266272104)]$$

$$= 6.316241 - 1.065088$$

$$= 5.251153 \mu\text{m}.$$

$$\textcircled{8} W = 1.5 \times L_p$$

$$W = 1.5 \times 5.251153$$

$$= 7.876729 \mu\text{m}.$$



```

%-----
% Srinivas N EE-457 DP 2
%-----

clearvars

clc

close all

%-----

G = 10^9;

M = 10^6;

c = 10^-2;

m = 10^-3;

u = 10^-6;

n = 10^-9;

p = 10^-12;

f = 10^-15;

%-----

f0 = 16*G;

substrate_Thickness = 0.508*m;

er = 2.2; % Duroid 5880

er_t = 2.1; % Teflon

uc = 2.99792458 *10^8; % m/s

n_0 = 376.7303; % Ohms

Z0 = 50;

%-----

lfs = uc/f0; % Freespace wavelength

ko = 2*pi / lfs; %

hmax = (0.3/(2*pi*sqrt(er)))*lfs; % maximum thickness

%-----

Print_Real_Unit('lfs',lfs,'m')

Print_Real_Unit('ko',ko,'rad/m')

Print_Real_Unit('hmax',hmax,'m')

```

```

Print_Break

%-----

% Design 01

%-----

%h = 1.5748*m; %design param
h = 0.508*m;

%-----

lambda_g = lfs/sqrt(er);
Le = (1/2)*lambda_g;
W_prime = 1.5*Le;

%-----

Er_eff = [(1/2)*(er+1)]+[((1/2)*(er-1))]*[(1+12*(h/W_prime))]^(1/2);
delta_L = 0.412 * h * ((Er_eff + 0.3) / (Er_eff - 0.258)) * (((W_prime / h) +
0.264) / ((W_prime / h) + 0.8));
Lp = Le - 2*delta_L;
W = 1.5*Lp;

%-----

Print_Real_Unit('Er_eff',Er_eff,'')
Print_Real_Unit('delta_L',delta_L,'m')
Print_Real_Unit('Lp',Lp,'m')
Print_Real_Unit('W',W,'m')

%-----

Print_Break

Print_Real_Unit('lambda_g',lambda_g,'m')
Print_Real_Unit('Le',Le,'m')
Print_Real_Unit('W_prime',W_prime,'m')

%-----

[Gedge,G1,G12,B1,~,~]=...
EE457_Microstrip_Patch_Conductance(Le,W,h,ko,lfs,n_0);
Rin = Z0;

```

```

Redge = 1/Gedge;
xf = (Le/pi)*acos(sqrt(Rin/Redge));
x0 = (1/2)*Le - xf;
Gedge = 2*(G1+G12);
%-----

Print_Break
Print_Real_Unit('G1',G1,'S')
Print_Real_Unit('G12',G12,'S')
Print_Real_Unit('B1',B1,'S')
Print_Real_Unit('Gedge',Gedge,'S')
Print_Real_Unit('Redge',Redge,'Ohm') % Resistance at the edge of the patch
Print_Real_Unit('xf',xf,'m')

lfs = 18.7370 mm
ko = 335.3352 rad/m
hmax = 603.1575 um
-----

Er_eff = 2.0680
delta_L = 266.272104 um
Lp = 5.78369 mm
W = 8.67554 mm
-----

lambda_g = 12.632482 mm
Le = 6.316241 mm
W_prime = 9.4743615 mm
-----

G1 = 2.0849 mS
G12 = 569.1455 um
B1 = 4.4371 mS
Gedge = 5.3081 mS
Redge = 189.33921 Ohm
xf = 2.0700 mm

```

```
lambda0 = lfs;  
f0 = 16*G;  
BWf = 3.7771 * ((er - 1) / (er^2)) * (h / lambda0) * ( W/Lp) * f0;  
BWp = (BWf*100)/f0;  
Print_Real_Unit('BWf',BWf,'Hz')  
Print_Real_Unit('BWp',BWp,'%')  
BWf = 628.492714 MHz  
BWp = 3.92807 %
```